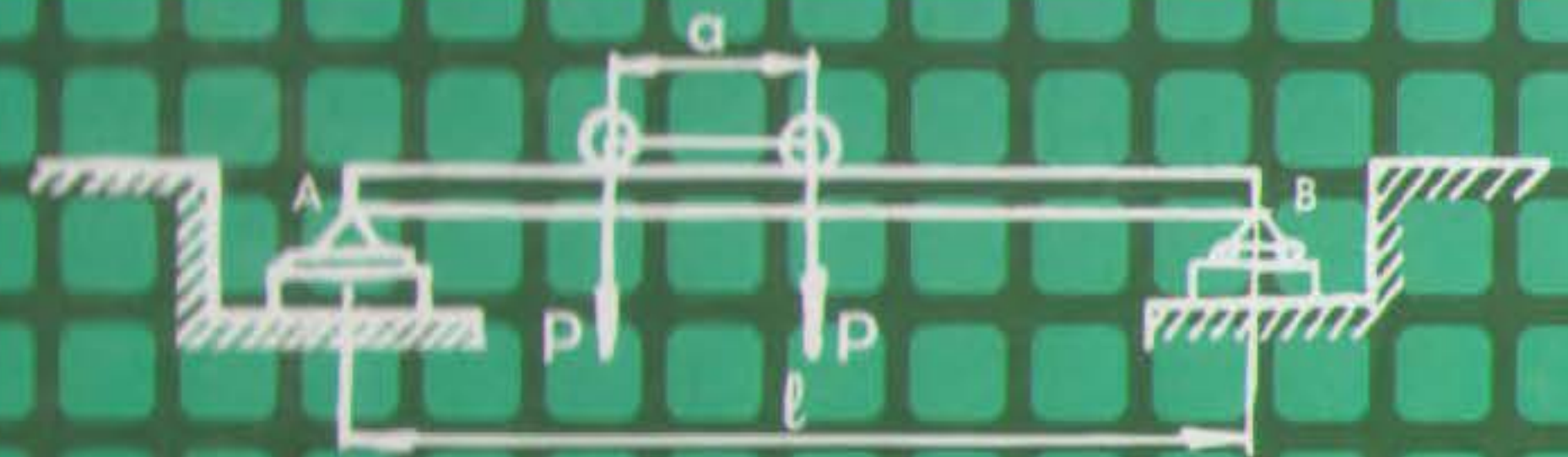
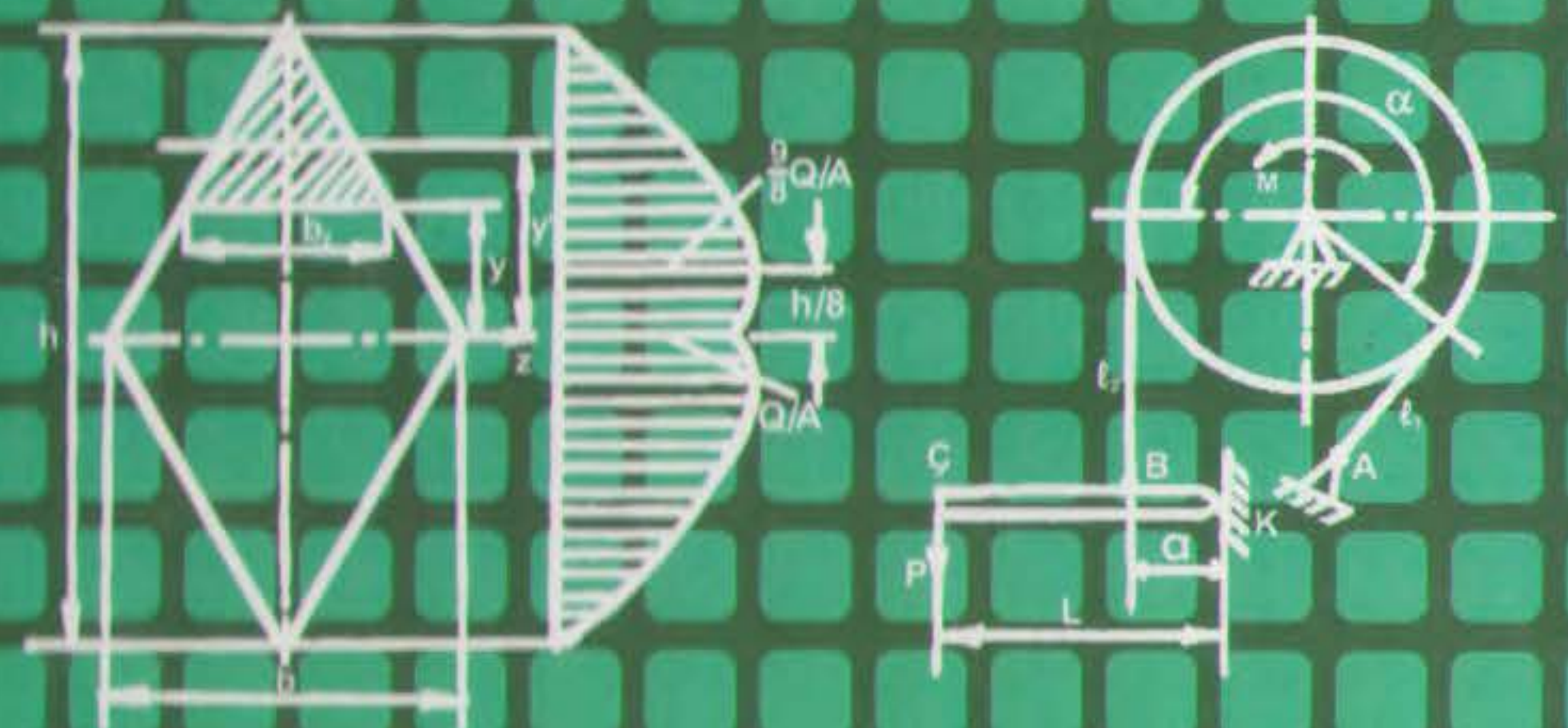


**MATERIALLARYŇ GARŞYLYGY
DERSI BOÝUNÇA MESELELER ÝYGÝNDYSY**



$$\sigma = E \varepsilon$$

**MATERIALLARYŇ GARŞYLYGY
DERSI BOÝUNÇA
MESELELER ÝYGÝNDYSY**



$$\tau = G \gamma$$



**TÜRKMENISTANYŇ ILKINJI PREZIDENTI
BEÝIK SAPARMYRAT TÜRKMENBAŞY**



TÜRKMENISTANYŇ DÖWLET TUGRASY



TÜRKMENISTANYŇ DÖWLET BAÝDAGY

TÜRKMENISTANYŇ DÖWLET SENASY

**Janym gurban saňa, erkana ýurdum,
Mert pederleň ruhy bardyr köňülde.
Bitarap, garassyz topragyň nurdur,
Baýdagyň belentdir dünýäň önünde.**

Gaýtalama:

**Halkyň guran Baky beýik binasy,
Berkarar döwletim, jigerim-janym.
Başlaryň täji sen, diller senasy,
Dünýä dursun, sen dur, Türkmenistanym!**

**Gardaşdyr tireler, amandyr iller,
Owal-ahyr birdir biziň ganymyz.
Harasatlar almaz, syndyrmaz siller,
Nesiller döş gerip gorar şanymyz.**

Gaýtalama:

**Halkyň guran Baky beýik binasy,
Berkarar döwletim, jigerim-janym.
Başlaryň täji sen, diller senasy,
Dünýä dursun, sen dur, Türkmenistanym!**

B.Asyrow, D.Myradow

MATERIALLARYŇ GARŞYLYGY *dersi boýunça meseleler ýygındysy*

Ýokary okuw mekdepleri üçin okuw gollanmasy

Türkmenistanyň bilim ministrligi

tarapyndan hödürlenildi

Aşgabat
TDKP - neşirýaty

2009

Aşyrow B., Myradow D. Materiallaryň garşylygy dersi boýunça meseleler ýygındysy. Ýokary okuw mekdepleri üçin okuw gollanmasy. – Aşgabat, 2009.

Okuw gollanmasynda ýokary okuw mekdeplerinde materiallaryň garşylygy dersi boýunça mesele çözmegiň usullary görkezilen. Gollanma iki bölümden ybarat, birinji bölümde nusgawy meseleleriň şertleri, ikinji bölümde bolsa, meseleleriň çözüwleri, görkezmeleri we jogaplary getirilýär.

Kitap tehniki ýokary okuw mekdepleri üçin tassyklanan okuw maksatnamasy esasynda taýýarlanyldy.

Meseleler ýygındysy ýaş mugallymlar, aspirantlar we talyplar üçin niýetlenen.

SÖZBAŞY

TÜRKMENISTANYŇ PREZIDENTI
GURBANGULY BERDIMUHAMEDOW:

*“Güýçli döwletde ylym esasy orny eýeleýär, diýmek,
biz ylmyň iň täze gazananlary bilen aýakdaş
gitmelidiris.”*

Türkmenistanyň Prezidenti Hormatly Gurbanguly Berdimuhamedowyň ýurdumyzyň jemgyýetçilik – önümçilik gurluşyny döwrebaplaşdyrmak boýunça işläp düzen syýasy we ykdysady maksatnamalary Beýik Galkynyşlar zamanamyzda täze kämil ýaşayyş keşbini döretmegi baş maksat edinjän strategiýadyr. Onuň esasy sütünleriniň biri-de ýurdumyzda bilim ulgamyny kämilleşdirmäge, ylym pudagyny ösdürüp, halkara derejesine çykarmaga gönükdirilen özgertmelerdir. Ol halkymyza ylmy-tehniki progresiň iň soňky gazananlary bilen aýakdaş gidip, dühyä siwilizasiýasyna sazlaşykly goşulyp gitmäge mümkinçilik berýän ýoldur.

Hormatly Prezidentimiziň öçmez-ýitmez taglymatlaryny durmuşa ornaşdyrmakda türkmen talyplaryna halkara derejesinde ylym-bilim bermek we arassa ahlakly, watançylyk ruhunda terbiýelemek iň wajyp meseleleriň biri bolup durýar.

Döwletiň ykdysady kuwwatyny pugtalandyryjak we ony has belentliklere alyp gitjek döwrebap inžener hünärmenlerini taýýarlamak hem aýratyn ähmiýete eýedir. Şu babatda hakykata akyl ýetirmek baradaky ylmylaryň esasylarynyň biri bolan “Materiallaryň garşylygy” ylmyna uly orun degişlidir. Onuň üçin tehniki ýokary okuw mekdepleriniň talyplary “Materiallaryň garşylygy” dersiniň çylşyrymly hasaplamalarynyň ajaýyp usullaryndan ýeterlik derejede baş alyp çykmalydyrlar.

“Materiallaryň garşylygy” umumy tehniki ders bolup, gelejekki inženerleri taýýarlamakda tehniki bilimleriň binýady bolup hyzmat edýär. Galyberse-de, bu kursuň amaly bölegi talyplarda inženerlik pikirlenmäniň ösmegine, olaryň dünýägarayşynyň giňelmegine ýokary derejede ýardam berýär.

Talyplar “Materiallaryň garşylygy” kursuny öwrenende, köplenç, meseleleri çözmekde uly kynçylyklar çekýärler.

Meseleler ýygındysynyň türkmen dilinde taýýarlanylýp, ýokary okuw mekdepleriniň talyplaryna ýetirilmegi, ýurdumyzda döwrebap inženerçilik meseleleriň çözülmegine ýardam berýär. Şeýle maksat bilen eliňizdäki ýygındy ýurdumyzyň tehniki ýokary okuw mekdeplerinde okaýan talyplar üçin niýetlenilip, talyplara materiallaryň garsylygy dersi boýunça meseleleri çözmegiň usullaryny göwnejaý özleşdirmegi maksat edinýär. Gollanma awtorlaryň köp ýyllaryň dowamynda toplan ylmy-mugallymçylyk tejribeleri esasynda taýýarlanylýdy. Ýygındynyň köp bölegi aýdyň meseleler bolup, olaryň jogaplary, görkezmeleri we çözüwleri kitabyň ikinji böleginde ýerleşdirilendir. Şeýle hem talyplaryň işjeň pikirlenmegi we özbaşdak özleşdirmegi üçin birnäçe çylşyrymly meseleleriň çözüwi gollanmada düşündirişsiz berilýär.

Meseleler ýygındysynyň düzümine girýän temalar tehniki ýokary okuw mekdepleri üçin tassyklanan okuw maksatnamasyna laýyklykda beýan edildi.

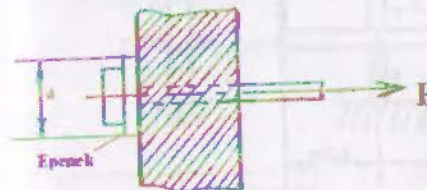
Kitabyň ilkinji gezek türkmen dilinde taýýarlanylýandygy bilen baglylykda awtorlar kitapda goýberilmegi mümkin bolan käbir nogsanlyklar üçin jogapkärçiligi öz üstlerinden aýyrmaýarlar. Ýygındy boýunça gelip gowşan bellikler we teklipler onuň geljekki neşirlerinde göz önünde tutular. Kitap çapa taýýarlananda beren gymmatly maslahatlary üçin professor Ç. Amansähedowa, teksti redaksiya eden dosent S. Gülürowa we tehniki taýdan ýardam eden B. Abdyrahmanowa, S. A. Nyýazow adyndaky TOHU-nyň talyplary P. Annaýewe, B. Berdiýewe, N. Artykowa, S. Paşsykowa, A. Myradowa, A. Erlekowa awtorlar uly minnetdarlyk bildirýärler.

Awtorlar şu kitabyň çykmagyna beren uly kömekleri üçin Ýewropa Birleşiginiň TESIS-TEMPUS maksatnamasynyň CD_JEP-25064 belgili “Ýewropanyň uniwersitetleri bilen hyzmatdaşlykda Türkmenistanda oba hojalyk bilimlerini ösdürmek” atly taslamasyna öz minnetdarlygyny bildirýär.

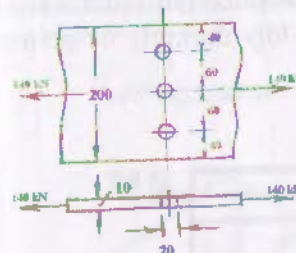
I BAP SÜÝNME WE GYSYLMA

1.1 Statiki kesgitlenýän ulgamlaryň hasaby

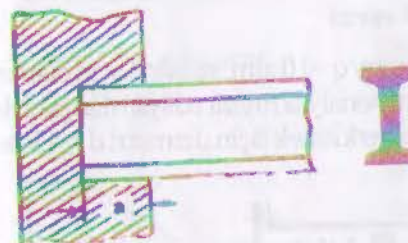
1.1. Kese kesigi $16 \times 16 \text{ sm}^2$ bolan agaç sütün gysylanda dartgynlygy 1 kN/sm^2 -dan köp bolmadyk ýagdaýynda näçe in uly ýiki saklap biler?



1.2-nji surat



1.3-nji surat



1.4-nji surat

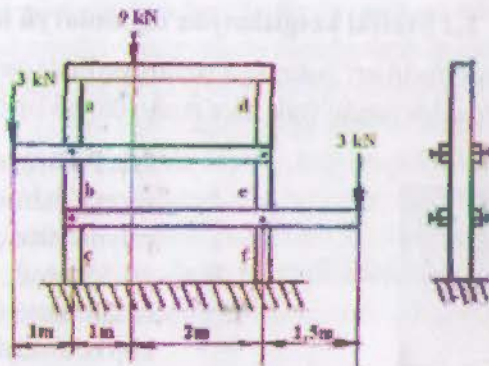
1.5. Uzynlygy birmeňzeş we ok boýunça täsir edýän birmeňzeş güýç bilen ýüklenen iki simiň biri mis, beýlekisi bolsa polat materialdan ýasalan. Mis simiň diametri 1 mm. Eger iki sim hem deň uzalýan bolsalar, polat simiň diametri näçä deň holar?

1.2. P güýç bilen dartylan (surata seret) diametri 25 mm bolan çatyda ýüze çykýan dartgynlyk 10 kN/sm^2 . Epenegiň diwara bolan basyşy $0,14 \text{ kN/sm}^2$ -dan köp bolmadyk ýagdaýda epeneğiň diametrini kesgitlemeli.

1.3. Polat zolak tegelek berçin deşikler bilen gowşadylan we boý güýji bilen dartylan (surata seret). Howply kesikde dartgynlygyň orta bahasyny kesgitlemeli.

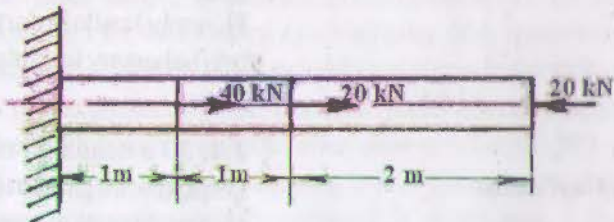
1.4. 30 a belgili iki tawraly balka kerpiç diwara girizilen (surata seret). Balka $Q=60 \text{ kN}$ basyş güýç bilen kerpiç diwary endigan basýar. Eger kerpiç örümiň rugsat edilýän dartgynlygy $[\sigma] = 0,09 \text{ kN/sm}^2$ bolsa, balkanyň diwara girýän uzynlygyny kesgitlemeli. Balkanyň inini kesgitlenen sortdan almaly.

1.6. Kese kesigi $10 \times 10 \text{ sm}^2$ bolan agač diregleriň her biri suratda görkezilişi ýaly ýüklenen. Diregleriň häsiýetli kesiklerindäki dartgynlyklary kesgitlemeli.



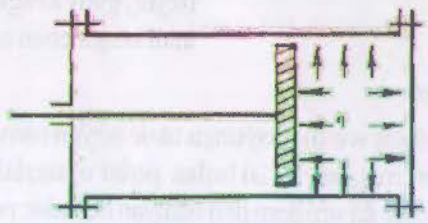
1.6-njy surat

1.7. Kese kesiginiň meýdany 10 sm^2 bolan polat sterženiň (surata seret) hemme böleklerindäki dartgynlyklary we doly durkuny üýtgetmesi kesgitlemeli.

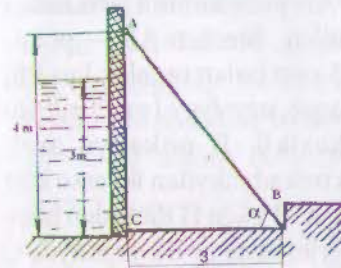


1.7-nji surat

1.8. Bug maşynynyň silindrindäki iş basyşy $q = 10 \text{ atm}$; silindriň içki diametri $D = 350 \text{ mm}$ (surata seret). Eger boltuň materialyna rugsat edilýän dartgynlyk $[\sigma] = 4 \text{ kN/sm}^2$ bolsa, gapagy silindre berkitmek üçin diametri $d = 18 \text{ mm}$ bolan näçe bolt gerek bolar?

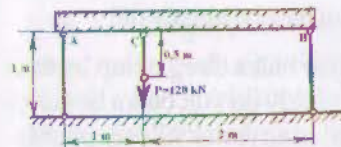


1.8-nji surat



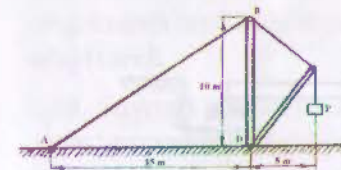
1.9-njy surat

1.9. Diametri $d = 15 \text{ sm}$ bolan tegelek kesikli agač AB direg (surata seret) suw geçirmeýän germewajy agdarylmakdan saklaýar. Diregiň materialyna rugsat edilýän dartgynlygy $0,2 \text{ kN/sm}^2$ diýip kabul edip, diregleriň iň uly aralyklaryny kesgitlemeli.



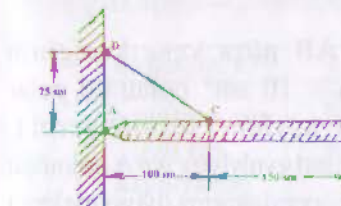
1.10-njy surat

1.10. Suratda görkezilişi ýaly ýüklenen, gaty AB balka, A we B direglere agram salýar. A diregiň materialy-polat, kese kesigi 10 sm^2 , B diregiň materialy-agač, kese kesigi 100 sm^2 , Ç steržen-mis, kese kesigi 30 sm^2 . Ýüküň asylan nokadynyň aşak süýşmesini kesgitlemeli.



1.11-nji surat

1.11. Göteriji kranyň AB dartyjysy (surat seret) 500 mm^2 kese kesikli tros bolup hyzmat edýär. Trosuň materialyna rugsat edilýän dartgynlyk 4 kN/sm^2 . Dartyjynyň berklik şerti boýunça kran näçe ýüki göterip biler?



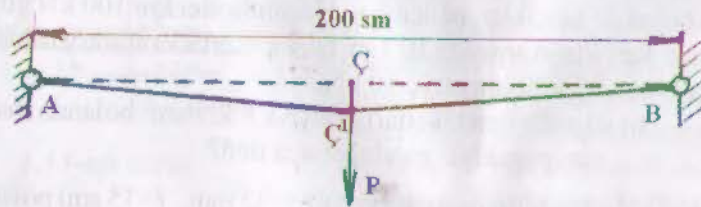
1.12-nji surat

1.12. Gaty AB steržen (surata seret) P güýç bilen ýüklenen we diametri 20 mm bolan tegelek kese kesikli DÇ polat çekiji bilen saklanýar. Iň uly rugsat edilýän güýji we B nokadyň aşak süýşmesini kesgitlemeli. ÇD sterženiň materialyna rugsat edilýän dartgynlyk $[\sigma] = 16 \text{ kN/sm}^2$.

1.13. Gəbə AB sürə surətində tərkibləri

1.16. Polat simliyi yük asylan. Dürküny üylgetmə çenli simin ölçəgləri:

1.22. Diametri 1mm bolan polat sim gorizontaal A we B (surata seret) gozganmaýan nokatlaryň arasynda dartylýp çekilen. Simiň uzynlygynyň ortasyna C nokatda kem-kemden artýan P ýük asylan. Simiň uzalmasy 0,5 % bolanda, ol üzülýär. Şu pursatda P ýük, C nokadyň aşak süýşmesi we üzülen pursatynda simiň dartgynlygy nämä deň? Üzülmä pursadyna çenli simiň durkuny üýtgetmesini maýýşgak diýip hasap etmeli.



1.22-nji surat



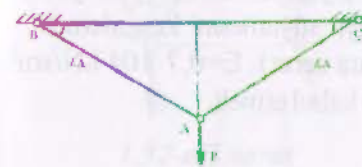
1.23-nji surat

- ✓ 1.23. Tekiz nusgada iki tenzometr oturdylan. A tenzometr nusganyň boý oky boýunça, B tenzometr bolsa, oka perpendikulyar ýerleşdirilen. Degişlilikde, tenzometrleriň ulaltmagy $K_A=950$, $K_B=1100$. Tenzometrleriň bazalary birmeňzeş: $S_A=S_B=20 \text{ mm}$:

Basgançakly ösýän ýüklenmede alnan görkezijiler tablisada getirilen. Maýýşgaklyk boý E modulyň orta bahasyny we kese durkuny üýtgetmäniň koeffisiýentini μ (Puassonyň koeffisiýentini) hasaplamaly. Nusganyň kesiginiň meýdany $A=1 \text{ sm}^2$.

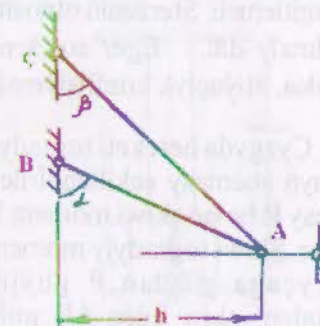
Yüklenme P, kN	Tenzometrler boýunça hasabat	
	$n_A, \text{ mm}$	$n_B, \text{ mm}$
2	4,5	36
12	14,5	32,5
22	24	30
32	34,5	25,5

1.24. İçinden ýandyrylýan dwigateliň silindrini berkidýän şpilkanyň (hyrly sterženiň) diametrini saýlamaly. Şpilkalara güýçler deň ýaýran diýip hasap etmeli. Berlen: silindriň içki diametri $D=100 \text{ mm}$; silindriň içindäki gazyň iň uly basyşy $p=10 \text{ MPa}=1 \text{ kN/sm}^2$, şpilkalaryň sany $n=8$, şpilkanyň materialyna rugsat edilyän dartgynlyk 6 kN/sm^2 -e deň.



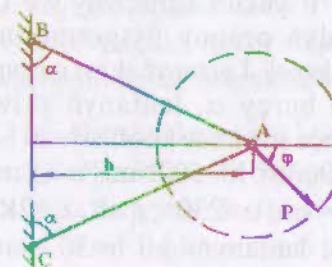
1.25-nji surat

1.25. Hemişelik göwrümleri bolan sterženler A düwne berkidilen. α burçuň haýsy ululygynda düwne goýlan rugsat edilyän güýjüň iň uly bahasy bolar? Sterženiň materialynyň rugsat edilyän dartgynlygy $[\sigma]$ deň bolanda güýjüň ululygyny kesgitlemeli.



1.26-nji surat

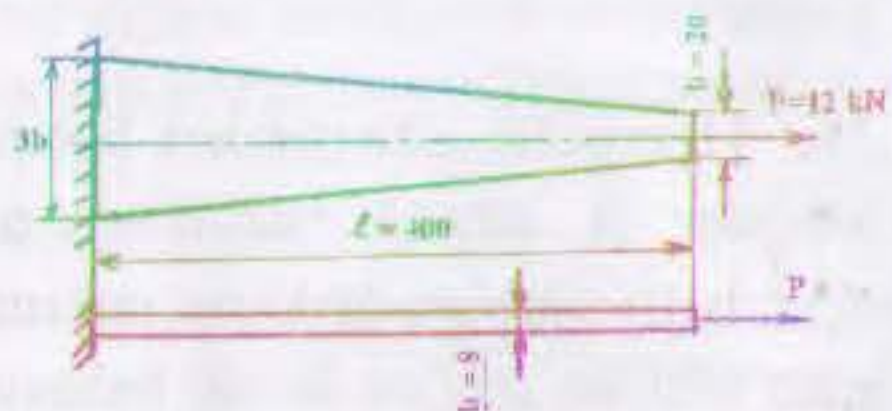
1.26. Sterženleriň materialy we gyzdrylýan temperaturasy birmeňzeş bolanda we β burçlaryň haýsy gatnaşygynda sterženlerde temperatura dartgynlyklary döremeýär? Dereg üsti BÇ-den A düwne çenli aralyk hemişelik ($h = \text{const}$).



1.27-nji surat

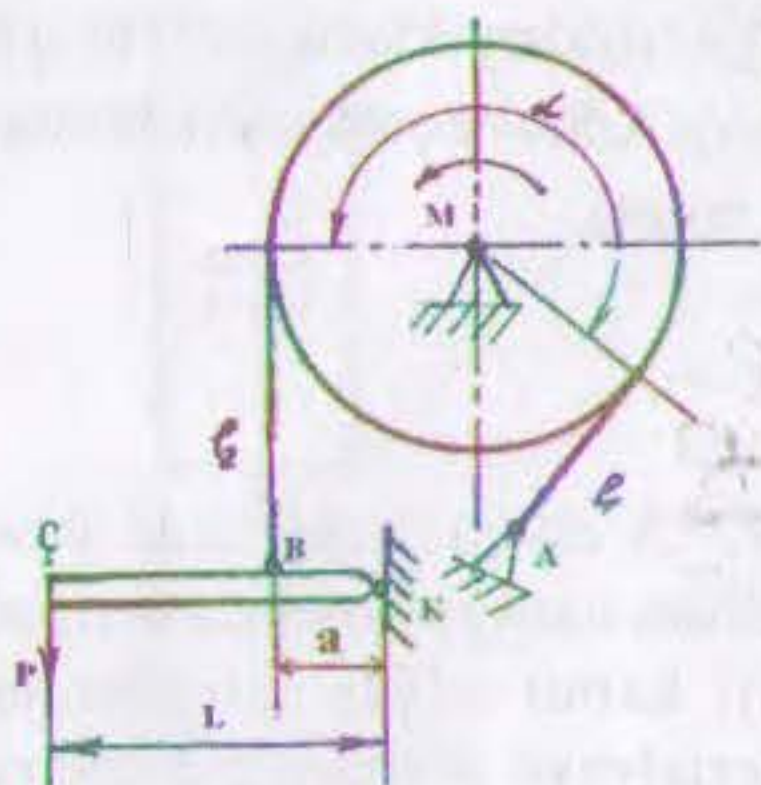
1.27. A düwün tekizlikde ýuwaş aýlanýan ululygy boýunça hemişelik güýji kabul edýär. Sterženleriň materialynyň massasynyň minimal bahasynda α burçuň ululygyny kesgitlemeli. Sterženleriň meýdany birmeňzeş berklik şertinden kesgitlenilýär.

1.28. Öňünden gyzdyrylan kiçi radiusy r gurşaw, radiusy R bolan tigre geýdirilen. Eger gurşawyň kese kesiginiň meýdany A we maýyşgaklyk moduly E bolsa, gurşaw sowadylandan soň gurşawdaky dartýş güýjüni we dartgynlygy kesgitlemeli (tigri gysylmaýan diýip hasap etmeli).



1.29-nji surat

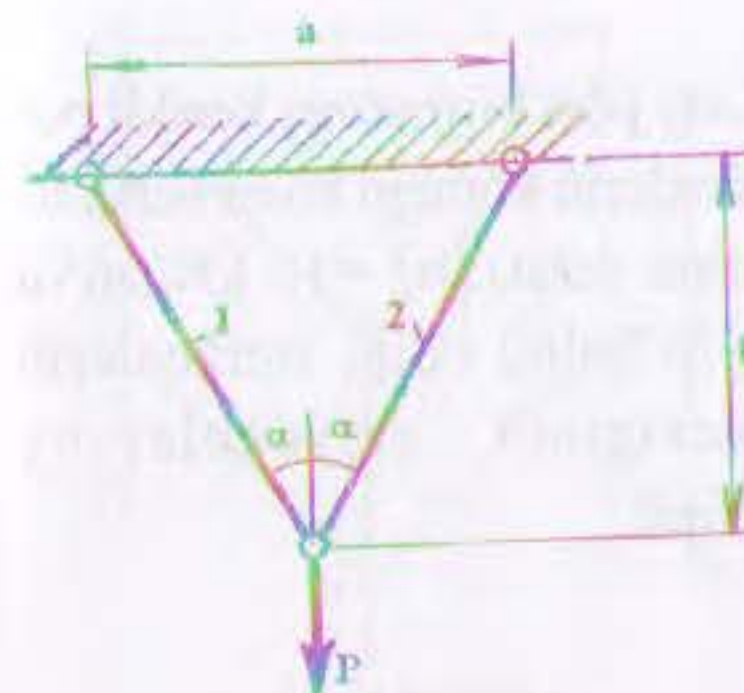
1.30. Dinamiki koeffisiýenti $k_d = 2$ bolan birdenkä goýlan süýndürji güýçden polat sterženiň kese kesiginiň meýdanyny kesgitlemeli. Sterženiň otositel durkuny üýtgetmesi $1/1800$ -den köp bolmaly däl. Eger sterženiň materialynyň berklik çägi $\sigma_b = 42 \text{ kN/sm}^2$ bolsa, ätiýaçlyk koeffisiýentini kesgitlemeli.



1.31-nji surat

1.29. Üýtgeýän kesikli dýuralýumin zolagyň süýnmesini kesgitlemeli (surata seret). $E = 0,7 \cdot 10^4 \text{ kN/sm}^2$ diýip kabul etmeli.

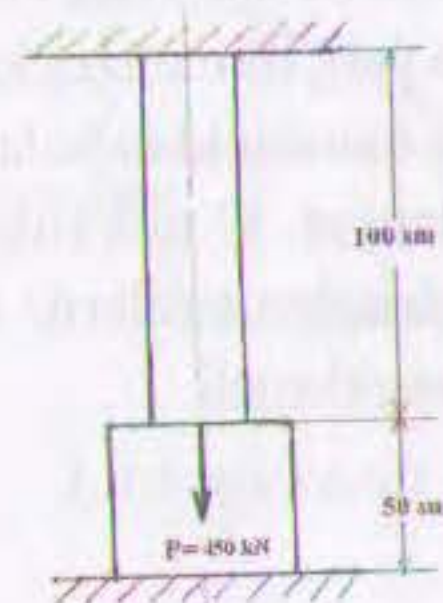
1.31. Çyzgyda hereketi togtadyjy enjamyň shemasy şekillendirilen. Radiusy R bolan şkiwi moment M aýlaýar. Şkiwi togtadyjy momenti ÇK ryçaga goýlan P güýjüň täsirinden şkiw bilen AB polat lentanyň arasynda döreyän sürtülme güýjüni döredýär. M momenti deňagramlaşdyrmak üçin gerek bolan P ýüküň agramyny we Ç nokadyň ornuny üýtgetmesini kesgitlemeli. Lentanyň şkiwi gurşap alýan burçy α , lentanyň şkiw boýunça sürtülme koeffisiýenti f -deň. Berlen: $M = 500 \text{ Nm}$; $R = 0,2 \text{ m}$; $L = 5a = 1 \text{ m}$; $\alpha = 230^\circ$; $\ell_1 = R$, $\ell_2 = 2R$; $f = 0,2$; lentanyň ini $b = 30 \text{ mm}$; galyňlygy $h = 1 \text{ mm}$. KÇ ryçagy absolýut gaty diýip hasap etmeli.



1.32-nji surat

1.32. Iki birmeňzeş steržene P güýç goýlan (surata seret). Sterženli ulgama iň az material harç bolar ýaly h aralyk nähili bolmaly?

1.2 Statiki kesgitlenmeýän sterženli ulgamlaryň hasaby

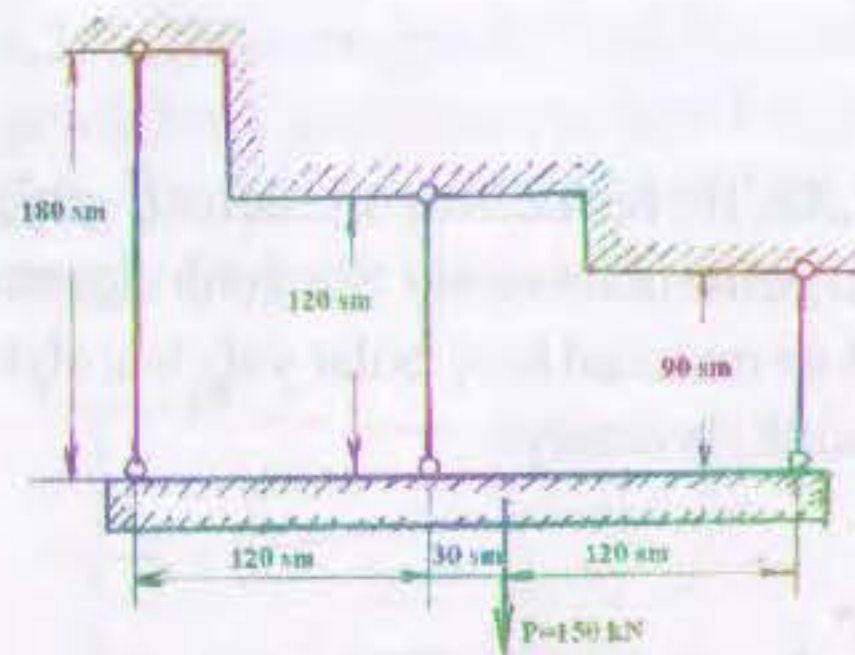


1.33-nji surat

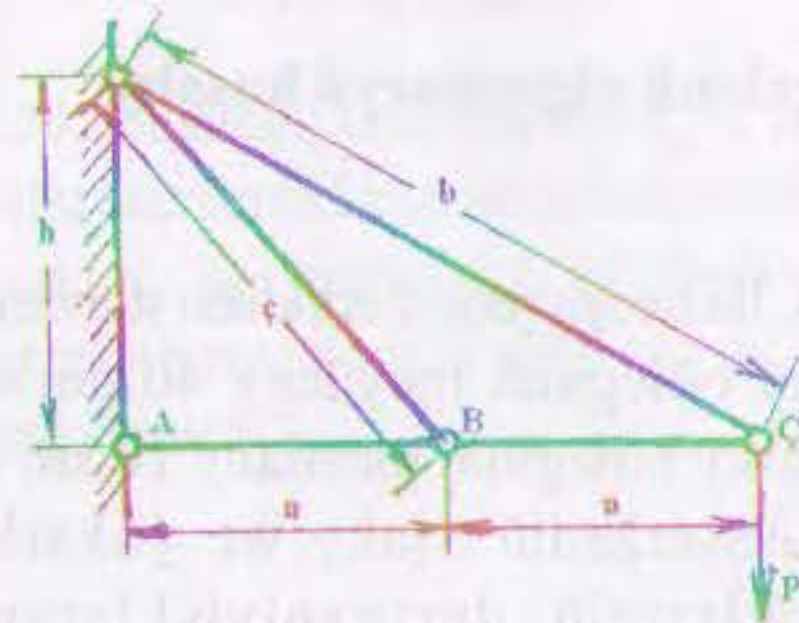
1.33. Iki tarapy jebis berkidilen sterženiň aşaky böleginiň meýdany 40 sm^2 -a, ýokarky böleginiň meýdany 10 sm^2 -a deň. Sterženiň aşaky we ýokarky bölekleriniň dartgynlylyklaryny kesgitlemeli.

1.34. Tros merkezi böleginiň diametri $d_1 = 5 \text{ mm}$ bolan mis simden we bu bölegi gurşap alan diametri $d_2 = 2,5 \text{ mm}$ bolan dokuz polat simden ybarat. Simleri parallel hasap edip, $P = 5 \text{ kN}$ ýük asylanda, trosuň simlerindäki dartgynlygyny kesgitlemeli.

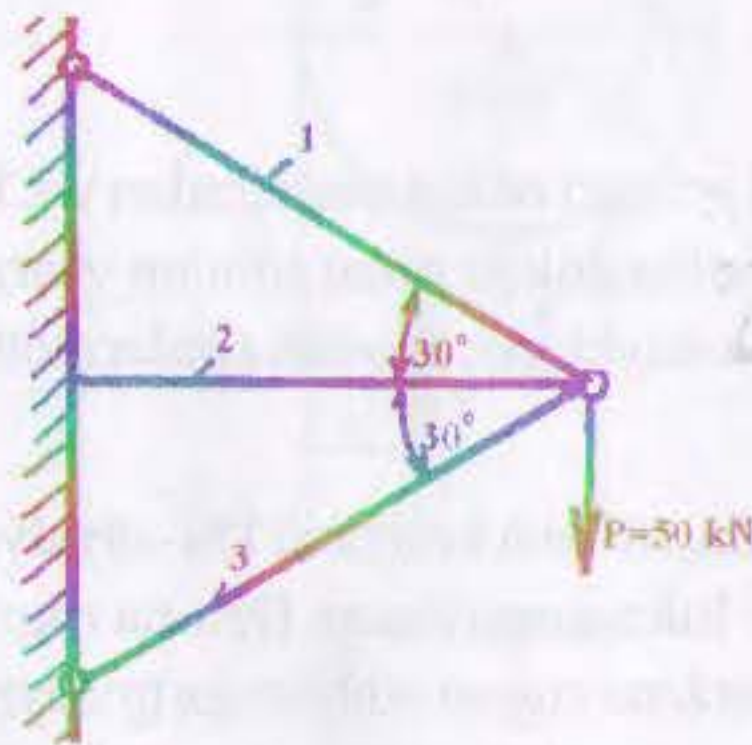
1.35. Kwadrat kese kesikli demirbeton sütün, sütüniň kesiginiň 1%-ini tutýan tegelek kese-kesikli dört polat sterženler bilen armirlenen. Betona rugsat edilýän dartgynlyk $0,6 \text{ kN/sm}^2$, polat steržene rugsat edilýän dartgynlyk 12 kN/sm^2 bolsa, sütüniň taraplary we sterženiň diametri näçe bolmaly? Poladyň maýyşgaklyk modulynyň betonyň maýyşgaklyk modulyna gatnaşygy 10-a deň. Sütüniň göterýän ýüki 1000 kN -a deň.



1.36-njy surat



1.37-nji surat

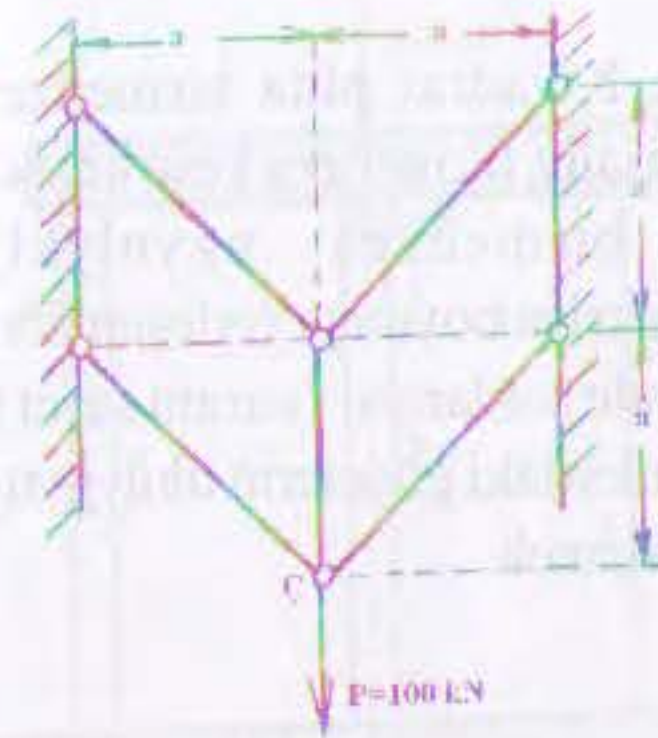


1.38-nji surat

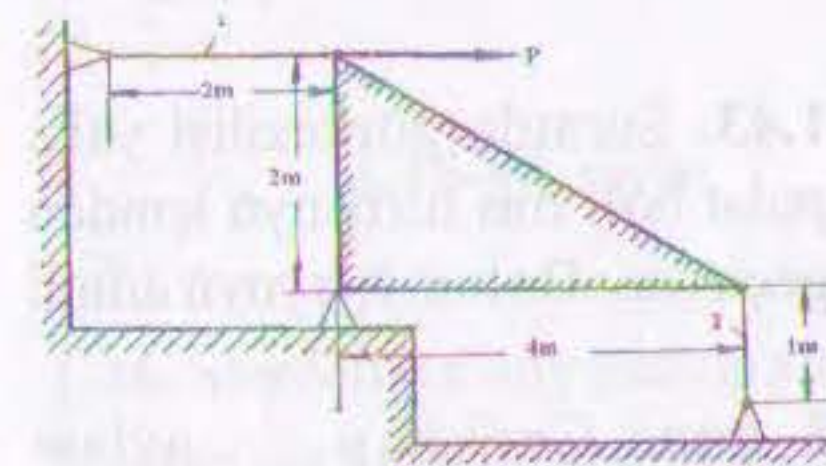
1.36. Gaty pürs birmeñzeş kesikli polat sterženleriň kömegi bilen berkidilen (surata seret). $[\sigma] = 16 \text{ kN/sm}^2$ -a deň diýip kabul edip, sterženleriň kese-kesiginiň meýdanlaryny kesgitlemeli.

1.37. Gaty AÇ balka, A nokatda diwara şarnirli berkidilen we suratda görkezilişi ýaly, birmeñzeş kesikli we birmeñzeş materialdan bolan iki sim bilen saklanýar. Ç nokatda goýlan ýüküň täsirinden simlerde döreyän güýçleri kesgitlemeli.

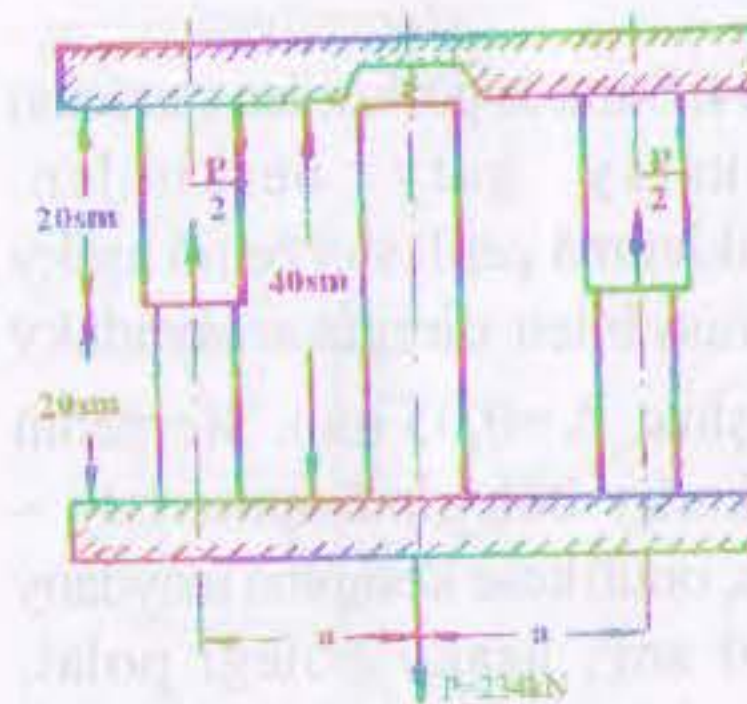
1.38. Bir nokatda birmeñzeş materialdan üç steržen şarnirli berkidilen (surata seret). Kese-kesikleriniň meýdanlary: birinji sterženiňki 2 sm^2 , ikinji sterženiňki 3 sm^2 we üçünjiniňki 4 sm^2 bolsa, sterženlerdäki dartgynlylyklary kesgitlemeli.



1.39-njy surat



1.40-njy surat

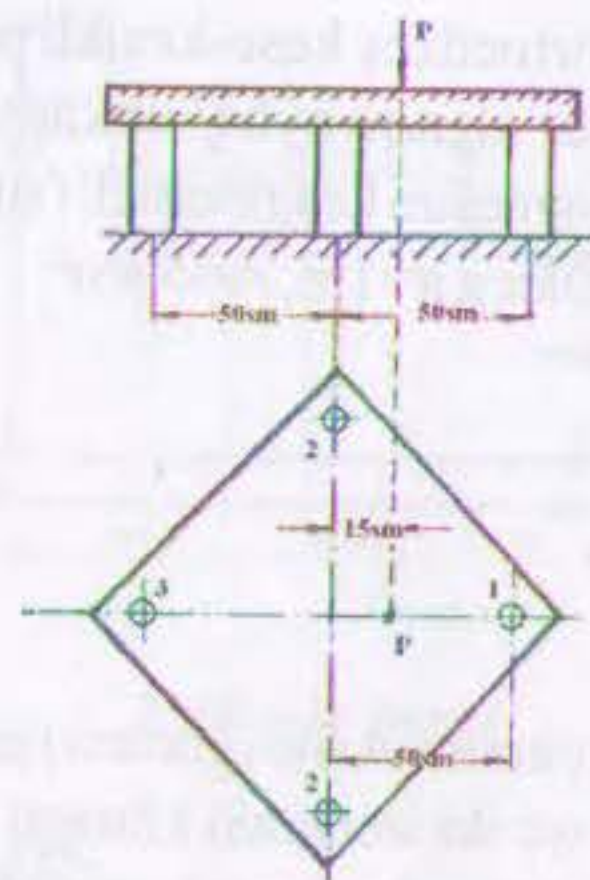


1.41-nji surat

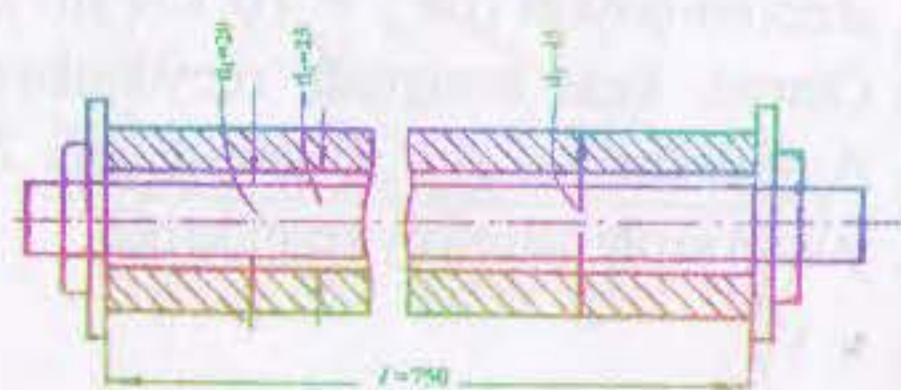
1.39. Birmeñzeş kese-kesikli polat sterženler ulgamynyň Ç nokadynyň aşak süýşmesini kesgitlemeli (surata seret). Ölçeg $a = 1 \text{ m}$, $A = 5 \text{ sm}^2$.

1.40. Gaty konstruksiya (gurnaw) şarnirli diregiň we iki sterženiň kömegi bilen binýatda berkidilen (surata seret). Birinji steržen-polat ($[\sigma_p] = 16 \text{ kN/sm}^2$), ikinji steržen-çoyun ($[\sigma_{\text{ç}}] = 10 \text{ kN/sm}^2$). Olaryň kese kesiginiň meýdanlary $A_{\text{ç}} = 50 \text{ sm}^2$ -a, $A_p = 30 \text{ sm}^2$ -a deň. P ýüküň iň uly bahasyny kesgitlemeli.

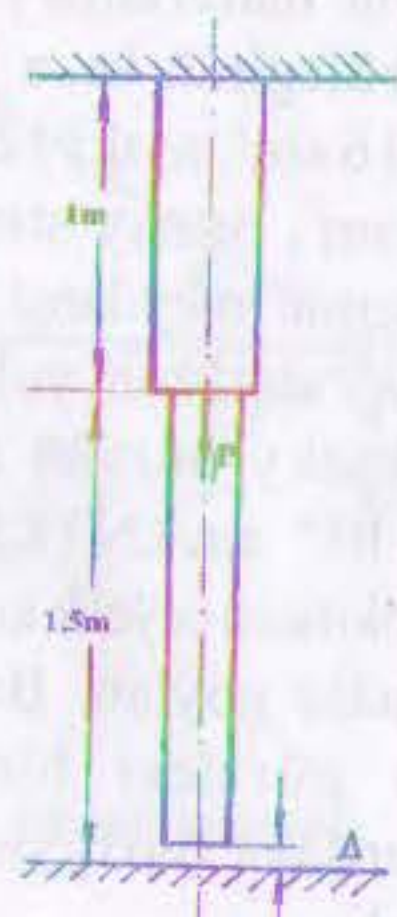
1.41. Iki gaty pürs suratda görkezilişi ýaly üç steržen bilen birikdirilen. Çetki sterženleriň materiallary – polat, ýokarky böleginiň kese kesiginiň meýdany 16 sm^2 , aşaky böleginiňki bolsa 10 sm^2 , ortaky steržen-mis, kese kesiginiň meýdany 20 sm^2 -a deň. Ortaky sterženiň ýokarky üsti bilen ýokarky pürsüň arasynda $\alpha = 1,25 \cdot 10^{-4} \text{ sm/kN}$ (1 kN ýükde pružiniň çökmesi) çyýelik koeffisiyenti bolan pružin goýlan. Berlen ýük boýunça pürsleri birikdirýän sterženlerdäki dartgynlylyklary kesgitlemeli.



1.42-nji surat



1.43-nji surat



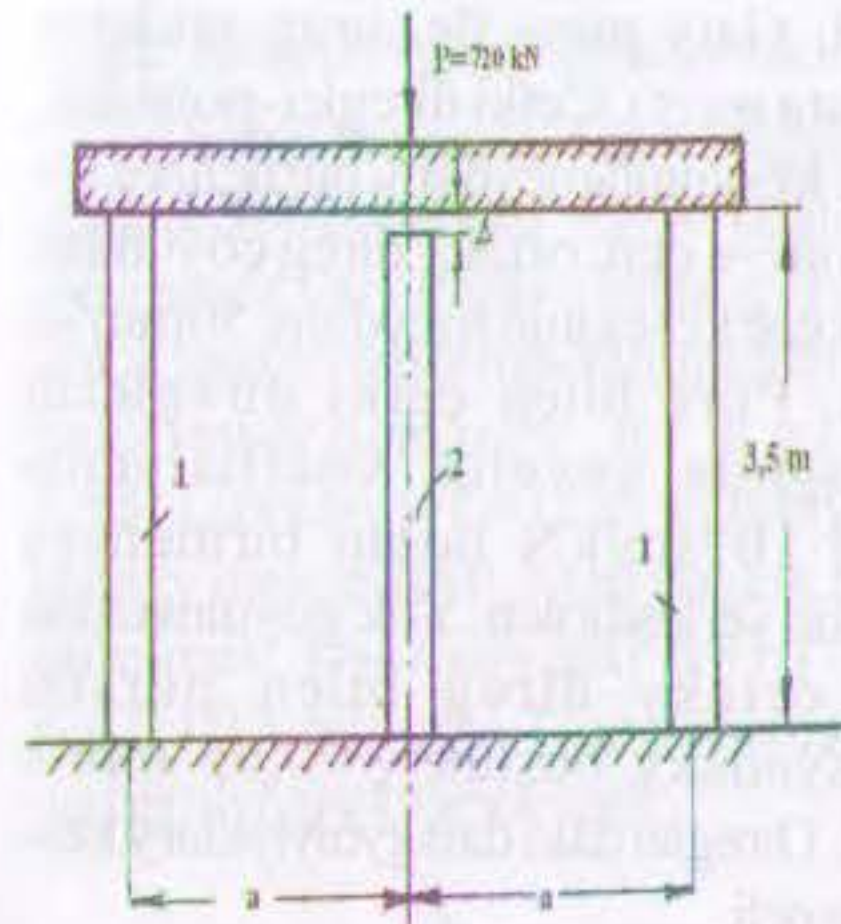
1.44-nji surat

1.42. Kwadrat plita birmeňzeş materially, birmeňzeş kese kesikli we birmeňzeş uzynlykly simmetriýa boýunça ýerleşen dört sütünde saklanýar (surata seret). Sütünlerdäki güýçleriň ululygyny kesgitlemeli.

1.43. Suratda görkezilişi ýaly, polat bolt mis turbanyň içinden geçirilen. Boltuň hyrynyň ädimi

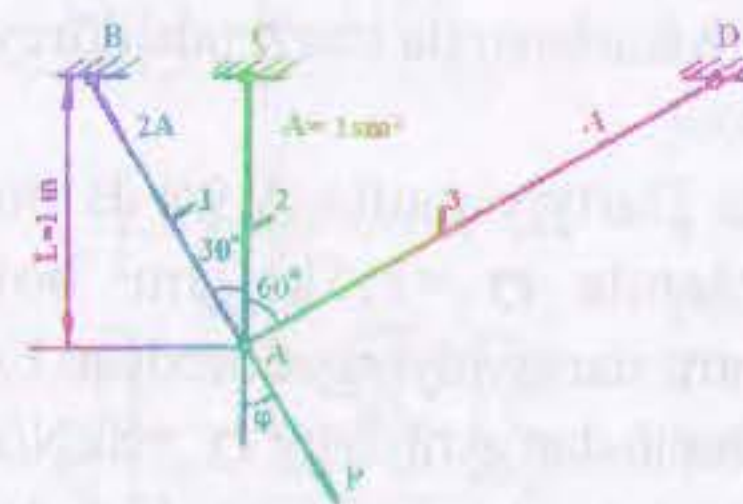
3 mm. Gaýkany $\frac{1}{4}$ aýlaw çekdireniňde boltda we turbada nähili dartgynlyklar döreýär?

1.44. Suratda görkezilen sterženiň ýokarsy gaty berkidilen. Ýüklenmä çenli sterženiň aşaky gyrasy bilen diregiň arasyndaky boşluk $\Delta = 0,05$ mm. Sterženiň ýokarky böleginiň materialy – mis, onuň kese kesiginiň meýdany 150 sm^2 , aşaky bölegi polat, kese-kesiginiň meýdany 50 sm^2 . Steržen $P = 200 \text{ kN}$ güýç bilen ýüklenende, onuň ýokarky we aşaky böleklerindäki dartgynlyklary kesgitlemeli.



1.45-nji surat

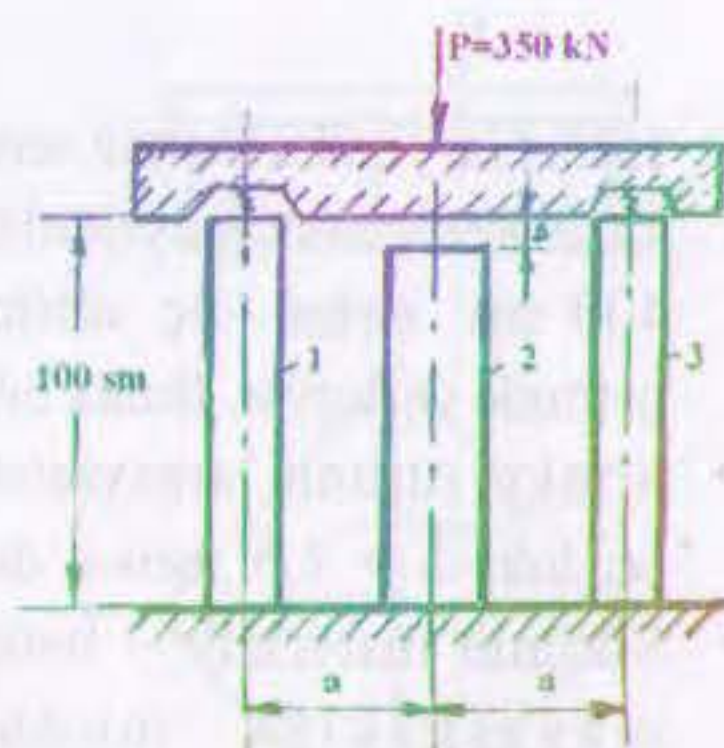
1.46. Steržen we ony gurşap alan turba bir wagtda P güýç bilen dartylýar. Steržen we turba dürli-dürli materiallardan we olaryň uzynlyklary l -e deň, kese kesikleriniň meýdany bolsa, degişlilikde, A_1 we A_2 deň. Maýyşgaklyk modullary E_1 we E_2 . Ýüklenmeden soň bu dartgynlyklaryň gatnaşygy m bolar ýaly, steržende we turbada nähili deslapky dartgynlyklary σ_1 we σ_2 oýandyrmaly.



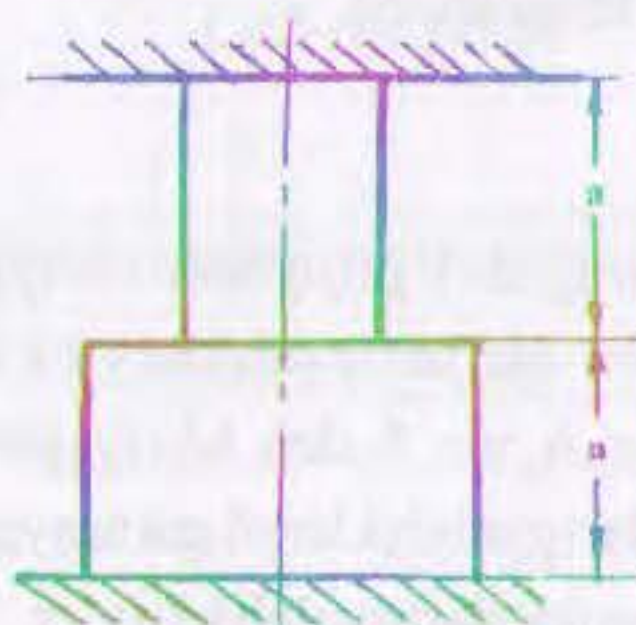
1.47-nji surat

1.45. Gaty balka (surata seret) kese kesiginiň meýdanlary 400 sm^2 bolan üç sütüniň üstünde ýerleşýär. Balka bilen ortaky sütüniň arasyndaky boşluk $\Delta = 1,5 \text{ mm}$ -e deň. Sütüniň materialy – beton, maýyşgaklyk moduly $E = 1400 \text{ kN/sm}^2$. Sütünlerde döreýän dartgynlyklary kesgitlemeli.

1.47. A düwün wertikal boýunça $\Delta = 0,05 \text{ sm}$ süýşýän bolsa, üç sterženli düwne goýlan güýjüň ululygyny we ugruny tapmaly. $E = 2 \cdot 10^3 \text{ kN/sm}^2$ -a deň diýip kabul etmeli.

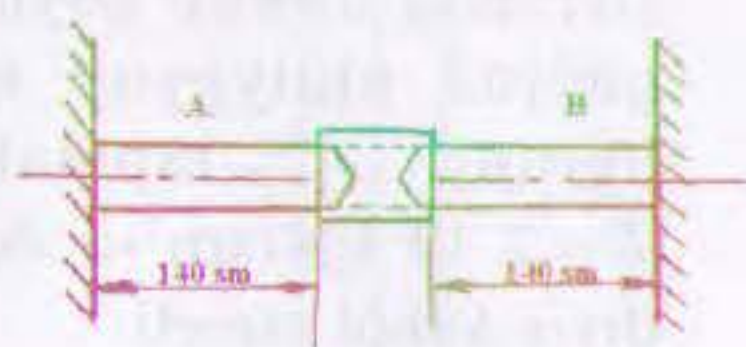


1.48-nji surat



1.49-nji surat

1.50. Uzynlygy $\ell = 2\text{ m}$ polat sterženiň iki tarapy diwara berkidilen. Sterženiň haýsy hem bolsa bir tarapy diwaryň içinde $\Delta = 0,05\text{ mm}$ boşlukda ornuny erkin üýtgedip bilýär. Temperatura 40°S ýokarlananda steržende döreyän dartgynlylygy kesgitlemeli.



1.50-nji surat

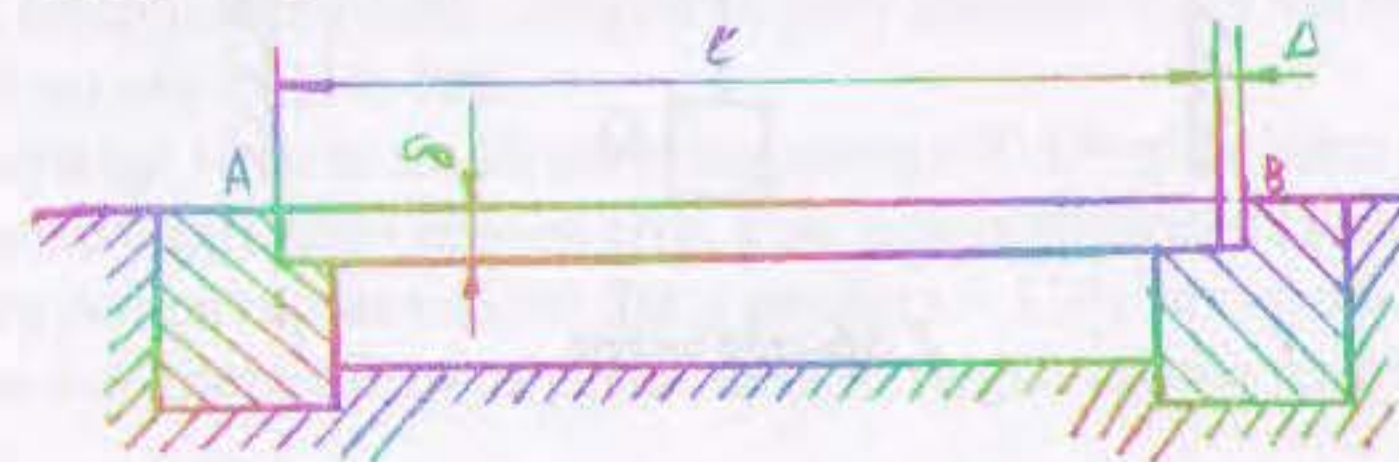
1.48. Gaty pürsi üç direg saklaýar (surata seret). Çetki diregler-polatdan, kese kesiginiň meýdany birmeňzeş we 20 mm^2 -a deň, ortaky direg çöýundan we kese kesiginiň meýdany 50 mm^2 -a deň. Pürs bilen çetki diregleriň arasynda çeyelik koeffisiýenti $\alpha = 5 \cdot 10^{-4}\text{ sm/kN}$ bolan birmeňzeş pružin ýerleşdirilen. Ýük goýulmazdan öň ortaky direg bilen pürsüň arasyndaky boşluk $\Delta = 0,05\text{ mm}$ -e deň. Direglerdäki dartgynlylyklary kesgitlemeli.

1.49. Polat steržen (surata seret) iki tekizligiň arasynda $t_1 = +5^\circ\text{S}$ temperaturada berkidilen; ýokarky bölegiň kese kesiginiň meýdany $A_1 = 5\text{ sm}^2$ aşaky böleginiňki bolsa $A_2 = 10\text{ sm}^2$. Temperatura $t_2 = +25^\circ\text{S}$ ýokarlananda sterženiň ýokarky we aşaky böleklerinde döreyän dartgynlylyklary kesgitlemeli.

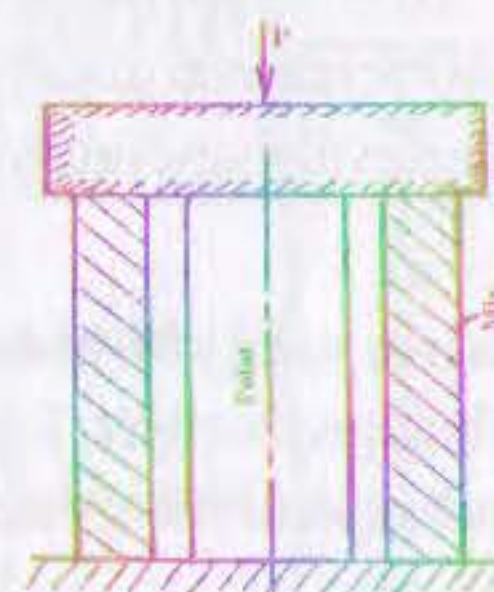
1.51. Dartyjy mufta A we B polat steržende $\sigma_1 = 1,5\text{ kN/sm}^2$ bolan süýnme dartgynlylygy döredýär. Eger sterženiň dartgynlylygy $\sigma_2 = 8\text{ kN/sm}^2$ bolar ýaly temperatura $\Delta t = -10^\circ\text{S}$ üýtgedilende, muftanyň kömegi bilen sterženiň uzynlygyny näçe üýtgetmeli?

1.52. Her haýsynyň kese kesikleriniň meýdany $37,5\text{ sm}^2$ we uzynlyklary 50 sm bolan inwar we mis turbajyklary 0°S temperaturada bir-birine seplenip goýlan. Soň bolsa olar $+36,4^\circ$ çenli gyzdyrylýar we olaryň umumy uzynlyklary üýtgemez ýaly P güýç bilen gysylyar. Bu güýjüň ululygy näçe bolýar we ýokarlandyrylan temperaturada turbajyklaryň her haýsynyň uzynlyklary näçä deň? Inwar üçin $\alpha_i = 0$ we $E = 2 \cdot 10^4\text{ kN/sm}^2$.

1.53. Uzynlygy $\ell = 12\text{ m}$, galyňlygy $\delta = 40\text{ sm}$ bolan köpriniň demirbeton plitasy direge $\Delta = 0,3\text{ sm}$ boşluk bilen goýlan. Demirbetonyň uzynlygyna giňelmek koeffisiýenti $\alpha = 10^{-5}$ -e deň, maýyşgaklyk moduly bolsa, $E = 2 \cdot 10^3\text{ kN/sm}^2$. Temperatura $\Delta t = 30^\circ\text{S}$ ýokarlananda plitadaky dartgynlylygy kesgitlemeli.

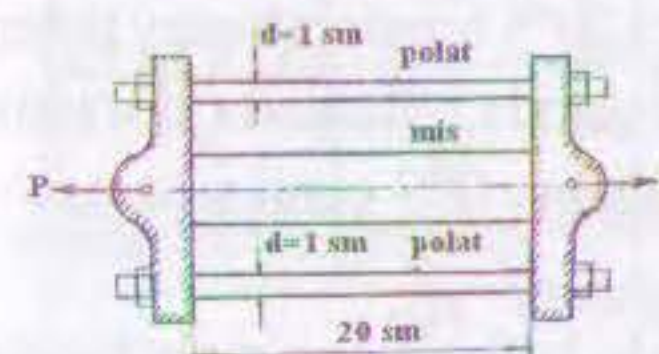


1.53-nji surat



1.54-nji surat

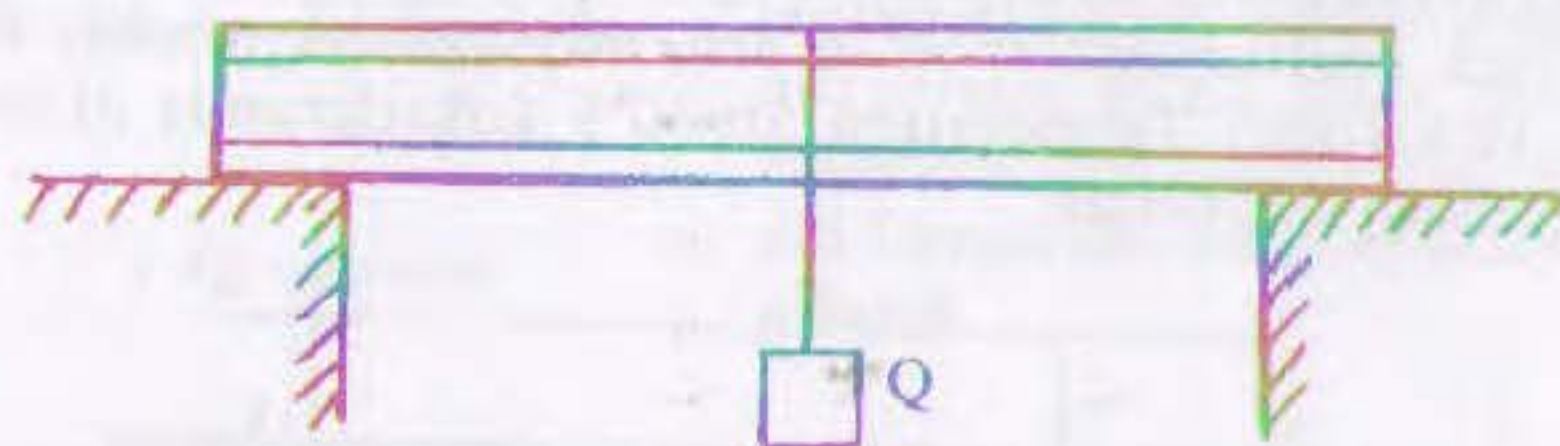
1.54. Gaty plitanyň üsti bilen 45 kN ýük meýdany 15 sm^2 polat silindre we meýdany 20 sm^2 içi boş mis silindre geçirilýär (surata seret). Güýç iki silindriň hem oklary boýunça täsir edýär. Ýük goýlandan soň temperatura 30°S ýokarlanýar. Ýüküň temperatura üýtgemezden öňki we üýtgäninden soňky ýaýraýşyny tapmaly.



1.55-nji surat

1.55. Suratda görkezilişi ýaly, iki gaty guýma polat boltlar bilen berkidilen. Uzynlygy $20,02\text{ sm}$ we kesekesiginiň meýdany 6 sm^2 bolan mis sterženi guýmanyň arasynda ýerleşdirmek üçin, sonuň ýaly-da guýmany süýşürmek üçin P güýjüň ululygyny tapmaly. P güýç aýrylan-dan soň guýmanyň arasyndaky uzynlygy tapmaly.

1.56. 16-njy belgili polat iki tawraly balka iki diregiň üstünde ýerleşdirilen we $Q = 10 \text{ kN}$ ýük bilen diregleriň ortasynda ýüklenen (surata seret). Balkanyň direginde gorizonta ornuny üýtgetmesine sürtülme güýji päsgel berýär. Balka bilen diregiň üstüniň sürtülme koeffisiýenti $f = 0,3$ -e deň. Balkada dartgynlylygyň artmagyna çenli iň uly temperaturanyň tapawudyny kesgitlemeli we temperatura dartgynlylygyny kesgitlemeli.



1.56-njy surat

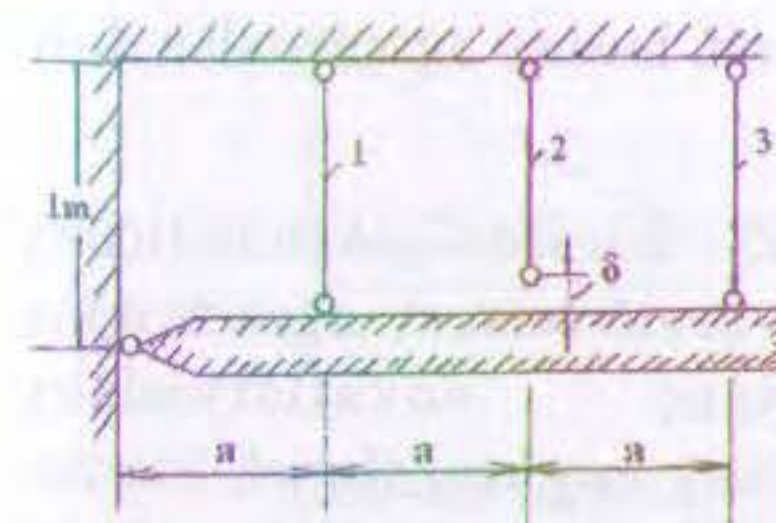
1.57. Tomus wagtynda relsde gysylma bolmaz ýaly relsleriň sepinde zerur bolan boşlugyň ululygyny kesgitlemeli. Relsler $+10^\circ\text{S}$ temperaturada ýerleşdirilip goýulýar; Tomusdaky iň uly temperatura $+60^\circ\text{S}$; relsleriň uzynlygy 8 m -e deň. Relsler boşluksyz ýerleşdirilip goýlanda dartgynlylygyň ululygy nähili bolar?

1.58. Polat bug geçiriji turbanyň $+15^\circ\text{S}$ temperaturada uzynlygy 30 m deň. Bu turbadan $+180^\circ\text{S}$ temperatura çenli gyzdyrylan bug goýberilýär. Eger turbanyň giňelmegine hiç hili päsgelçilik bolmasa, turbanyň uzynlygy näçä deň bolar?

Eger turba uzalmaýan bolsa, turbadaky dartgynlylyk näçä deň bolar?

1.59. $t_1 = 135^\circ\text{S}$ -a çenli gyzdyrylan mis halka, $t_2 = 20^\circ\text{S}$ temperaturasy bolan polat wala geýdirilen. a) halka 20°S sowadylanda, halkada döreyän dartgynlylygy kesgitlemeli; b) waly we halkany 0°S çenli sowatsaň, halkadaky dartgynlylyk näçe ýokarlanar?

ç) halkadaky dartgynlylyk nola deň bolar ýaly halkany we waly haýsy temperatura çenli gyzdyrmaly? $E_m = 10^4 \text{ kN/sm}^2$, $\alpha_m = 1,6 \cdot 10^{-5}$, $\alpha_p = 1,25 \cdot 10^{-5}$.



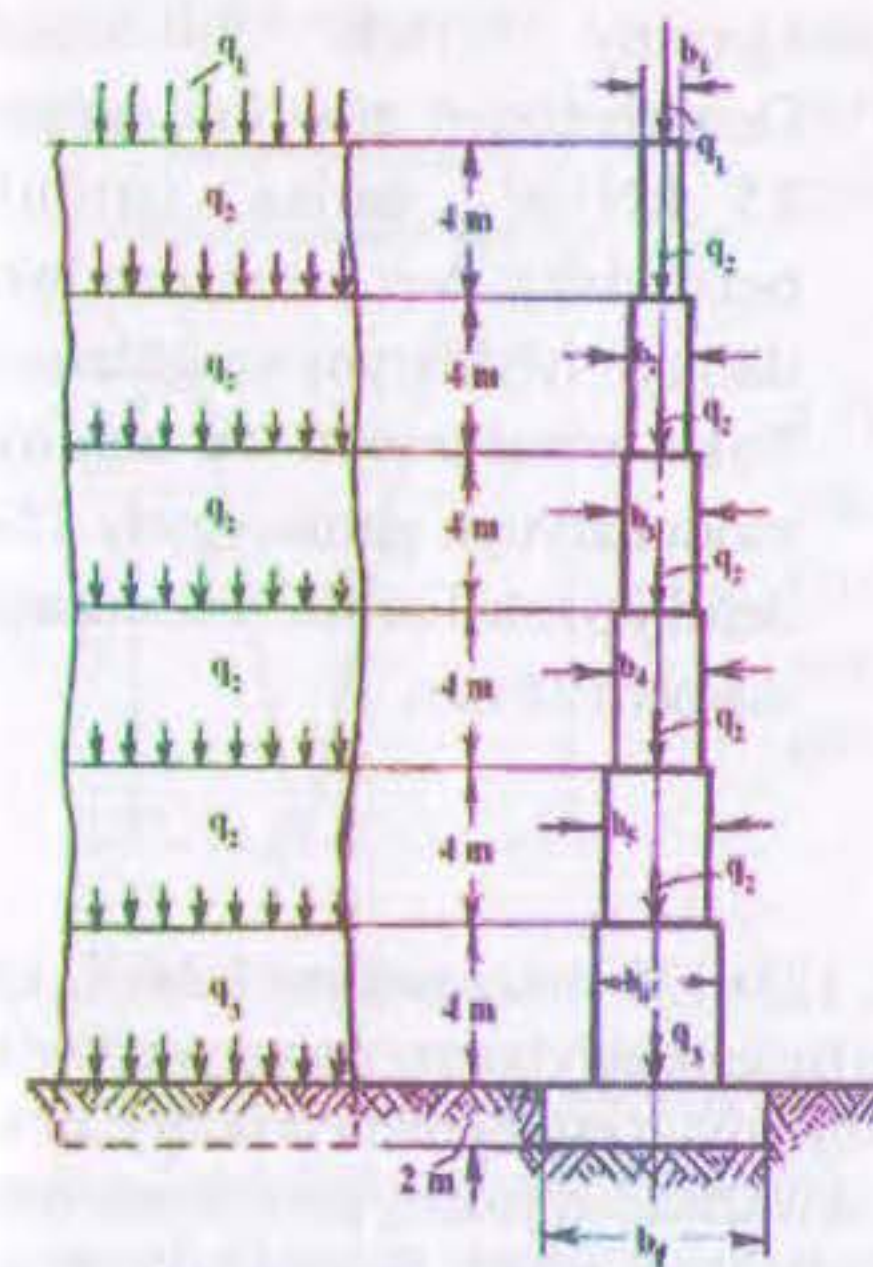
1.60-njy surat

1.60. Gaty pürs kese kesigi 20 sm^2 bolan birmeňzeş meýdanly üç polat sterženden asylan. Ortaky steržen taslama ölçeginden $\delta = 0,5 \text{ mm}$ gysga ýerine ýetirilen (surata seret). Konstruksiýa ýygnalandan soň sterženlerdäki dartgynlylyklary kesgitlemeli.

1.3 Hususy agramy hasaba almak

1.61. Hemişelik kese kesikli, beýikligi 8 m bolan sütüniň hususy agramyndan iň aşaky kesigindäki gysma dartgynlylygyny kesgitlemeli. Örümiň bir kub metriniň agramy 20 kNa deň.

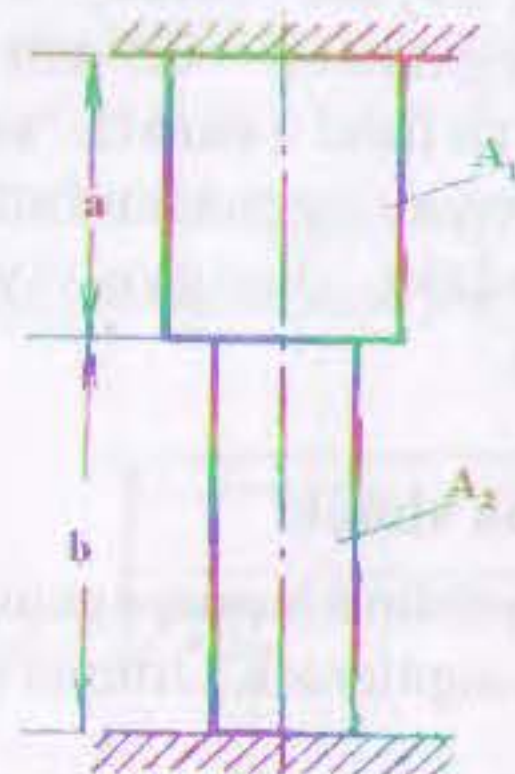
1.62. Beýikligi 10 m bolan kwadrat daş sütün 500 kN güýç bilen ýüklenen bolsa, hususy agramyny hasaba alyp, kese kesiginiň ölçegini kesgitlemeli. Örümiň gysylma rugsat edilyän dartgynlylygy $0,1 \text{ kN/sm}^2$ -a, udel agramy bolsa 2 -ä deň. Sterženiň uzynlygyna dartgynlylygyň ýaýraýşynyň epýuryny gurmaly.



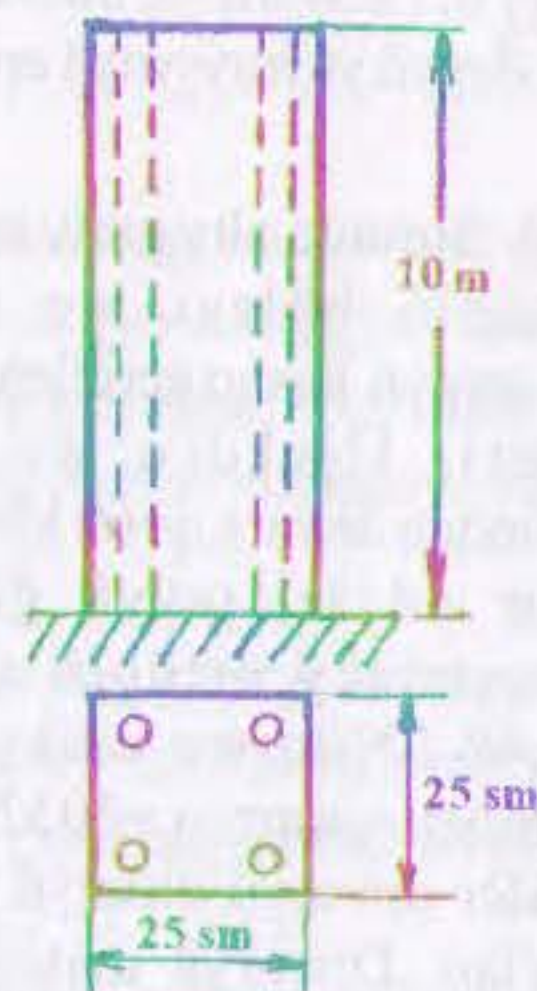
1.63-nji surat

1.63. Suratda alty gatly jaýyň ön ýüzüniň bölegi we kerpiç diwarynyň kesigi getirilen (surata seret). Üçekden we jaýyň üstünden diwara $q = 60 \text{ kN/m}$ ýük täsir edýär, jaýyň gatynyň arasyndaky örtügiň agramy $q_2 = 40 \text{ kN/m}$ we aşaky gatyň polunyň agramy $q_3 = 30 \text{ kN/m}$. Bu ýükler diwaryň okunyň boýuna goýlan. Diwaryň materialynyň göwrüm agramy 20 kN/m^3 -a deň. Rugsat edilyän dartgynlylyk $[\sigma] = 0,06 \text{ kN/m}^2$ bolsa, diwarlaryň iň kiçi galyňlygyny we binýadyň düşeginiň gumuna rugsat edilyän dartgynlylyk $0,05 \text{ kN/sm}^2$ bolsa, binýadyň inini kesgitlemeli.

1.64. Uzynlygy 120 m bolan polat sterženiň hususy agramyndan doly uzalmasyny kesgitlemeli.



1.65-nji surat

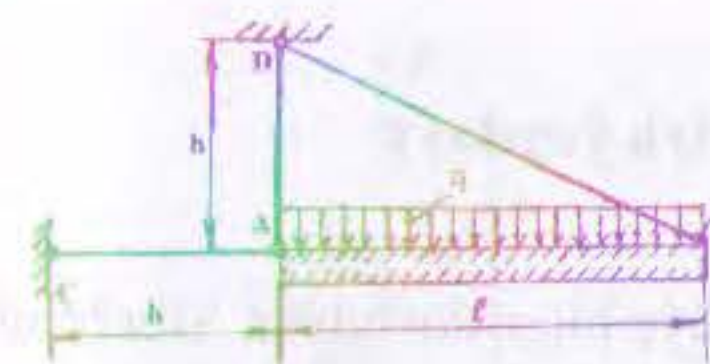


1.66-nji surat

1.67. Umumy uzynlygy $\ell=1200$ m, 125×125 mm kwadrat kesikli, içki deşiginiň diametri $d=50$ mm bolan köp başgançakly buraw ştangasy göwrüm agramy $\gamma=18 \cdot 10^{-6}$ kN/m² bolan suwuk toýun ergini bilen doldurylan we skwažina (guýa) çümdürilen. Ştanga skwažinadan ýokary göterilende onuň aşaky bölegine $P=60$ kN dartýan ýük täsir edýär. Ştangadaky iň uly dartgynlygy we onuň absolýut durkuny üýtgetmesini kesgitlemeli.

1.65. Suratda şekillendirilen sterženiň hususy agramyndan daýanç nokatlaryndaky gaýtargylary kesgitlemeli. Steržen ýokarky we aşaky bölekleriniň udel agramy γ we maýyşgaklyk moduly E bolan birmeňzeş materialdan ýasalan.

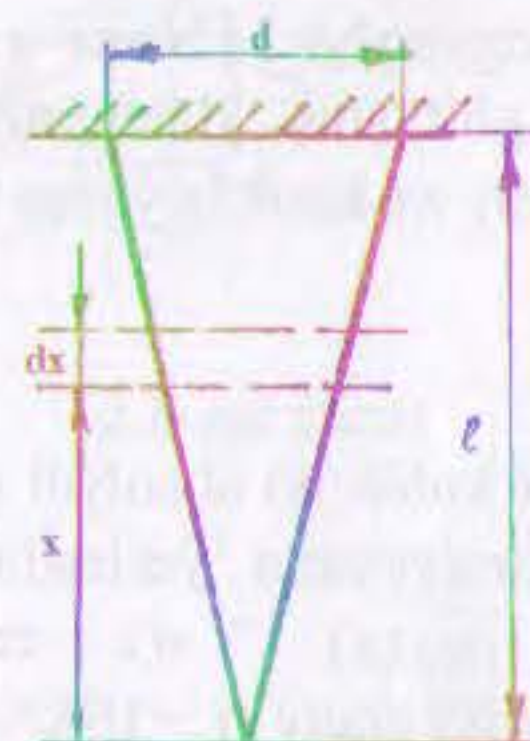
1.66. Suratda görkezilen ölçegli demirbeton sütün diňe hususy agramy bilen ýüklenen. Demirbetonyň göwrüm agramy 25 kN/m^3 bolsa, sütüniň betondaky we armaturadaky dartgynlyklaryny kesgitlemeli. Polat armaturanyň we betonyň modullarynyň gatnaşygyny 15-e deň diýip kabul etmeli. Armaturanyň diametri 25 mm.



1.68-nji surat



1.69-nji surat



1.70-nji surat

1.71. Hususy agramy bilen ýüklenen polat steržen ýokarsyndan wertikal asylan. Eger dartgynlyk 3 kN/sm^2 —dan ýokary bolmasa we poladyň udel agramy 7,85 bolsa, sterženiň rugsat edilyän iň uly uzynlygy näçä deň bolar? Sterženiň uzynlygyna dartgynlygyň ýaýraýşynyň epýuryny gurmaly.

1.68. Absolýut gaty AB pürs $q=5 \text{ kN/m}$ bolan hususy agramy bilen ýüklenen. Berkidiji AÇ we AD sterženleriň jemlenen agramy iň az bolar ýaly h uzynlygy kesgitlemeli. Srterženler polatdan $\gamma=78,5 \text{ kN/m}^3$, süýnmä rugsat edilyän dartgynlyk $[\sigma]_s=16 \text{ kN/sm}^2$, gysylma $[\sigma]_g=8 \text{ kN/sm}^2$. Sterženleriň kesikleri deň berklik şertinde saýlanylýar. $\ell=4 \text{ m}$ kabul edip, berkidiji sterženleriň iň az agramyny hasaplamaly.

1.69. Suratda görkezilişi ýaly, uzynlygy ℓ kese kesiginiň meýdany A we udel agramy γ bolan materialdan ýasalan sterženiň ýokarsy we aşagy berkidilen. Sterženiň hususy agramyndan ýokarky we aşaky kesiklerindäki dartgynlyklaryny kesgitlemeli we sterženiň uzynlygyna dartgynlygyň ýaýraýşynyň epýuryny çyzmaly.

1.70. Hususy agramynyň täsirinden konus şekilli sterženiň uzalmasyny kesgitlemeli (surata seret). Sterženiň uzynlygy ℓ , esasynyň diametri d we materialynyň göwrüm agramy γ deň.

II bap Çyzyk we tekiz dartgynlylyk ýagdaýy

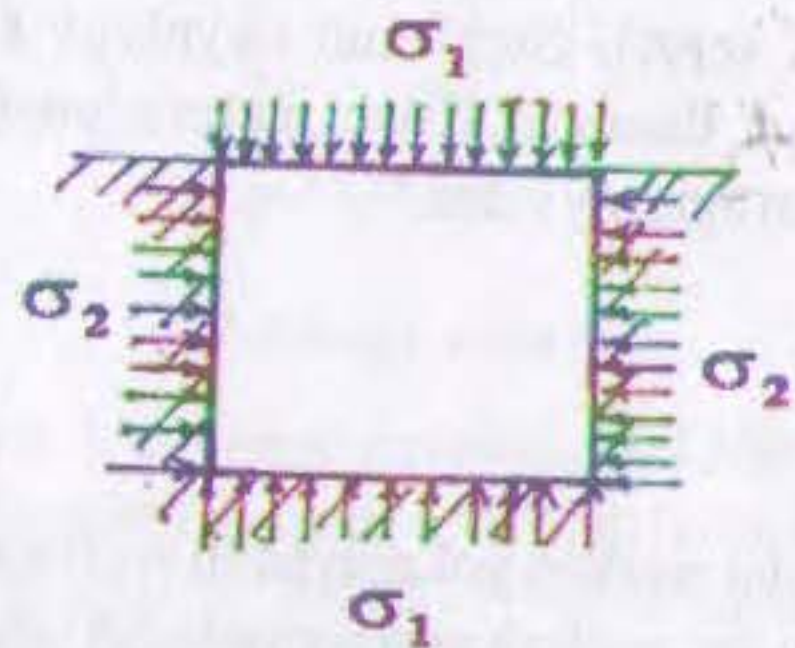
2.1. Diametri 6 sm bolan steržen 250 kN güýç bilen dartylýar. Sterženiň okuna 30° burç boýunça ýapgytlanan kesigiň normal we galtaşma dartgynlylyklaryny kesgitlemeli. Haýsy kesik boýunça galtaşma dartgynlylygyň iň uly bolýandygyny kesgitlemeli we onuň ululygyny hasaplamaly.

2.2. Diametri 7,5 sm bolan steržen 350 kN güýç bilen dartylýar. Kese kesikdäki doly dartgynlylygy kesgitlemeli. Sterženiň okuna 15° burç boýunça ýapgytlanan kesigiň doly we galtaşma dartgynlylygyny kesgitlemeli.

2.3. Tegelek kesikli steržen 150 kN güýç bilen dartylýar. Islendik kesikde galtaşma dartgynlylyk 6 kN/sm^2 -dan uly bolmadyk ýagdaýynda sterženiň diametrini kesgitlemeli.

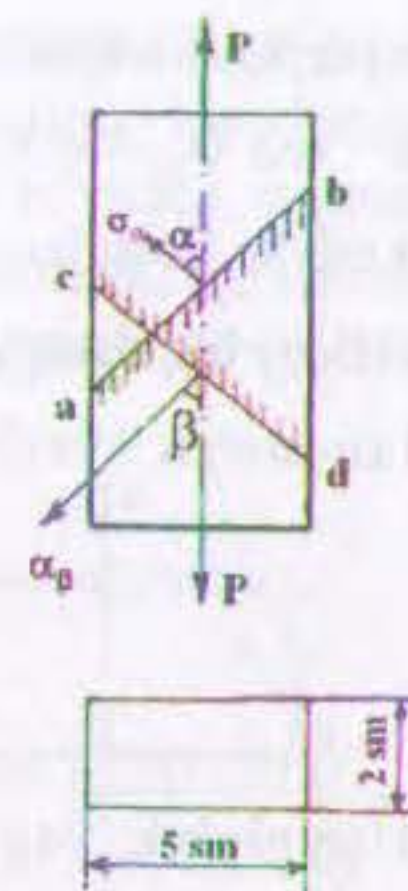
2.4. Dartylan sterženiň haýsy hem bolsa bir ýapgytlanan meýdançasýnda normal dartgynlylyk 7 kN/sm^2 -a, galtaşma dartgynlylyk bolsa 5 kN/sm^2 -a deň. Iň uly normal we galtaşma dartgynlylyklary kesgitlemeli.

2.5. Dartylan sterženiň kese-kesiginde normal dartgynlylyk 5 kN/sm^2 -a deň. Haýsy hem bolsa bir ýapgytlanan kesikde galtaşma dartgynlylyk $1,6 \text{ kN/sm}^2$ -a deň. Ýapgytlanan kesigiň ýagdaýyny we kesik boýunça täsir edýän normal dartgynlylygy kesgitlemeli.

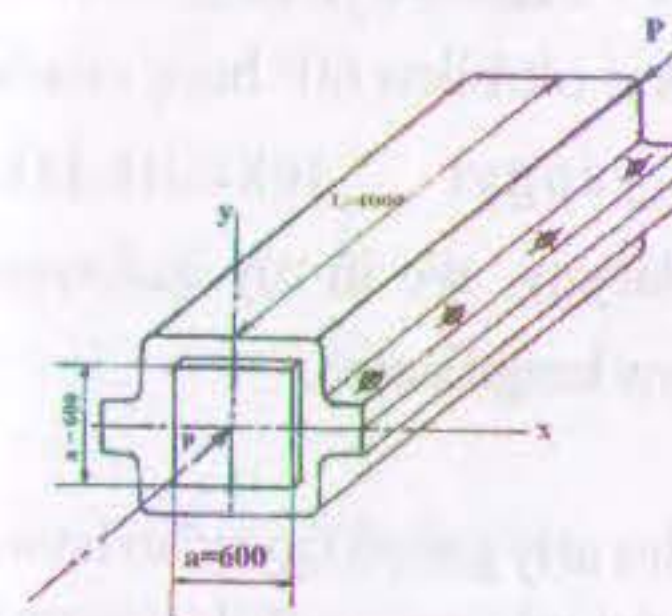


2.6-njy surat

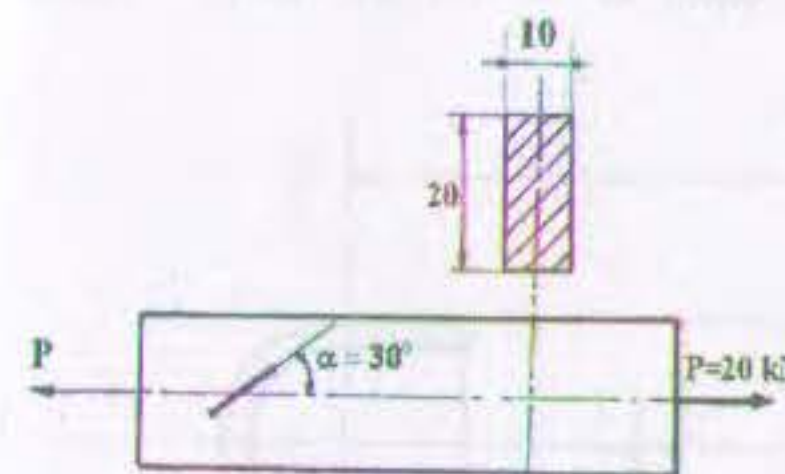
2.6. Polat kubik iki absolýut gaty diwaryň aralygynda ýerleşdirilen (surata seret) we erkin gapdalyndaky grany $\sigma_1 = 16 \text{ kN/sm}^2$ dartgynlylyk döredýän gysylma sezewar bolýar. Eger $\mu = 0,3$ bolsa, kubigiň gapdal granyndaky basyşy kesgitlemeli.



2.7-nji surat



2.8-nji surat



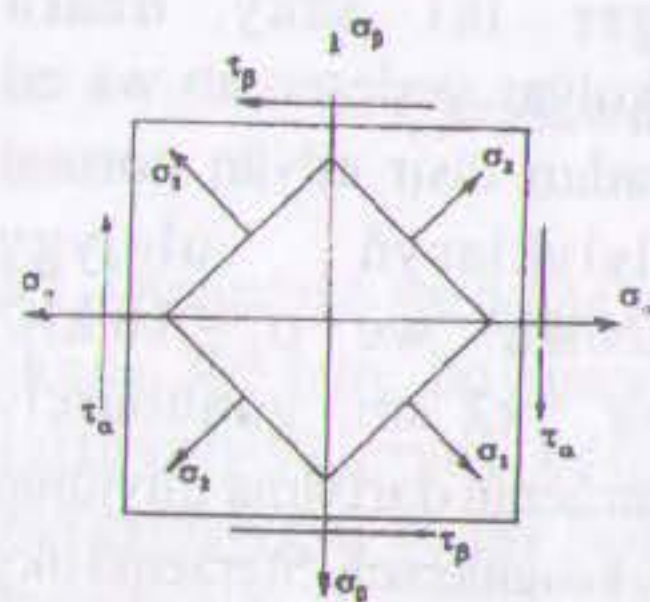
2.9-njy surat

2.7. Eger iki sany özara perpendikulýar ýerleşen ab we cd meýdançadan täsir edýän normal dartgynlylyklaryň ululygy $\sigma_a = 16 \text{ kN/sm}^2$ we $\sigma_b = 16 \text{ kN/sm}^2$ bolsa, $5 \times 2 \text{ sm}$ gönüburçly kesikli sterženiň dartylma güýjüniň ululygyny kesgitlemeli. Sterženiň oky bilen ab we cd meýdança normalyň emele getiren burçunyň ululygyny hasaplamaly.

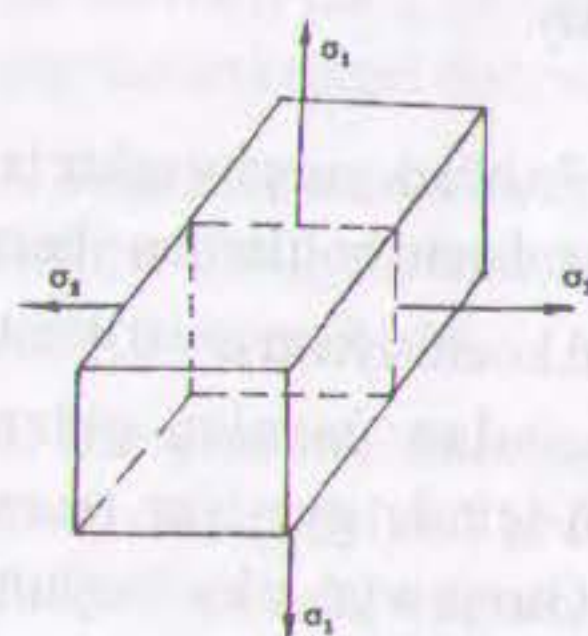
2.8. Gaty iki bölek gurşaw sekiz bolt bilen gaýymlanan boltlardan ybarat. Puassonyň koeffisiýenti $\mu = 0,4$ bolan plastmassadan ýasalan prizma gurşawyň içinde gysylýar (surata seret). Gurşawyň oky boýunça plastmassa prizma $P = 100 \text{ kN}$ güýç bilen gysylýar. Boltlara talap edilyän diametri kesgitlemeli.

Bolt üçin $[\sigma_s] = 10 \text{ kN/sm}^2$ diýip kabul etmeli.

2.9. Suratda görkezilişi ýaly, süýndürilýän nusga tenzometr oturdylan. Tenzometriň bazasy $S = 20 \text{ mm}$, ulaldyş koeffisiýenti $k = 1000$, berlen ýüklenmede tenzometriň görkezmesi $\Delta = 6,5 \text{ mm}$. Eger $E = 2,1 \cdot 10^4 \text{ kN/sm}^2$ bolsa, nusganyň materialy üçin Puassonyň koeffisiýentini kesgitlemeli.

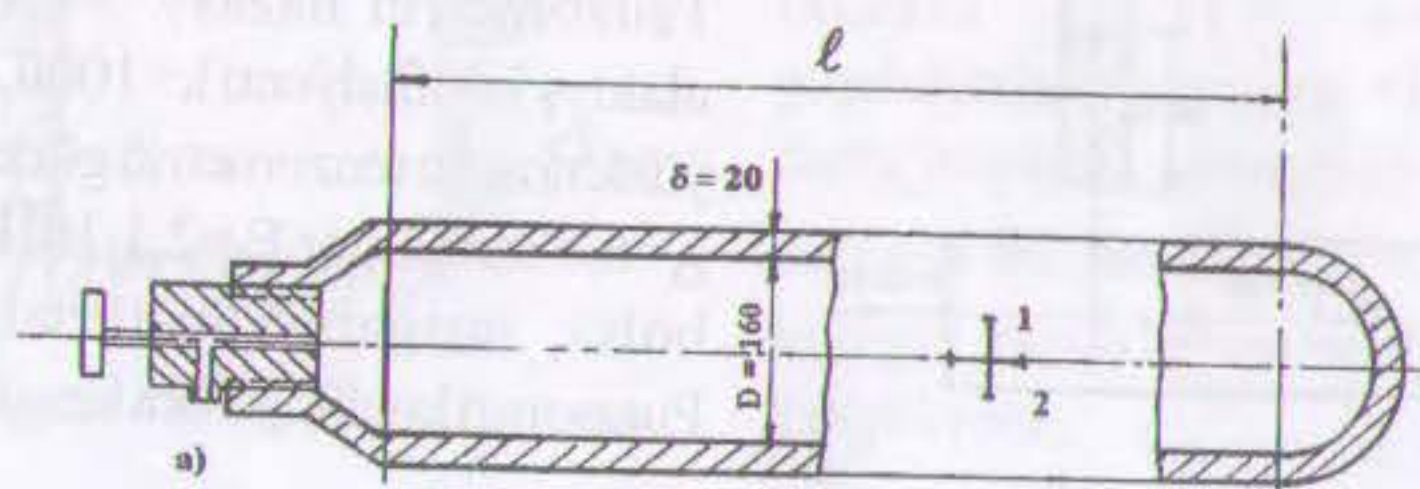


2.10-njy surat



2.11-nji surat

2.12. Suratda görkezilişi ýaly, silindrik ýuka diwarly gabyň (gysylan howa üçin ballon) üstüne iki datçik ýelimlenen. Eger elektriktenzometriki enjamyň kömegi bilen kesgitlenen datçigiň bazasynyň ugrundaky durkuny üýtgetme degişlilikde $\varepsilon_1 = 330 \cdot 10^{-6}$ we $\varepsilon_2 = 84 \cdot 10^{-6}$ bolsalar, ballondaky howanyň basyş ıy kesgitlemeli. Ballonyň materialy üçin $E = 2 \cdot 10^4 \text{ kN/sm}^2$, $\nu = 0,25$.

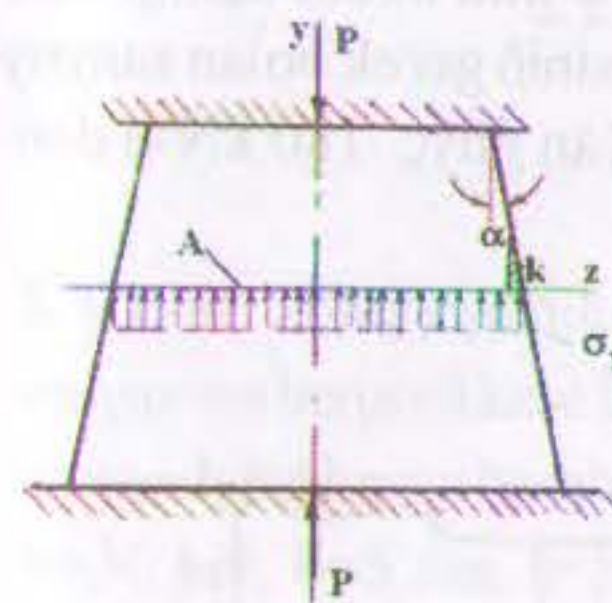


2.12-nji surat

2.10. Eger iki özara perpendikulýar granlara $\sigma_\alpha = 12 \text{ kN/sm}^2$ we $\sigma_\beta = 6 \text{ kN/sm}^2$; $\tau = 3 \text{ kN/sm}^2$ täsir edýän bolsalar, suratda görkezilen element üçin baş dartgynlylygy we baş meýdançanyň ýerleşişini kesgitlemeli.

2.11. Tekiz dartgynlylyk ýagdaýyna sezewar bolan elementiň nokadyndaky baş dartgynlylyklar $\sigma_1 = 12 \text{ kN/sm}^2$ -a, $\sigma_2 = 10 \text{ kN/sm}^2$ -a deň (surata seret). Wertikal ok bilen 60° burç emele getirýän ýapgyt tekizlikdäki dartgynlylyklaryny we iň uly galtaşma dartgynlylygyny kesgitlemeli.

2.13. Bir ugra dartýan dartgynlylykdan $\sigma_y = 14 \text{ kN/sm}^2$ ölçegi $b = 40 \text{ sm}$ bolan alýumin kwadrat list $\Delta b = 0,8 \text{ mm}$ uzalýar. Eger liste şol bir ululykda we ugry boýunça σ_y perpendikulýar goşmaça dartýan σ_x dartgynlylyk täsir edýän bolsa, iki ugra uzalmany kesgitlemeli. Puassonyň koeffisiýenti $\mu = 0,3$. Eger goşmaça dartgynlylyk gysýan bolsa, durkuny üýtgetme nähili bolar?



2.14-nji surat

2.14 Tekiz trapesiýa görnüşli nusga presiň ýassygynyň aralygynda P güýç bilen gysylýar. Normal dartgynlylyk σ_y gorizontalk tekizlik boýunça endigan ýaýran diýip hasap edip, nusganyň ýapgytlanan granyndaky K nokadyň τ_{xy} we σ_z dartgynlylygyny tapmaly.

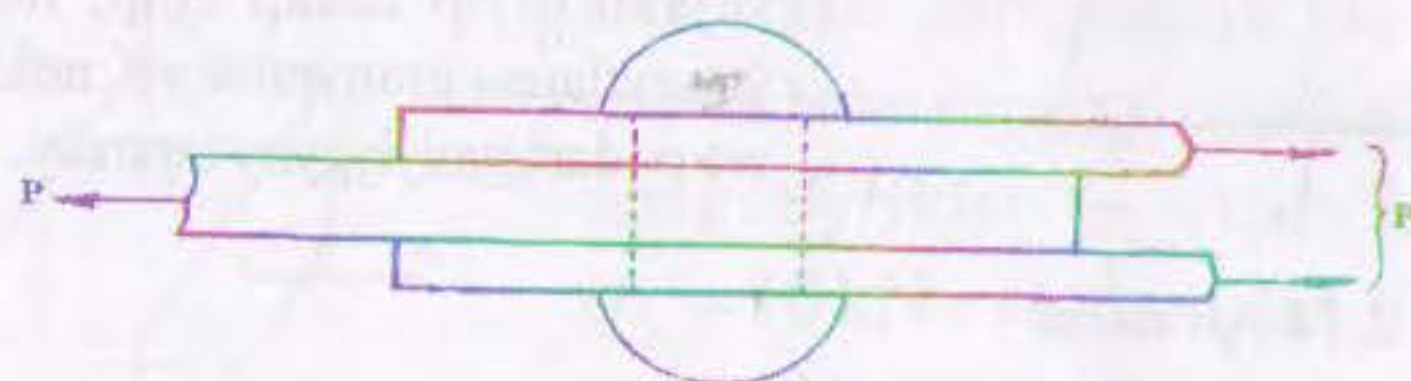
III bap

Süýşme we towlanma

3.1. Süýşme (kesilme, ýenjilme, owranma)

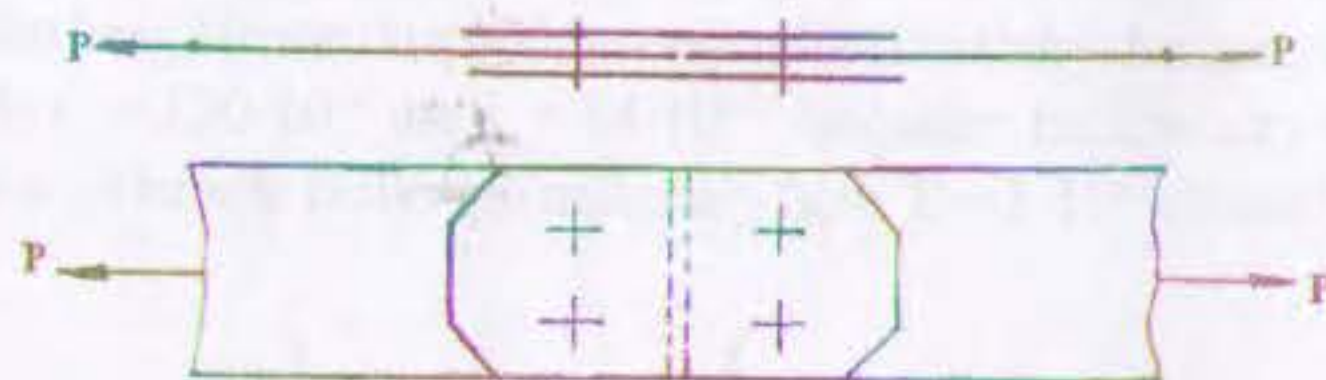
3.1. Galyňlygy 5 mm bolan iki listi galyňlygy 12 mm bolan üçünji liste birikdirmek üçin, diametri 20 mm deň berçinlemäniň gerek bolan sanyny kesgitlemeli (surata seret). Birikdirmä täsir edýän güýç 180 kN-a deň. Rugsat edilýän dartgynlylyklar:

$$[\tau] = 10 \text{ kN/sm}^2; [\sigma_y] = 28 \text{ kN/sm}^2$$



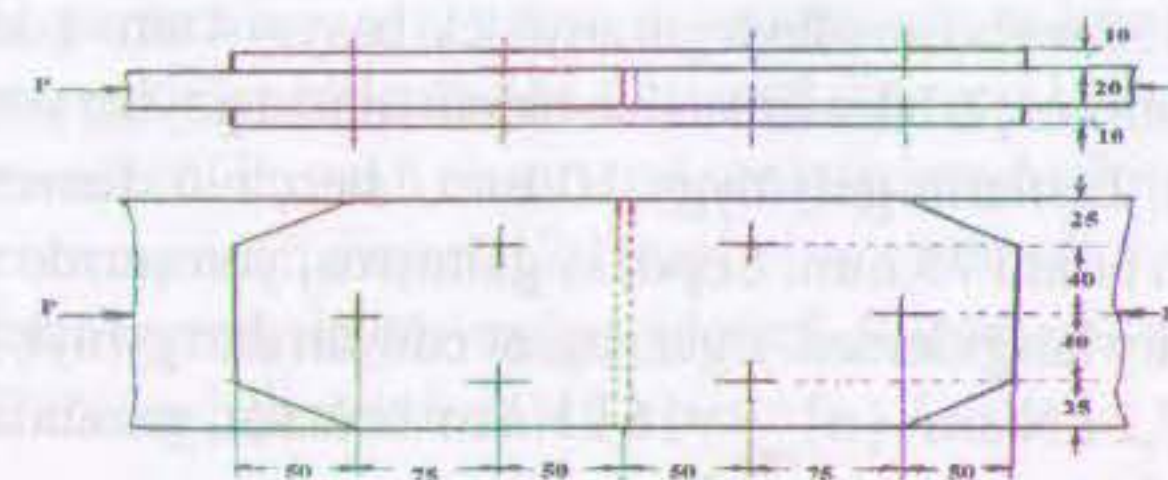
3.1-nji surat

3.2. $12 \times 150 \text{ mm}^2$ kese kesikli list galyňlygy 6 mm bolan urna bilen örtülen (surata seret). Birikdirmede diametri 20 mm bolan berçin ulanylan. Süýndürýän güýç 120 kN. Kesilmede we ýenjilmede berçiniň, şonuň ýaly-da listiň we urnanyň howply kesiginde üzülme dartgynlylyklaryny kesgitlemeli.



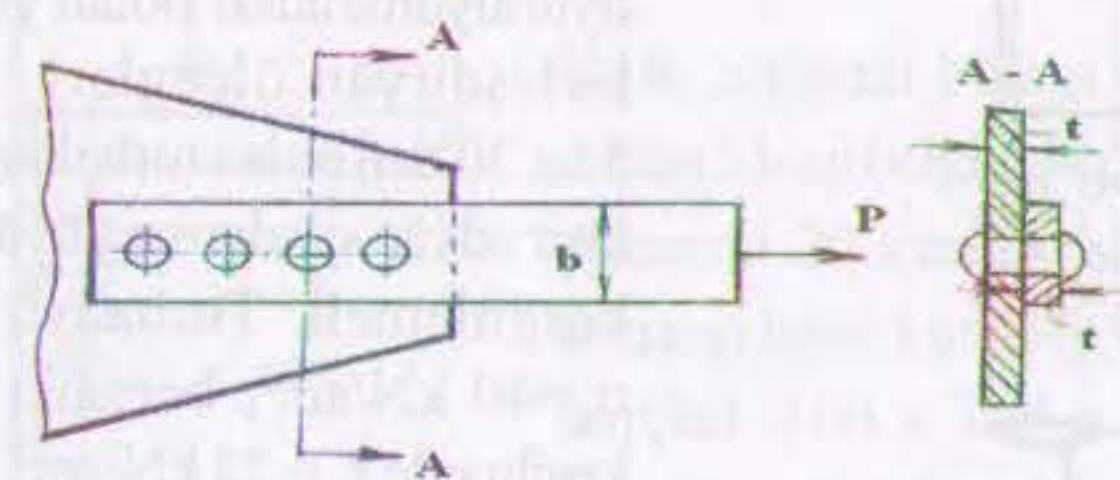
3.2-nji surat

3.3. Iki listiň sepinde diametri 26 mm bolan berçin ulanylan. Birikdirme suratda görkezilişi ýaly ýerine ýetirilen. Rugsat edilýän dartgynlylyklar: $[\tau] = 10 \text{ kN/sm}^2$; $[\sigma_y] = 28 \text{ kN/sm}^2$, $[\sigma_s] = 16 \text{ kN/sm}^2$. Sepe rugsat edilýän iň uly süýnme güýjüni kesgitlemeli.

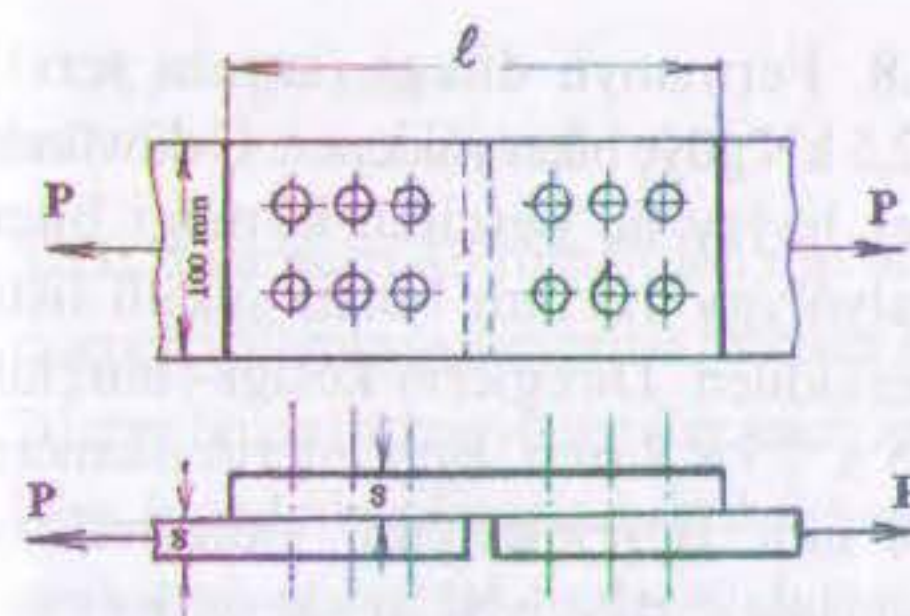


3.3-nji surat

3.4. Polat zolagy şekilli liste birikdirmek üçin (surata seret) zerur berçin sanyny we berçiniň kese kesiginiň diametrini kesgitlemeli. Berçin deşigi bilen gowşadylan kesigi hasaba alyp, polat zolagyň berkligini barlamaly. Berlen: $P=30 \text{ kN}$, $b=5 \text{ sm}$, $t=5 \text{ mm}$, polat zolagyň materialyna rugsat edilýän dartgynlylyk $[\sigma] = 16 \text{ kN/sm}^2$, berçiniň materialy üçin $[\tau] = 10 \text{ kN/sm}^2$ (kesmede), $[\sigma]_{\text{ýenj.}} = 26 \text{ kN/sm}^2$ (ýenjilmede).



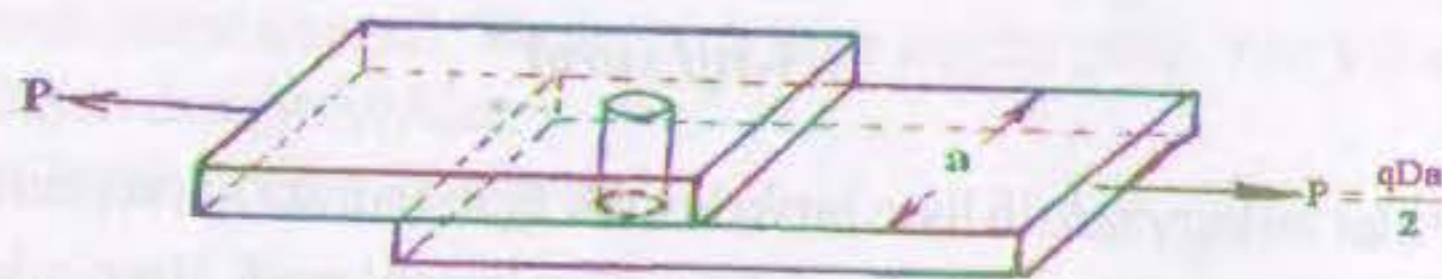
3.4-nji surat



3.5-nji surat

3.5. Ölçeği 100 x 8 mm iki polat listi galyňlygy 8 mm bolan urnanyň kömegi bilen birikdirmek üçin iki setirli berçinleme tikiğine näçe berçin gerek bolar. Urnanyň talap edýän uzynlygyny kesgitlemeli. Berlen: $P=80 \text{ kN}$, $[\sigma]=26 \text{ kN/sm}^2$, $[\tau]=10 \text{ kN/sm}^2$.

3.6. Diametri 150 sm bolan silindr gazanyň içki basyşy 4 atm-e deň. Gazanyň boý tikini bir setir berçin bilen listleri bir-biriniň üstüne goýlup ýerine ýetirilen (surata seret). Listleriň galyňlygy 10 mm, berçiniň diametri 20 mm, berçinlemäniň ädimi 75 mm. Sepdäki galtaşma, ýemşirme we süýnme dartgynlylyklary kesgitlemeli. Eger rugsat edilýän dartgynlylyklar $[\sigma]=10 \text{ kN/sm}^2$, $[\tau]=7,2 \text{ kN/sm}^2$, $[\sigma]_{\text{ýenj.}}=16 \text{ kN/sm}^2$ bolsalar, gazandaky aňryçäk rugsat edilýän basyşy kesgitlemeli.

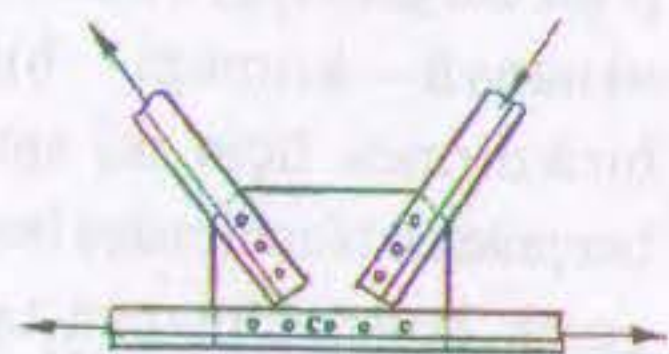


3.6-njy surat



3.7-nji surat

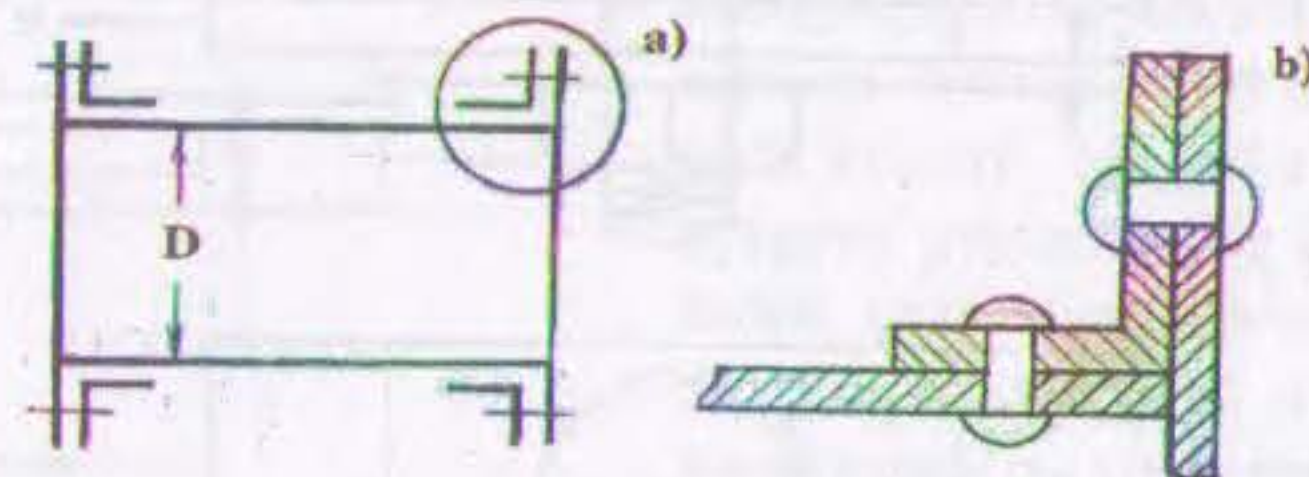
3.7. Diametri $d = 3,5 \text{ mm}$, materialy dýuralýuminiden bolan ýigrimi berçiniň birleşdirýän ölçegleri 30×28 we 33×30 deň bolan turbalara (surata seret) täsir edýän syndyrma güýjüniň ululygyny kesgitlemeli. Turbanyň berklik çägi $\sigma_b = 40 \text{ kN/sm}^2$, berçiniň berklik çägi: kesilmede $\tau_b = 22 \text{ kN/sm}^2$, ýenjilmede $\sigma_{\text{ýenj.}} = 52 \text{ kN/sm}^2$.



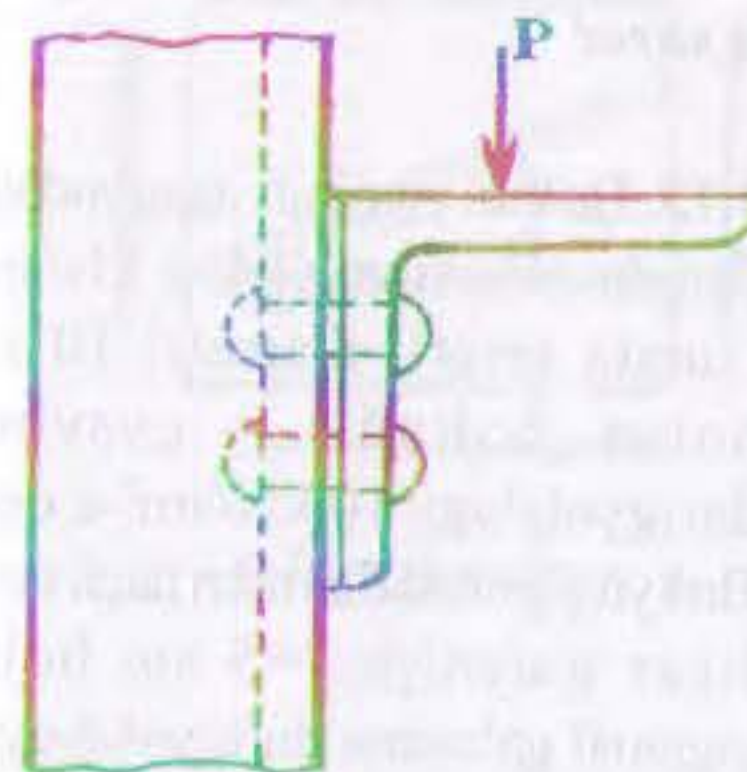
3.8-nji surat

3.8. Fermanyň diregi (surata seret) 52,5 kN güýç bilen ýüklenen. Ç düwünde her haýsy üç berçiniň kömegi bilen galyňlygy 10 mm bolan şekilli liste berkidilen. Diregleriň kesigi—burçluk $75 \times 75 \times 8 \text{ mm}$. Berçinleriň diametri 20 mm. Berçinlerdäki galtaşma we ýenjilme dartgynlylyklary kesgitlemeli.

3.9. Suratda görkezilişi ýaly, gazanyň gapagy diwar bilen berçinlenilip, burçlugyň kömegi bilen birleşdirilen. Gazanyň diametri 100 mm; gazandaky basyş 10 atm-e deň. Gazanyň diwarynyň we burçlugyň tekjesiniň galyňlygy 10 mm. Eger berçinleriň diametri 20 mm bolsa, gazanyň diwaryny burçluk bilen birikdirýän berçinleriň sanyny kesgitlemeli. Rugsat edilýän dartgynlylyk: kesilmede 7 kN/sm^2 , ýenjilmede 16 kN/sm^2 .



3.9-njy surat

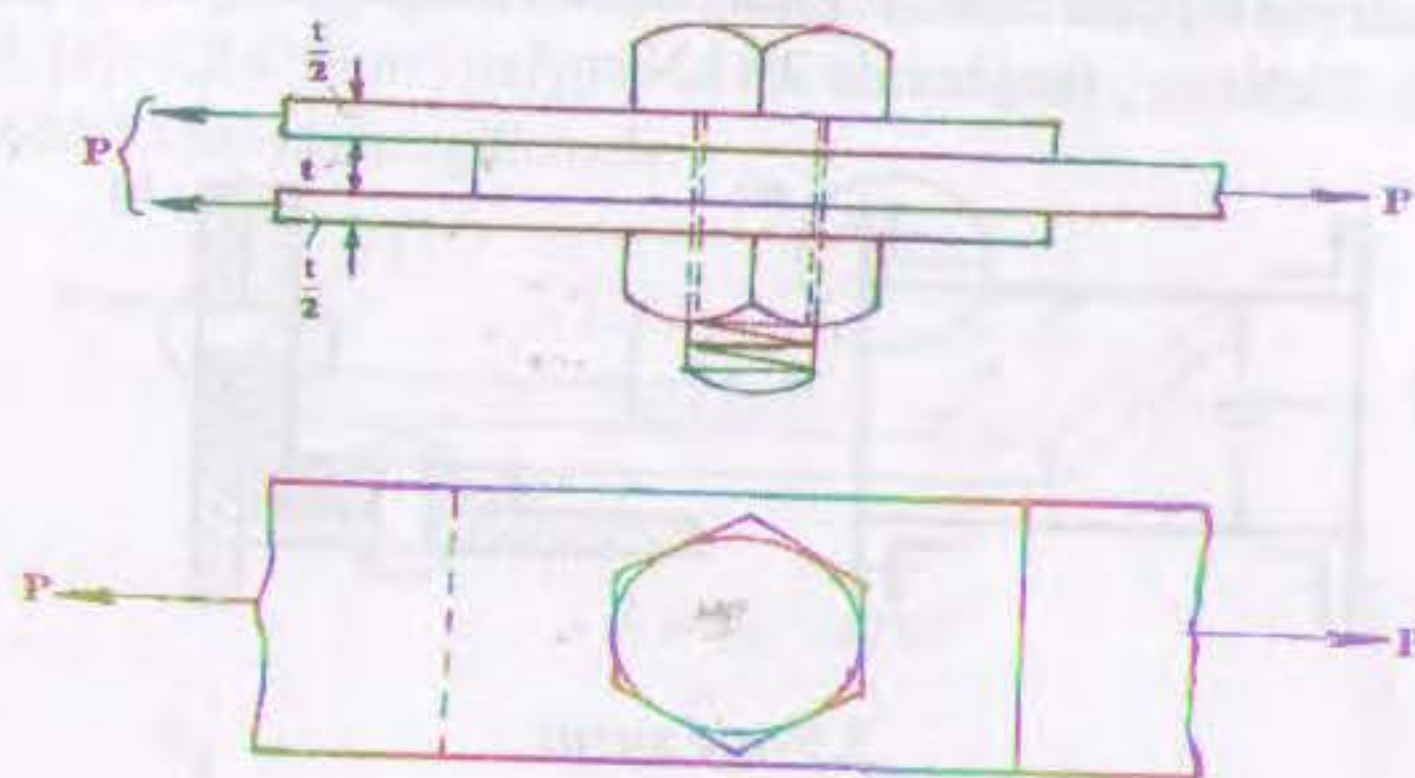


3.10-njy surat

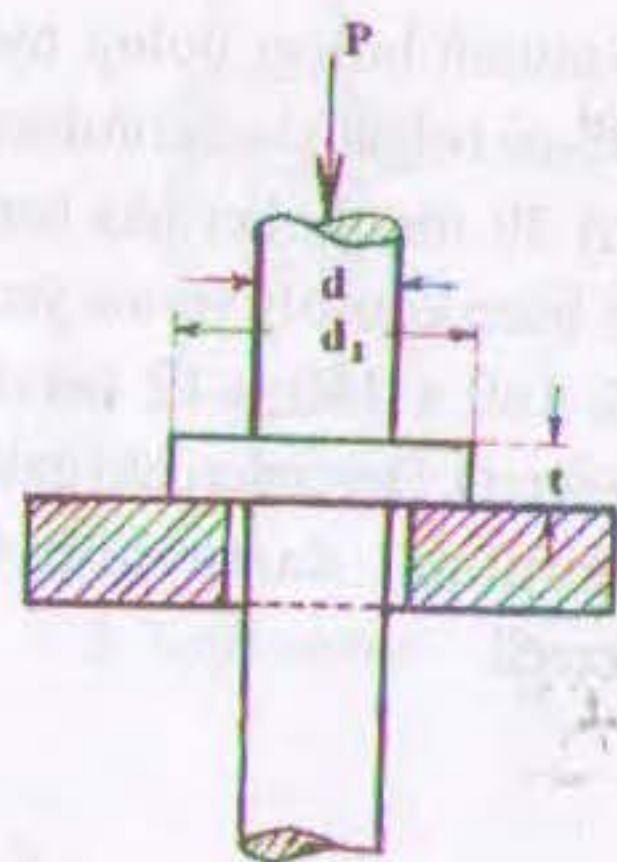
3.10. Sütüniň bölegi bolup hyzmat edýän 33-nji belgili şwelleriň diwaryna diametri 20 mm bolan baş berçiniň kömegi bilen konsoly ýerine ýetirýän burçluk $160 \times 160 \times 12$ berkidilen (surata seret). Berçinlerdäki galtaşma we ýenjilme dartgynlylyklary kesgitlemeli.

3.11. Diametri 40 mm bolan mis steržen örän kiçi boşluk bilen daşky diametri 60 mm bolan polat turbada goýlan. Sterženiň iki gyrasy diametri 20 mm bolan turbanyň we sterženiň içinden geçýän gaty şpilkalaryň kömegi bilen birikdirilen. Eger konstruksiýanyň gyzygynlygy 40°S ýokarlanýan bolsa, şpilkanyň galtaşma dartgynlylygyny kesgitlemeli. Şpilkanyň durkuny üýtgetmegini hasaba almaly däl.

3.12. Suratda görkezilen boltuň birikdirmedäki diametrini kesgitlemeli. Süýndürme güýç $P=200 \text{ kN}$, galyňlyk $t=2 \text{ sm}$. Boltuň materialy üçin rugsat edilýän dartgynlylyklar: kesilmede 8 kN/sm^2 , ýenjilmede 20 kN/sm^2 .



3.12-nji surat



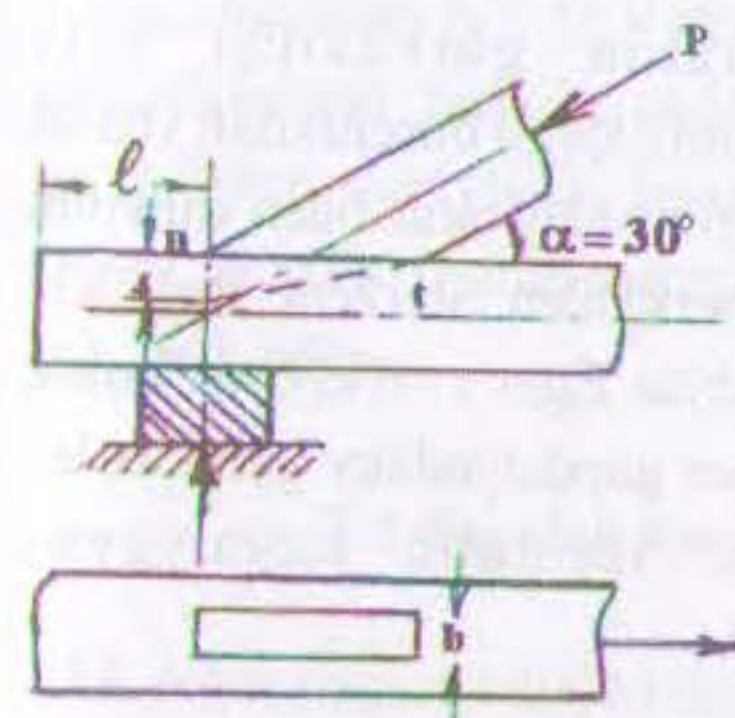
3.13-nji surat



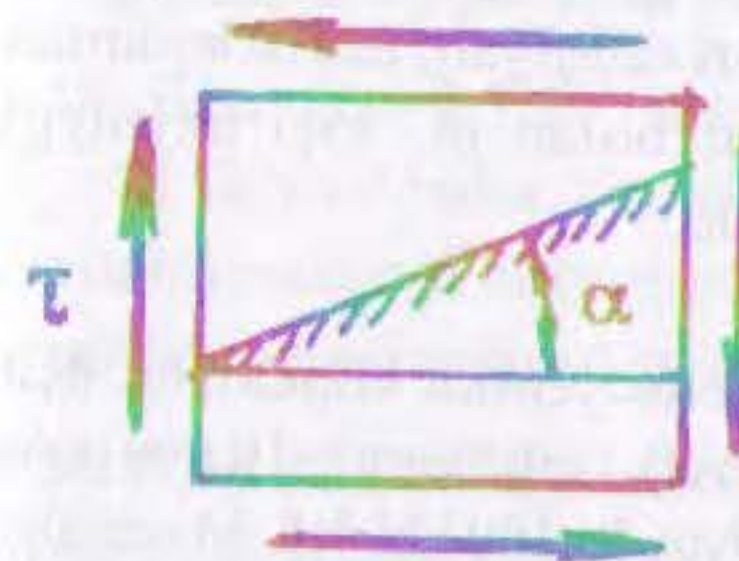
3.14-nji surat

3.13. Boltuň çigniniň aşagyndaky ýenjilme dartgynlylyk 4 kN/sm^2 (surata seret), diametri 10 sm bolan boltuň gysylma dartgynlylygy 10 kN/sm^2 -a deň. Boltuň çigniniň diametri näçä deň? Eger galyňlyk $t=5 \text{ sm}$ bolsa çigniniň galtaşma dartgynlylygyny kesgitlemeli.

3.14. Eger agajyň süýnmä rugsat edilýän dartgynlylygy $[\sigma]=5,6 \text{ kN/sm}^2$ -a deň bolsa, kesigi $2 \times 4 \text{ sm}^2$ (surata seret) bolan tekiz agaç nusga näçe dartuw güýjüni goýmak bolar? Şu dartuw güýjünde nusganyň kellesindäki owranma dartgynlylygy näçä deň bolar?



3.15-nji surat



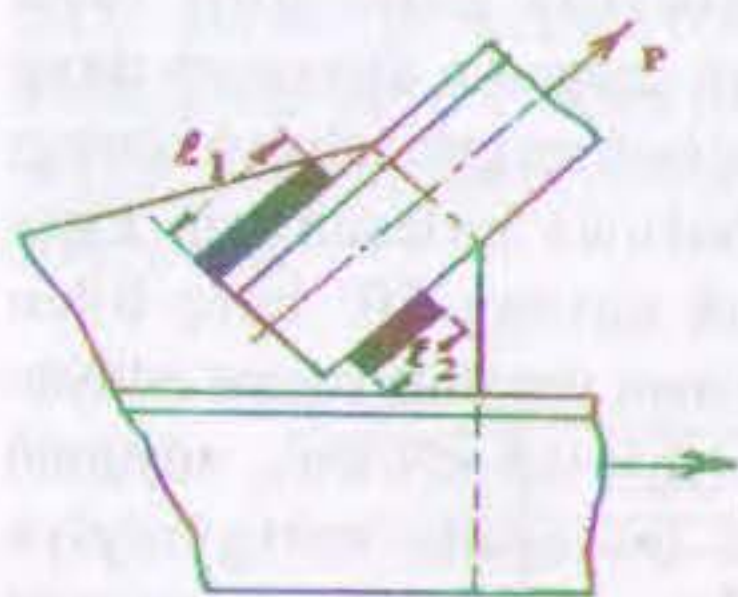
3.16-nji surat

3.15. Suratda görkezilişi ýaly, fermanyň eşegarka aýagynyň direg düwni ini $b=6 \text{ sm}$ çykyndynyň kömegi bilen dartuwa birleşdirilen. Eger süýümiň ugruna 30° burç bilen ýapgytlanan ýenjilmä rugsat edilýän dartgynlylyk $0,5 \text{ kN/sm}^2$, süýümiň ugruna owranma dartgynlylyk $0,08 \text{ kN/sm}^2$, eşegarka germewiň aýagyny gysýan güýç $P=20 \text{ kN}$ bolsa, çykyndynyň beýikligini we dartuwyň ahyrynyň uzynlygyny kesgitlemeli. n -t çyzyk boýunça güýç täsir etmeýär diýip hasap etmeli.

3.16. Arassa süýşmä sezewar bolýan elementiň galtaşma dartgynlylygy $\tau=5 \text{ kN/sm}^2$ deň, suratda görkezilişi ýaly süýşme tekizligine $\alpha=30^\circ$ burç boýunça ýapgytlanan meýdançada dartgynlylyk tegelegini gurup, normal, galtaşma we doly dartgynlylyklary kesgitlemeli.

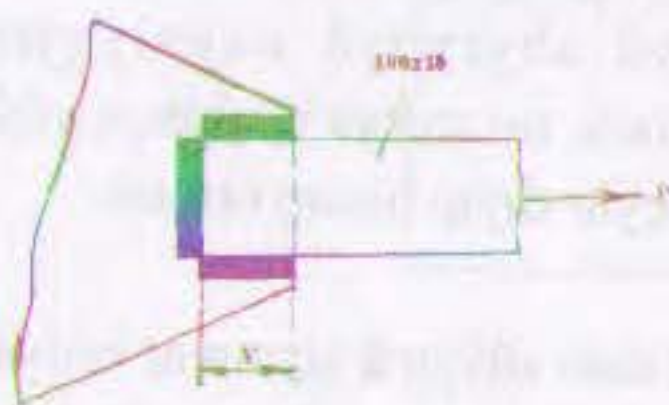
3.17. Gapyrgalarynyň ölçegi 20 sm bolan polat kubuň dört granlary $\tau=10 \text{ kN/sm}^2$ galtaşma dartgynlylyklar bilen ýüklenen. Absolyt we otnositel süýşmeleriň ululygyny tapmaly. Süýşmede maýyşgaklyk moduly $G=8 \cdot 10^3 \text{ kN/sm}^2$.

3.18. Tekiz polat nusga ýüklenmä çenli nusganyň okuna $\alpha=30^\circ$ burç boýunça ýapgytlanan çyzyk çyzylan. Eger nusga $=12 \text{ kN/sm}^2$ dartgynlylyga çenli süýndürilse, burç näçe ululykda üýtgär? $E=2 \cdot 10^4 \text{ kN/sm}^2$, $\mu=0,25$.



3.19-njy surat

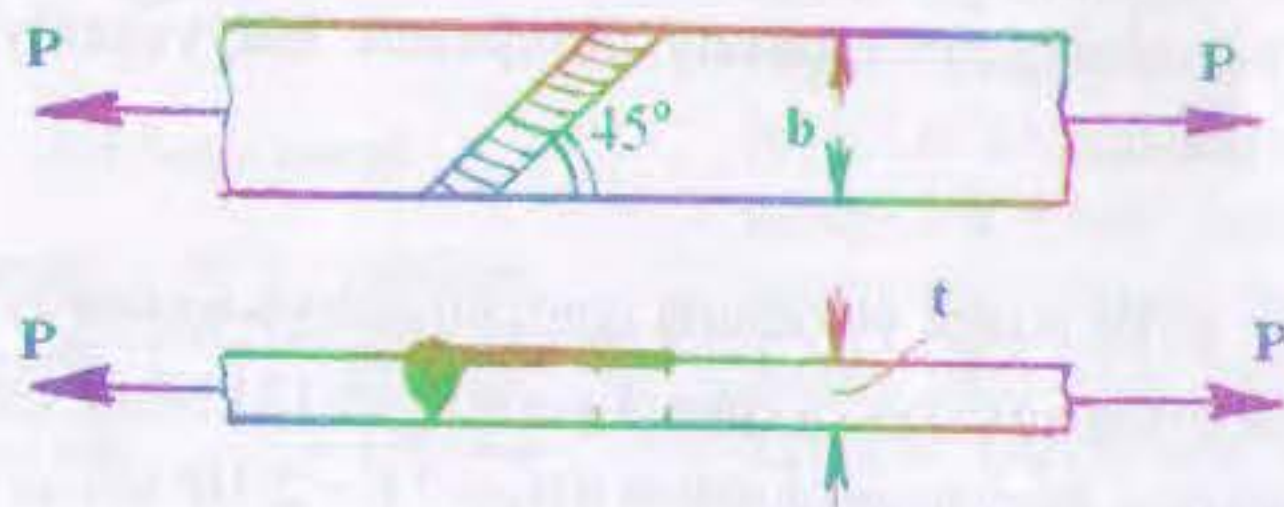
3.19. Suratda görkezilişi ýaly 80 x 80x8 mm ölçegli burçlukdan ybarat bolan steržen maňlaý tikin bilen düwnüň şekil listine berkidilen. Steržene $P=62$ kN güýç täsir edýär. Eger $\tau=8$ kN/sm² bolsa, burçlugyň her gapdalyndaky gerek bolan kebşirleme tikininiň uzynlygyny kesgitlemeli.



3.20-nji surat

3.20. Eger listiň süýnme dartgynlylygy 14kN/sm², kebşirlemäniň kesilmä rugsat edilyän dartgynlylygy 8kN/sm² bolsa, suratda görkezilişi ýaly, listi birleşdirmek üçin zerur bolan iň kiçi uzynlygy kesgitlemeli.

3.21. Materialyň peýdalanylyşynyň koeffisiýentini köpeltmek üçin kebşirleme tikinleri ýapgyt edilen (surata seret). Galyňlygy $t=10$ mm polat listler birikdirilende süýndürýän güýjüň ululygy $P=100$ kN deň. Materialyň peýdalanylyşyny 100% hasap edip, listiň zerur bolan inini kesgitlemeli. Gyýa kebşirleme tikin süýndürýän güýjüň ugruna 45° burç boýunça ýerleşdirilen. Eger kebşirleme tikinine rugsat edilyän dartgynlylyklar $[\sigma]_{keb}=10$ kN/sm², $[\tau]_{keb}=8$ kN/sm² bolsalar, aýratynlykda normal we galtaşma dartgynlylyklar boýunça tikininiň berkligini barlamaly.



3.21-nji surat

3.22. Meýdany $A=55,9$ sm² bolan şweller, şekilli liste iki maňlaý we bir dilik tikinleriň birikdirmedäki berkligini barlamaly. Şweller $P=800$ kN güýç bilen dartylýar. Esasy materiala rugsat edilyän dartgynlylyk $[\sigma]_s=16$ MPa, tikininiň materialy üçin kesilmä rugsat edilyän dartgynlylyk $[\tau]_{tik}=8$ MPa.

3.2 Tegelek kesikli sterženleriň towlanmasy

3.23. Eger rugsat edilyän dartgynlylyk $[\tau]=7$ kN/sm² bolsa, 15 kN·m aýlaw momenti geçirýän bitewi tegelek kesikli walyň diametrini kesgitlemeli.

3.24. 300 aýl./min. we 450 a.g. geçirilýän bitewi kesikli walyň diametrini kesgitlemeli. Walyň 2 m uzynlygynda towlanma burçy 1°-dan ýokary bolmaly däl, iň uly galtaşma dartgynlylyk 4 kN/sm²; $G=8 \cdot 10^3$ kN/sm².

3.25. Eger $G_a=2,7 \cdot 10^3$ kN/sm², $G_p=8 \cdot 10^3$ kN/sm², $\gamma_a=26$ kN/m³, $\gamma_p=78,5$ kN/m³ bolsa, birmeňzeş towlanma momentinde we otnositel towlanma burçunda taslanan polat we alýumin ergininden ýasalan birmeňzeş uzynlykda bitewi wallaryň agramlaryny deňeşdirmeli.

3.26. Polat bitewi walyň gerek bolan diametrini kesgitlemek üçin rugsat edilyän galtaşma dartgynlylyk 8 kN/sm², 1 m uzynlykda rugsat edilyän towlanma burçy 1°-a deň. Towlanma momentiniň haýsy ululygynda diametri kesgitlemek üçin çäklenmek mümkin, rugsat edilyän dartgynlylyk boýunçamy ýa-da diňe rugsat edilyän towlanma burçy boýunça?

3.27. Uzynlygy 6 m we diametri 10 sm bitewi wal 4° burç boýunça towlanan. Eger $G=8 \cdot 10^3$ kN/sm² bolsa, iň uly galtaşma dartgynlylyk näçä deň?

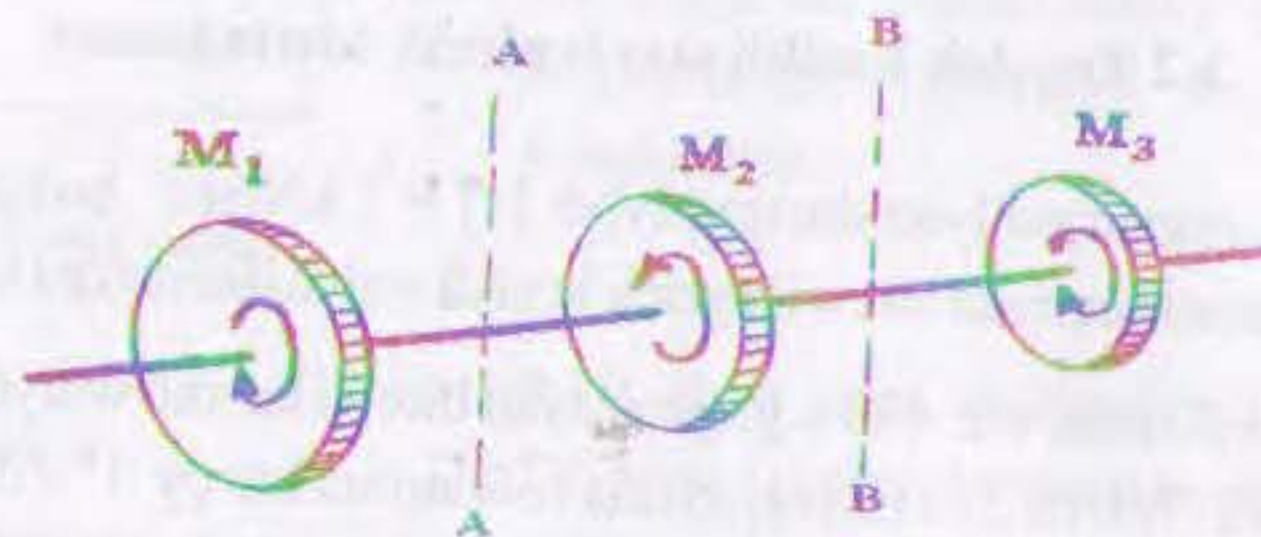
3.28. Walyň diametrini kesgitlemegiň ýakynlaşdyrylan formulasy

$$d = 2,53 \sqrt[3]{40 \frac{N}{n}}$$

görnüşe eýe. Bu ýerde d —walyň diametri, N — walyň

geçirýän kuwwaty a.g., n —walyň minutdaky aýlaw sany. Bu formula süýşmede rugsat edilyän dartgynlylygyň haýsy ululygyna laýyk getirilip çykarylan?

3.29. Walyň AA we BB kesiklerinde $M_1=130 \text{ kNsm}$, $M_2=300 \text{ kNsm}$ aýlaw momentlerden iň uly galtaşma dartgynlyklary kesgitlemeli. AA kesikde walyň diametri 5 sm, BB kesikde bolsa 7,5 sm-e deň.



3.29-njy surat

3.30. Uzynlygy 200 mm-e, diametri 20 mm-e deň bolan polat nusga towlanma synag edilyär. Synagyň netijesi tablisada getirilen:

Towlanma momenti, kN m	0,02	0,04	0,06	0,08	0,1	0,12	0,14	0,16	0,18
Towlanma burçy, köpeldilen 2000 (radianda)	6,1	12,5	18,9	25,2	31,4	37,8	44,3	50,5	56,9
Towlanma momenti, kN m	0,2	0,22	0,24	0,26	0,28	0,3	0,32	0,34	
Towlanma burçy, köpeldilen 2000 (radianda)	63	69,5	75,8	82,1	88,5	95,4	110	148	

Towlanma burçuna baglylykda galtaşma dartgynlygynyň diagrammasyny gurmaly we towlanmada maýyşgaklyk modulyny kesgitlemeli. Seredilyän ýagdaý üçin proporsionallyk çäginin ululygyny tapmaly.

3.31. Materialy ýumşak polatdan bolan steržen 60 kN güýç bilen süýndürilende 0,113 mm uzalýar. Sterženiň diametri 25 mm-e, uzynlygy bolsa 20 sm-e deň. Bu steržen 20 kN·sm towlanma moment bilen ýüklenende, 15 sm uzynlykda 0,55° burç bilen towlanýar. E, G we μ ululyklaryny kesgitlemeli.

3.32. Bug turbinanyň kuwwaty kesgitlelenende aýlanýan walyň towlanma burçy ölçenen we 6 m uzynlykda 1,2°-a deň bolýar. Walyň daşky we içki diametrleri degişlilikde 25 sm-e we 17 sm-e deň. Walyň aýlaw tizligi 250 aýl./min; $G = 8 \cdot 10^3 \text{ kN/sm}^2$. Walyň geçirýän kuwwatyny we onda döreyän galtaşma dartgynlygyny kesgitlemeli.

3.33. Walyň geçirýän kuwwatyny kesgitlemek üçin onuň daşky emele getirijisine 45° burç boýunça ýerleşen çyzgynyň ugruna tenzometriň kömegi bilen uzalmasy ölçelýär. Ölçelen otnositel uzalma $\varepsilon = 0,000425$ -e deň. Walyň daşky diametri 40 sm, içki diametri bolsa 24 sm. Maýyşgaklyk moduly $G = 8 \cdot 10^3 \text{ kN/sm}^2$. Eger wal 120 aýl/min tizlik bilen aýlanan bolsa, onuň geçirýän kuwwatyny kesgitlemeli. Iň uly galtaşma dartgynlyk nähili ululykda bolar?

3.34. Içki diametri daşky diametriniň 60% düzyän içi boş wal, diametri 40 sm bolan bitewi wal bilen çalşyrylýar. Iki walyň rugsat edilyän galtaşma dartgynlyklarynyň birmeňzeşlik şertinden içi boş walyň daşky diametrini kesgitlemeli. Bitewi we içi boş wallaryň agramlaryny deňeşdirmeli.

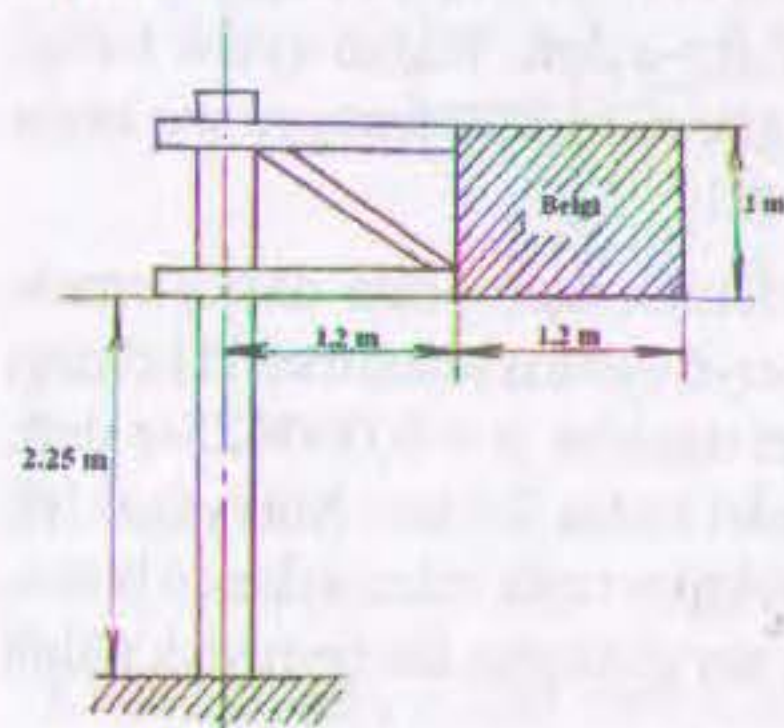
3.35. Bitewi tegelek walyň agramyny 20% azaltmak üçin, diametri içki diametrinden iki esse köp bolan içi boş wal bilen çalşyrylýar. Eger bitewi walyň galtaşma dartgynlygy 6 kN/sm^2 deň bolsa, içi boş walyň dartgynlygy näçe bolar?

3.36. Birmeňzeş agramly we birmeňzeş towlanma momentini geçirýän iki walyň biri bitewi, beýlekisiniň bolsa içi boş. Eger içi boş walyň içki diametri daşky diametriniň 0,6 bölegini düzyän bolsa, haýsy walda iň uly galtaşma dartgynlyk bolar we näçe esse uly bolar?

3.37. Uzynlygy 1,8 m bolan içi boş polat wal 6 kNm towlanma moment bilen ýüklenen. Eger galtaşma dartgynlyk 7 kN/sm^2 , towlanma burçy 2° bolsa, walyň daşky we içki diametrlerini kesgitlemeli.

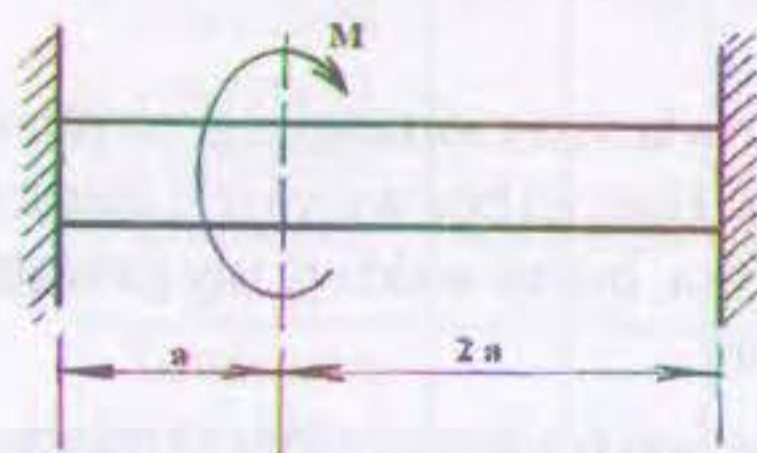
3.38. Absissasy minutdaky aýlaw sany, ordinatasy – zerur diamerti bolan bitewi polat walyň egrisini gurmaly. 6 kN/sm^2 rugsat edilýän galtaşma dartgynlygynda walyň geçirýän kuwwaty 50 a.g. Aýlaw sanyny 16...16000 aýl./min çäginde üýtgetmeli.

3.39. Orta diametri $d_{\text{ort}} = 12,5 \text{ sm}$ bolan ýuka diwarly turba $M_t = 625 \text{ kN sm}$ towlanma moment goýlan. Galtaşma dartgynlyk 7 kN/sm^2 geçmeýän ýagdaýda turbanyň diwarynyň galyňlygy nähili bolar? Eger $G = 8 \cdot 10^3 \text{ kN/sm}^2$ bolsa turbanyň 1 m uzynlygyndaky towlanma burçuny tapmaly.



3.40-njy surat

3.41. Turba şekilli walyň orta diametri 10 sm-e, galyňlygy 3 mm-e deň. Towlanma burçy 3,7 m uzynlykda 1° -a deň. Walyň geçirýän kuwwaty 50 a.g. bolsa, onuň aýlaw tizligini kesgitlemeli.



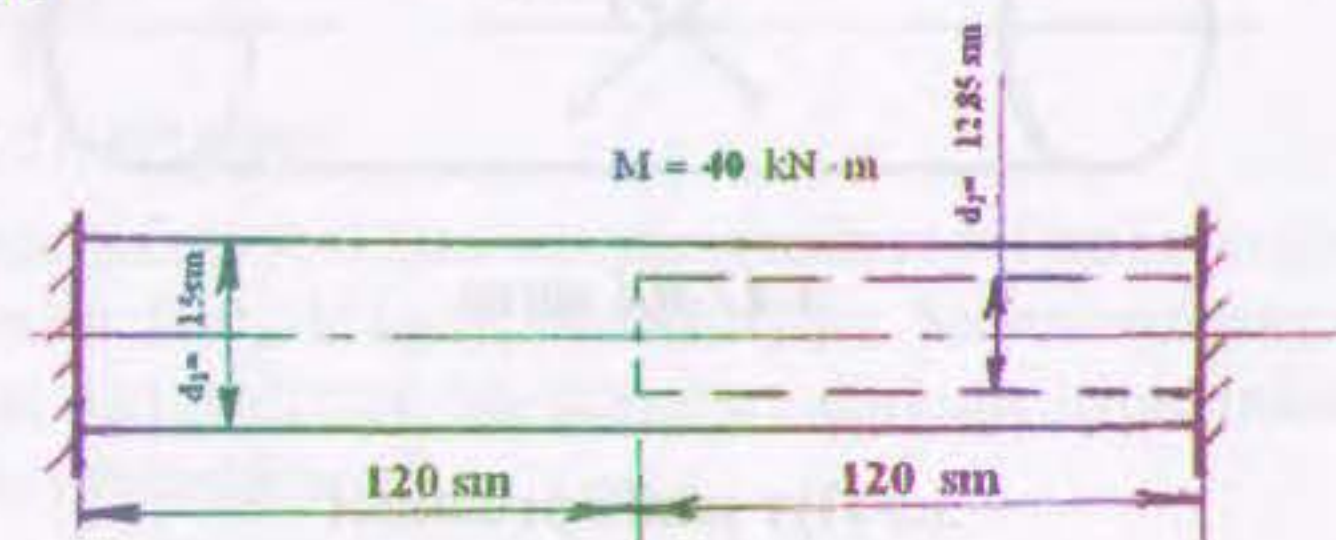
3.42-njy surat

3.40. Suratda görkezilişi ýaly, polat turba ýol belgisini dikmek üçin sütün bolup hyzmat edýär. Ýol belgisine şemalyň in uly basyşy 2 kN/sm^2 -a deň diýip hasap etmeli. Belginiň aşaky gysgyjynda turbanyň towlanma burçy 6° -dan köp bolmaly däl. Towlanmadan turbanyň kesigindäki in uly galtaşma dartgynlyk $3,5 \text{ kN/sm}^2$ ýokary bolmaly däl. Eger turbanyň galyňlygy $t = 3 \text{ mm}$ bolsa, onuň orta diametrini kesgitlemeli. Şemalyň basyşy diňe ştrihlenen meýdana täsir edýär diýip hasaplamaly.

3.42. Suratda görkezilişi ýaly, tegelek kesikli sterženiň ahyrlary gaty berkidilen. Aralyk kesikde steržene 12 kN m moment goýlan. Eger sterženiň diametri 8 sm bolsa, in uly galtaşma dartgynlygyny kesgitlemeli.

3.43. Daşky diametri 7,5 sm bolan mis turba şol bir diametrli polat turbanyň içinde ýerleşdirilen. Turbalaryň galyňlygy 3 mm-e deň. Turbalaryň ahyrlary biri-biri bilen gaty berkidilen we 1 kN m moment goýlan. Turbalardaky in uly galtaşma dartgynlyklary, turbalaryň aralarynda towlanma momentiň ýaýraýşyny we 3 m uzynlykda towlanma burçuny kesgitlemeli. $G = 4 \cdot 10^3 \text{ kN/sm}^2$, $G_p = 8 \cdot 10^3 \text{ kN/sm}^2$.

3.44. Bir bölegi bitewi, beýlekisi bolsa içi boş bolan polat steržen towlanma moment bilen ýüklenen (surata seret). Sterženiň sag we çep böleklerindäki in uly galtaşma dartgynlygy we ortasyndaky kesigiň towlanma burçuny kesgitlemeli.

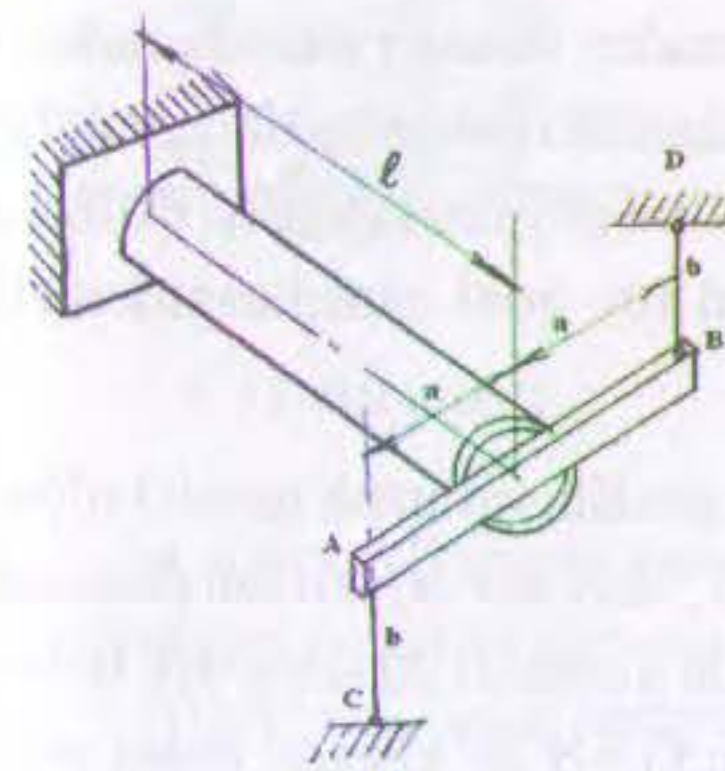


3.44-njy surat

3.45. Diametri $2r$ bolan tegelek kesikli pürsün materialynyň

$G_p = G \left(1 + \frac{3\rho}{r} \right)$ kanun boýunça üýtgeýän maýýşgaklyk moduly bar. Pürs

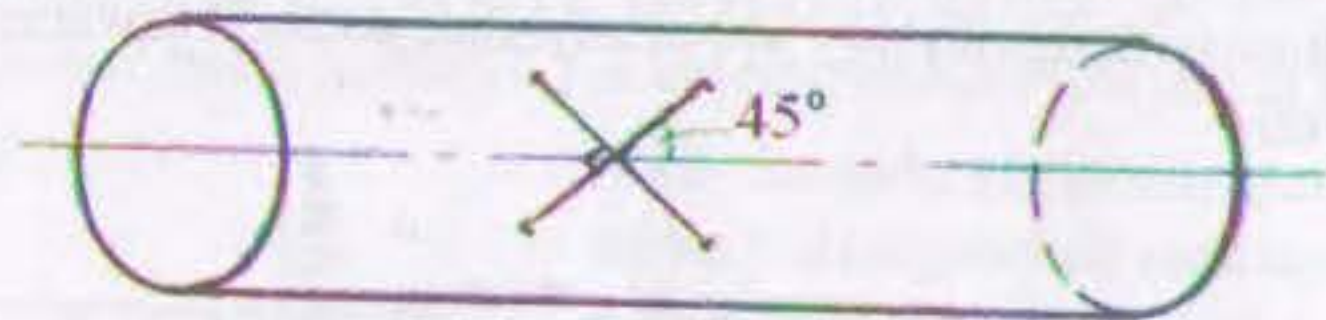
M moment bilen towlananda dartgynlygyň paýlanyşynyň aňlatmasyny we epýuryny kesgitlemeli.



3.46-njy surat

3.46. Diametri D bolan bitewi walyň bir tarapy gaty berkidilen. Walyň beýleki tarapyna keseligine goýlan gaty AB pürs berkidilen. Bu pürs birmeňzeş AC we BD sterženler bilen birleşdirilen (surata seret). Sterženler $\Delta t^\circ S$ -a çenli sowadylýar. Eger sterženlerdäki normal dartgynlyklar waldaky in uly galtaşma dartgynlyga deň bolsa, sterženiň kese kesiginiň meýdanyny kesgitlemeli.

3.47. Diametri 50 mm bolan polat walyň üst ýüzüne oka 45° burç boýunça bir-birine perpendikulýar iki datçik ýelimlenen. Datçikleriň görkezýän otnositel durk üýtgemeleriniň alamatlary dürli-dürli, absolýut ululyklary birmeňzeş we $6,5 \cdot 10^{-4}$ -e deň. Wala goýlan towlanma momentiň ululygyny we ugruny kesgitlemeli.



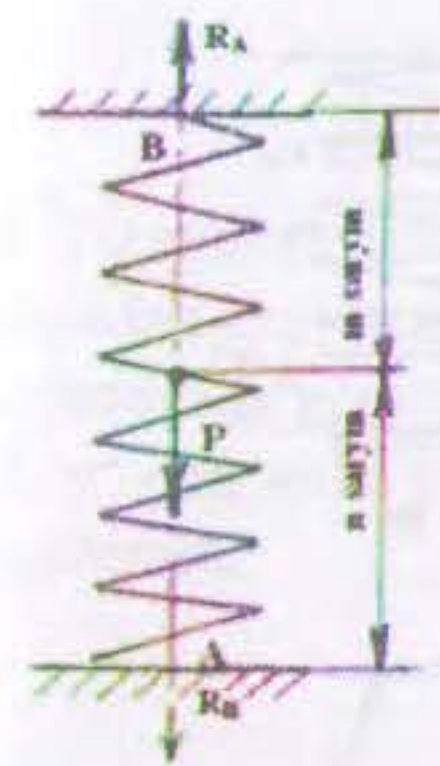
3.47-nji surat

3.3 Hyr şekilli pružinler

3.48. Diametri 18 mm bolan tegelek kesikli silindrik hyr şekilli pružin $P=0,5$ kN güýç bilen ýüklenen. Pružiniň sarymynyň orta diametri $D=125$ mm-e deň. Maýyşgaklyk moduly $G = 8 \cdot 10^3$ kN/sm². Pružiniň materialyndaky iň uly galtaşma dartgynlygyny kesgitlemeli. Eger pružiniň çökmesi 6 mm-e deň bolsa, sarymynyň sanynyň näçe bolýandygyny kesgitlemeli.

3.49. Silindrik hyr şekilli pružin 6 mm-lik simden ýasalan we orta radiusy 7,5 sm bolan 20 sarymdan ybarat. Eger pružindäki galtaşma dartgynlyk 9 kN/sm² bolsa, ok boýunça täsir edýän dartma güýjüni tapmaly. Pružiniň uzalmasyny we durkuny üýtgetmesiniň iň uly udel işini kesgitlemeli. $G = 8 \cdot 10^3$ kN/sm².

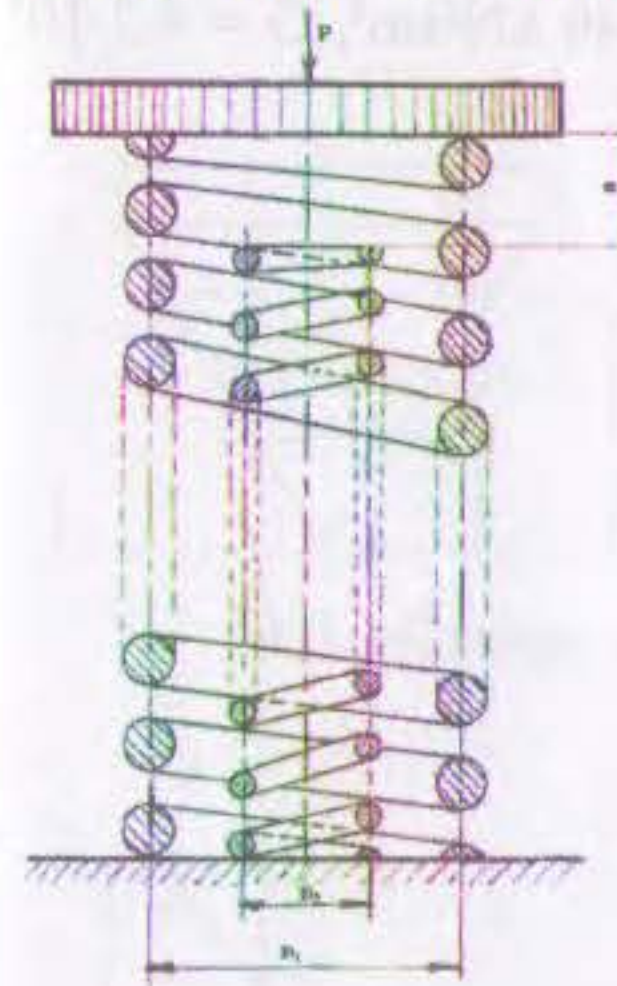
3.50. 6 kN ýükden 2 sm çökyän hyr şekilli pružin ýasamak gerek bolýar. Eger rugsat edilýän galtaşma dartgynlyk 7,5 kN/sm²-a, pružini ýasamak üçin silindriň töweregindäki emele getirijiniň diametri 20 sm-e deň bolsa, pružiniň siminiň diametrini kesgitlemeli. Eger $G = 8 \cdot 10^3$ kN/sm² bolsa, näçe mukdarda sarym gerek bolar?



3.51-nji surat

3.51. Diametri $d=2,2$ sm we orta radiusy $R=12$ sm bolan silindrik polat pružiniň A we B taraplary berkidilen we Ç nokatda $P=1,6$ kN güýç bilen ýüklenen (surata seret). Sarymlaryň sany $m=10$, $n=6$. Berkitmedäki gaýtargylary, pružiniň iň uly dartgynlygyny we Ç nokadyň ornuny üýtgetmesini kesgitlemeli.

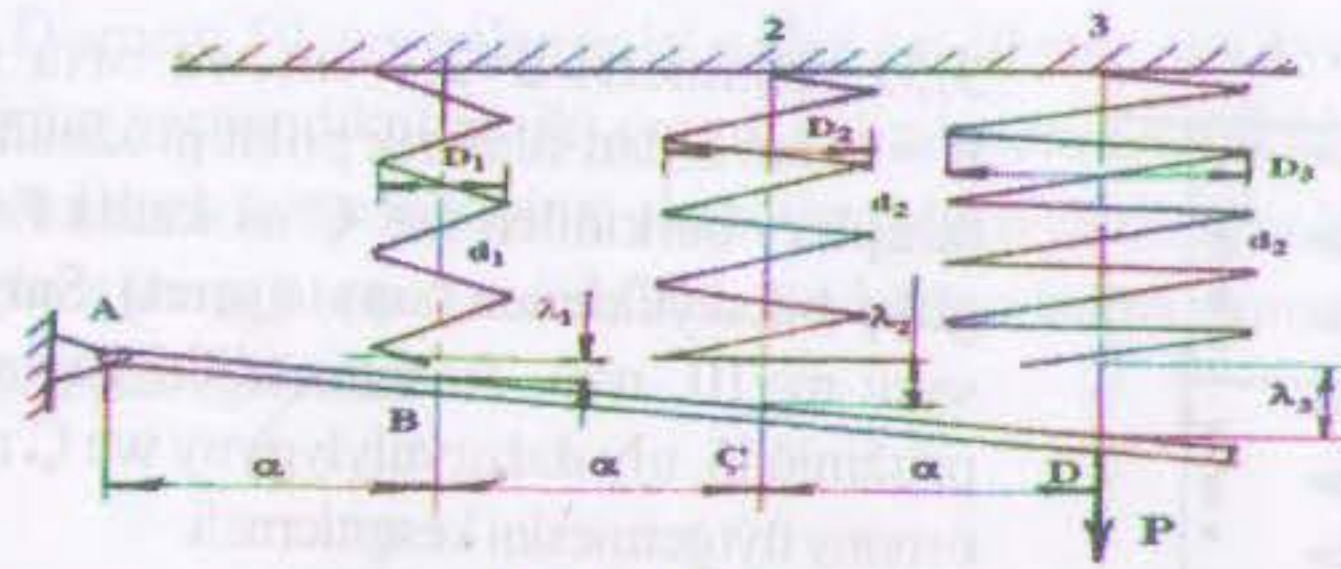
3.52. Orta radiusy $R=12$ sm we siminiň radiusy $r=1$ sm bolan silindr görnüşli polat pružin $P=0,3$ kN güýç bilen dartylýar. Sarymlaryň sany $n=25$. Iň uly galtaşma dartgynlygy, uzalmany we durkuny üýtgetmäniň potensial energiýasyny kesgitlemeli.



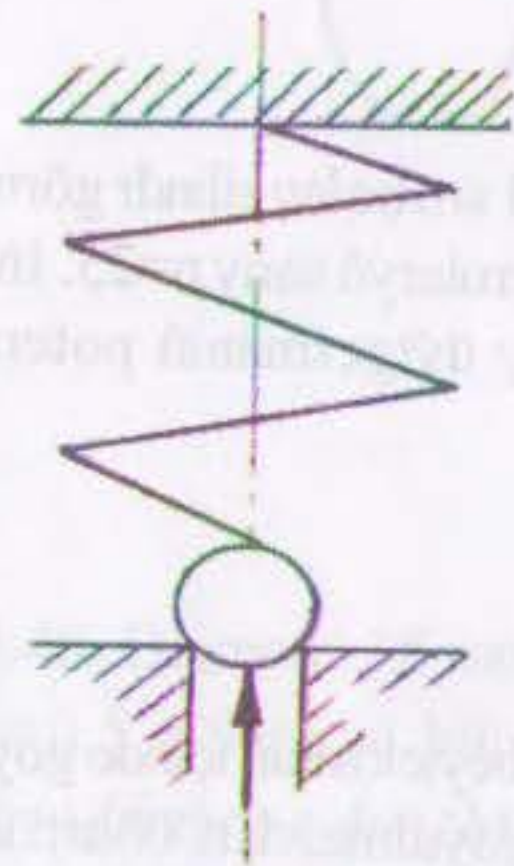
3.53-nji surat

3.53. Iki pružiniň biri beýlekisiniň içinde goýlan. Plita $P=1,2$ kN güýç goýulmazdan, öňürti ikinji pružin birinjiden $\delta=2$ sm gysga (surata seret). Pružiniň iň uly galtaşma dartgynlygyny τ_{max} we plitanyň ornuny üýtgetmegini tapmaly.

3.54. Gaty AD ryçag birmeňzeş sarym sanly we $Q = 4$ kN güýç bilen ýüklenen üç pružinden asylan. Eger dartgynlyk hemmesinde birmeňzeş $\tau = 50$ kN/sm² bolsa, her pružiniň siminiň diametrini hasaplamaly. Pružinleriň sarymynyň orta diametri $D_1=6$ sm, $D_2=8$ sm, $D_3=10$ sm.



3.54-nji surat



3.55-nji surat

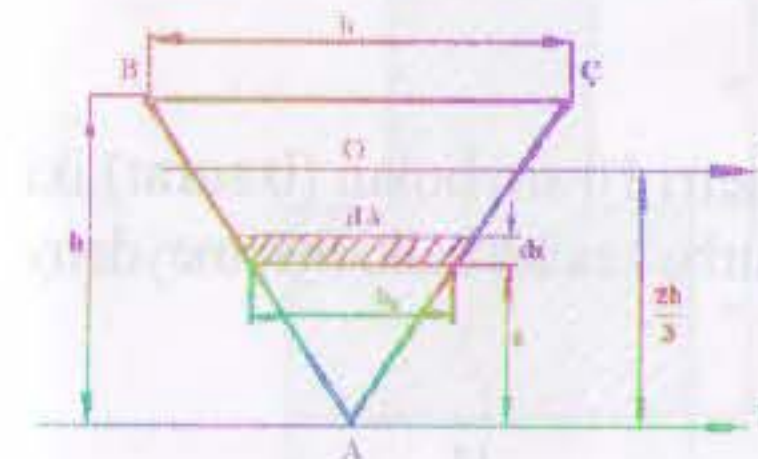
3.55. Klapanyň şarigi $P=0,15$ kN güýç bilen pružini gysýar. Eger sarymyň diametri $D=20$ mm, işleýän sarymyň sany $n=6$ bolsa, simiň kesigini saýlamaly. Pružin bronzadan ýasalan bolsa, pružini näçe gysmaly, rugsat edilýän dartgynlyk $[\tau]=40$ kN/sm², $G = 4,2 \cdot 10^3$ kN/sm².

IV bap Tekiz kesikleriň geometriki häsiýetleri

4.1. Taraplarynyň ölçegleri $b \times h = 12 \times 20$ sm bolan gönüburçlugyň esasyndan geçýän oka görä inersiýa momentini we onuň taraplaryndan geçýän oklara görä merkezden daşlaşýan inersiýa momentini hasaplamaly.
4.2. y_1 oka görä parallelogramyň (surata seret) inersiýa momentini kesgitlemeli.

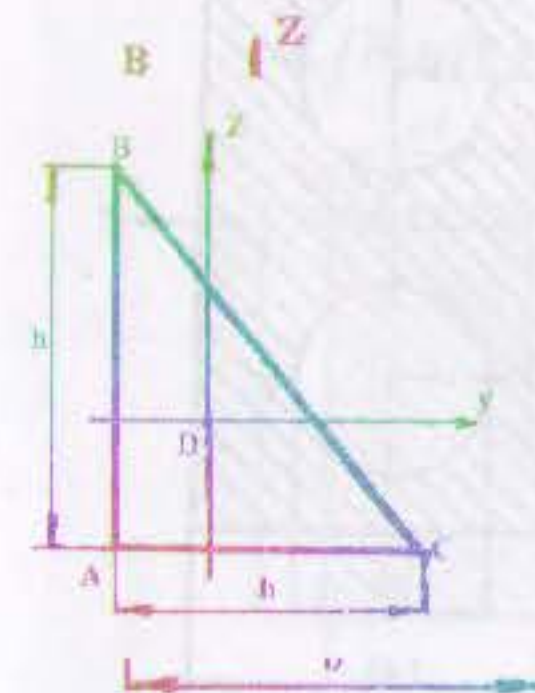


4.2-nji surat



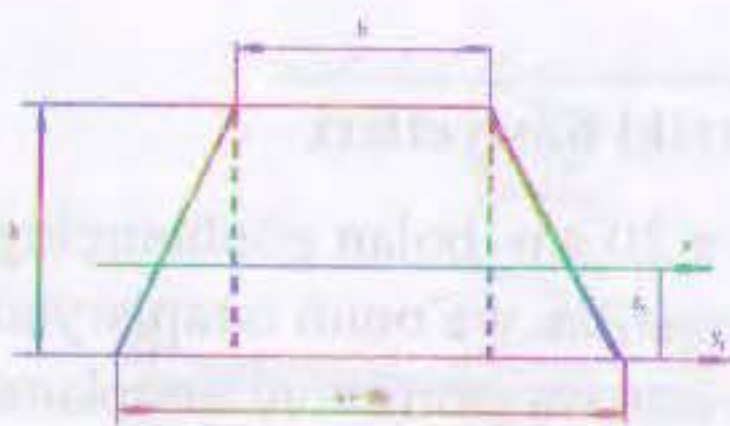
4.3-nji surat

4.3. ABC üçburçlugyň A depesinden geçýän, esasya parallel y_1 oka görä inersiýa momentini hasaplamaly.

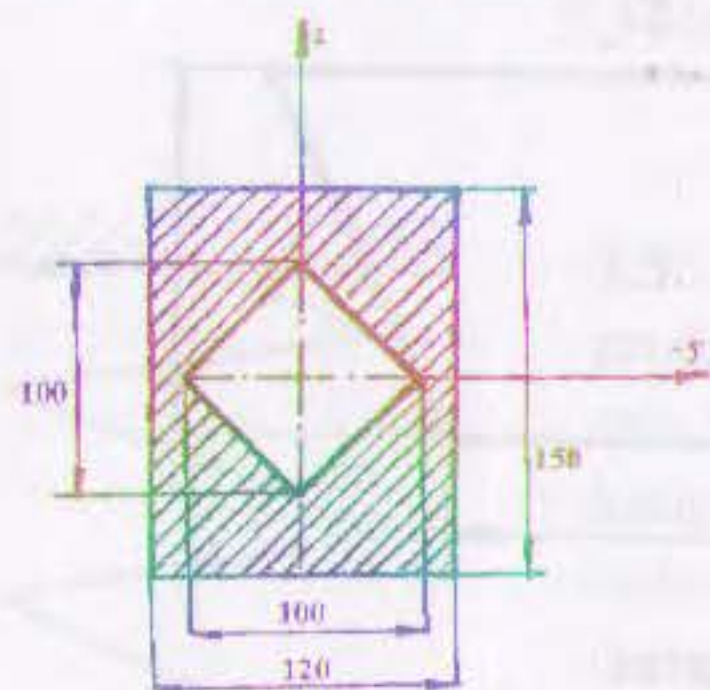


4.4-nji surat

4.4. Katetlerine parallel (surata seret) merkezi oklara Oy we Oz görä ABC üçburçlugyň merkezden daşlaşýan we oka görä inersiýa momentlerini kesgitlemeli, şonuň ýaly-da üçburçlugyň AB esasyndan geçýän oka görä inersiýa momentini hasaplamaly.

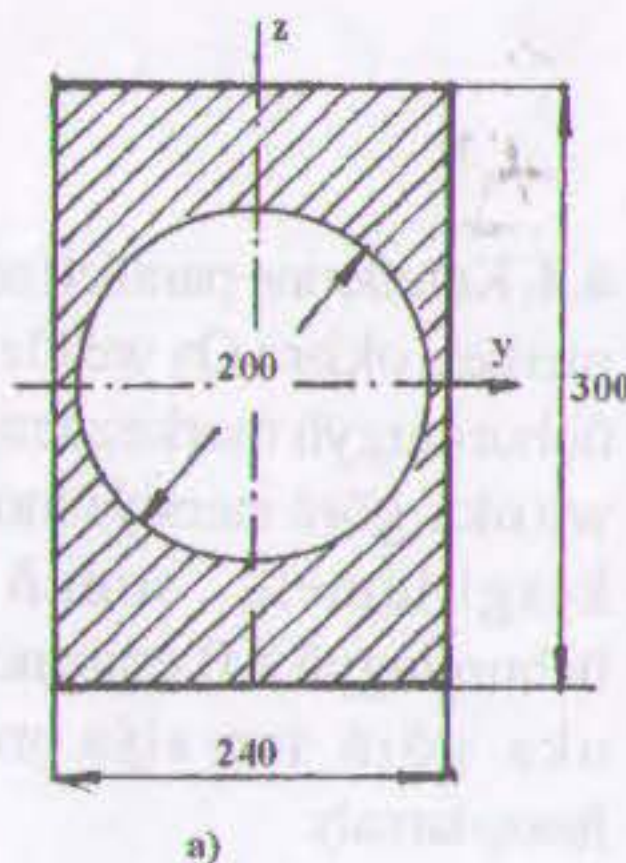


4.5-nji surat

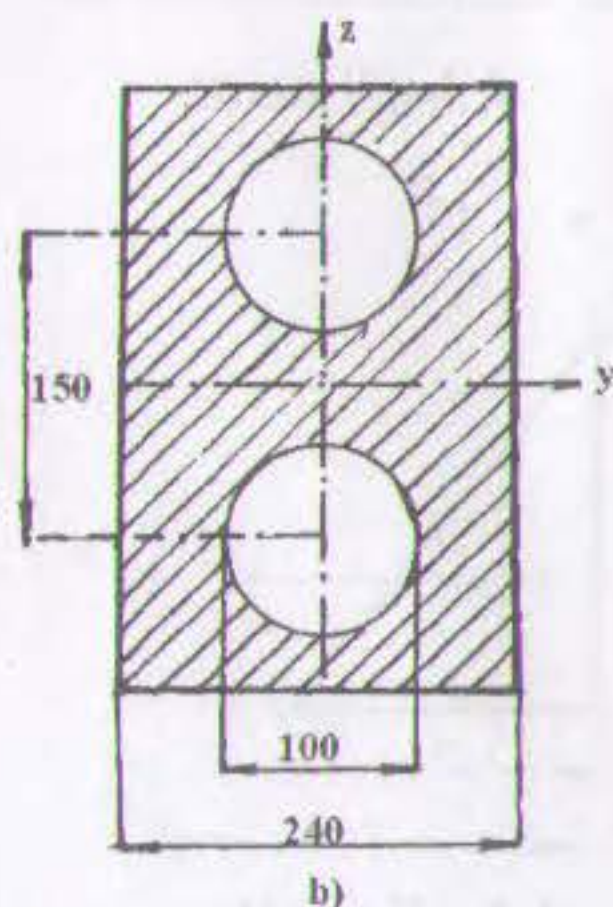


4.6-nji surat

4.7. Diametri 20 sm bolan bir deşigi, diametri 10 sm bolan (b surat) iki deşik bilen çalyssaň, suratda şekillendirilen turba kesikli balkanyň meýdany we inersiýa momenti nähili üýtgeýär?



a)

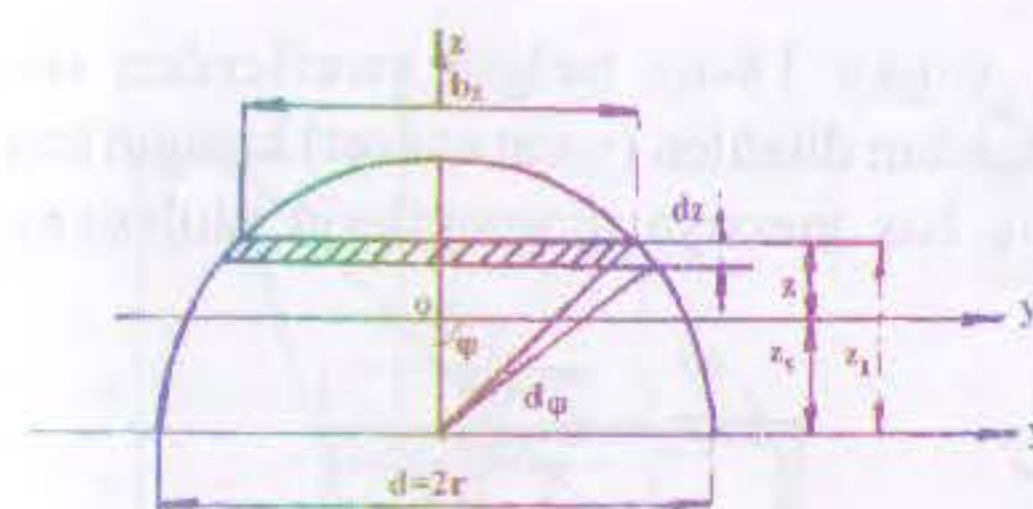


b)

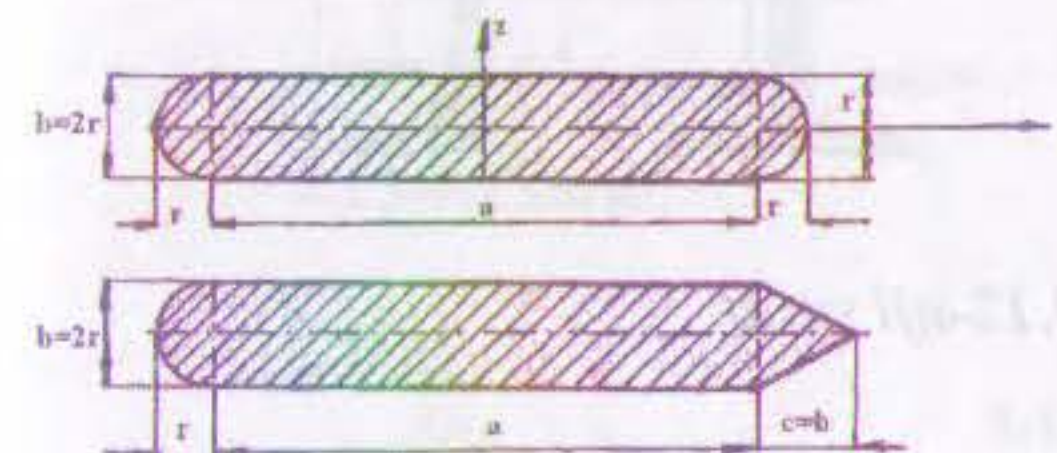
4.7-nji surat

4.5. Esasyna parallel merkezi oka görä deň gapdally trapesiýanyň (surata seret) inersiýa momentini hasaplamaly.

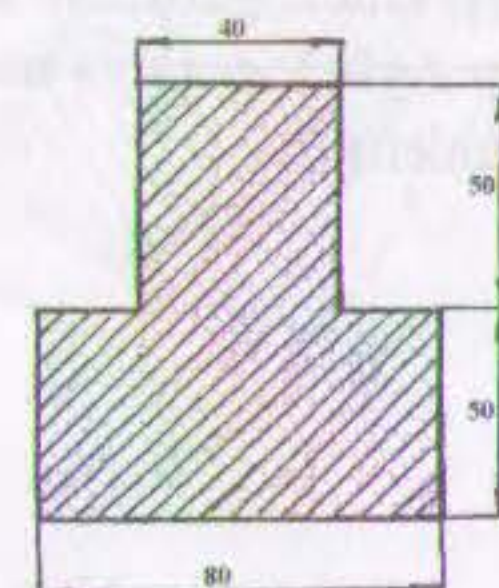
4.6. Suratda şekillendirilen kesigiň bitarap okuna görä inersiýa momentini kesgitlemeli. Ölçepler mm-de görkezilen.



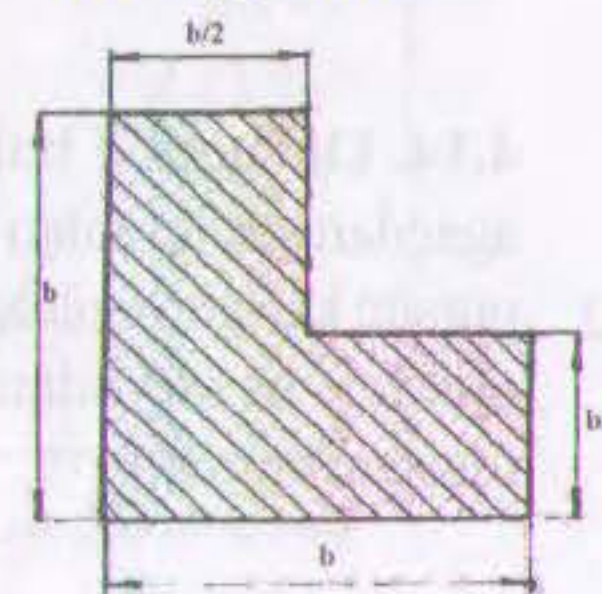
4.8-nji surat



4.9-nji surat



4.10-nji surat



4.11-nji surat

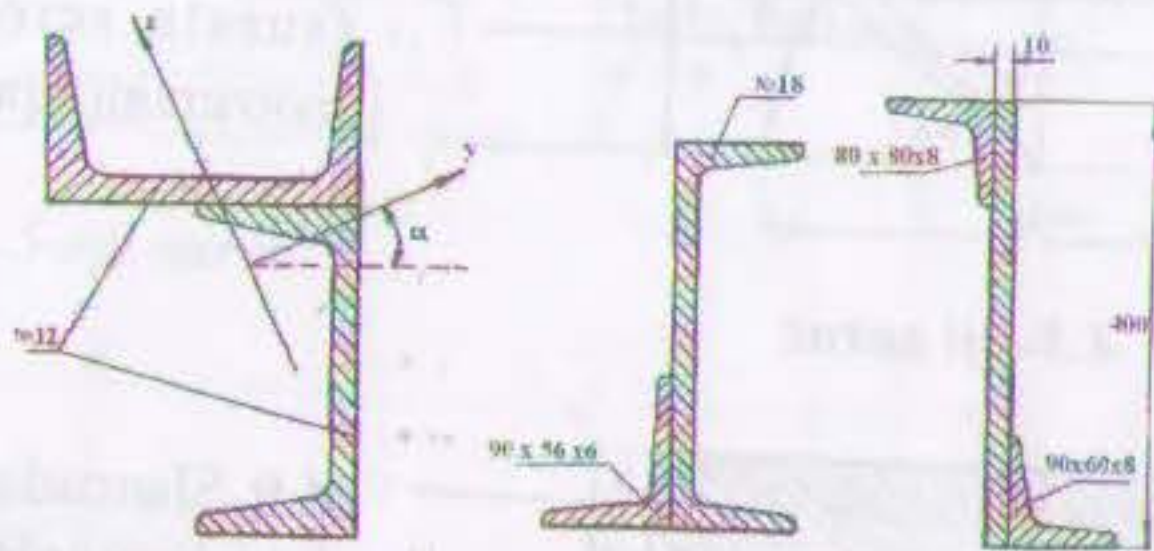
4.8. Baş merkezi inersiýa okuna görä ýarymtegelegiň (surata seret) inersiýa momentini tapmaly.

4.9. Shemada şekillendirilen köpri sütüniň kesiginiň baş inersiýa momentlerini kesgitlemeli.

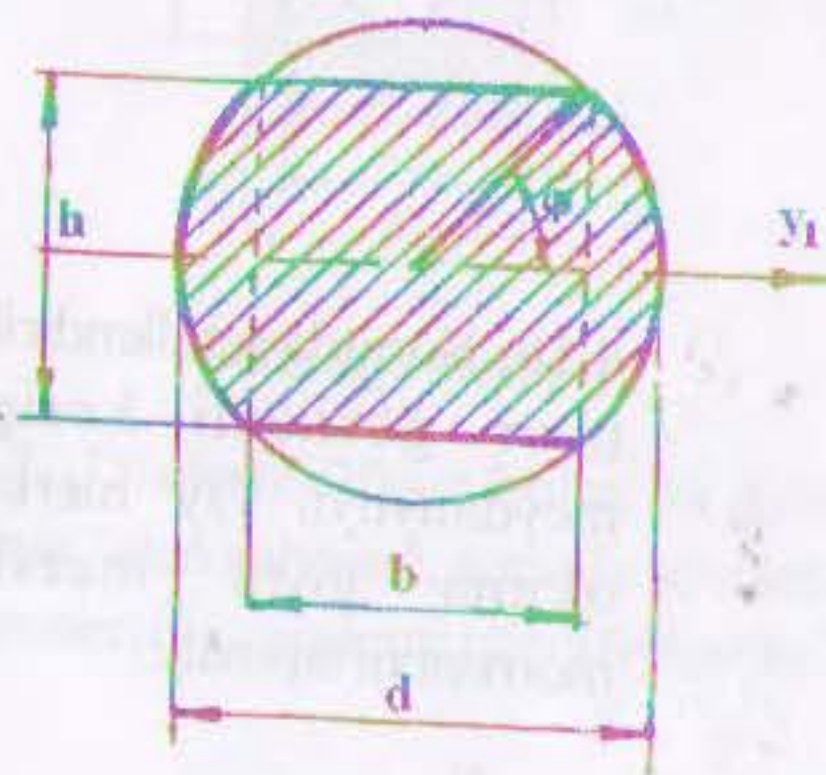
4.10. Suratda şekillendirilen tawr görnüşli kesigiň meýdanynyň Oy merkezi okuna görä inersiýa momentini tapmaly.

4.11. Suratda görkezilen galyň diwarly burçlugyň profiliniň baş inersiýa momentini tapmaly. Şeýle-de burçlugyň polkalaryna parallel merkezi oklara görä merkezden daşlaşýan inersiýa momentini tapmaly.

4.12. Sozulan profillerden, ýagny 18-nji belgili şwellerden we 90x56x6 mm-e deň bolan burçlukdan düzülen (surata seret) kesigiň baş inersiýa okunyň ýagdaýyny we baş inersiýa momentleriň ululygyny kesgitlemeli.

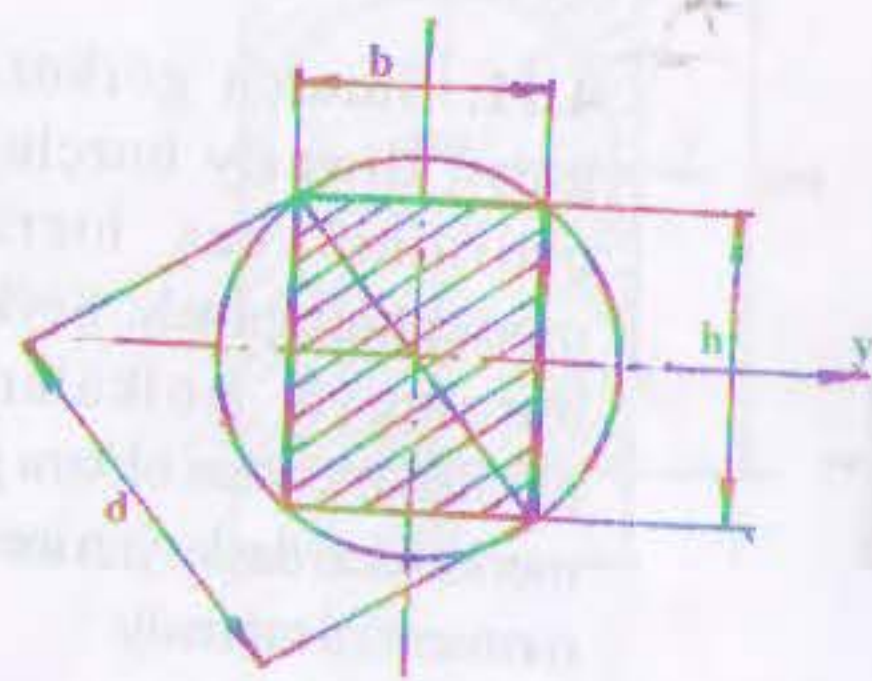


4.12-nji surat



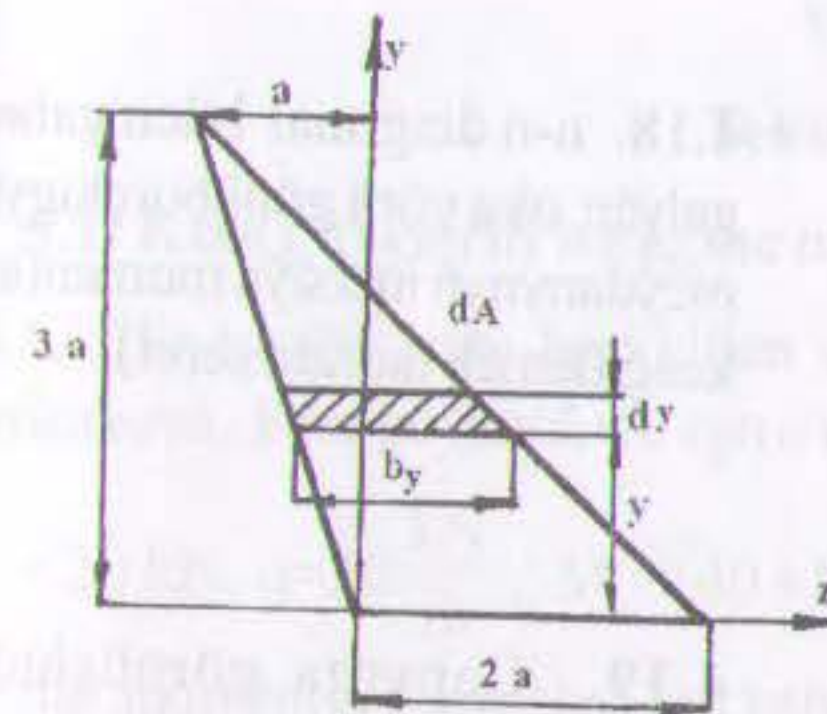
4.13-nji surat

4.13. Tegelekden segment kesilip alnyp emele getirilen kesigiň y okuna görä inersiýa momentini kesgitlemeli.



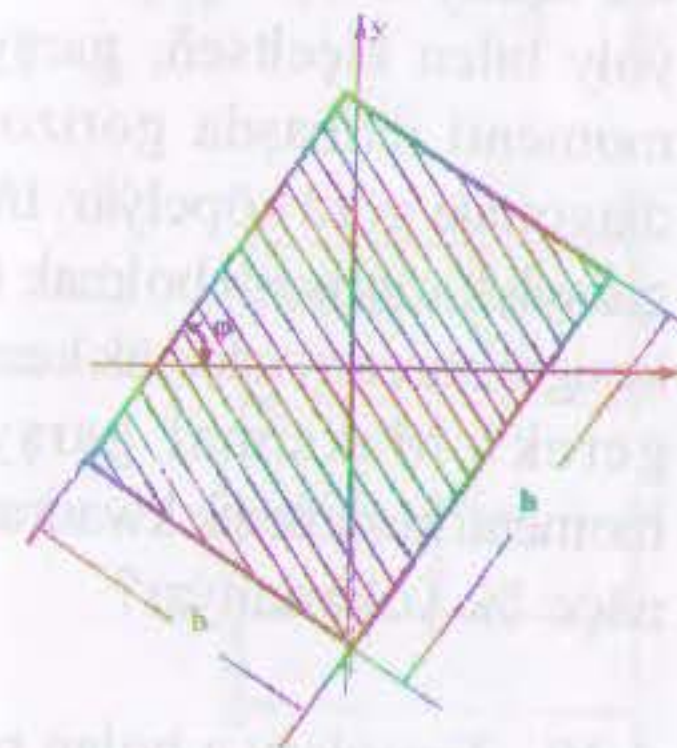
4.14-nji surat

4.14. Diametri d bolan togalak agaçdan kesilip alnan gönüburçly pürsüň kesigini egilme berkliginiň nukdaý nazaryndan iň oňaly ölçegini tapmaly.



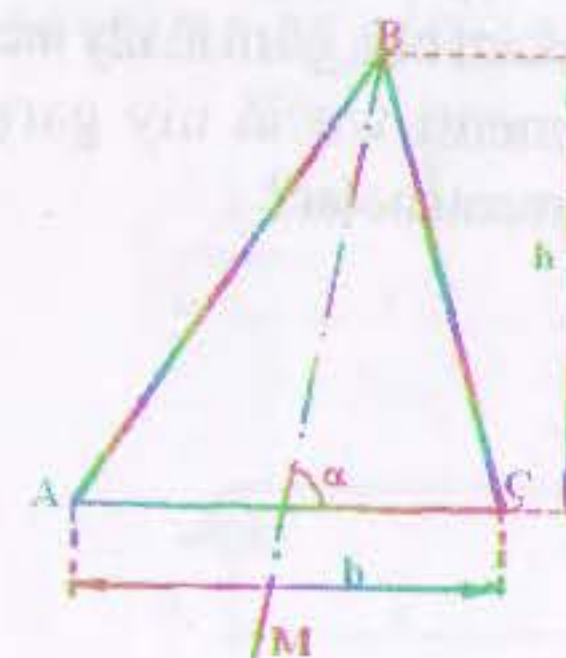
4.15-nji surat

4.15. Baş merkezi okuň ugruny we baş merkezi inersiýa momentlerini kesgitlemeli (surata seret).



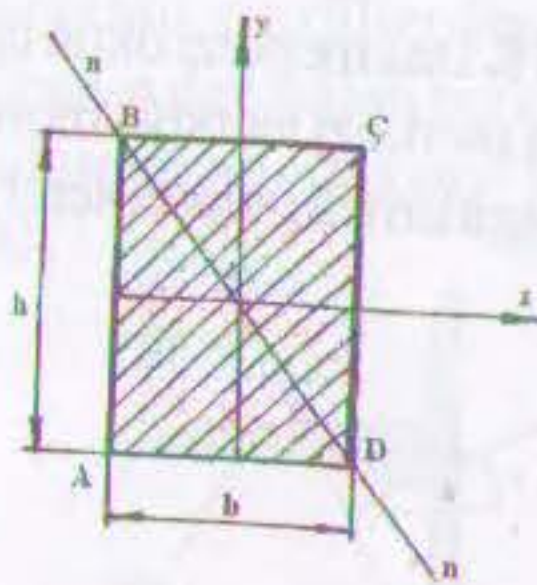
4.16-nji surat

4.16. φ burç boýunça öwrülen ok üçin gönüburçlugyň merkezden daşlaşýan inersiýa momentini tapmaly (surata seret).

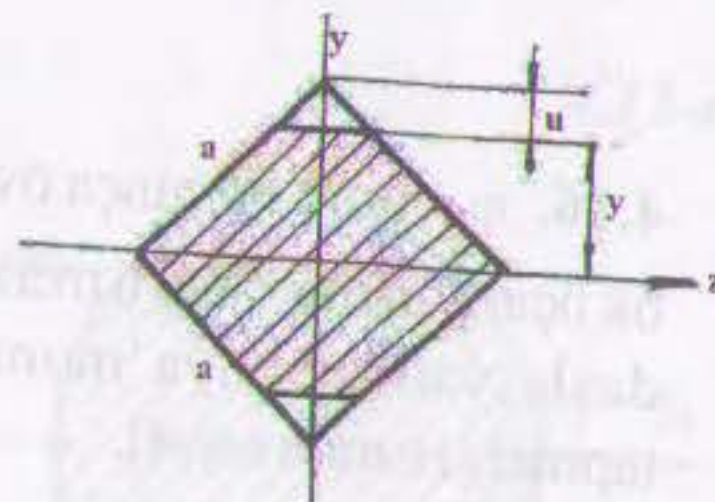


4.17-nji surat

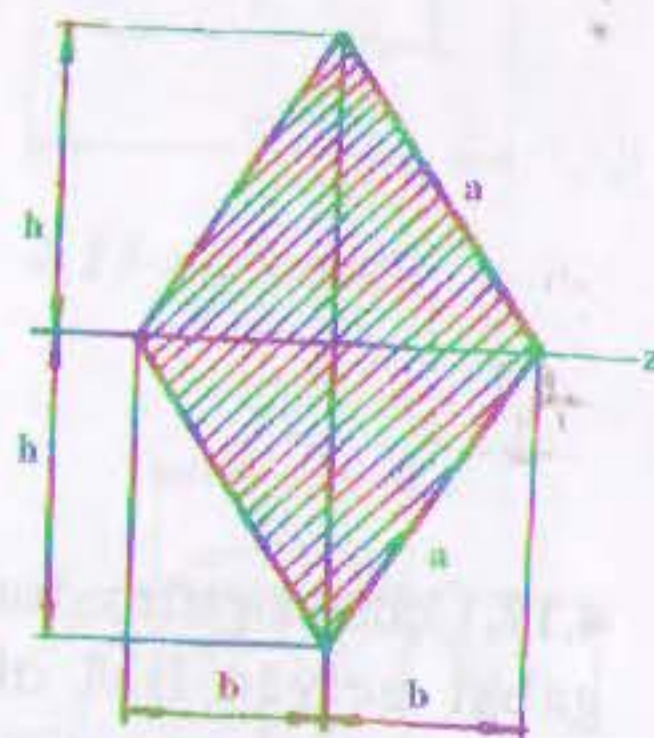
4.17. Üçburçlugyň medianasy bilen gabat gelyän BM oka görä üçburçlugyň inersiýa momentini kesgitlemeli (surata seret).



4.18-nji surat



4.19-nji surat



4.20-nji surat

4.18. n-n diagonal bilen gabat gelyän oka görä gönüburçlugyň meýdanynyň inersiýa momentini kesgitlemeli (surata seret).

4.19. Gapyrga görnüşinde goýlan kwadrat kesigiň uly bolmadyk u ululyk bilen ýokarky we aşaky burçlaryny kesmek ýoly bilen kiçeltseň, garşylyk momenti ilkibaşda gorizontala görä köpelyär. Iň uly garşylyk momenti bolmak üçin kesigiň burçuny näçeräk kesmek gerek? Maksimal garşylyk momenti kesilmedik kwadratdan näçe % ýokarlanýar?

4.20. Taraplary a bolan romb görnüşli kesigiň (surata seret) b we h ölçegleriniň haýsy gatnaşyklarynda gorizontala merkezi oka görä iň uly inersiýa momenti we iň uly garşylyk momenti bolar?

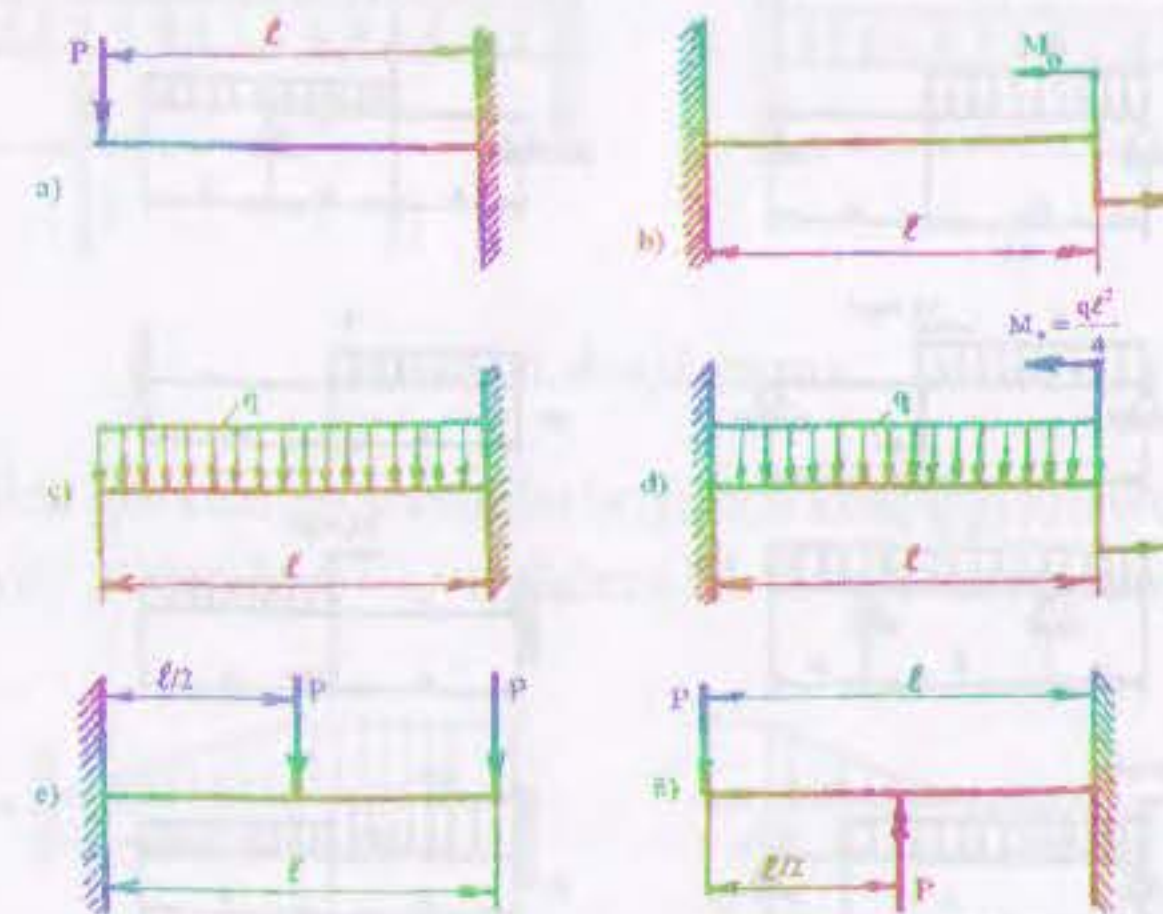
V bap

Tekiz egilme

5.1. Kese güýçleriň we egme momentleriň epýurlaryny gurmak

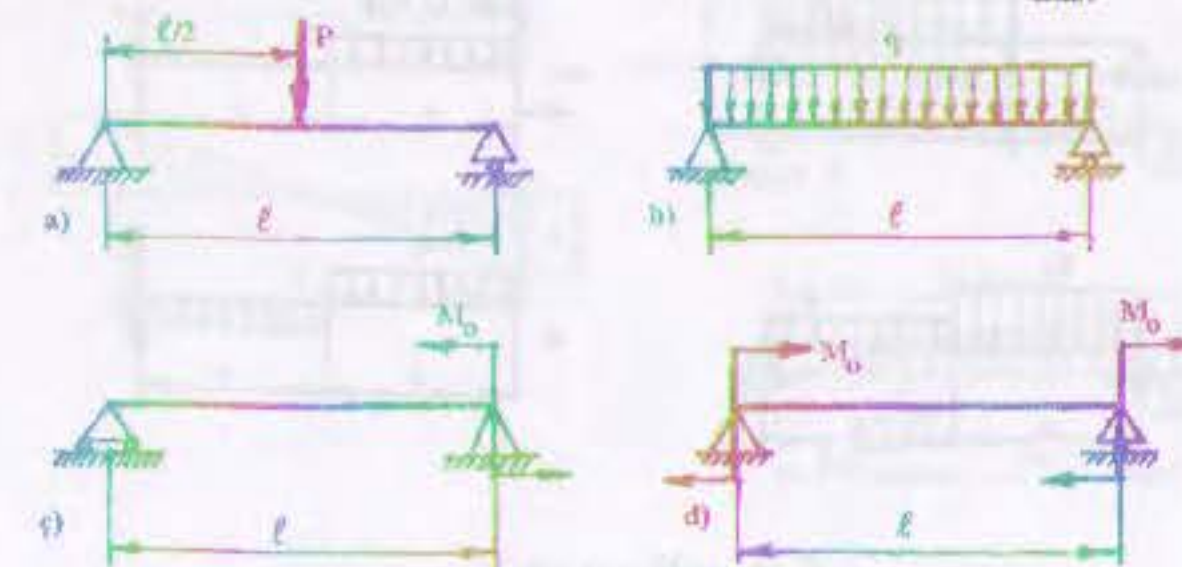
5.1. Bir tarapy gaty berkidilen we suratda görkezilişi ýaly ýüklenen balkalaryň, kese güýjüniň we egme momentiniň epýurlaryny gurmaly. Eger

$P = 20 \text{ kN}$, $q = 20 \frac{\text{kN}}{\text{m}}$, $M_0 = 40 \text{ kN m}$ we $\ell = 2 \text{ m}$ bolsa, kese güýjüň we egme momentiniň iň uly absolýut bahalaryny hasaplamaly.



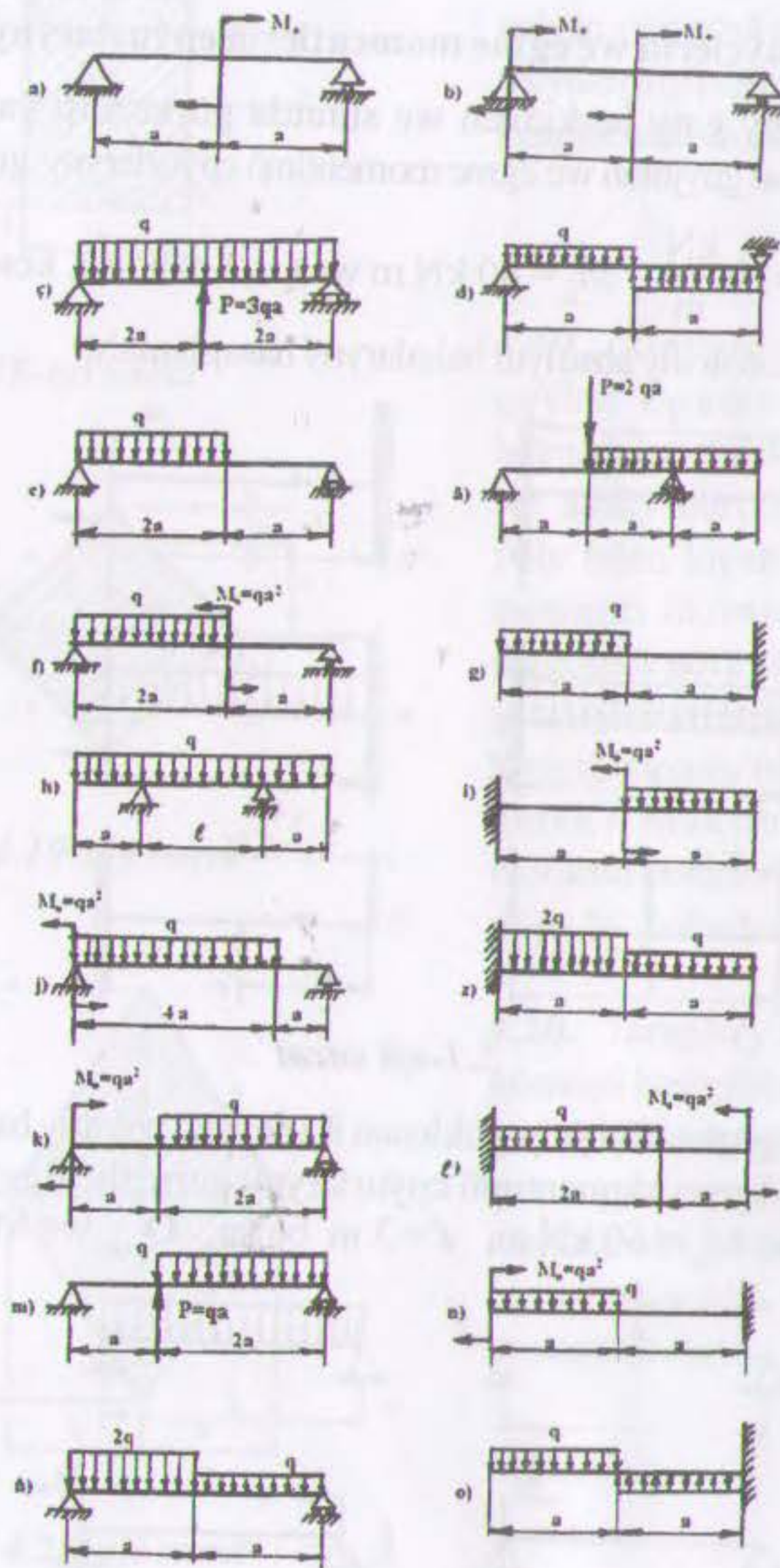
5.1-nji surat

5.2. Suratda görkezilişi ýaly, ýüklenen iki daýanç nokatly balkalaryň kese güýjüniň we egme momentiniň epýurlaryny gurmaly. Eger $P = 60 \text{ kN}$, $q = 20 \text{ kN/m}$, $M_0 = 60 \text{ kN m}$, $\ell = 3 \text{ m}$ bolsa, Q_{\max} we M_{\max} tapmaly.



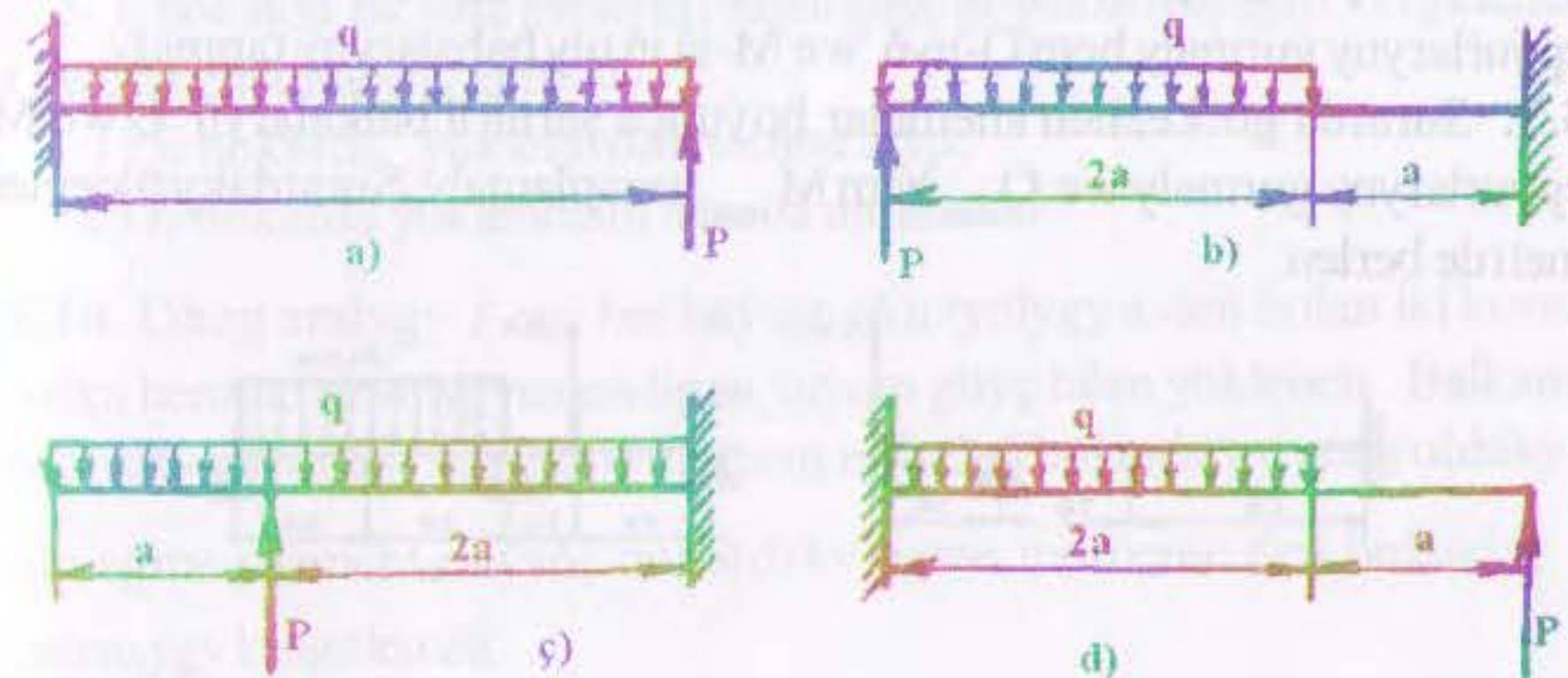
5.2-nji surat

5.3. Suratda şekillendirilen balkalaryň Q we M epýurlaryny gurmaly.



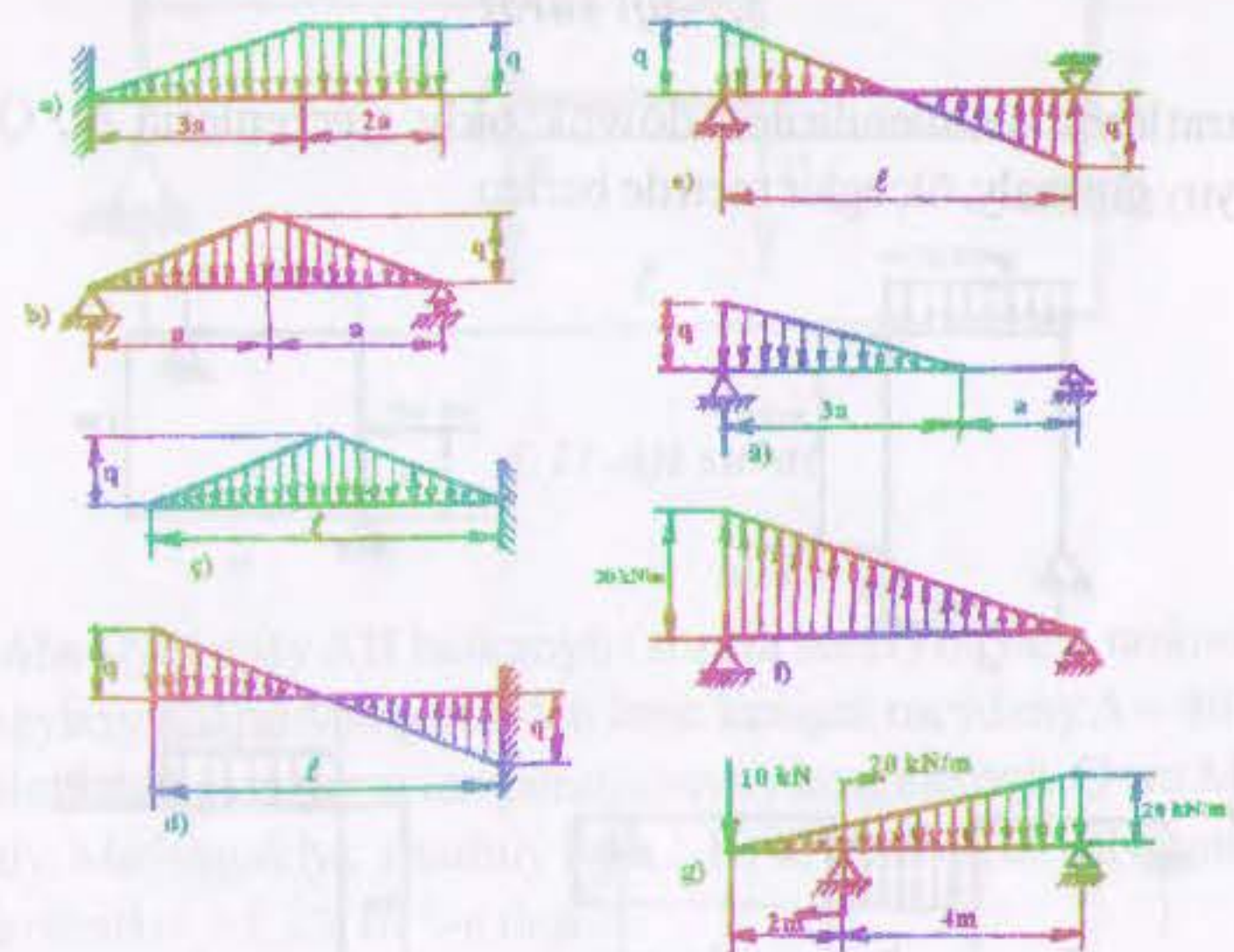
5.3-nji surat

5.4. P güýjüň haýsy bahasynda suratda şekillendirilen balkalaryň daýanç nokadyndaky kesiklerde egme moment nola deň? Güýjüň şu bahasynda Q we M epýurlaryny gurmaly.



5.4-nji surat

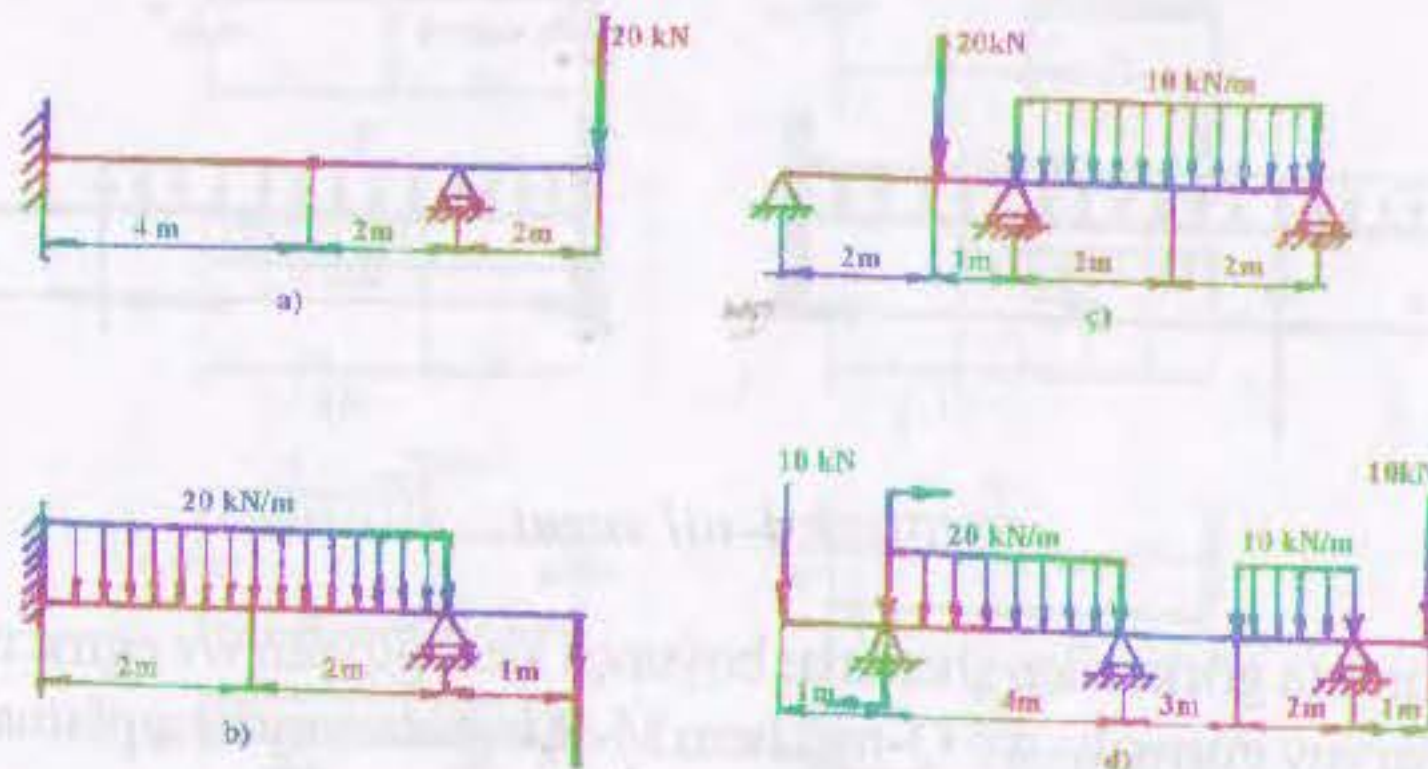
5.5. Suratda görkezilen shemalar boýunça kese güýjüň we egme momentini epýurlaryny gurmaly we Q-nyň hem M-iň bahalaryny hasaplamaly.



5.5-nji surat

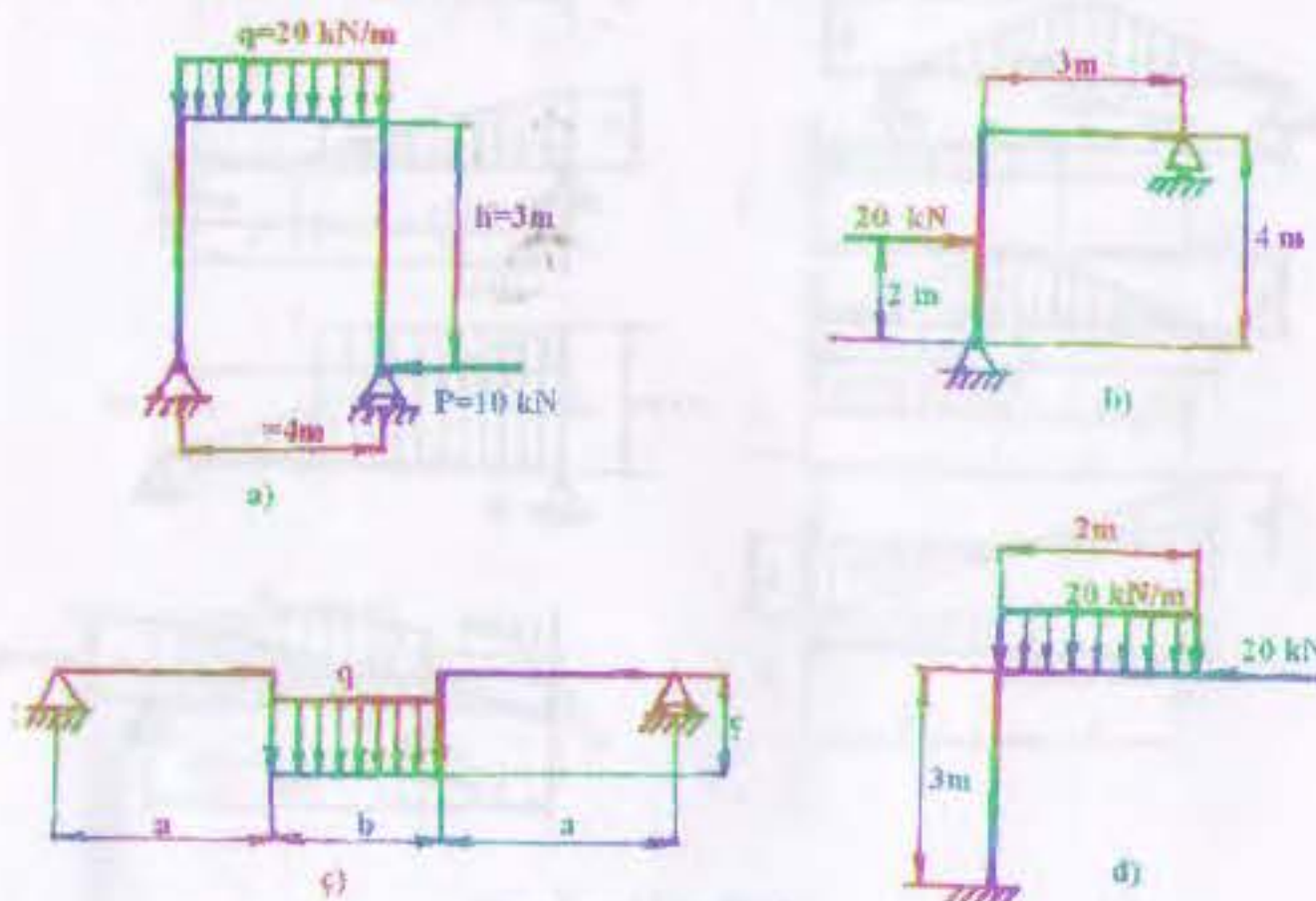
5.6. $q(x) = \frac{4}{\ell^2} q(\ell x - x^2)$ deňleme boýunça üýtgeýän ýaýran güýç bilen ýüklenen prolyoty ℓ bolan iki daýanç nokatly balkanyň Q we M epýurlaryny gurmaly hem Q -nyň we M -iň iň uly bahalaryny tapmaly.

5.7. Suratda görkezilen shemalar boýunça şarnirli balkalaryň Q we M epýurlaryny gurmaly we Q_{\max} hem M_{\max} hasaplamaly. Suratdaky ölçegler metrde berlen.



5.7-nji surat

5.8. Suratlarda şekillendirilen döwür okly sterženleriň N , Q we M epýurlaryny gurmaly, ölçegler metrde berlen.



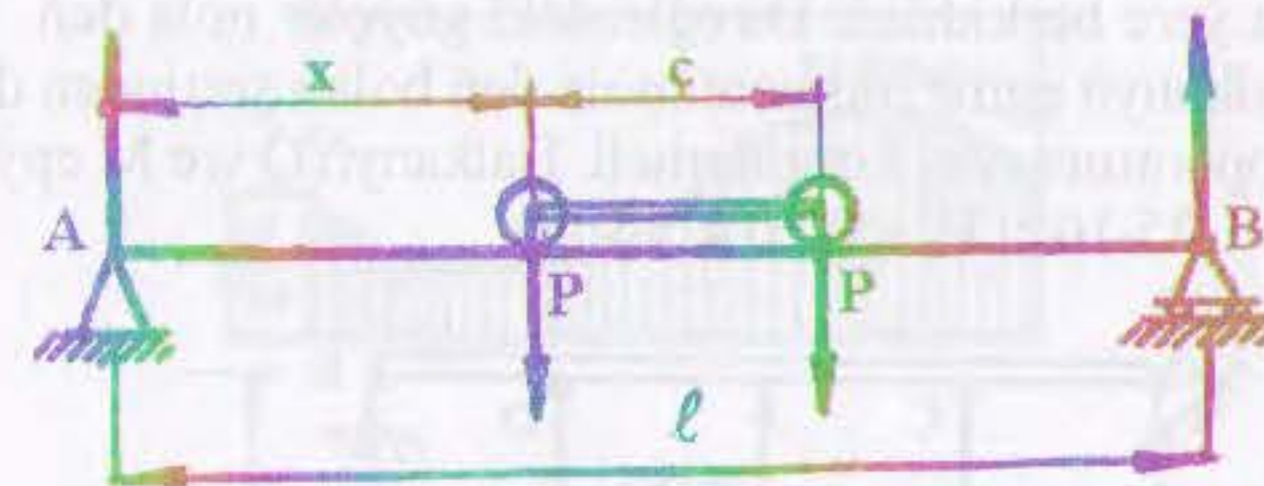
5.8-nji surat

5.9. ABCDE balka A we D nokatlarda şarnirli berkidilen. $AB = 0,6$ m; $BC = 0,6$ m; $CD = 1,8$ m; $DE = 1$ m. B nokatda balka $P = 25$ kN bir ýere jemlenen güýç bilen ýüklenen. Ç nokatda egme moment nola deň bolar ýaly, E nokatda bir ýere jemlenen nähili güýç goýulmalydygyny kesgitlemeli. Q we M epýurlaryny gurmaly:

- 1) E nokatda ýüklenmäni hasaba alyp;
- 2) E nokatda ýüklenmäni hasaba almazdan.

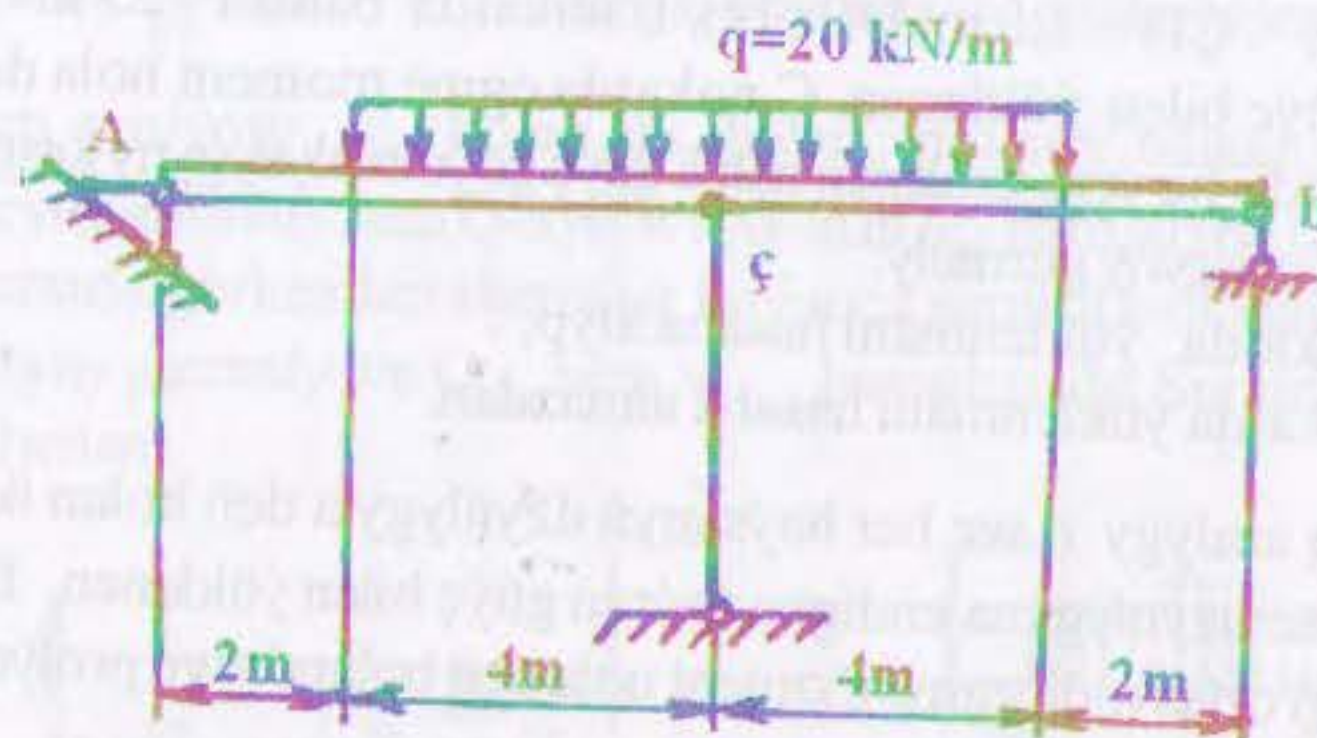
5.10. Direg aralygy ℓ we her haýsynyň uzynlygy a deň bolan iki konsol balka hemme uzynlygyna endigan ýaýran güýç bilen ýüklenen. Balkanyň prolyotynyň ortasynda egme moment nola deň bolanda we prolyotdaky iň uly egme moment daýanç nokatdaky egme momente deň bolanda, $\frac{\ell}{a}$ gatnaşygy kesgitlemeli.

5.11. Köpri kranyň balkasy boýunça her okdan P basyşy geçirýän iki okly arabajyk süýşýär. Egme momentiň iň uly bahasyny almak üçin arabajygy prolyotda nähili ýerleşdirmeli?



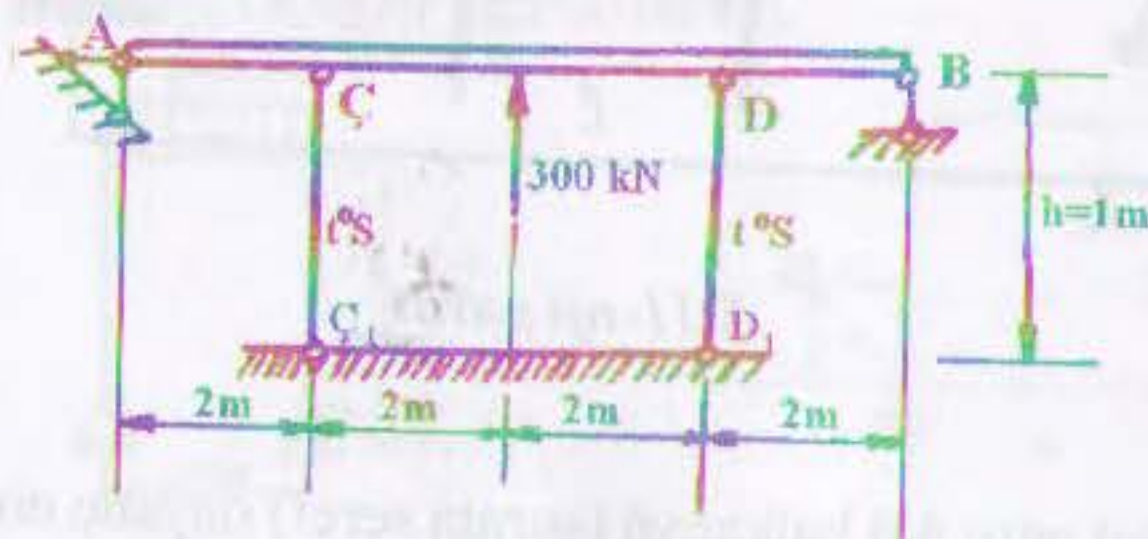
5.11-nji surat

5.12. Absolýut gaty AB balkanyň (surata seret) daýanç nokatlaryndaky gaýtargylary nol bolýan şertinden kese kesigiň meýdany $A = 40$ sm² bolan polat sterženiň gyzdyрма temperaturasyny kesgitlemeli. Q we M epýuryny gurmaly. Maýýşgaklyk moduly $E_p = 2 \cdot 10^4$ kN/sm²-a, uzynlygyna giňelmek koeffisiýenti $\alpha_p = 1,25 \cdot 10^{-5}$ -e deň.



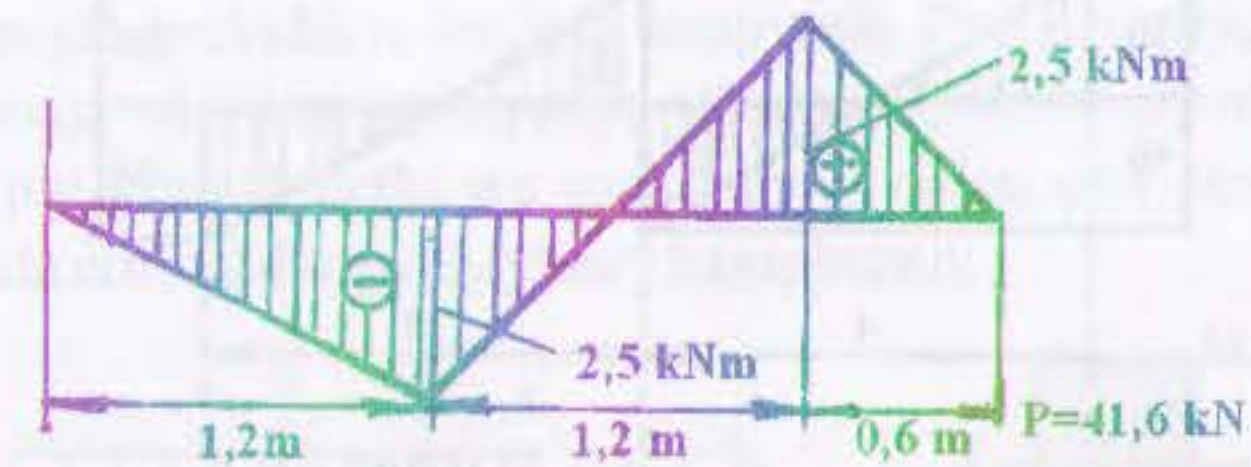
5.12-nji surat

5.13. Absolyut gaty AB balkanyň ortasyna $P=300$ kN ýük ýüklenen we her haýsynyň kesikleriniň meýdany $A=30$ sm² bolan polat diregler bilen Ç we D nokatlarda ýere berkidilen. Direglerdäki güýçler nola deň. Ç we D kesiklerde balkanyň egme momenti nola deň bolan şertinden diregleriň sowatma temperaturasyny kesgitlemeli. Balkanyň Q we M epýurlaryny gurmaly ($\alpha_p=1,25 \cdot 10^{-5}$, $E_p=2 \cdot 10^4$ kN/sm²).



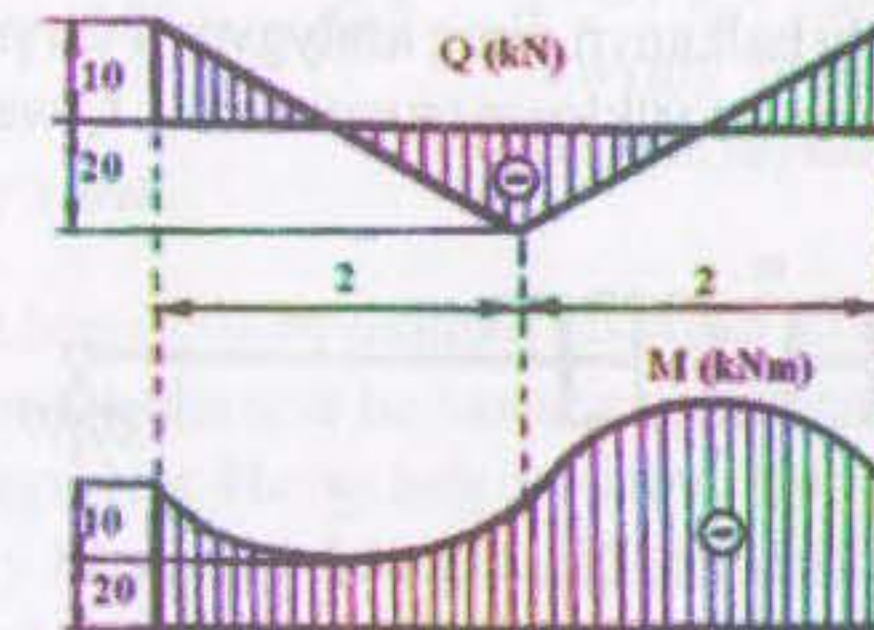
5.13-nji surat

5.14. Suratda A we Ç nokatlarda şarnirli berkidilen balkanyň epýury şekillendirilen. Ýüklenmäni, Q epýuryny şekillendirmek we direglerdäki gaýtargylary tapmak talap edilýär.

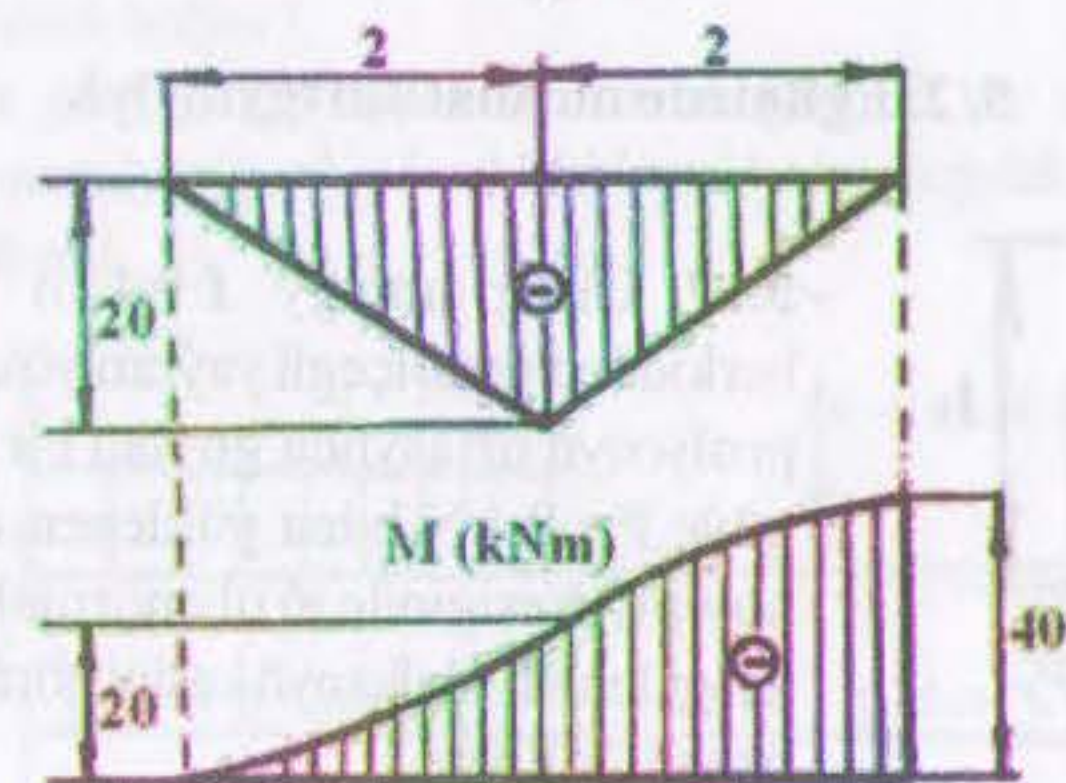


5.14-nji surat

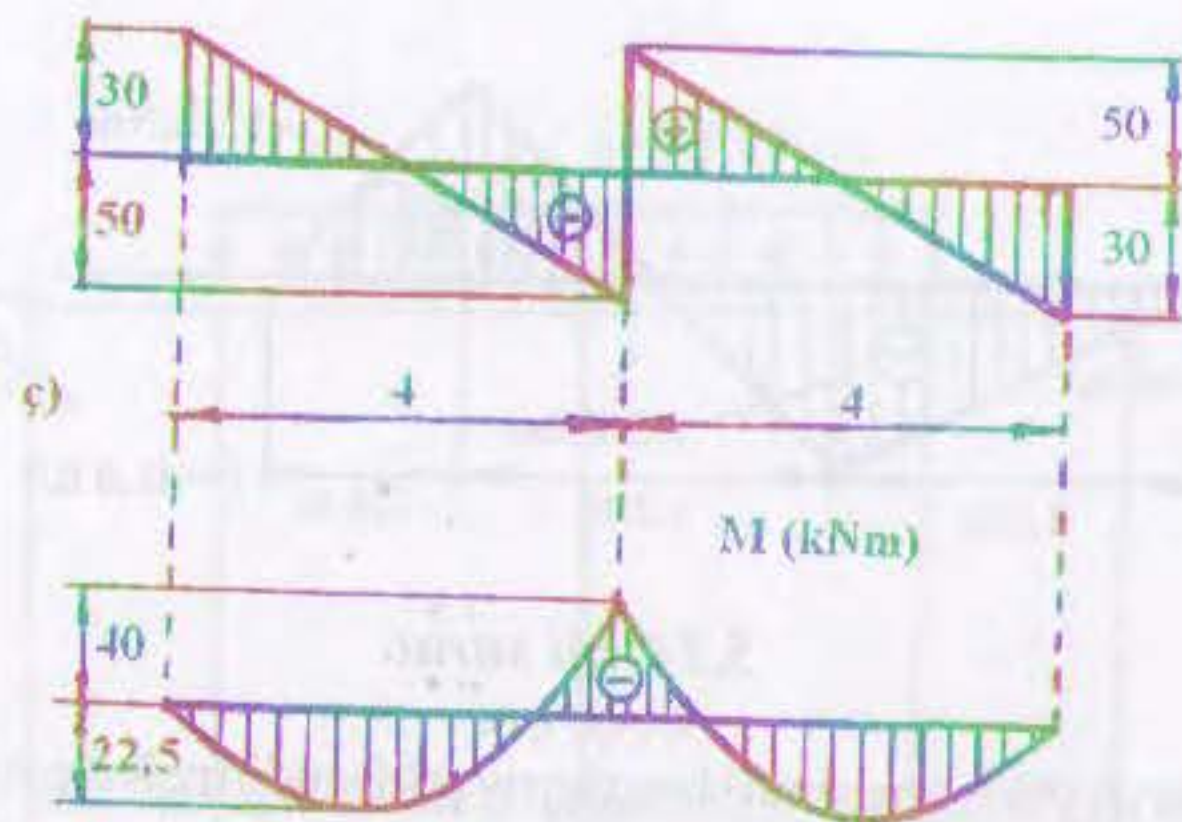
5.15. Balkalaryň ýüklenmesiniň shemasyny şekillendirmeli we suratda getirilen kese güýjüň hem-de egme momentiň epýury boýunça goýlan güýçleriň ululygyny kesgitlemeli. Uzynlyk metrde görkezilen, Q – kN, M – kNm.



a

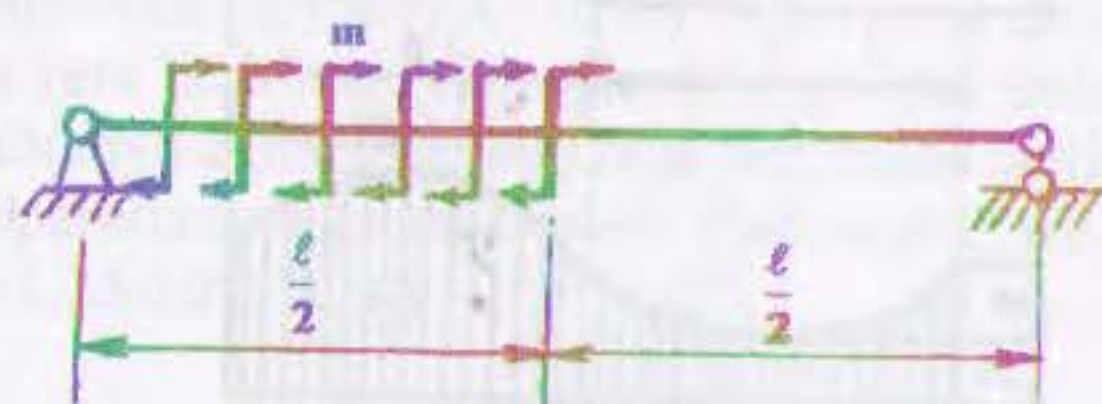


b



5.15-nji surat

5.16. Iki daýanç nokatly balkanyň direk aralygynyň ýarysyna hemişelik depginli ýaýran daşky moment ýüklenen (surata seret). Q we M epýurlaryny gurmaly.



5.16-nji surat

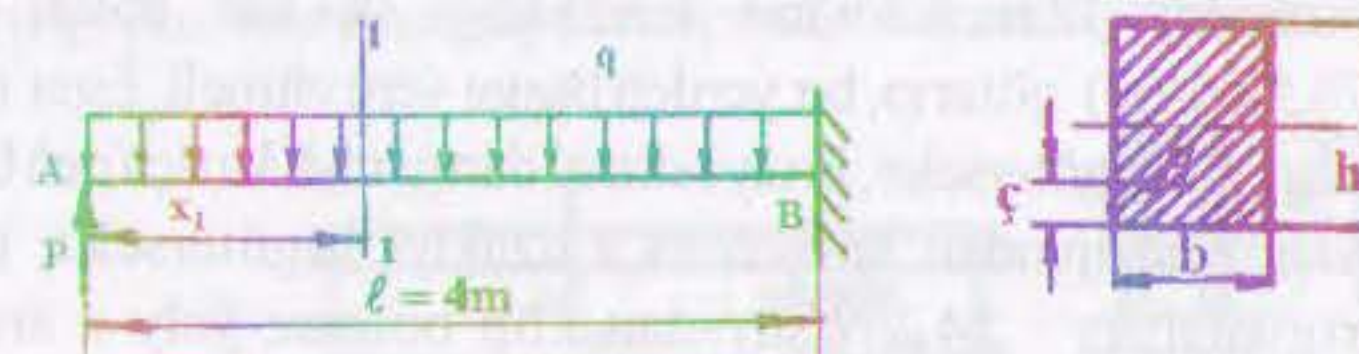
5.2. Egilmede normal dartgynlylyk



5.17-nji surat

5.17. Direk aralygy $\ell = 4$ m bolan şarnirli berkidilen deňölçegli ýaýran ýük $q = 4$ kN/m we prolýotyň ortasynda goýlan bir ýere jemlenen güýç $P = 2$ kN bilen ýüklenen ağaç balkanyň howply kesiginde iň uly normal dartgynlylygy kesgitlemeli. Balkanyň kesigi gönüburçluk ölçegi $b \times h = 12 \times 20$ sm².

5.18. 20×30 sm ölçegli gönüburçly kese kesikli ağaç balkanyň bir tarapy diwara pugta berkidilen, beýleki tarapynda $P = 5$ kN güýç we balkanyň uzynlygyna $q = 6$ kN/m ýaýran güýç ýüklenen. Q we M epýurlaryny gurmaly we howply kesigiň çetki we aşaky gyrasyndan $\zeta = 4$ sm uzaklykdaky nokadynda normal dartgynlylyklary hasaplamaly.



5.18-nji surat



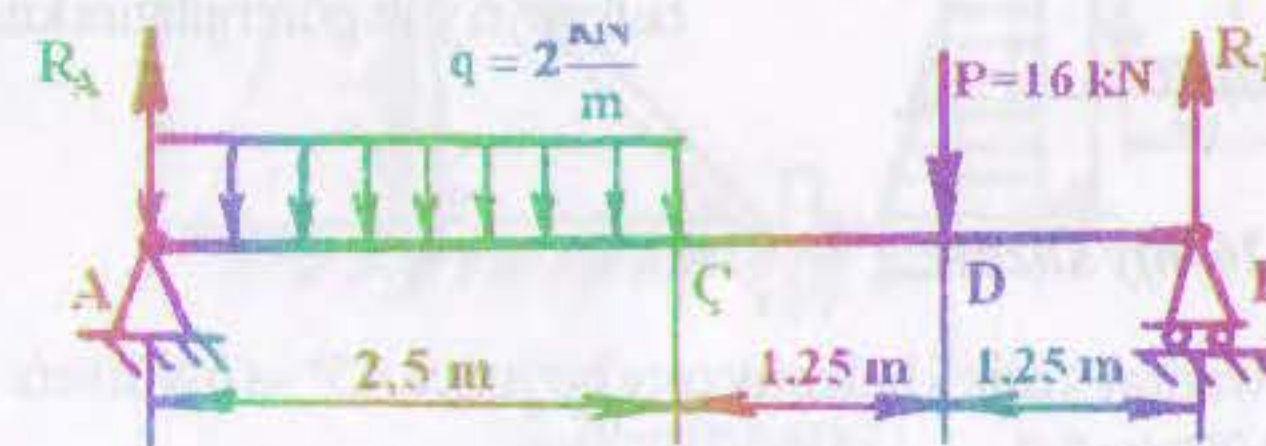
5.19-nji surat

5.19. Suratda görkezilen prolýoty 6 m, $P = 60$ kN güýç bilen ýüklenen iki tawraly balkanyň DÖST boýunça kesigini saýlamaly.

5.20. Diwaryň hemişelik beýikligini saklaýan iki sany 20 a belgili sozulyp ýasalan iki tawraly balka setir boýunça ýerleşdirilen. Olar bir sany iki tawraly balka bilen çalşyrylýar. Haýsy belgili iki tawraly balkany çalşyp bolar?

5.21. Uzynlygy 12 m, daşky diametri 25 sm we diwarynyň galyňlygy 1 sm bolan çöýün turba iki daýanç nokatlaryň üstünde ýerleşdirilen we suw bilen doldurylan. Eger çöýüniň udel agramy 7,8 bolsa, turbadaky iň uly normal dartgynlylyk nähili bolýar?

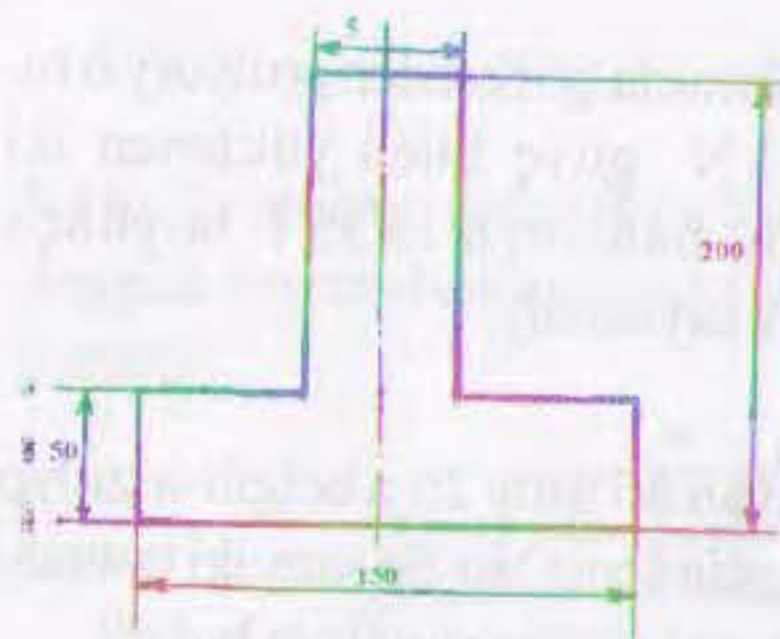
5.22. Suratda görkezilen balka üçin kese güýjüň we egme momentiň epýurlaryny gurmaly. Eger $[\sigma] = 11$ kN/sm² bolsa, tegelek kesikli balkanyň diametrini tapmaly.



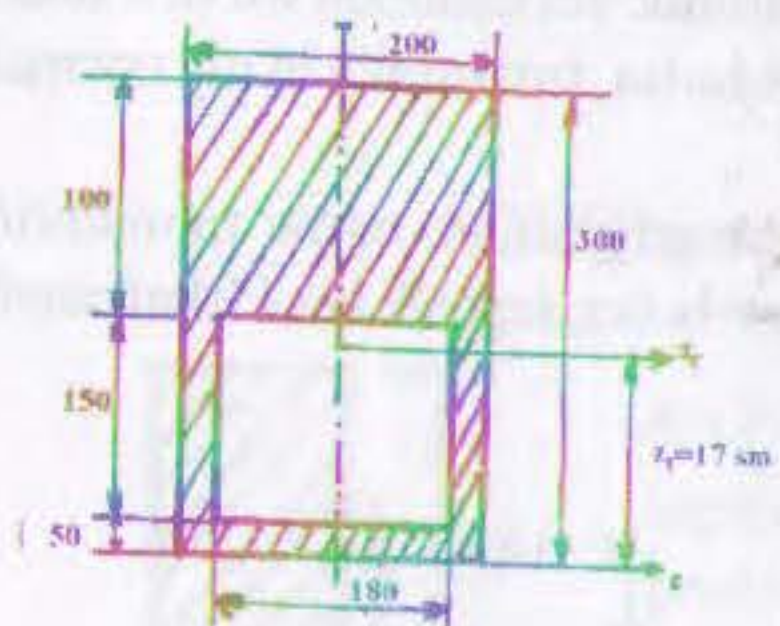
5.22-nji surat

5.23. Birmeñzeş uzynlygy, meýdany we materialy bolan iki balkanyň biriniň kese kesigi kwadrat, beýlekisiniňki bolsa tegelek. Tegelek kesikli balka üçin balkanyň direg aralygynyň ortasynda goýlan howpsuz güýjiň ululygy 10 kN-a deň. Direg aralygynyň ortasynda goýlan howpsuz güýjüň ululygy kwadrat kesikli balka üçin nähili bolar?

5.24. Iki işçi uzynlygy 12 m, kwadrat kese kesigi $3 \times 3 \text{ sm}^2$ bolan polat sterženi ($\gamma = 78,5 \text{ kN/m}^3$) göterip, bir ýerden başga ýere eltmeli. Eger işçiler sterženiň ujundan tutup göterseler, iň uly normal dartgynlyk näçä deň bolar? Eger her işçi sterženiň ujundan birmeñzeş a uzaklykda göterseler, iň uly normal dartgynlyk 14 kN/sm^2 -dan köp bolmaz ýaly a aralygy kesgitlemeli.



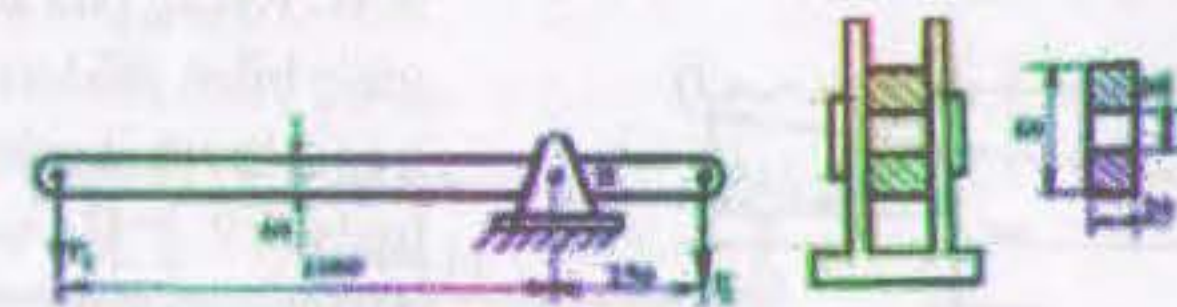
5.25-nji surat



5.26-njy surat

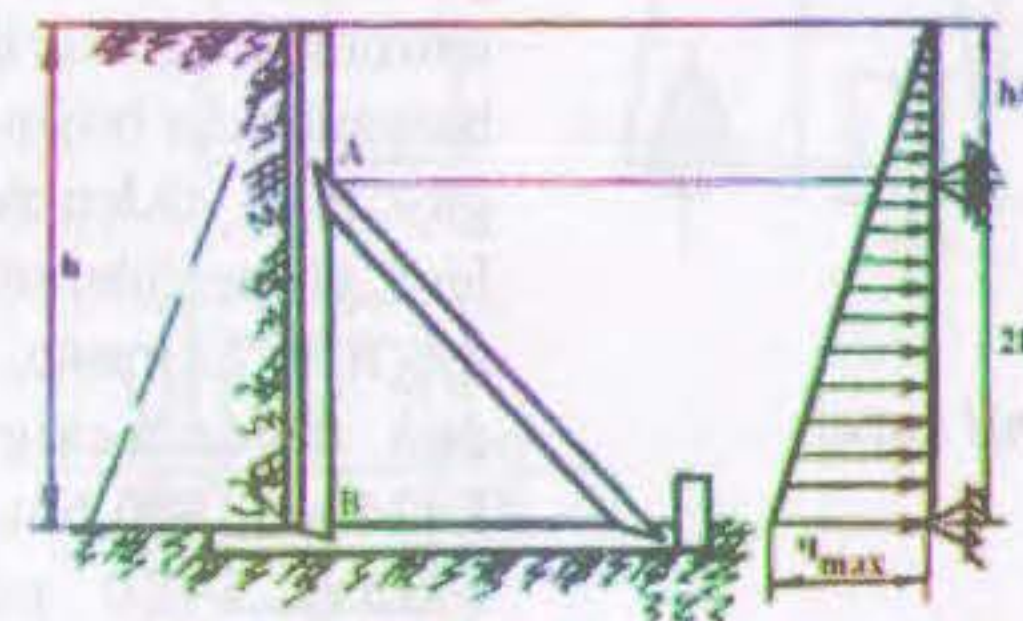
5.27. Eger kwadrat kesikli balkany oky boýunça 45° -a öwürseň, onuň yük göterijiligi nähili üýtgär?

5.28. Ştanganyň deşiginiň içinden geçirilen şarnirli bolta, B nokatda (surata seret) direňýän, gönüburçly kese kesikli $20 \times 60 \text{ mm}$ ştanga, togtadyjy enjamyň polat ryçagy bolup hyzmat edýär. Deşiň merkezi ştanganyň okunda ýerleşýär, onuň diametri $d = 30 \text{ mm}$. Boltuň deşiginiň kesigi gowşadýandygyny hasaba alyp we rugsat edilyän dartgynlyk $[\sigma] = 14 \text{ kN/sm}^2$ bolsa, ryçagyň soňuna goýlan howpsuz güýçleri tapmaly. Suratdaky ölçegler mm-de berlen.



5.28-nji surat

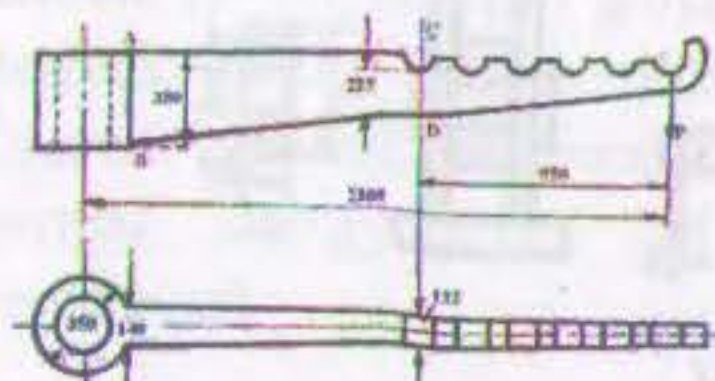
5.29. Suratda şekillendirilen direg diwarynyň kwadrat kesigini we tagta örtügiň galyňlygyny saýlap almaly. Her 2 m-den goýlan sütün kese goýlan purse direlen we söýeg bilen saklanýar, her sütüni A we B nokatlarda şarnirli diregi bolan balka hökmünde seredip bolýar. Sütünler tagta örtügiň üsti bilen geçirilýän topragyň basyşy bilen ýüklenen. Sütünde döreýän boý güýç hasaba alynmaýar. Ini $b = 20 \text{ sm}$ bolan tagta örtügiňi diregde kesilen şarnirli daýanç nokatlary bolan balka diýip hasap etmeli. Gum üýşmeginiň beýikligi 1,5 m. Topragyň basyşy çyzyk kanuny boýunça 0-dan $q_{\text{max}} = 13 \text{ kN/m}^3$ -a çenli artýar. Egilmede rugsat edilyän dartgynlyk $[\sigma] = 1 \text{ kN/sm}^2$.



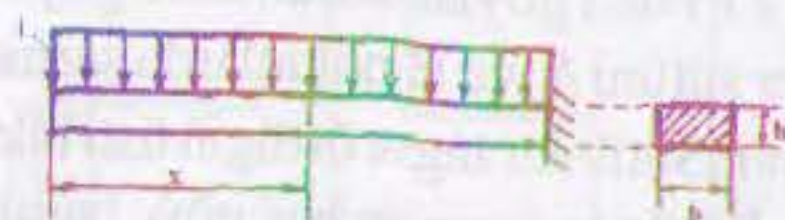
5.29-njy surat



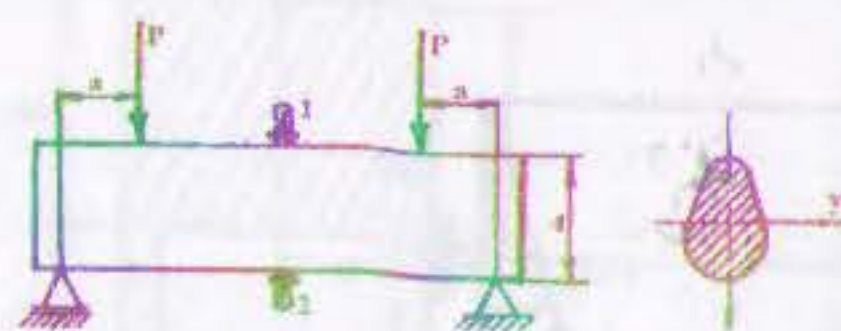
5.30-njy surat



5.31-nji surat



5.32-nji surat



5.33-nji surat

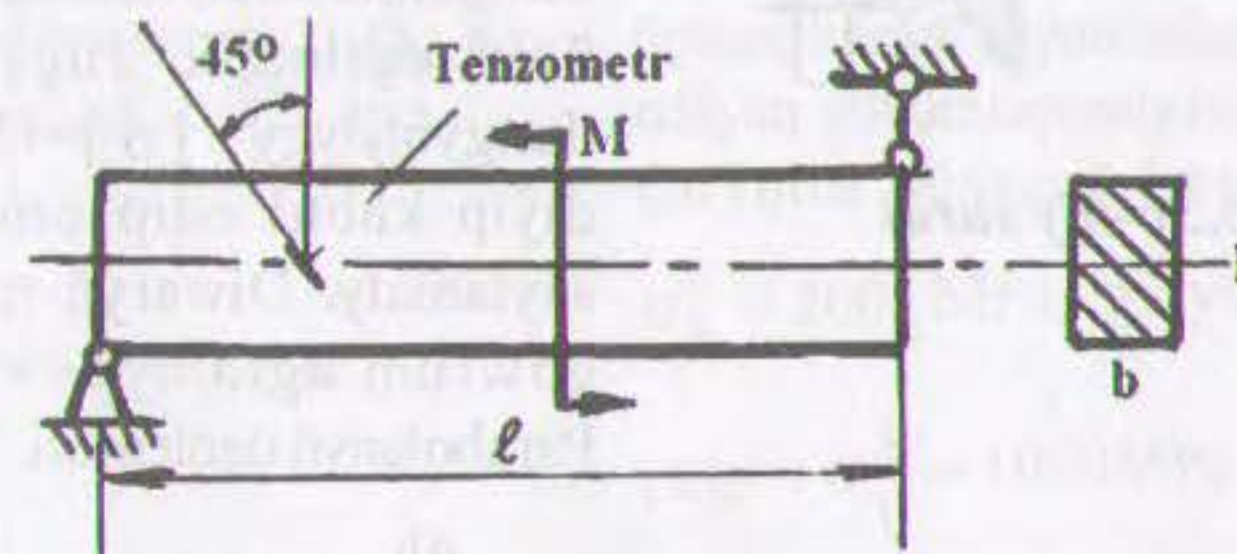
5.30. Eger balkanyň oky töweregiň dugasy boýunça egilýän bolsa, hemişelik h beýiklikli (kesigiň ini üýtgeýär) gönüburçly kesigi bolan balka haýsy şekilde bolmaly?

5.31. Ryçag (surata seret) $P = 80 \text{ kN}$ güýç bilen ýüklenen. AB ýa-da ÇD kesikleriň haýsysy „howply“ bolýar? Howply kesikde dartgynlyk näçä deň?

5.32. Konsol egilmede deň garşylykly balka görnüşinde taslanýar. Konsolyň kese kesigi, beýikligi hemişelik h deň bolan gönüburçluk. Kesigiň ininiň üýtgemek kanunyny $b = b(x)$ anyklamaly. Konsolyň her kesiginde maksimal dartgynlyk $[\sigma]$ - rugsat edilýäne deň.

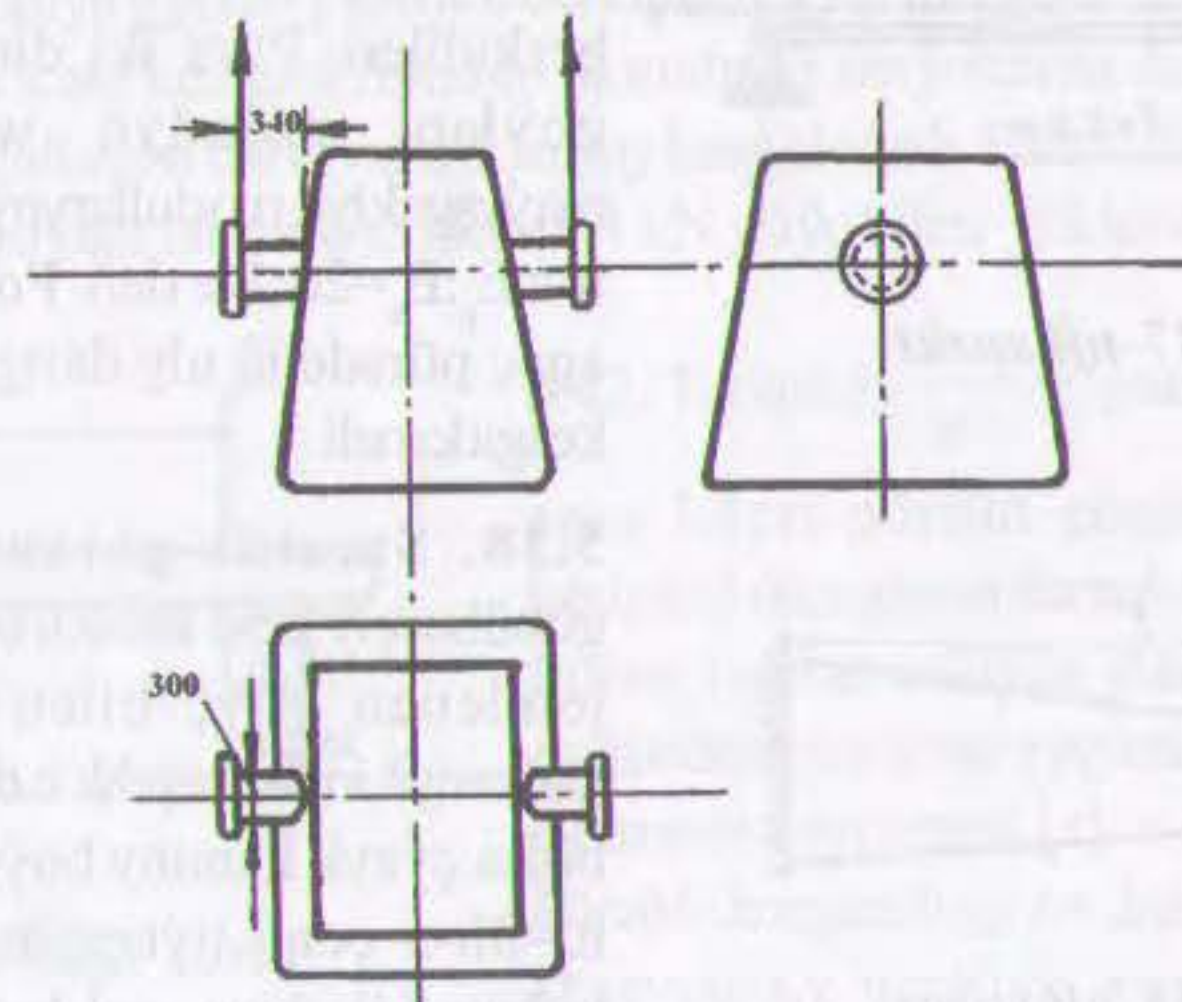
5.33. Çoýun balka ($E = 1,2 \cdot 10^4 \text{ kN/sm}^2$) synag edilende, suratda görkezilen shema boýunça 1 we 2 tenzometriň görkezijileri, ölçenilen başgaçaklar boýunça $P = 50 \text{ kN}$ güýç bilen ýüklenende tenzometrleriň görkezijileriniň orta artmasy $\Delta n_1 = -15 \text{ mm-e}$, $\Delta n_2 = 5 \text{ mm-e}$ deň. Eger kesigiň beýikligi $h = 24 \text{ sm}$, $a = 0,6 \text{ m}$, tenzometriň bazasy $\ell = 20 \text{ mm}$, ulaltma koeffisiýenti $K = 1000$ bolsa, baş merkezi oka görä kesigiň inersiýa momentiniň ululygyny kesgitlemeli.

5.34. Suratda şekillendirilişi ýaly, balkanyň bitarap okunda kesekesigine 45° burç boýunça tenzometr ýerleşdirilen. Balka ýüklenenden soň B bazasy bolan tenzometr ΔB uzalma görkezýär. Abzalyň görkezen bahasynda momentini ululygyny nähili kesgitläp bolýar? Balkanyň kese-kesiginiň ini b we beýikligi h , maýyşgaklyk moduly E we Puassonyň koeffisiýenti μ -e deň bolan materialdan ýerine ýetirilen.

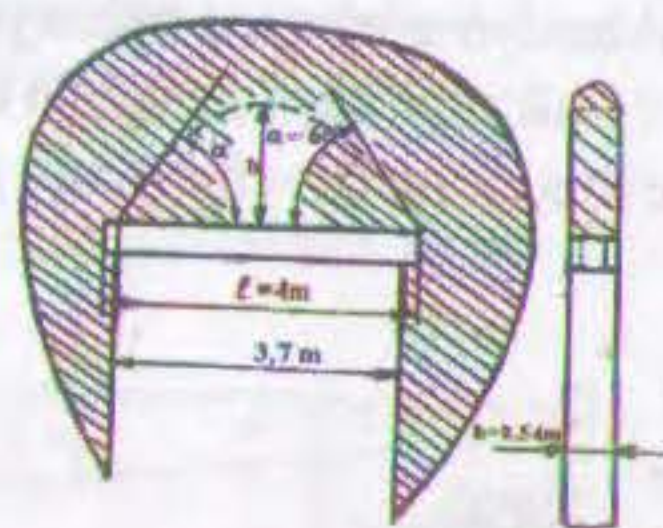


5.34-nji surat

5.35. Eredilip galyba guýlan poladyň galyp bilen bilelikdäki agramy 430 kN (surata seret). Galybyň sapfasynyň boýnundaky dartgynlygy tapmaly.



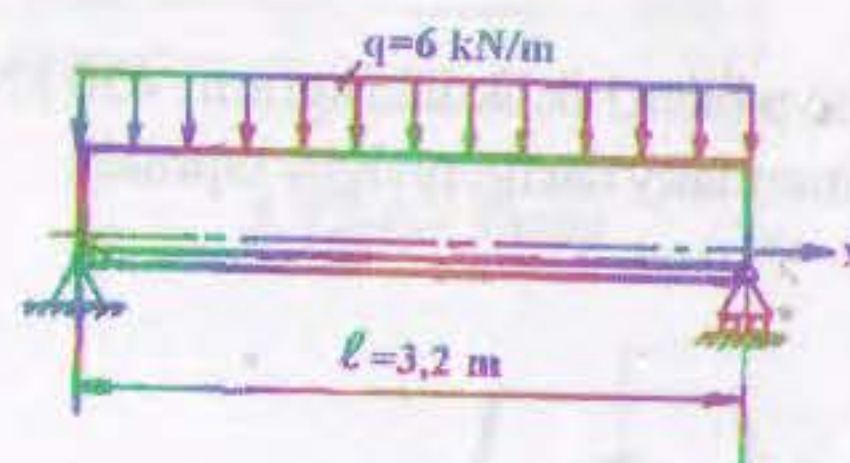
5.35-nji surat



5.36-nji surat

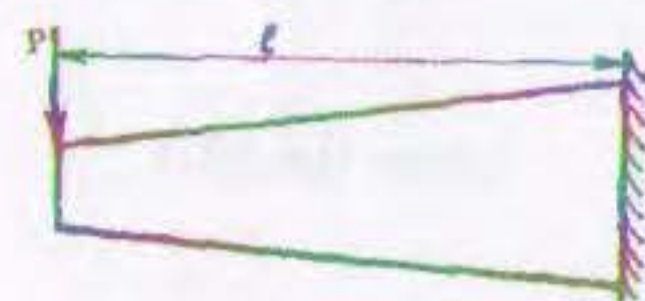
5.36. Diwarynyň galyňlygy $b = 54$ sm bolan gapy ýere iki birmeňzeş tawra bilen basyrylan. Balkanyň hasaplaýyş uzynlygy $\ell = 4$ m. Balka düşýän ýük diregde $\alpha = 60^\circ$ burç boýunça ýapgytlanan parabola boýunça çäklenen diwaryň böleginiň agramyna deň (surata seret). Balkanyň materialy üçin egilmede rugsat edilyän dartgynlylygy $[\sigma] = 15 \text{ kN/sm}^2$ deň diýip kabul edip onuň kesigini saýlamaly. Diwaryň materialynyň göwrüm agramy $\gamma = 16 \text{ kN/sm}^3$. Parabolanyň deňlemesi.

$$y = \frac{4h}{\ell^2} x(\ell - x).$$



5.37-nji surat

5.37. Uzynlygy $\ell = 3,2$ m, ini $b = 12$ sm, galyňlygy $b = 0,6$ sm (surata seret) polat list kesigi $b \times h = 12 \times 18$ sm agaç pürse berkidilen. Pürs iki diregde erkin goýlan, poladyň we agajyň maýýsgaklyk modullarynyň gatnaşygy $n = E_p : E_a = 20:1$ -e deň. Polat listde we agaç pürsde iň uly dartgynlylyklary kesgitlemeli.



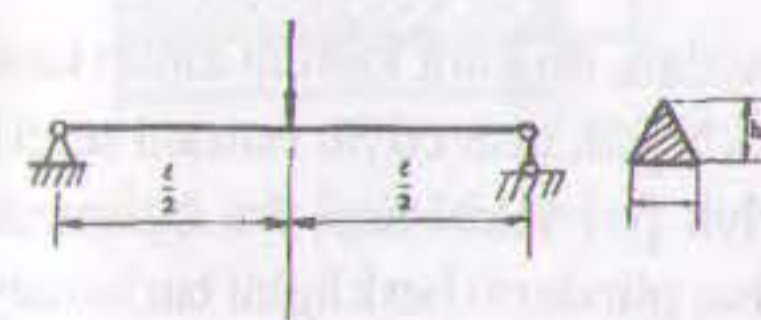
5.38-nji surat

5.38. Suratda görkezilişi ýaly, gönüburçly kese kesikli balka bir ýere jemlenen güýç bilen ýüklenen. Balkanyň ini hemişelik b deň, beýikligi bolsa çyzyk kanuny boýunça h_1 -den $h_2 = 3h_1$ -a çenli üýtgeýär. Egilmede balkanyň iň uly normal dartgynlylygyny kesgitlemeli.



5.39-nji surat

5.39. Uzynlygy ℓ we agramy $G = q\ell$ bolan bir jynsly göni balka gaty tekizlikde ýatyr. Balkanyň ujunda $M = q\ell^2/8$ moment goýlanda, onuň ýokary göterilýän böleginiň uzynlygyny kesgitlemeli.



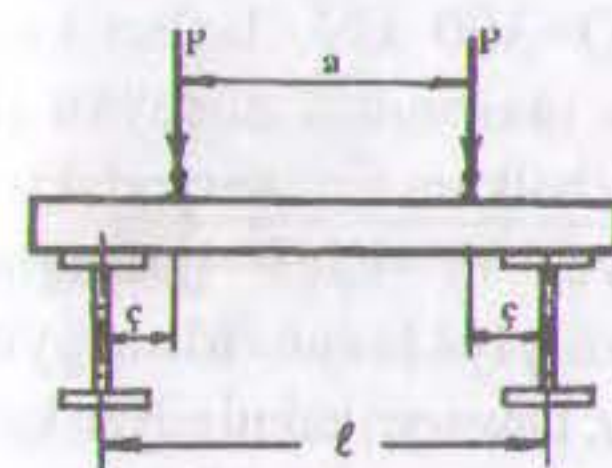
5.40-nji surat

5.40. Uzynlygy $\ell = 1$ m, beýikligi $h = 5$ sm, esasynyň ini $b = h$ bolan üçburç kesikli çöýün balkanyň rugsat edilyän ýüküni tapmaly (surata seret). Çöýnüň süýnmä berklik çägi $\sigma_b^s = 200$ MPa, gysylma berklik

çägi $\sigma_g^s = 1000$ MPa, berklik ätiýaçlygy $n = 3$ -e deň.

5.3. Egilmede galtaşma dartgynlylyk

5.41. Uzynlygy 2 m, ini 7,5 sm we beýikligi 15 sm bolan gönüburçly kese kesikli balkanyň gyralary şarnirli berkidilen. Çep diregden 75 sm uzaklykda ýerleşen we kese kesiginiň bitarap okundan 5 sm ýokarda durýan nokadyň normal we galtaşma dartgynlylyklaryny kesgitlemeli. Balka direg aralygynyň ortasynda goýlan bir ýere jemlenen 4 kN güýç bilen ýüklenen.



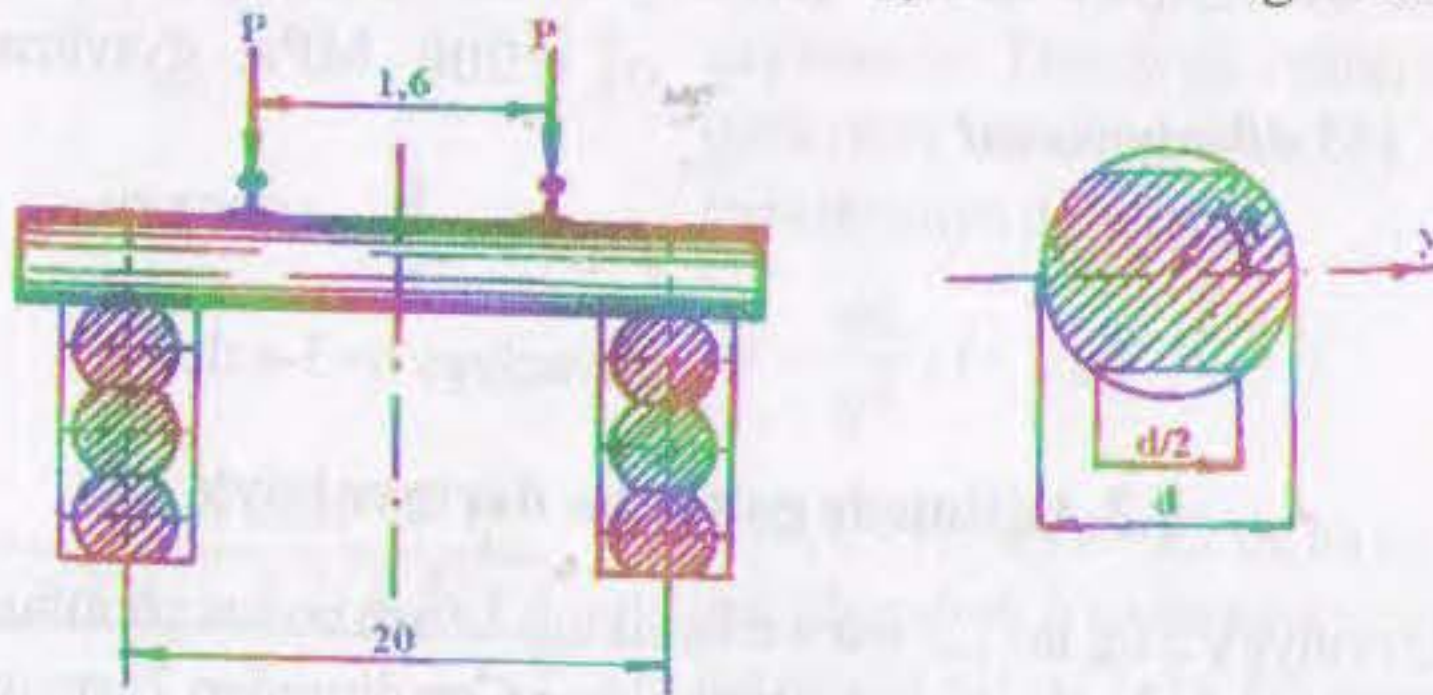
5.42-nji surat

5.42. Taraplary $\frac{h}{b} = \frac{4}{3}$ gatnaşykda bolan agaç köpri pürsüň gönüburçly kese kesiginiň ölçegini saýlamaly (surata seret). Pürse rugsat edilyän dartgynlylyklar: egilmede süýnme we gysylma $[\sigma] = 1 \text{ kN/sm}^2$, egilmede owranma $[\tau] = 0,25 \text{ kN/sm}^2$. Pürsüň direg aralygy $\ell = 2$ m, relsiň okunyň arasyndaky uzaklyk $a = 1,6$ m. Relsiň üstünden hereket edýän düzümiň tigriniň brusa geçirýän basyşy $P = 9,8$ kN.

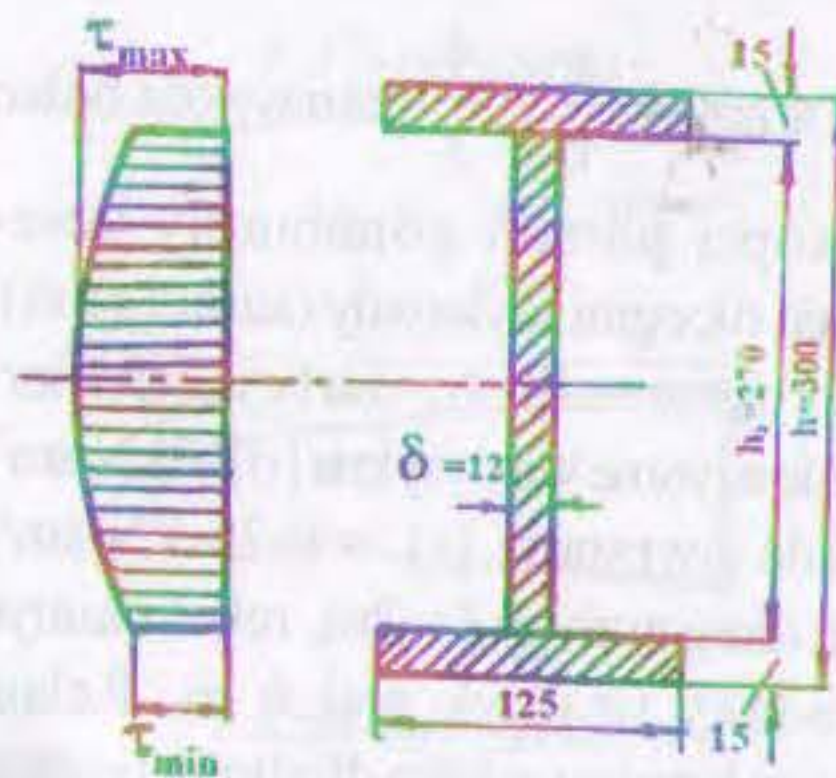
5.43. Diregde erkin ýatan direg aralygy 4 m-e deň 18-nji belgili iki tawraly balkanyň iň uly galtaşma dartgynlygyny kesgitlemeli. Balka 14 kN/sm^2 iň uly normal dartgynlyk döredýän direg aralygyň hemme ýerine goýlan endigan ýaýran güýç bilen ýüklenen.

5.44. Eger kese güýç $Q=60 \text{ kN}$ -e deň bolsa, daşky diametri $D=20 \text{ sm}$ we içki diametri $d=18 \text{ sm}$ bolan tegelek turbanyň egilmede iň uly galtaşma dartgynlygyny ululygyny kesgitlemeli.

5.45. Diametri $d=25 \text{ sm}$ bolan togalak agaçdan, iki kant kesilip alnan kese köpri pürslerine parowozyň tigrinden $P=60 \text{ kN}$ ýük täsir edýär (surata seret). Eger egilmede rugsat edilýän dartgynlyk $[\sigma]=1 \text{ kN/sm}^2$ we egilmede owranma dartgynlyk $[\tau]=0.2 \text{ kN/sm}^2$ bolsa, pürsleriň berkligini barlamaly.

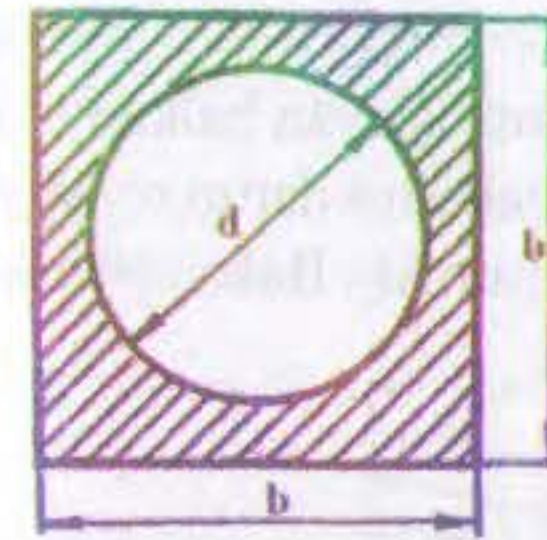


5.45-nji surat



5.46-njy surat

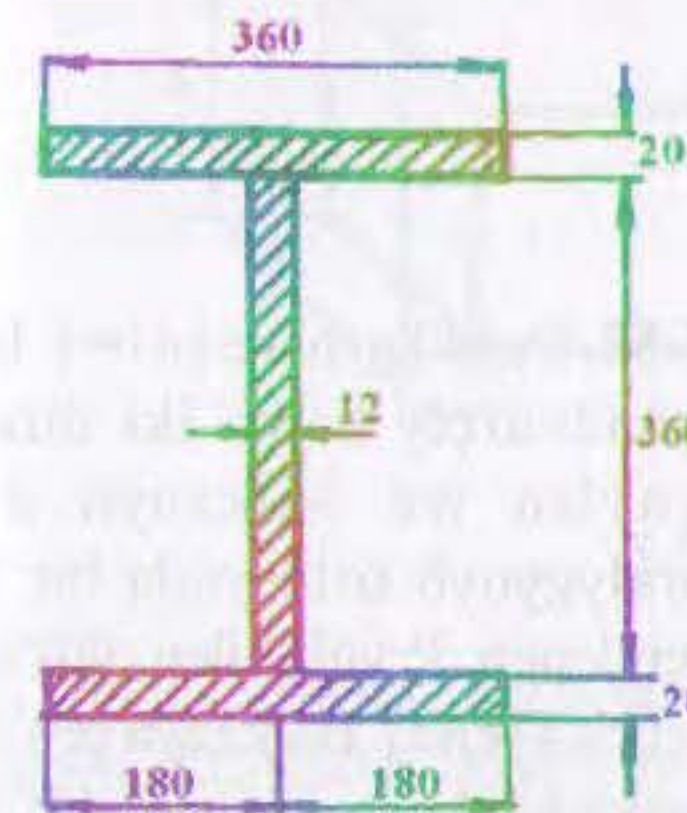
5.46. $Q=300 \text{ kN}$ bolan kese güýjüň täsirinden döredýän iki tawraly balkanyň diwaryndaky iň uly we iň kiçi galtaşma dartgynlyklaryň ululygyny tapmaly. Diwaryň kabul edýän kese güýjüni tapmaly. Balkanyň suratdaky kese kesiginiň ölçegleri mm-de görkezilen.



5.47-nji surat

5.47. Iki diregde erkin ýatan turba kesikli çöýün balka, diregden $a=0,7 \text{ m}$ aralykda goýlan iki deň simmetriýaly ýerleşen $P=60 \text{ kN}$ güýç bilen ýüklenen. Eger kesigiň ölçegleri $b=24 \text{ sm}$ we $d=20 \text{ sm}$, direg aralygy $\ell=3 \text{ m}$ (surata seret) bolsa, balkanyň howply kesigindäki iň uly normal we galtaşma dartgynlyklaryň ululyklaryny tapmaly.

5.48. Ululygy $Q=60 \text{ kN}$ bolan wertikal kese güýjüň täsirinden gönüburçly turba görnüşli balkanyň diwarynda ýüze çykýan iň uly galtaşma dartgynlygyny ululygyny kesgitlemeli. Kesigiň haýsy diwarynda galtaşma dartgynlygy uly bolýar? Kesigiň beýikligi we ini boýunça galtaşma dartgynlygyny ýaýraýşynyň epýuryny gurmaly.

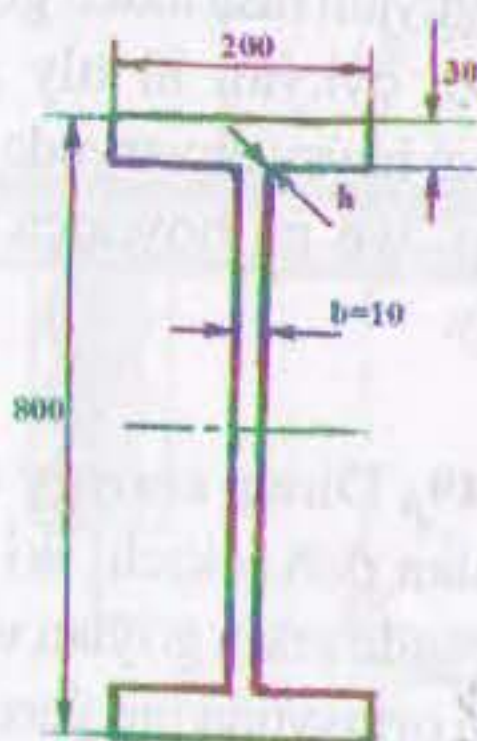


5.49-njy surat

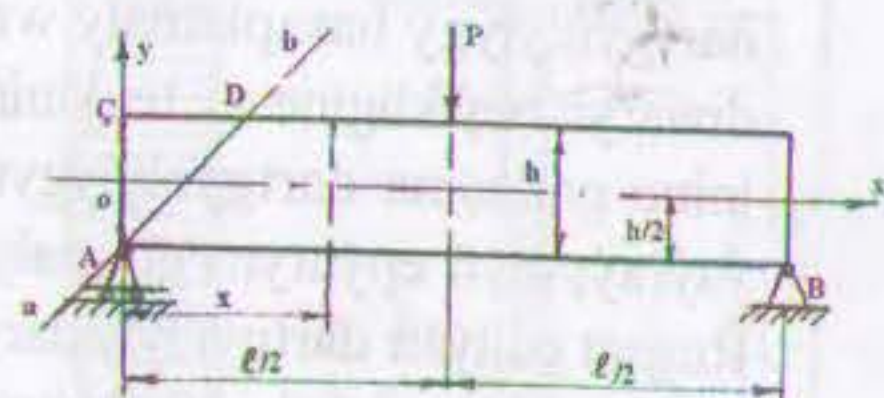
5.49. Direg aralygy $\ell=3 \text{ sm}$ bolan deň tekjeli iki tawra iki diregde erkin goýlan we prolyotyň ortasynda bir ýere jemlenen P güýç bilen ýüklenen. Normal dartgynlyk boýunça berklik şertinden balkanyň yük göterijiligini kesgitlemeli. Iň uly galtaşma dartgynlygy hasaplamaly we diwaryň beýikligine we tekjaniň inine galtaşma dartgynlygyny ýaýraýşynyň epýuryny gurmaly. Rugsat edilýän dartgynlyklary $[\sigma]=16 \text{ kN/sm}^2$, $[\tau]=10 \text{ kN/sm}^2$ deň diýip kabul etmeli.



5.50-nji surat



5.51-nji surat



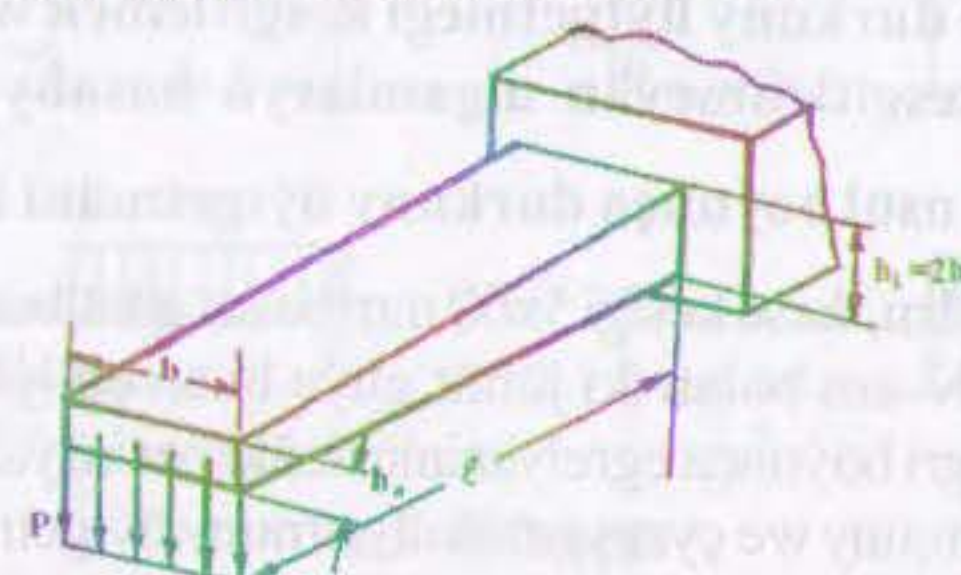
5.52-nji surat

5.50. Egilmä işleýän balkanyň kese kesiginde galtaşma dartgynlylygyň τ_{xy} epýuryny gurmaly. Balkanyň kesigi – romb.

5.51. Kebşirlenen iki tawraly balkanyň tigininiň galyňlygyny kesgitlemeli. Balkanyň kesigindeki kese güýç $Q=300$ kN. Kebşirleme tiginine rugsat edilýän dartgynlylyk $[\tau] = 50$ Mpa.

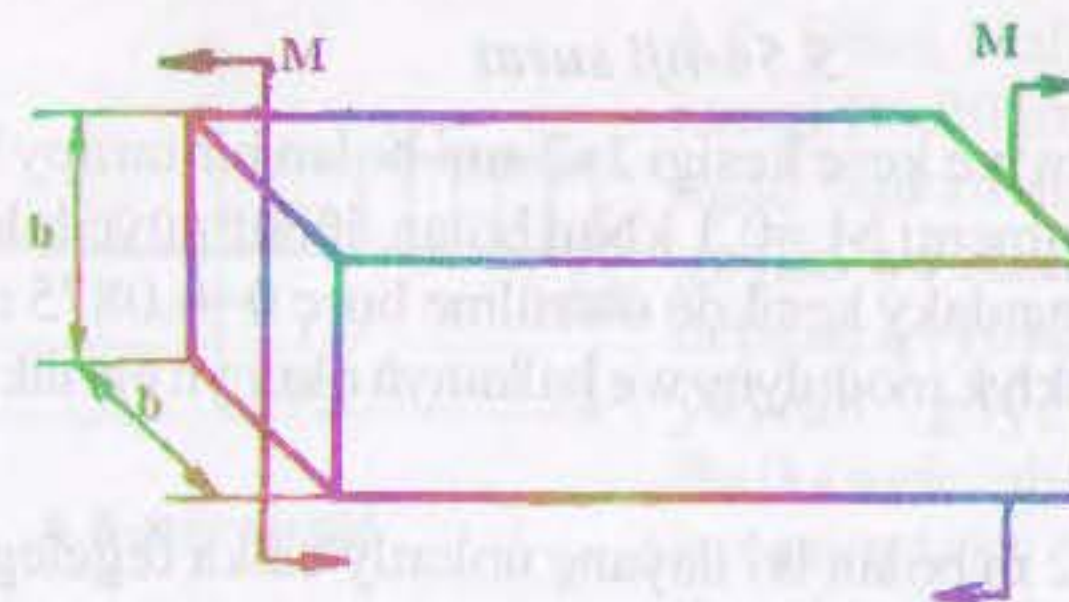
5.52. Beýikligi h we ini $b=1$ bolan gönüburçly balka iki deregde goýlan we balkanyň dereg aralygynyň ortasynda bir ýere jemlenen P ýük bilen ýüklenen (surata seret). Balkanyň çep dereg nokadyndan x okuna 45° burç boýunça geçirilen $a-b$ kesikdäki normal we galtaşma dartgynlylyklaryň epýurlaryny gurmaly.

5.53. Üýtgeýän galyňlygy h bolan pürsüň kese kesiginde galtaşma dartgynlylygynyň ýaýraýş kanunyny kesgitlemeli.



5.53-nji surat

5.54. Rezinden edilen gönüburçly kesikli pürsüň üstüne süýnmeýän ýuka lenta ýelmenen. Eger synagda lentanyň üzülmä güýji P -e deň bolsa, tekiz kesik çaklamasy esasynda pürsi eýgän momentiniň ululygyny kesgitlemeli. Lentanyň galyňlygyny h beýiklige görä ujypsyz diýip hasap etmeli.



5.54-nji surat

5.55. Dereg aralygy $\ell=4$ m bolan iki konsolly balka suratda görkezilişi ýaly ýüklenen. Konsolyň uzynlygy $a=0,5$ m. Eger C nokatda galtaşma dartgynlylyk $\tau_c = 1$ kN/sm² bolsa, balkanyň howply kesiginde iň uly normal we galtaşma dartgynlylyklaryň ululyklaryny kesgitlemeli. Kesigiň ölçegleri mm-de görkezilen.

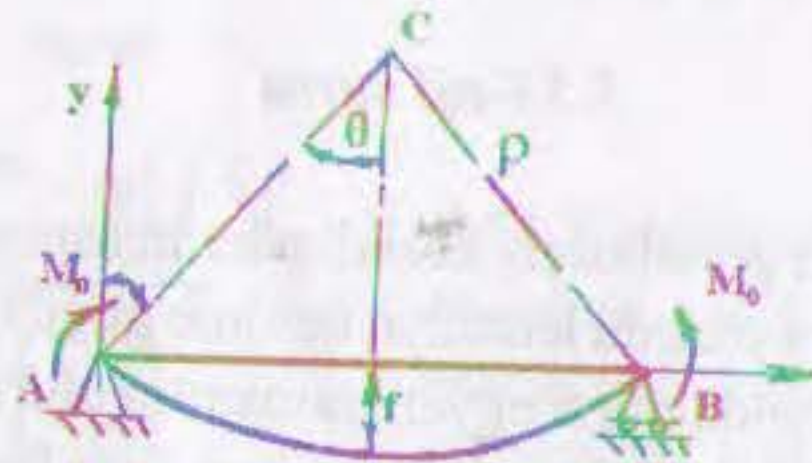
5.56. Deňýanly üçburçluk şekili bolan balkanyň kesiginiň beýikligine galtaşma dartgynlylygyň wertikal düzüjisiniň ýaýraýşynyň epýuryny gurmaly. Kese güýç Oz okuň boýy boýunça ugrukdyrylan.

VI bap

Egilmede durkuny üýtgetmegi kesgitlemek we statiki kesgitlenmeýän ulgamlaryň hasaby

6.1. Analitik usul boýunça durkuny üýtgetmäni kesgitlemek

6.1. Uzynlygy $\ell = 1\text{ m}$, kese kesigi $5 \times 60\text{ mm}$ bolan gönüburçly polat çyzgyç, momenti $M_0 = 1\text{ kN}\cdot\text{sm}$ bolan iki jübüt güýç bilen egilýär (surata seret). Çyzgyjyň haýsy egri boýunça egrelýäniniň deňlemesini ýazmaly we kesigiň iň uly öwrülme burçuny we çyzgyjyň iň uly ornuny üýtgetmesini tapmaly.



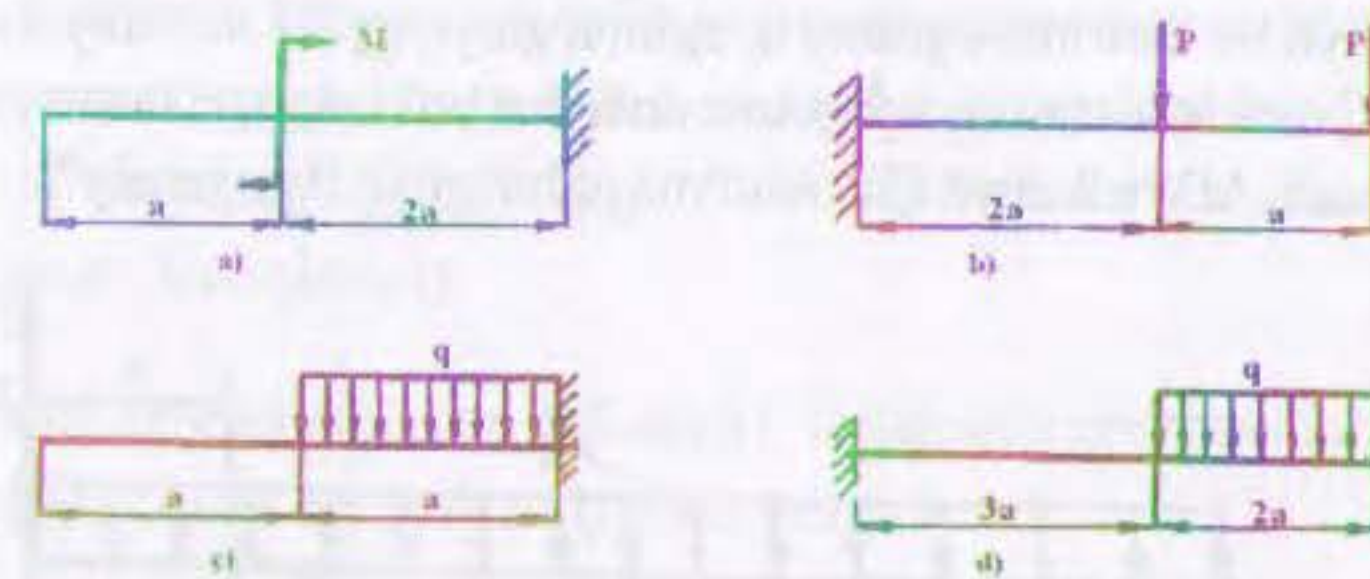
5.54-nji surat

6.2. Uzynlygy $\ell = 1\text{ m}$ we kese kesigi $2 \times 2\text{ sm}^2$ bolan bir tarapy berkidilen balkanyň ujunda momenti $M_0 = 0,1\text{ kNm}$ bolan jübüt güýç bilen egilýär. Eger balkanyň ahyryndaky kesikde öwrülme burç $\theta = 0,0875\text{ rad.}$ bolsa, materialyň maýyşgaklyk modulyny we balkanyň okunyň egrilik radiusyny tapmaly.

✓ 6.3. Direg aralygy 2 m bolan iki daýanç nokatly balka tegelegiň dugasy boýunça egrelýär. Direg aralygynyň ortasynda onuň ornuny üýtgetmesi $0,5\text{ sm}$ deň. $E = 2,1 \cdot 10^4\text{ kN/sm}^2$ we $I = 230\text{ sm}^4$ bahalarynda egme momentiň ululygyny we balkanyň egren okunyň egrelmesiniň radiusyny kesgitlemeli.

6.4. Togtaýjy güýjüň $T = 240\text{ kN}$ täsirinden köpri sütüniň kerpiç örüminiň materialynyň maýyşgaklyk modulyny kesgitlemek üçin onuň yokarky kesiginiň gorizonta ornuny üýtgetmesi ölçelýär we bu ululyk $8,75\text{ mm-e}$ deň bolýar. Eger binýadyň erneginden sütüniň beýikligi $h = 12\text{ m}$ bolsa, materialyň maýyşgaklyk modulyny kesgitlemeli. Ölçegleri suratda görkezilen.

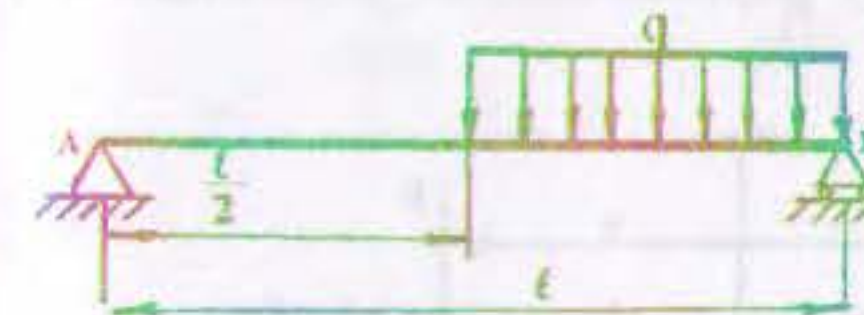
6.5. Maýyşgak çyzygyň differensial deňlemesini integrirlemek ýoly bilen suratdaky ýaly ýüklenen, bir tarapy berkidilen balkanyň erkin kesiginiň burç we çyzyk ornuny üýtgetmelerini tapmaly.



6.5-nji surat

6.6. Balkanyň ujundaky rugsat edilyän ornuny üýtgetme $[f] = \frac{\ell}{450}$ -den

köp bolmadyk ýagdaýynda, uzynlygy $\ell = 2\text{ m}$, bir tarapy berkidilen we hemme uzynlygyna endigan ýaýran güýç $q = 10\text{ kN/m}$ bilen ýüklenen balkanyň ikitawraly kesigini saýlamaly. Eger $[\sigma] = 14\text{ kN/sm}^2$ bolsa, balkanyň berkligini saýlanan iki tawra kanagatlandyryarmy?



6.6-nji surat

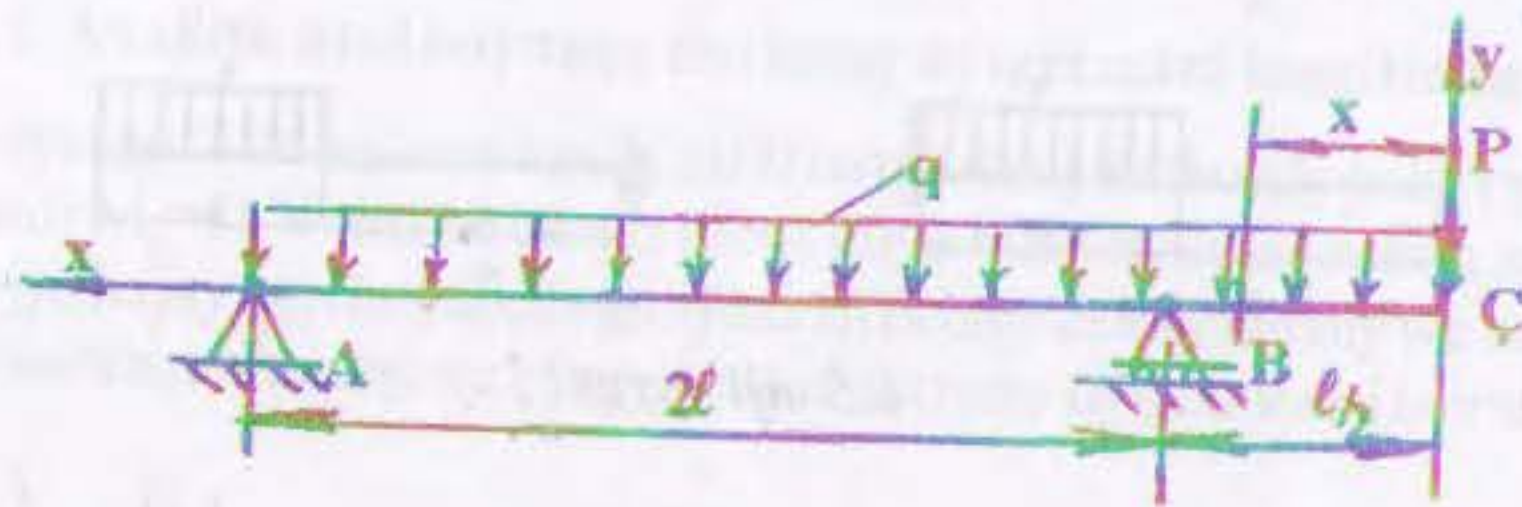
6.7. Direg aralygy $\ell = 4\text{ m}$, kese kesigi $18 \times 20\text{ sm}$ bolan gönüburçly agaç balkanyň soňy iki diregde goýlan we suratda görkezilişi ýaly depgini $q = 10\text{ kN/m}$ bolan endigan ýaýran güýç bilen ýüklenen. Balkanyň direg aralygynyň ortasyndaky egrelmäni we direglerdäki kesikleriň öwrülme burçlaryny tapmaly.

✓ 6.8. Sag diregi M moment bilen ýüklenen balkanyň iň uly egrelmesini kesgitlemeli we balkanyň direg aralygynyň ortasyndaky kesigiň egrelmesi bilen deňeşdirmeli.



6.8-nji surat

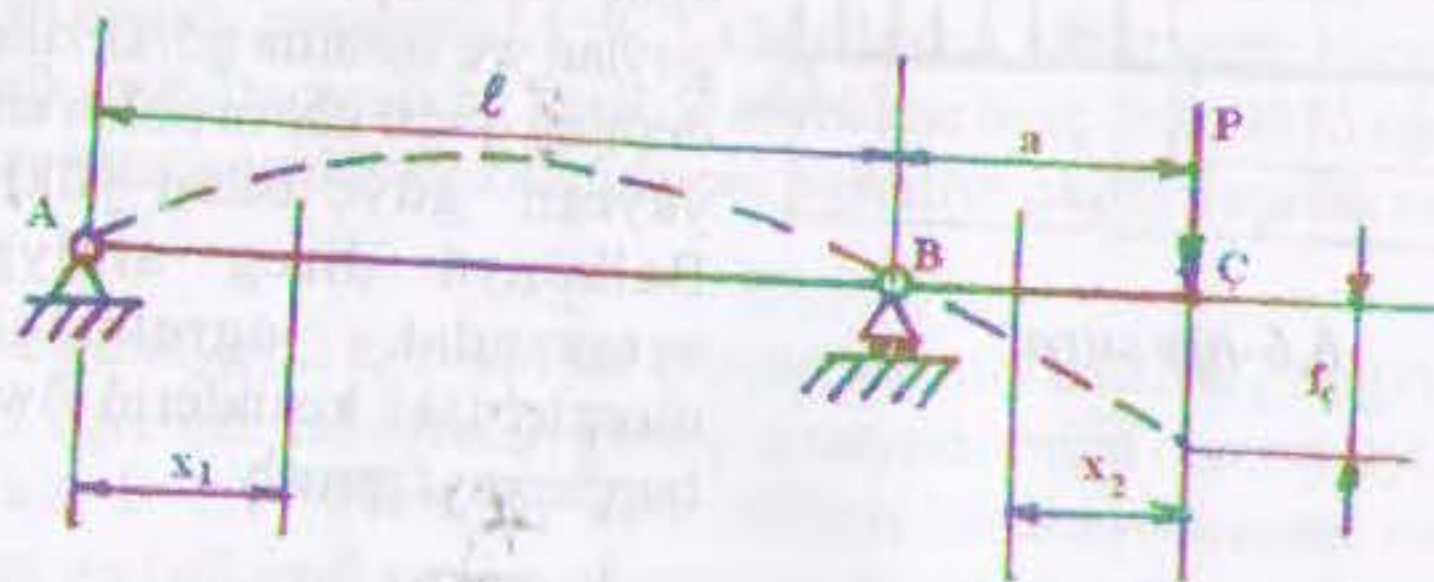
6.9. Balkanyň bir metriniň agramy q , egilmä gatylygy EI we uzynlygy 2ℓ -e deň bolsa, \dot{C} nokatda ornuny üýtgetme nola deň bolmak üçin hususy agramy bilen ýüklenen AB balkanyň \dot{C} nokadyna nähili güýç P goýmaly?



6.9-njy surat

6. 2. Energetiki usullar bilen sterženli ulgamlaryň durkuny üýtgetmegini kesgitlemek

6.10. Suratda şekillendirilen balkanyň egilmede durkunyň üýtgedilmeginiň potensial energiýasynyň aňlatmasyny peýdalanyp, erkin tarapyndaky egrelmesini kesgitlemeli.

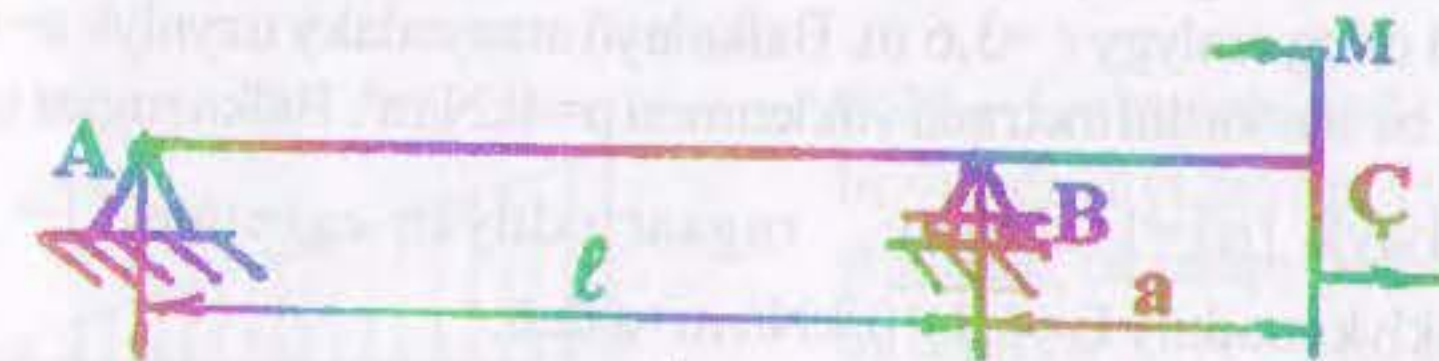


6.10-njy surat

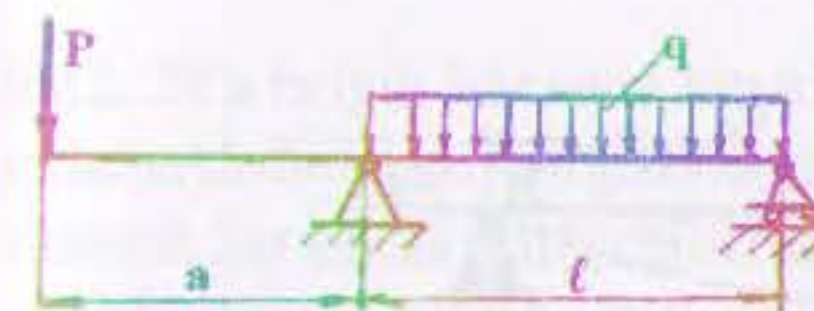
6.11. Diametri $d = 12$ sm bolan tegelek kesikli wal, $M_{cg} = 6$ kNm hemişelik moment bilen egilýär we $M_t = 8$ kNm moment bilen towlanýar. Walyň 1 metrinde durkuny üýtgetmäniň toplan potensial energiýasyny kesgitlemeli. Walyň materialynyň maýýşgaklyk modullary $E = 2,1 \cdot 10^4$ kN/sm², $G = 8,5 \cdot 10^3$ kN/sm².

6.12. Gönüburçly kese kesikli balka hemişelik egme moment bilen ýüklenen; iň uly normal dartgynlylygy σ deň, normal maýýşgaklyk moduly E , kese kesiginiň meýdany A , uzynlygy ℓ bolan balkanyň toplan potensial energiýasyny hasaplamaly.

6.13. Suratda şekillendirilen balkanyň \dot{C} kesiginiň egrelmesini we öwrülme burçuny Maxwell-Moruň usuly bilen kesgitlemeli.

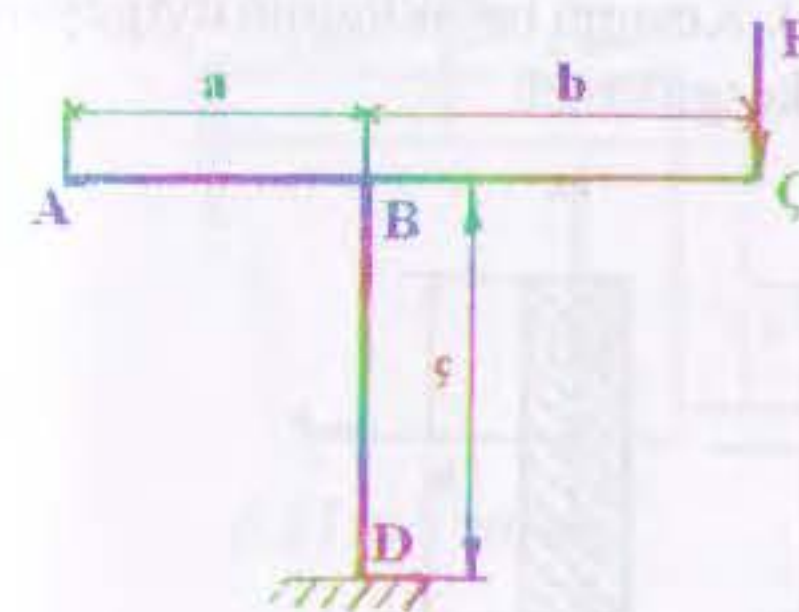


6.13-nji surat



6.14-nji surat

6.14. Suratda görkezilişi ýaly, ýüklenen polat balkanyň konsolynyň ahyryndaky kesikde Maxwell-Moruň usuly bilen egrelmesini we öwrülme burçuny kesgitlemeli. $P = 20$ kN, $q = 30$ kN/m, $\ell = 4$ m, $a = 1$ m, $I = 3500$ sm⁴.



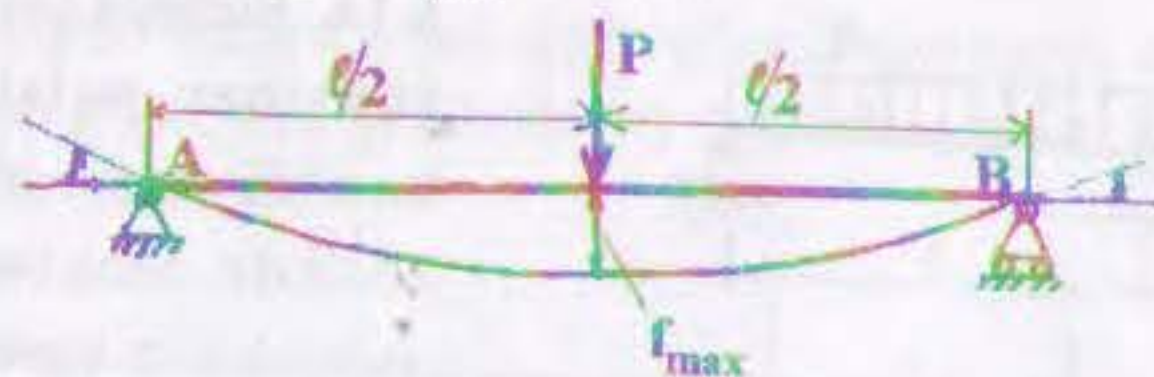
6.15-nji surat

6.15. Suratda şekillendirilen ABCD çarçuwanyň sag konsolynyň ahyrynda goýlan P ýüküň täsirinden çep konsolynyň ahyrynda ýerleşen A nokadyň egrelmesini Maxwell-Moruň usuly bilen kesgitlemeli.

6.16. Suwy akdyrmak üçin niýetlenen gorizontaly ýerleşen polat turba $l = 2,4$ m uzynlykda diwardan çykyp durýar. Turbanyň içki diametriniň daşkysyna bolan gatnaşygy $d:D=0,85$. Poladyň göwrüm agramy $\gamma_p = 78,5 \text{ kN/m}^3$ -a, suwuňky bolsa $\gamma_s = 10 \text{ kN/m}^3$ -a deň. Turbanyň materialynyň maýyşgaklyk moduly $E = 1,96 \cdot 10^4 \text{ kN/sm}^2$. Turbanyň erkin tarapyna rugsat edilýän egrelme $[f] = 0,003l$. Turbanyň içki we daşky diametrlerini kesgitlemeli.

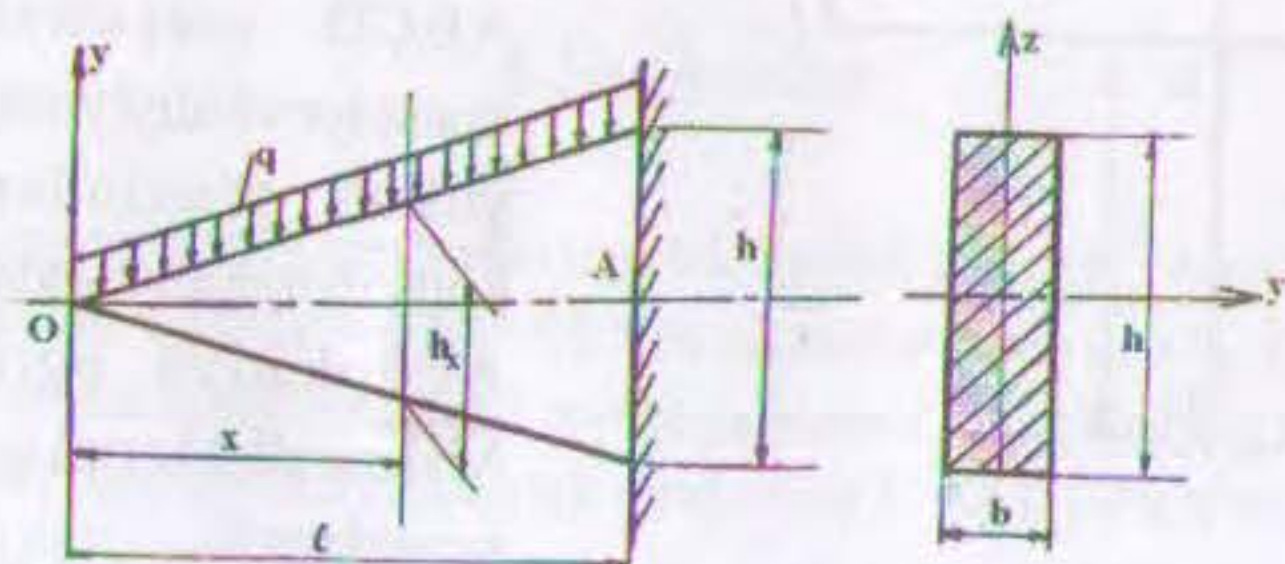
✓ 6.17. Berklik we gatylyk şertlerinden agaç örtgüli balkany hasaplamaly. Balkanyň direg aralygy $l = 3,6$ m. Balkanyň arasyndaky uzynlyk $a = 1,2$ m, örtügiň bir inedördül metriniň ýüklenmesi $p = 4 \text{ kN/m}^2$. Balka rugsat edilýän dartgynlylyk $[\sigma] = 1 \text{ kN/sm}^2$, rugsat edilýän egrelme $[f] = \frac{1}{350}l$ maýyşgaklyk moduly $E = 1,1 \cdot 10^3 \text{ kN/sm}^2$ -a deň.

6.18. Uzynlygy l we hemişelik beýikligi ($h = \text{const}$) hem üýtgeýän ini bolan iki daýanç nokatly balka P güýç bilen ýüklenen (surata seret). Maýyşgaklyk moduly E deň bolsa, θ_{\max} we f_{\max} tapmaly.

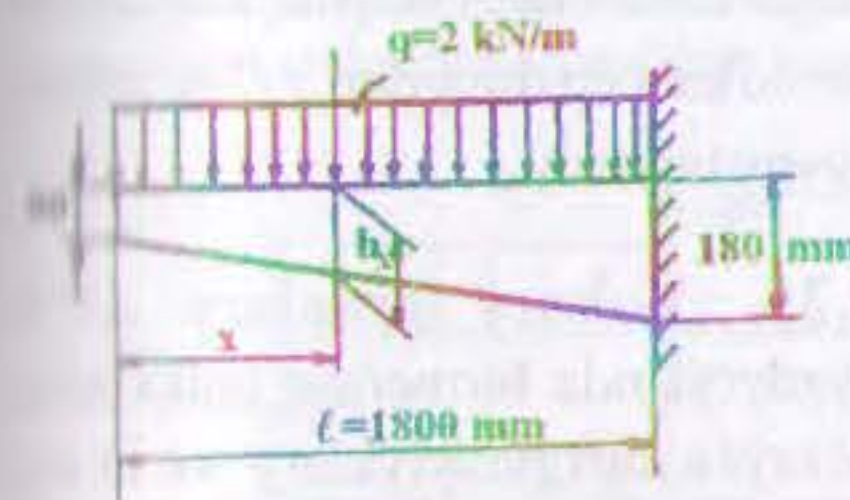


6.18-nji surat

6.19. Uzynlygy l we hemişelik ini bolan gönüburçly kesikli, hemme kesiklerinde deň garşylyk görkezýän bir tarapy berkidilen balka endigan ýaýran ýük bilen ýüklenen (surata seret). Kesigiň beýikliginiň üýtgeýän kanunyny we balkanyň iň uly egrelmesini kesgitlemeli.

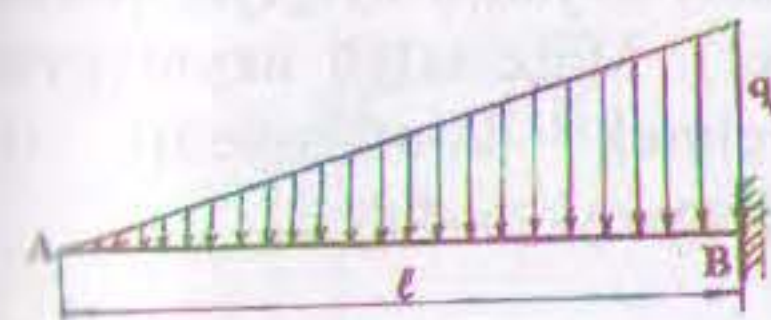


6.19-nji surat



6.20-nji surat

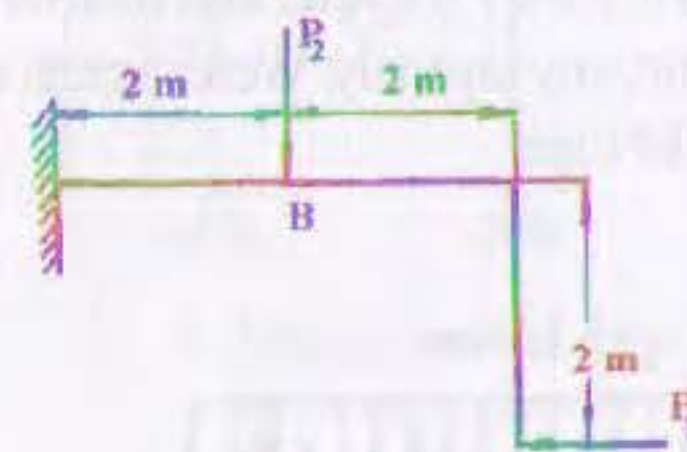
6.20. Suratda şekillendirilen gönüburçly kesikli balkanyň iň uly egrelmesini kesgitlemeli. Pürsün materialy sosna, sosnanyň maýyşgaklyk moduly $E = 10^3 \text{ kN/sm}^2$. Kesigiň ini $b = 60 \text{ mm}$.



6.21-nji surat

6.21. Üçburçlugyň kanuny boýunça üýtgeýän ýük bilen ýüklenen, bir tarapy berkidilen AB balkanyň A nokadynyň egrelmesiniň we öwrülme burçunyň ululygyny kesgitlemeli (surata seret).

6.22. 20 a belgili iki tawra kesikli, direg aralygy 6 m-e deň balkanyň bir tarapynyň diregi şarnirli gozganmaýan, beýleki tarapy diametri 10 sm bolan silindrik hyr şekilli pružin bilen saklanýar. Pružiniň sarymynyň sany $n = 10$, siminiň diametri 2 sm. Balka we pružin polatdan ýasalan, materialyň maýyşgaklyk modullary $E = 2 \cdot 10^4 \text{ kN/sm}^2$ -a we $G = 8 \cdot 10^3 \text{ kN/sm}^2$ -a deň. Balkanyň ortasynda goýlan wertikal güýjüň täsirinden toplanan potensial energiýany kesgitlemeli.



6.21-nji surat

✓ 6.23. Suratda görkezilişi ýaly, döwür oky bolan balka $P_1 = 10 \text{ kN}$ we $P_2 = 20 \text{ kN}$ güýçler bilen ýüklenen. Kesigiň inersiýa momenti 3000 sm^4 -e deň we balkanyň hemme uzynlygyna hemişelik. Maýyşgaklyk moduly $E = 2 \cdot 10^4 \text{ kN/sm}^2$ -a deň. P_1 güýjüň ugry boýunça A kesigiň ornuny üýtgetmesini we B kesigiň öwrülme burçuny kesgitlemeli.

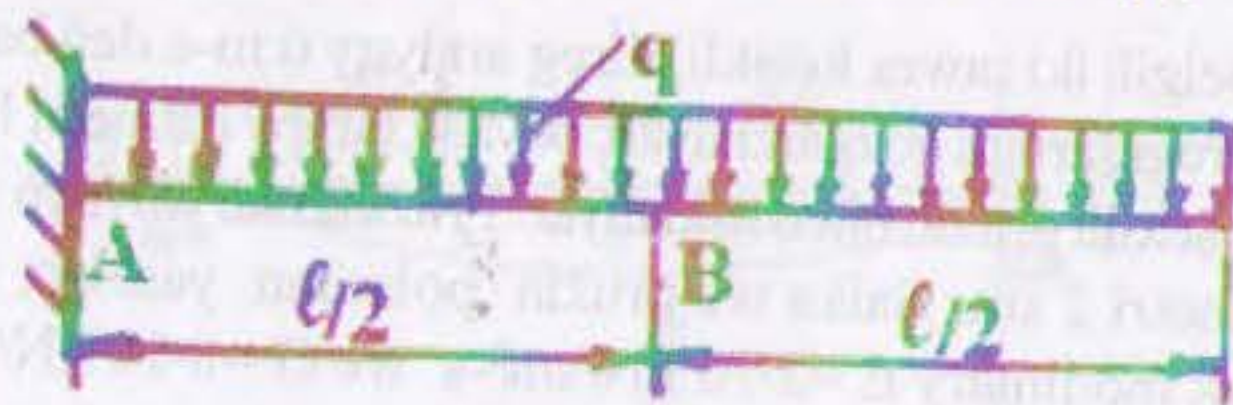
6.24. İki dayanç nokatda ýatan balka, sagat diliniň ugry boýunça aýlanyan iki jübüt güýçler bilen egilýär. Eger epme nokat çep diregden $\ell/3$ aralykda ýerleşen bolsa, bu momentleriň gatnaşygyny tapmaly.



6.25-nji surat

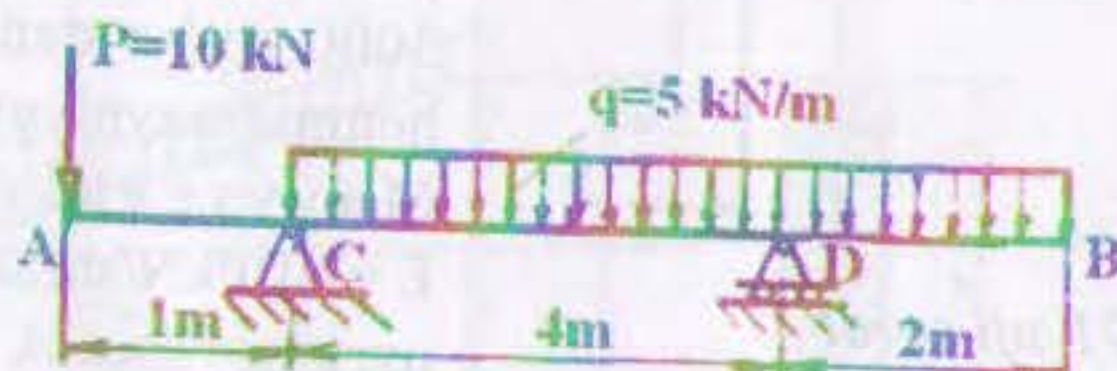
6.25. Ýokary granlary $\Delta t^\circ S$ gyzdyrylanda birmeňzeş balkalarda döreýän dartgynlylyklary we in uly egrelmeleri deňeşdirmeli. Balkanyň galyňlygyna temperatura çyzyk kanuny boýunça üýtgeýär (surata seret). Materialyň uzynlygyna giňelmek koeffisiýenti α , maýyşgaklyk moduly E.

6.26. Suratda görkezilen endigan ýaýran ýük bilen ýüklenen balkanyň B kesiginiň öwrülme burçuny kesgitlemeli. Wereşaginiň usulyny ulanmaly.



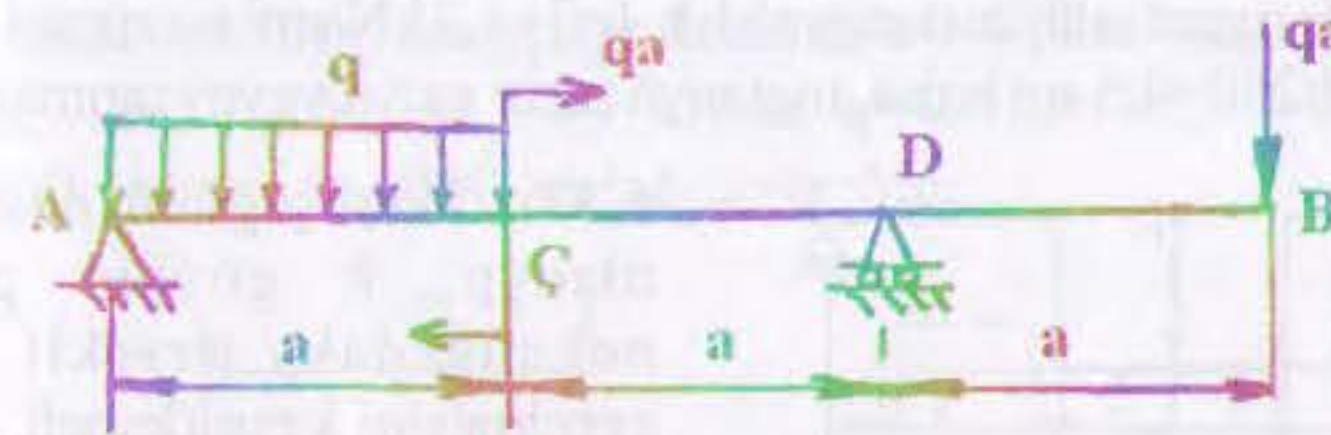
6.26-nji surat

6.27. Suratda görkezilen AB balkanyň q we P güýçleriniň täsirinden çep konsolyň ahyryndaky kesigiň öwrülme burçuny tapmaly. Wereşaginiň usulyny ulanmaly. Balkanyň gatylygy $EI = 4 \cdot 10^7 \text{ kN/sm}^2$.

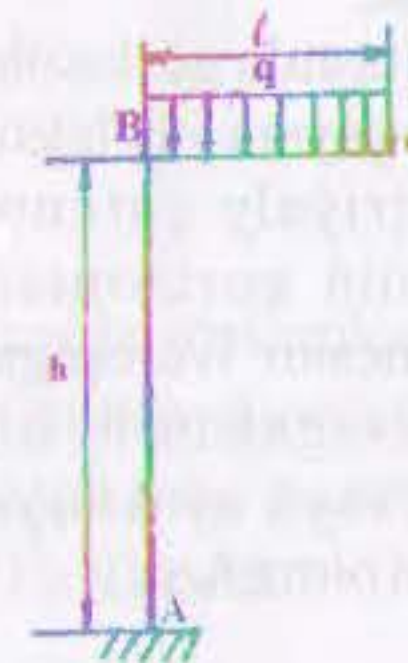


6.27-nji surat

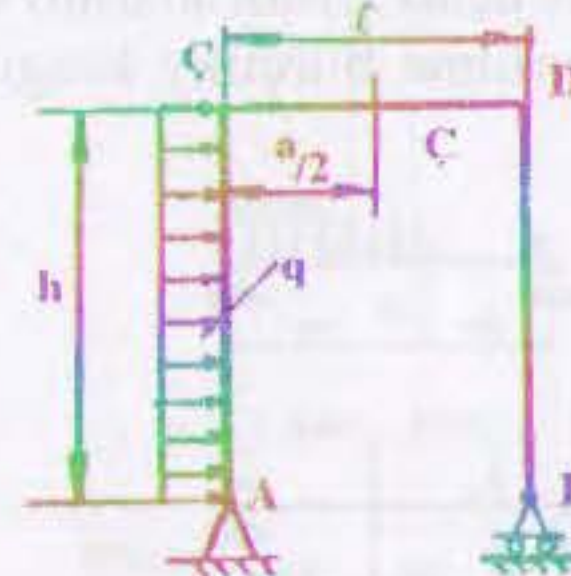
6.28. Wereşaginiň usulyny ulanyp, balkanyň B nokadynyň egrelmesini we diregdäki A nokadyny öwrülme burçuny kesgitlemeli.



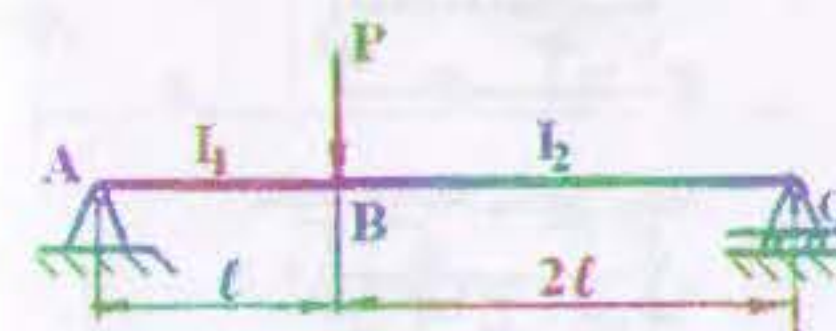
6.28-nji surat



6.29-nji surat



6.30-nji surat



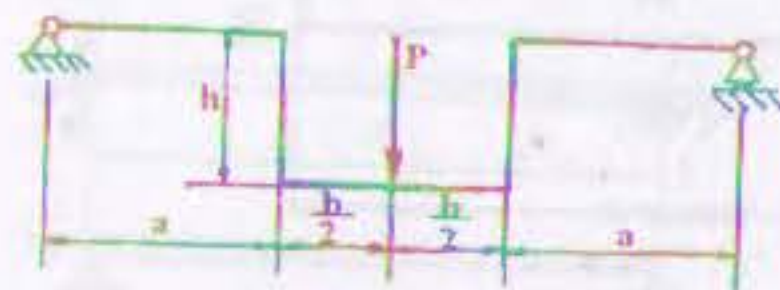
6.31-nji surat

6.29. Suratda şekillendirilen çarçuwanyň Wereşaginiň düzgünini ulanyp, erkin tarapyndaky wertikal ornuny üýtgetmesini kesgitlemeli.

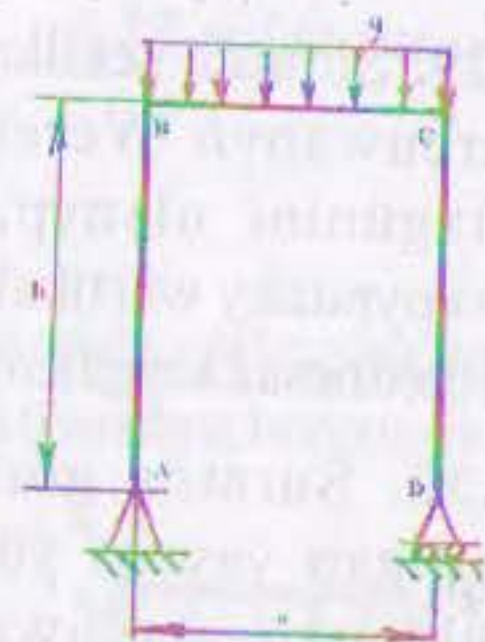
6.30. Suratda görkezilen endigan ýaýran ýük bilen ýüklenen çarçuwanyň B diregindäki gorizonta ornuny üýtgetmesini kesgitlemeli. Şonuň ýaly-da Wereşaginiň usulyny ulanyp, C kesigiň wertikal ornuny üýtgetmesini, D kesigiň öwrülme burçuny kesgitlemeli.

6.31. Suratda şekillendirilen polat balkanyň P güýjüň goýlan ýerinde, AB we BC bölekleriň inersiýa momentleriniň I_1 we I_2 haýsy gatnaşygynda in uly ornuny üýtgetmesi bolar? Eger $P = 6,25 \text{ kN}$, $\ell = 0,24 \text{ m}$, $I_1 = 16 \text{ sm}^4$ bolsa bu ornuny üýtgetmäni tapmaly.

6.32. Direg aralygy $\ell=1,25$ m bolan tagta pol metal balkanyň üstünde goýlan we $P=8,5\text{ kN/m}^2$ ýük bilen ýüklenen (poluň agramy + peýdaly ýük). Eger egilmede rugsat edilýän dartgynlyk $[\sigma]=1,2\text{ kN/sm}^2$ we rugsat edilýän egrelme $[f]=1/250=0,5$ sm bolsa, tagtanyň zerur galyňlygyny tapmaly.

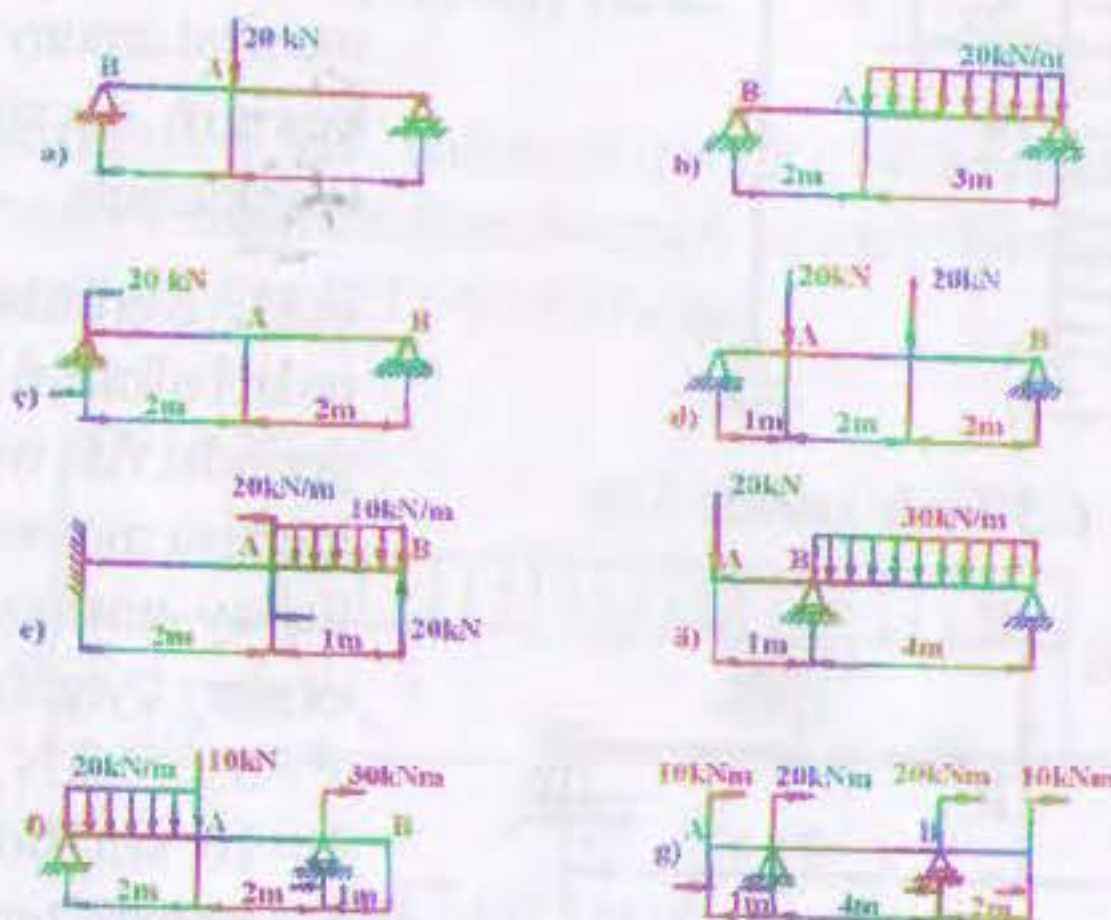


6.33-nji surat



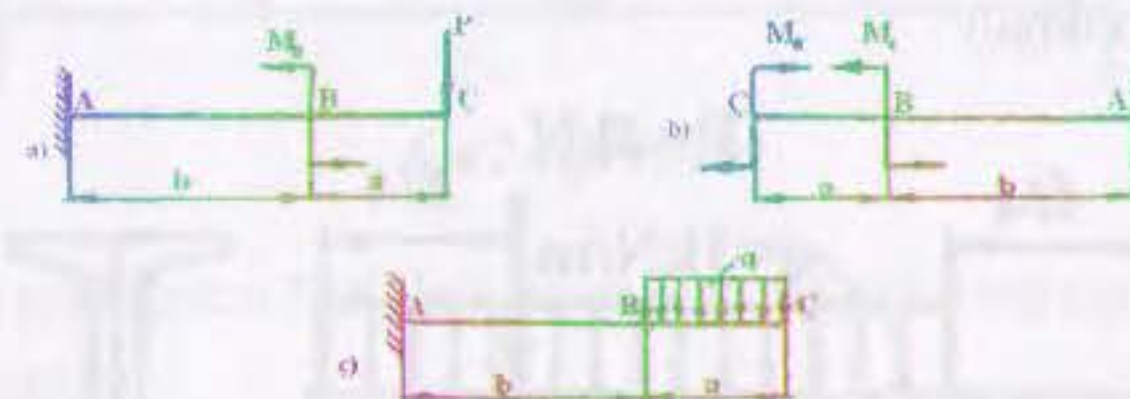
6.34-nji surat

6.35. Çyzgyda getirilen balkalaryň shemalary üçin O. Moruň usuly bilen A nokadynyň egrelmesini we B kesigiň öwrülme burçuny kesgitlemeli $E=2\cdot 10^4\text{ kN/sm}^2$.



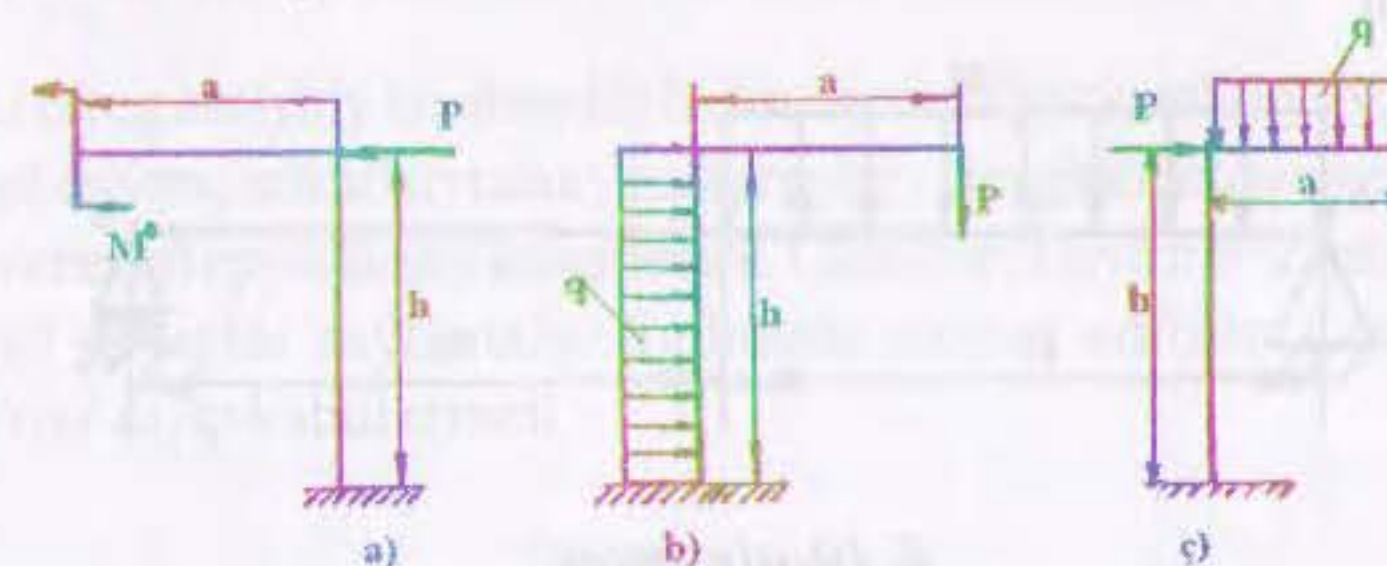
6.35-nji surat

6.36. Shemalarda görkezilen bir tarapy berkidilen we dürli güýçler bilen ýüklenen hemişelik kesikli ABC balkanyň Ç kesiginiň Simpson-Karnouhowyň usulyny ulanyp egrelmesini we öwrülme burçuny kesgitlemeli. Berlen: $P=20\text{ kN}$; $M_0=40\text{ kNm}$; $q=20\text{ kN/m}$; $b=3\text{ m}$, $a=2\text{ m}$; $E=2\cdot 10^4\text{ kN/sm}^2$; $I=4800\text{ sm}^4$; $\ell=a+b=5\text{ m}$.

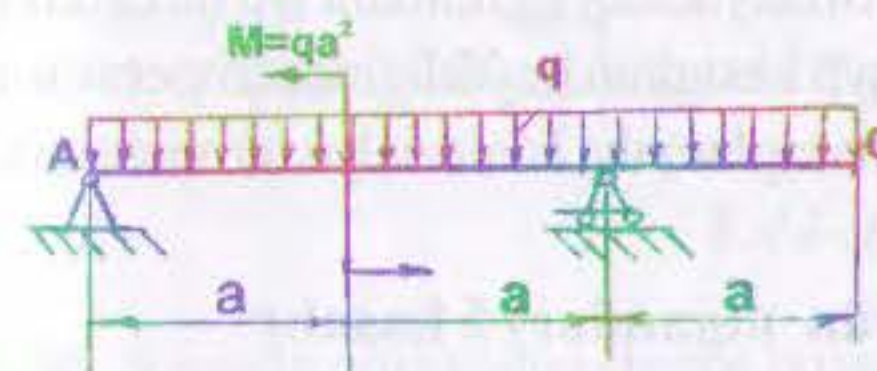


6.36-nji surat

6.37. Suratda görkezilen shemalar boýunça ýüklenen hemişelik kesikli polat çarçuwanyň erkin kesigindäki wertikal f , gorizont Δ ornuny üýtgetmelerini we öwrülme burçuny θ matrisa usuly bilen kesgitlemeli ($E=2\cdot 10^4\text{ kN/sm}^2$).



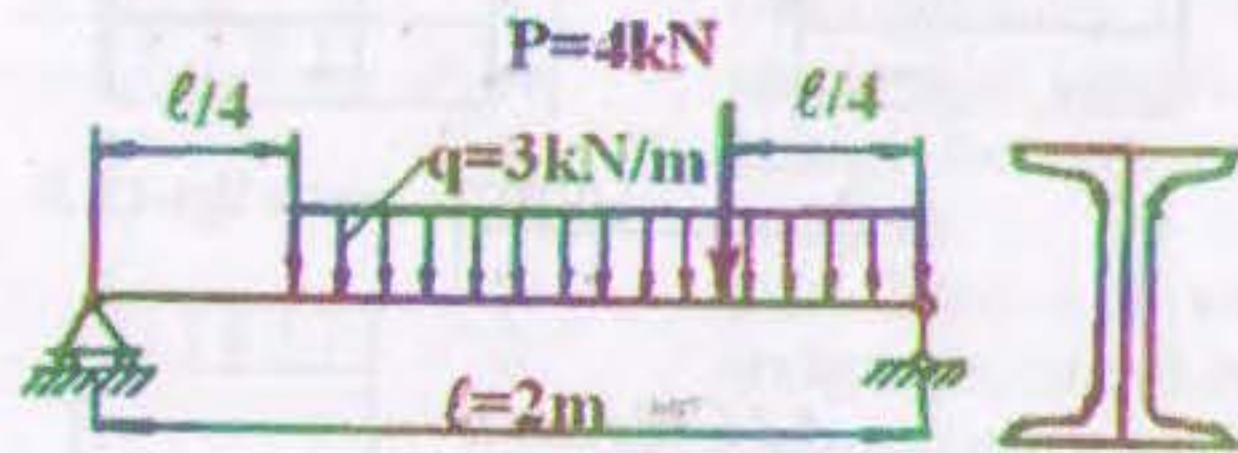
6.37-nji surat



6.38-nji surat

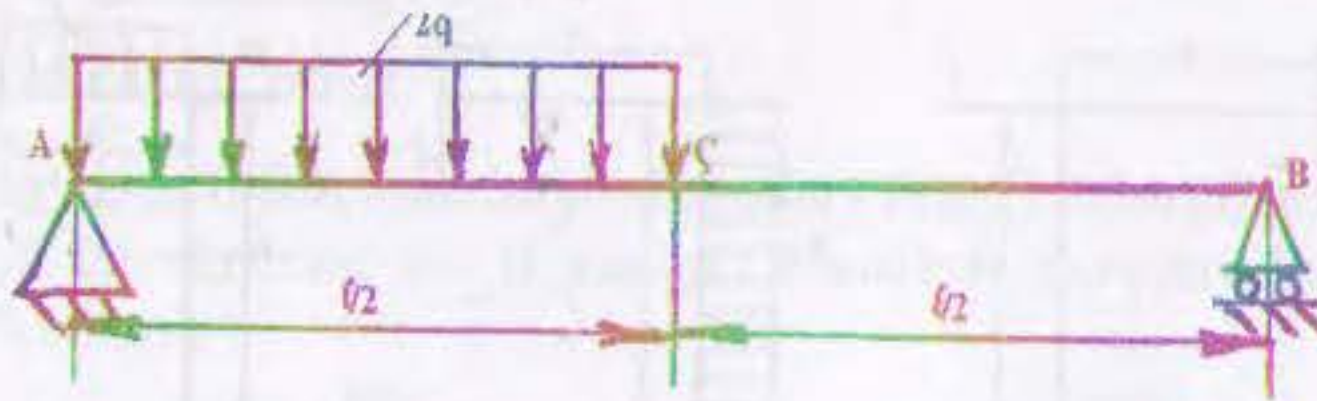
6.38. Matrisa usulyny ulanyp, suratda görkezilen balkanyň Ç nokadynyň egrelmesini we öwrülme burçuny kesgitlemeli.

6.39. 16-njy belgili Pr. 106 tipli iki şwellerden (bir şwelleriň inersiýa momenti $I=51,98 \text{ sm}^4$) ybarat bolan dýural balka, suratda görkezilişi ýaly, ýük bilen ýüklenen. Matrisa usulyny ulanyp, balkanyň ortasyndaky egrelmäni kesgitlemeli. $E = 7,5 \cdot 10^3 \text{ kN/sm}^2$. Balkanyň ortasyndaky egrelmesi $\ell/200$ -den ýokary geçmedik ýagdaýynda, balkanyň kesiginiň inersiýa momenti nähili bolmaly?



6.39-njy surat

6.40. Uzynlygy ℓ , depgini $2q$ bolan endigan ýaýran ýük bilen çep direginden ortasyna çenli ýüklenen iki daýanç nokatly balkanyň ortasyndaky egrelmäni kesgitlemeli.

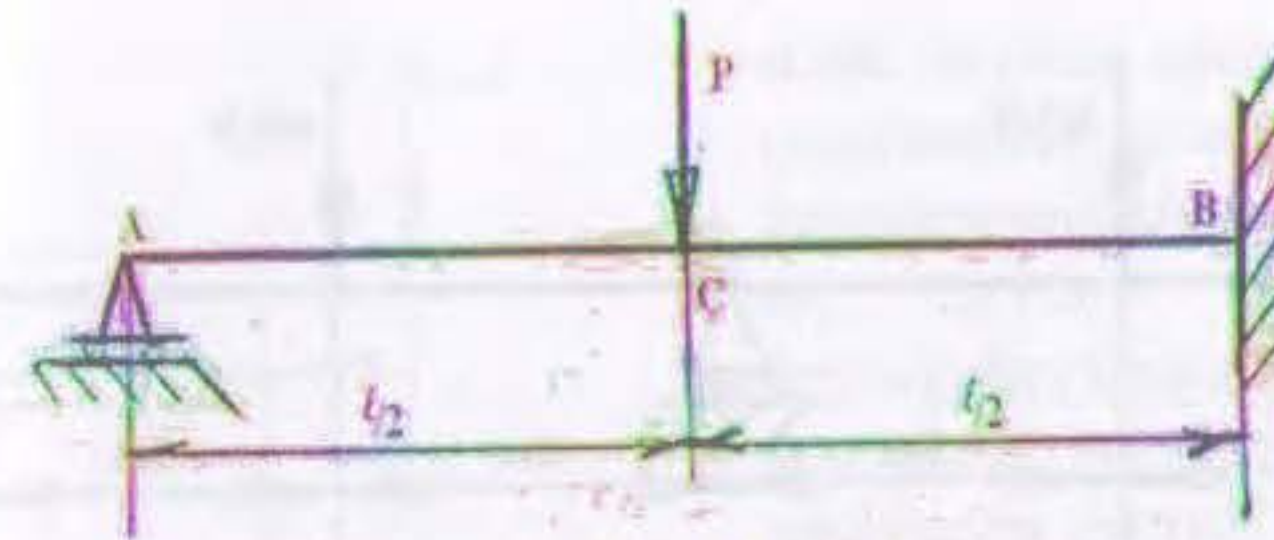


6.40-njy surat

6.41. Uzynlygy ℓ deň bolan hemişelik kesikli yönekeý balkanyň $\Delta t^\circ \text{S}$ bilen aşagy gyzdyrylanda, dereg aralygynyň ortasyndaky egrelmäni we diregdäki öwrülme burçuny kesgitlemeli. Balkanyň kesiginiň beýikligine temperatura çyzyk kanuny boýunça üýtgeýär diýip hasaplamaly. Materialyň temperatura giňelmek koeffisiýenti α deň.

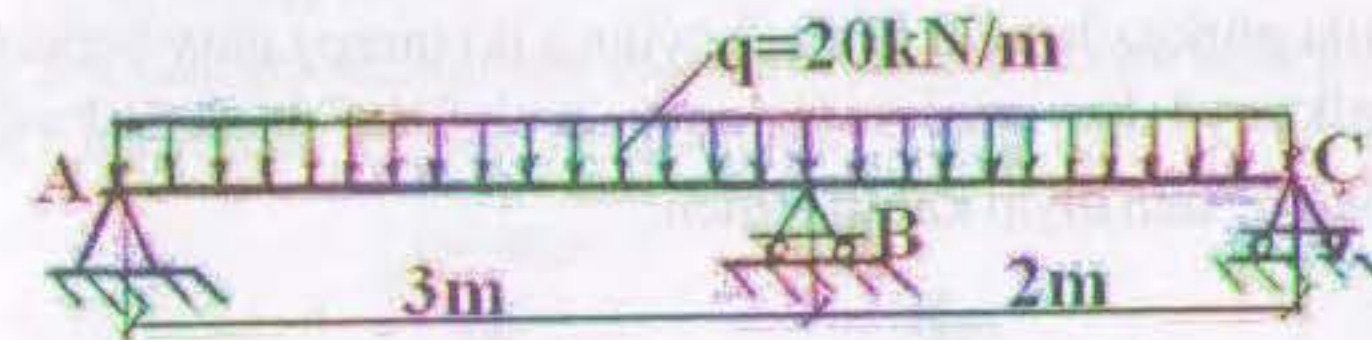
6.3. Statiki kesgitlenmeýän ulgamlaryň hasaby

6.42. AÇB balkanyň B gyrasy gaty we A gyrasy gozganýan şarnirli dereg bilen berkidilen. Balkanyň ortasyna $P=40 \text{ kN}$ güýç goýlan, kese güýjüniň we egme momentiniň epýurlaryny gurmaly.



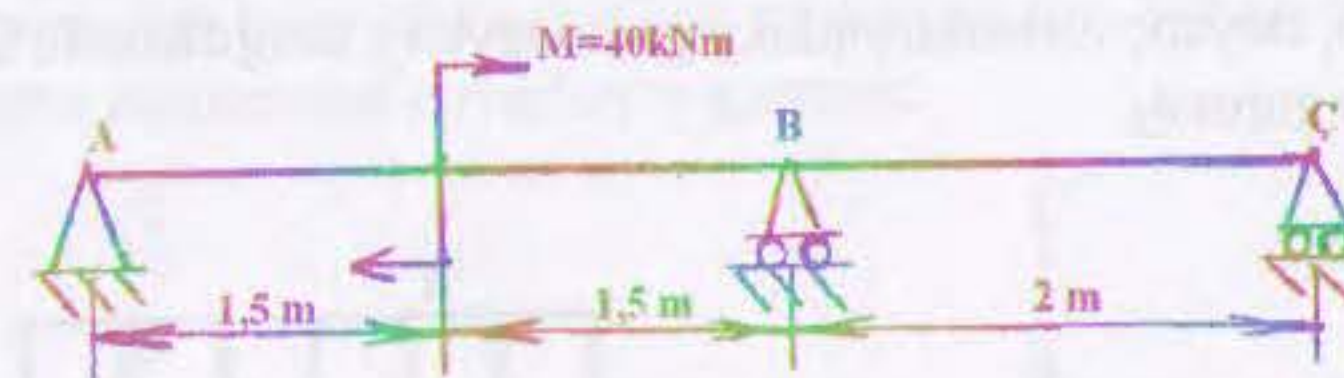
6.42-nji surat

6.43. Suratda görkezilen ABC balkanyň kese güýjüniň we egme momentiniň epýurlaryny gurmaly.



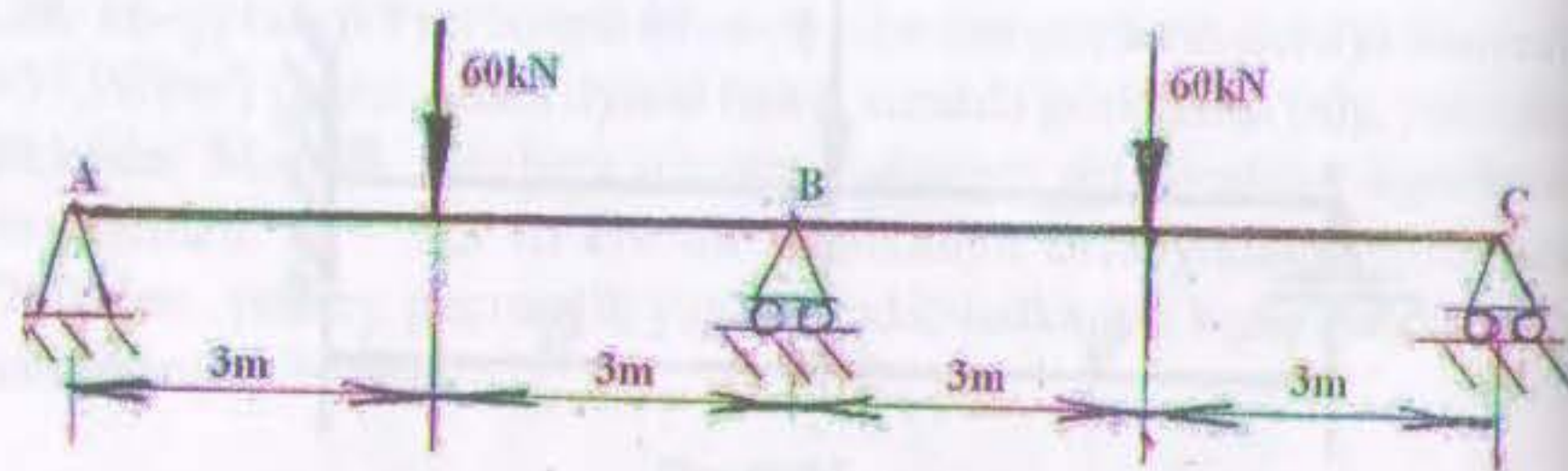
6.43-nji surat

6.44. Iki dereg aralykly kesilmedik balka suratda görkezilişi ýaly ýüklenen. Balkanyň daýanç nokatlaryndaky gaýtargylary kesgitlemeli we kese güýjüň, egme momentiniň epýurlaryny kesgitlemeli. Gönüburçlugyň $h:b=2$ gatnaşygynda balkanyň kesigini saýlamaly. Egilmede rugsat edilýän dartgynlyk $1,1 \text{ kN/sm}^2$ diýip kabul etmeli.



6.44-nji surat

6.45. Suratda görkezilen shema boýunça balkanyň daýanç nokatlaryndaky gaýtargylary we iň uly hem iň kiçi egme momentlerini kesgitlemeli. Rugsat edilýän dartgynlyk 16 kN/sm^2 bolanda, iki tawranyň belgisini saýlamaly.



6.45-nji surat

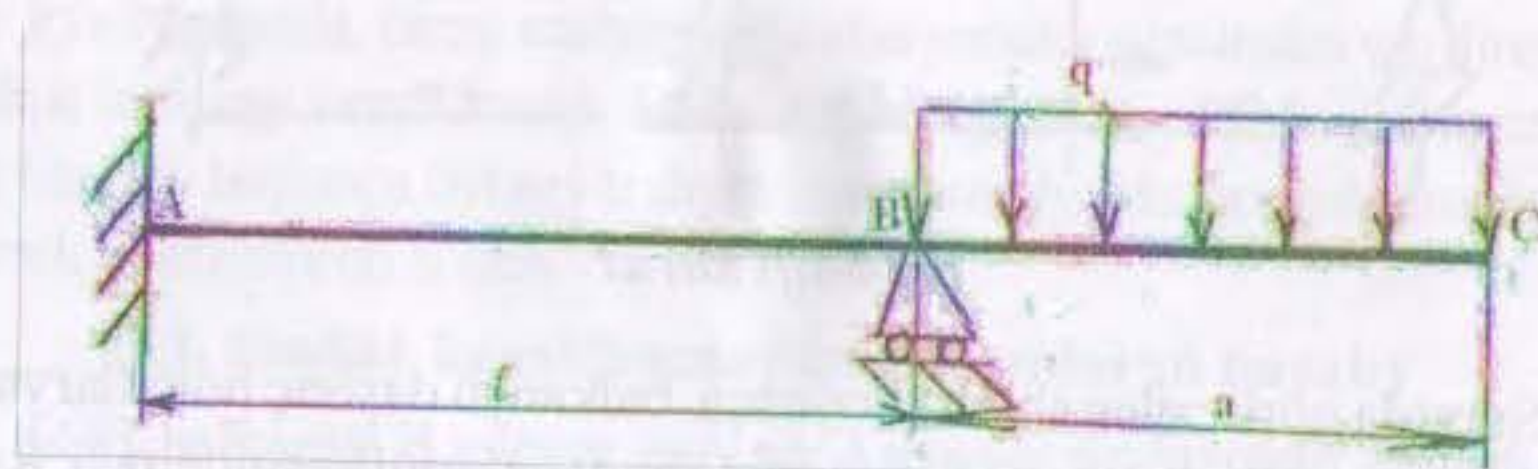
6.46. Shemada görkezilen çarçuwalaryň kese güýjüniň we egme momentiniň epýurlaryny gurmaly.

6.47. Suratda görkezilen ýüklenme boýunça iki tarapy gaty berkidilen iki tawraly balkanyň kesigini saýlamaly. $a=1,5$ m, $b=3$ m, $P=60$ kN, $[\sigma]=16$ kN/sm² deň diýip kabul etmeli.

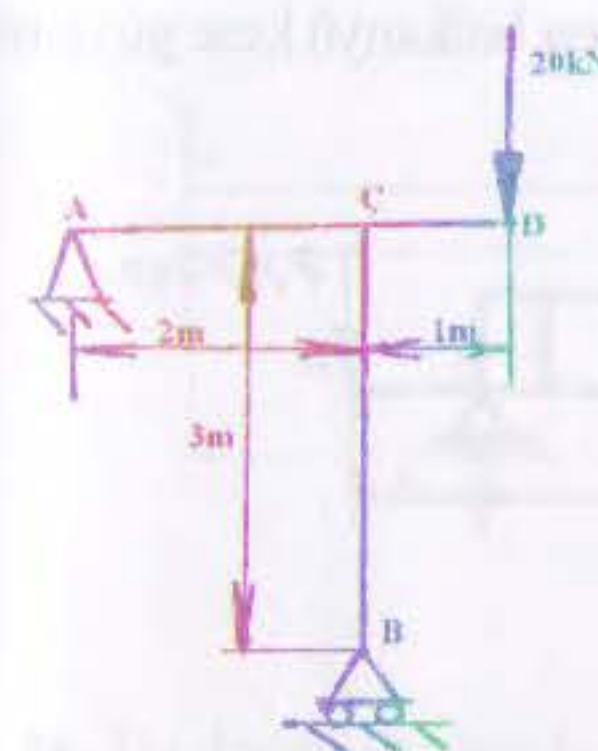


6.47-nji surat

6.48. Islendik usul bilen balkanyň statik kesgitlenmeyändigini açyp görkezmeli, daýanç nokatlaryndaky gaýtargylary kesgitlemeli, Q we M epýurlaryny gurmaly.

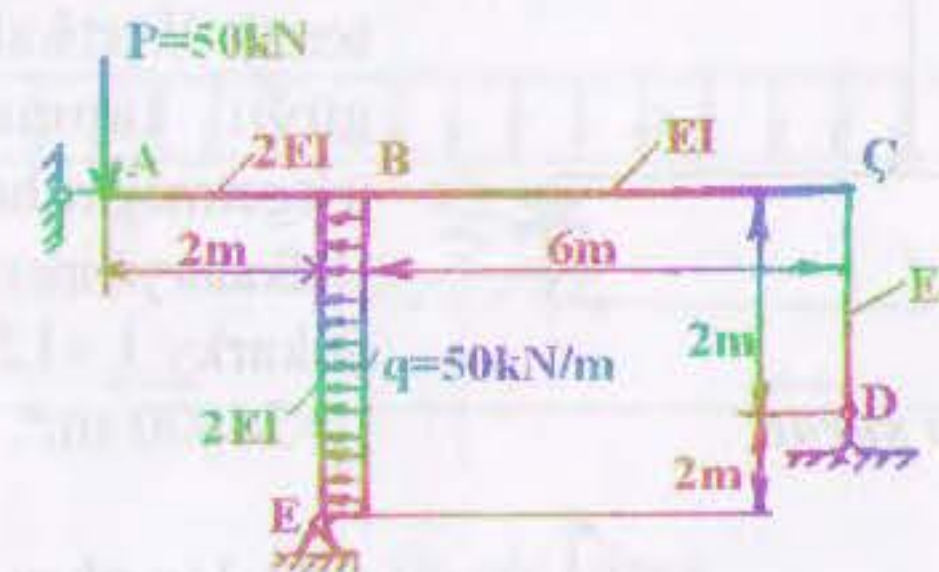


6.48-nji surat



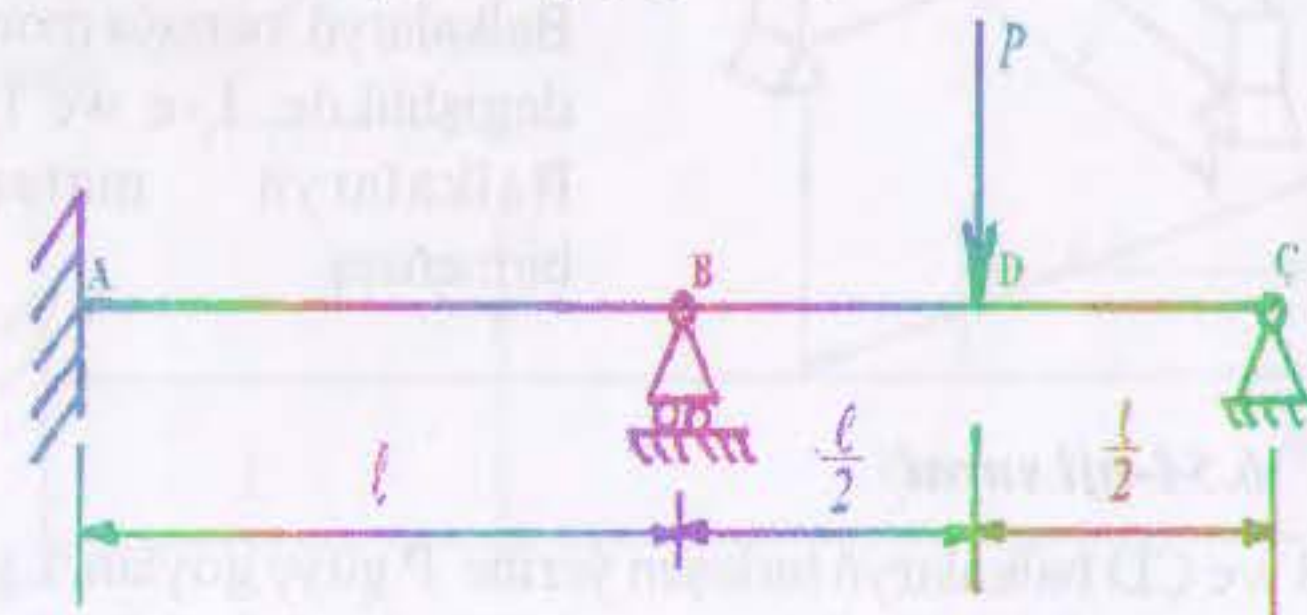
6.49-njy surat

6.50. Suratda şekillendirilen çarçuwanyň normal we kese güýçleriniň hem egme momentiniň epýurlaryny gurmaly.



6.50-nji surat

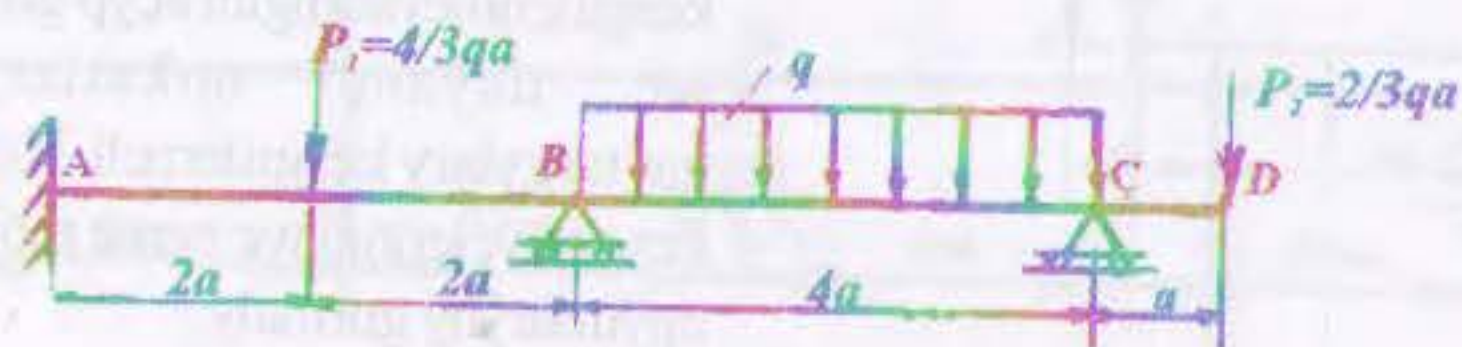
6.51. Iki direk aralykly balka sag direk aralygynyň ortasynda bir ýere jemlenen güýç bilen ýüklenen. Güýç usulyny ulanyp, balkanyň kese güýjüniň we egme momentiniň epýurlaryny gurmaly.



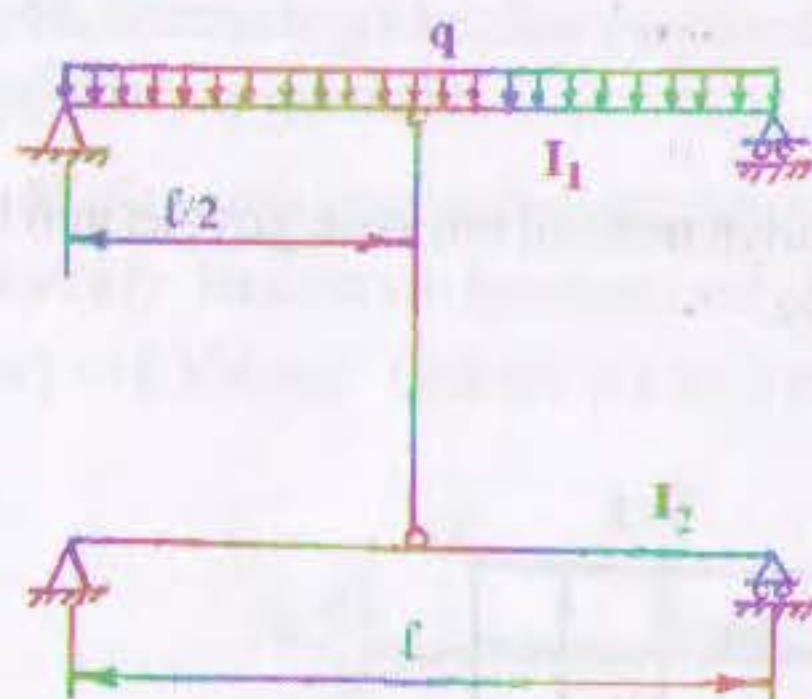
6.51-nji surat

6.49. Suratda shemasy görkezilen çarçuwanyň güýç usulyny ulanyp, statik kesgitlenmeyändigini açyp görkezmeli we daýanç nokatlaryndaky gaýtargylary kesgitlemeli. Normal we kese güýçleriniň we egme momentiniň epýurlaryny gurmaly.

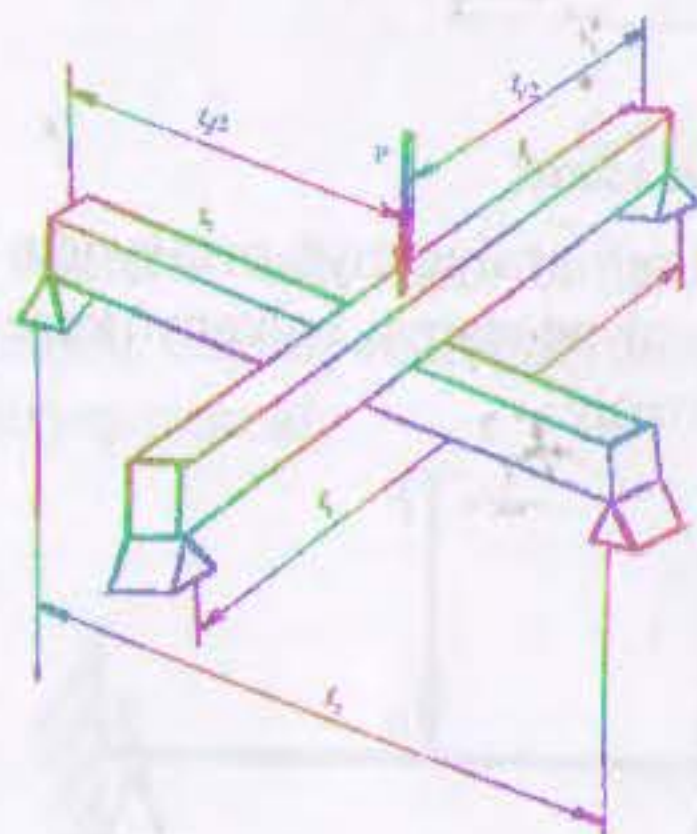
6.52. Matrisa usulyny ulanyp, suratda şekillendirilen balkanyň kese güýjüniň we egme momentiniň epýurlaryny gurmaly.



6.52-nji surat

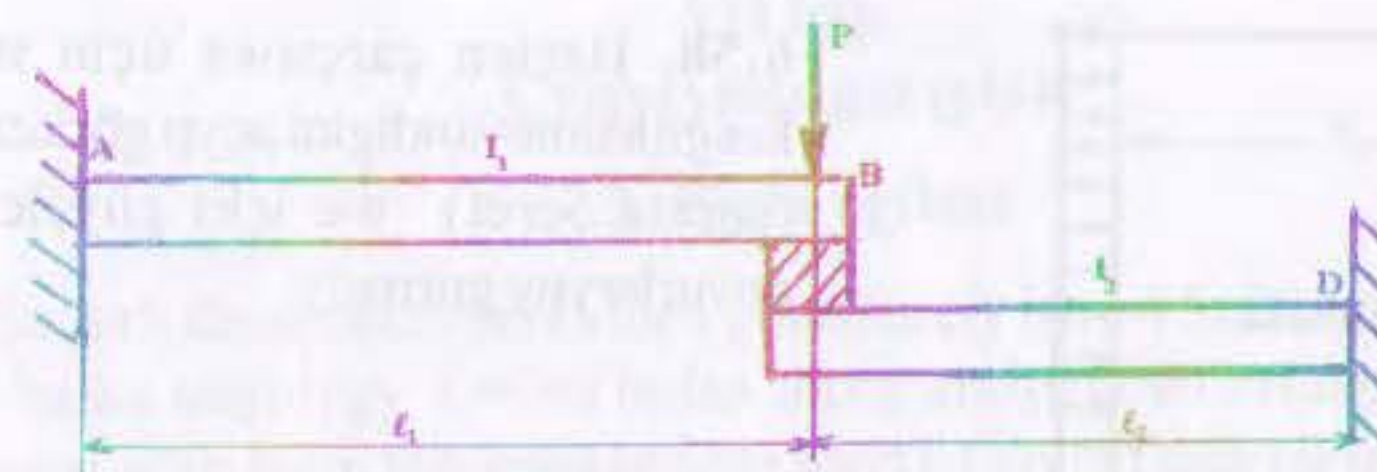


6.53-nji surat



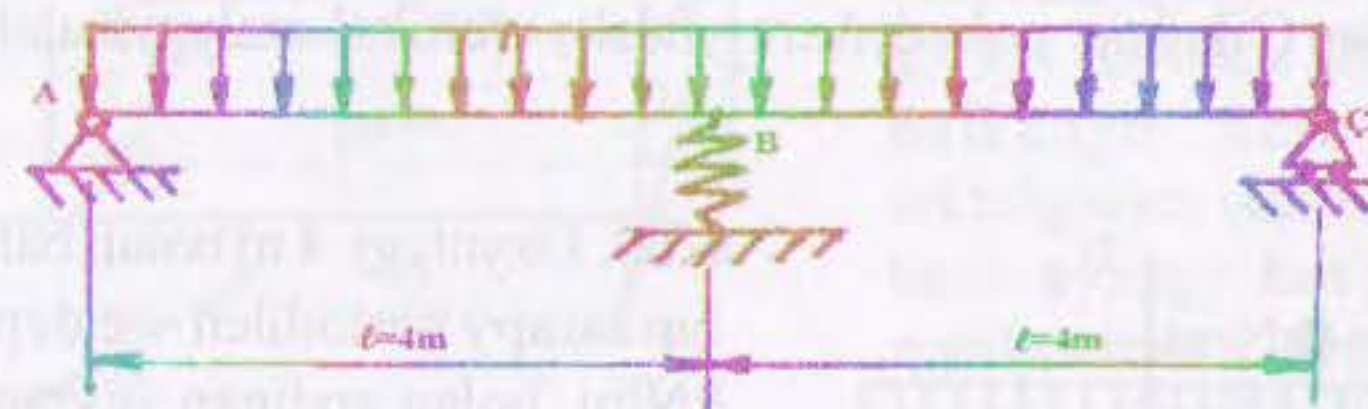
6.54-nji surat

6.55. Iki AB we ÇD balkalaryň birleşen ýerine P güýç goýlan. Eger direg aralyklarynyň we gatylyklarynyň gatnaşygy belli bolsa: $l_1:l_2=3:2$; $EI_1:EI_2=4:5$, P güýjüň balkalaryň arasyndaky paýlanylyşyny tapmaly.



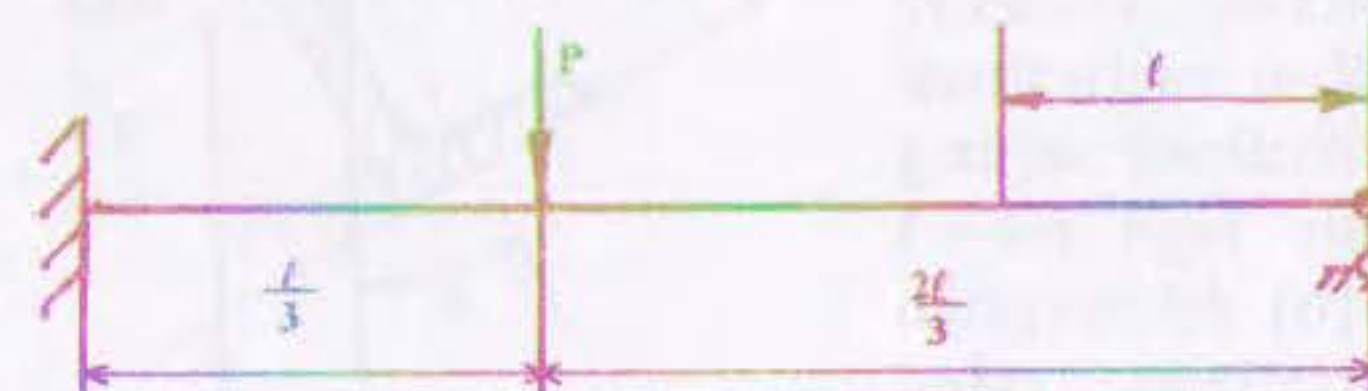
6.55-nji surat

6.56. Iki daýanç nokatda goýlan 24-nji belgili iki tawraly polat balkanyň ortasynda gatylygy $C=10$ kN/sm bolan pružin goýlan (surata seret). Durkuny üýtgetmegi deňeşdirmek usuly bilen ortaky diregiň gaýtargysyny kesgitlemeli.

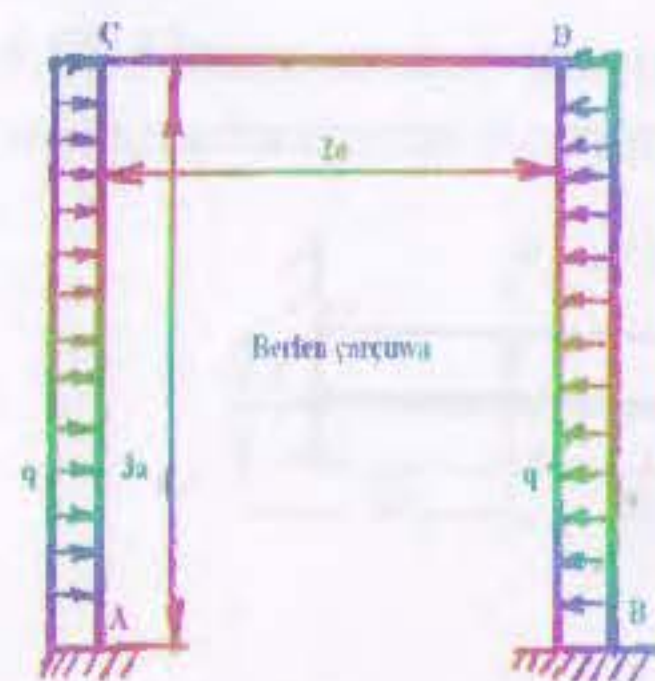


6.56-nji surat

6.57. Polat balkanyň okuna parallel edilip datçik ýelimlenen (surata seret). Eger elektrotenzometrik ölçeyjileriň görkezmesi boýunça datçigiň bazasynyň ugruna alnan durkuny üýtgetme $\varepsilon_A = -1 \cdot 10^{-4}$ bolsa, P güýjüň ululygyny kesgitlemeli.

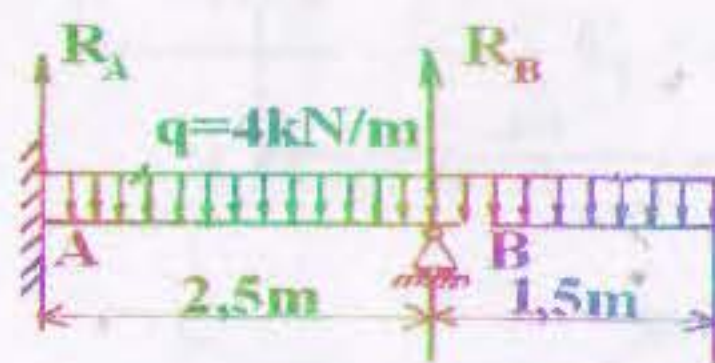


6.57-nji surat



6.58-nji surat

6.59. Direg aralary ℓ bolan iki direg aralykly ABC balka, depgini q bolan endigan ýaýran ýük bilen ýüklenen. Ortaky daýanç nokadyň gaýtargysy $q\ell$ -e deň. A we Ç daýanç nokadyň arasyndaky wertikal aralygyň ululygyny tapmaly.



6.60-njy surat

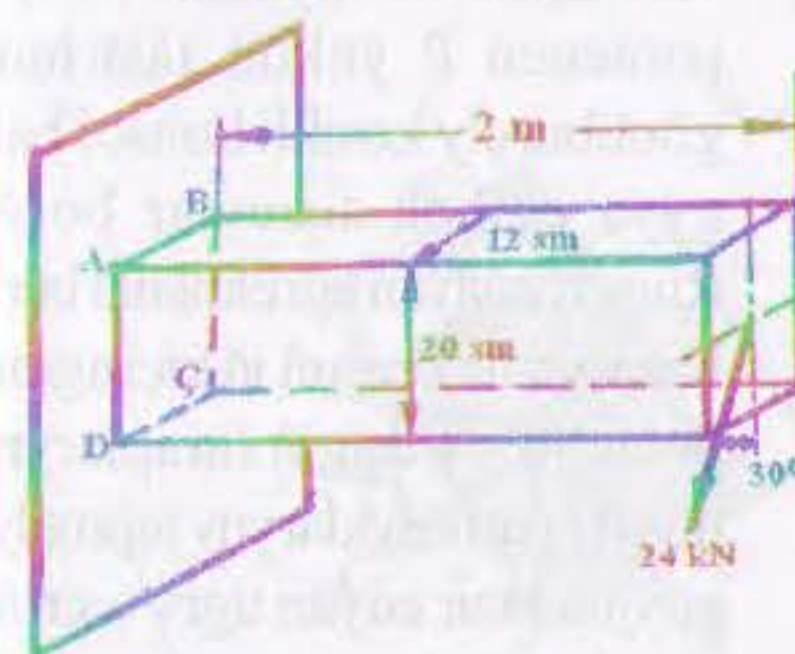
6.58. Berlen çarçuwa üçin statik kesgitlenmeýändigini açyp görkezmeli (surata seret) we içki güýçleriniň epýurlaryny gurmaly.

6.60. Uzynlygy 4 m bolan balkanyň bir tarapy berkidilen we depgini 4 kN/m bolan endigan ýaýran güýç bilen ýüklenen; balkanyň berkidilen A nokadyndan 2,5 m aralykda direg bilen goldaw berlende, berkidilen A nokatda egme moment nola deň bolýar. Goldaw beriji direge düşýän basyşy tapmaly we balkanyň kese güýjüniň we egme momentiniň epýurlaryny gurmaly.

VII bap Çylşyrymly garşylyk

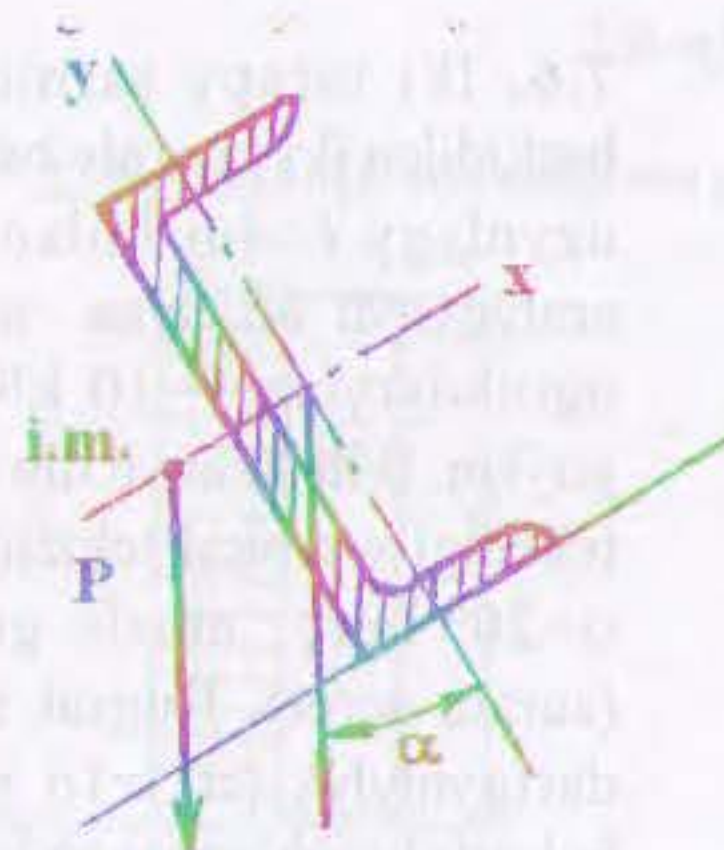
7.1. Gyýa egilme

7.1. Şarnirli direg bilen berkidilen gönüburçly $b \times h = 15 \times 20$ sm kese kesikli ağaç balka uzynlygy $\ell = 3$ m bolan direg aralygynyň ortasynda bir ýere jemlenen güýç bilen ýüklenen (surata seret). Güýjüň täsir tekizligi balkanyň okundan geçýän wertikal tekizlik bilen $\varphi = 15^\circ$ burç boýunça ýapgytlanan. Balkanyň kese kesiginde bitarap okunyň ýagdaýyny we gysylma dartgynlygyny kesgitlemeli. Balkanyň ortasyndaky kesigiň doly egrelmäniň ululygyny we ugruny kesgitlemeli.



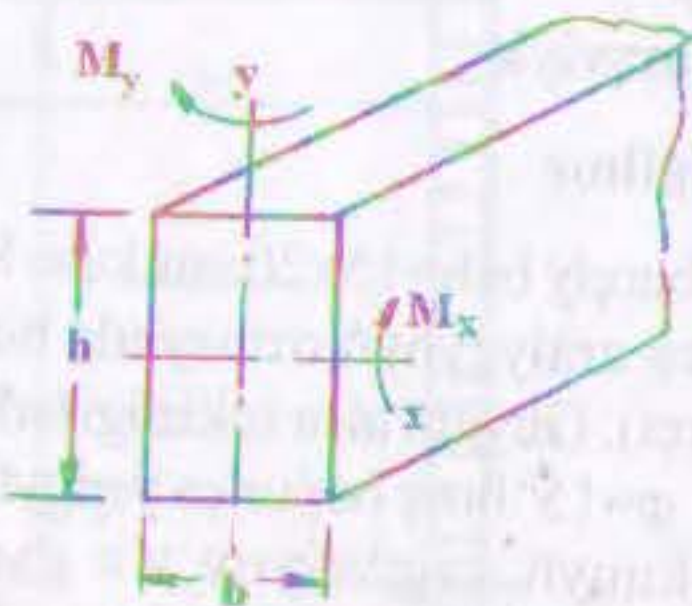
7.2-nji surat

7.2. Uzynlygy $\ell = 2$ m, kese kesigi 12×20 sm bolan gönüburçly ağaç balkanyň bir tarapy gaty berkidilen, beýleki tarapy bolsa, 2,4 kN ýük bilen ýüklenen. Güýç balkanyň kese kesiginiň tekizliginden täsir edýär we onuň täsir çyzygy kesigiň agyrlık merkezinden geçýär (surata seret). Berkidilen kesigiň gapdallary boýunça normal dartgynlygyny epýuryny gurmaly we balkanyň erkin tarapynda doly egrelmäni kesgitlemeli.

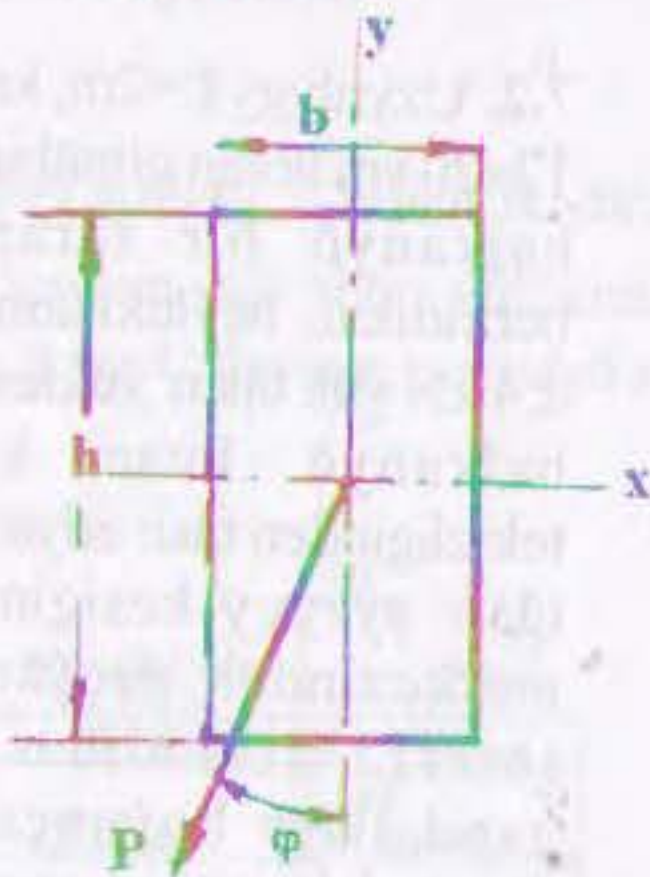


7.3-nji surat

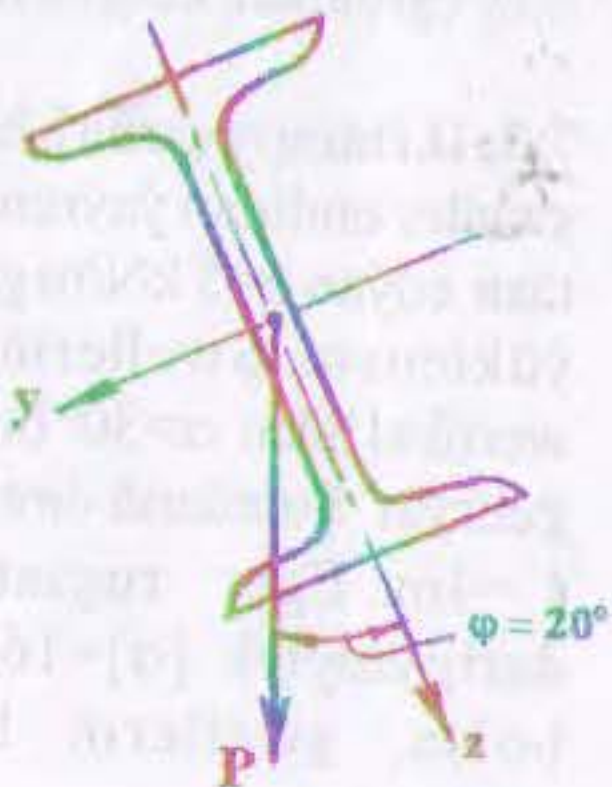
7.3. Iki tarapy şarnirli berkidilen şweller endigan ýaýran wertikal täsir edýän $q = 5$ kN/m güýç bilen ýüklenen. Şwelleriň diwary wertikal bilen $\alpha = 30^\circ$ burç emele getirýär. Şwelleriň direg aralygy $\ell = 4$ m. Eger rugsat edilyän dartgynlyk $[\sigma] = 16$ kN/sm² bolsa, şwelleriň belgisini saýlamaly.



7.4-nji surat



7.5-nji surat



7.6-nji surat

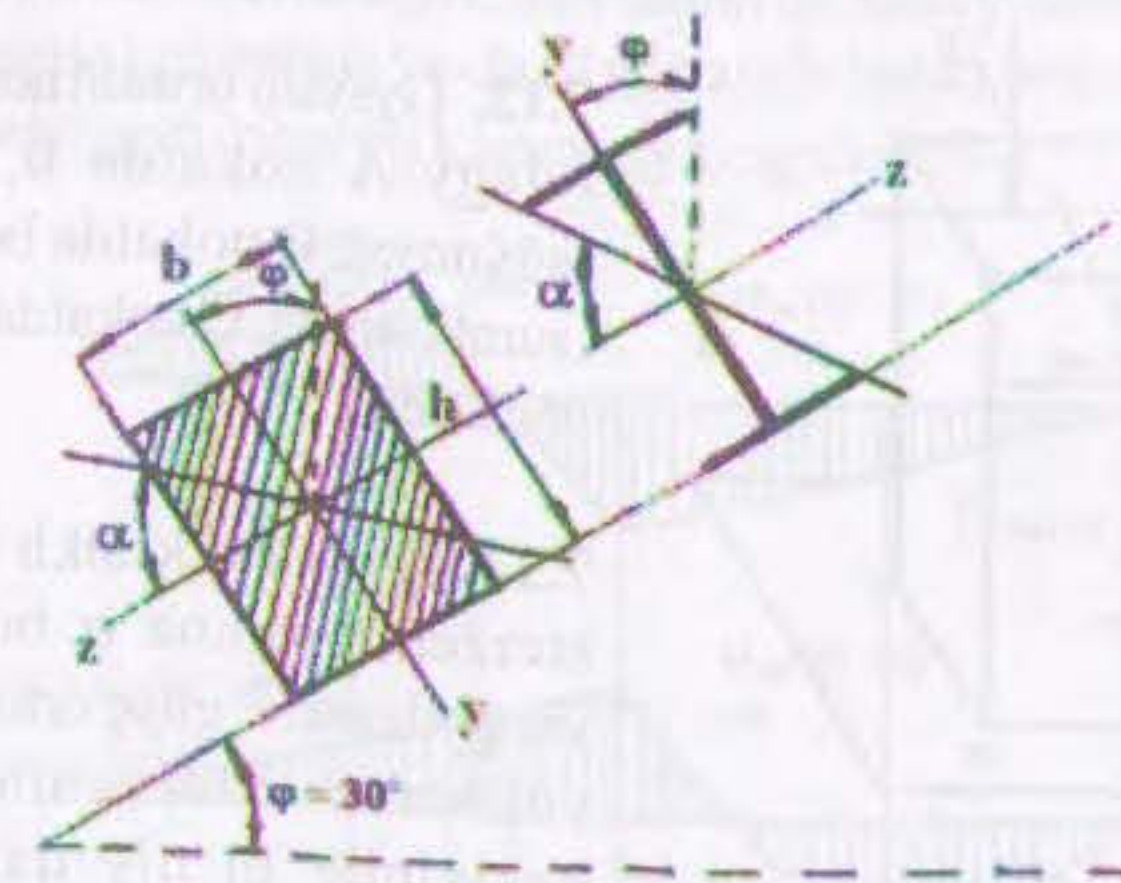
7.4. Gönüburçly kesikli brus M_x we M_y egme momentlerden gyýa egilmä sezewar bolýar. Brusuň iň az agramynda $k = \frac{h}{b}$ oňaýly gatnaşygyny kesgitlemeli.

7.5. Erkin tarapyndan bir ýere jemlenen P ýüküň täsirinden gönüburçly kesikli konsol balka gyýa egilmä sezewar bolýar. Rugsat edilyän egrelmäniň berlen bahasynda brusuň iň kiçi agramy bolar ýaly kesigiň taraplarynyň oňaýly gatnaşyklaryny tapmaly. P güýjüň täsir edýän ugry wertikal ok bilen α burçy emele getirýär.

7.6. Iki tarapy şarnir bilen berkidilen iki tawraly balkanyň uzynlygy $\ell = 4\text{ m}$ bolan dereg aralygynyň ortasyna wertikal ugrukdyrylan $P = 10\text{ kN}$ güýç goýlan. Ikitawranyň diwarynyň tekizligi wertikal tekizlik bilen $\alpha = 20^\circ$ burç emele getirýär (surata seret). Rugsat edilyän dartgynlylyk $[\sigma] = 16\text{ kN/sm}^2$ bolanda kesgitlenen sort boýunça balkanyň kesigini saýlamaly.

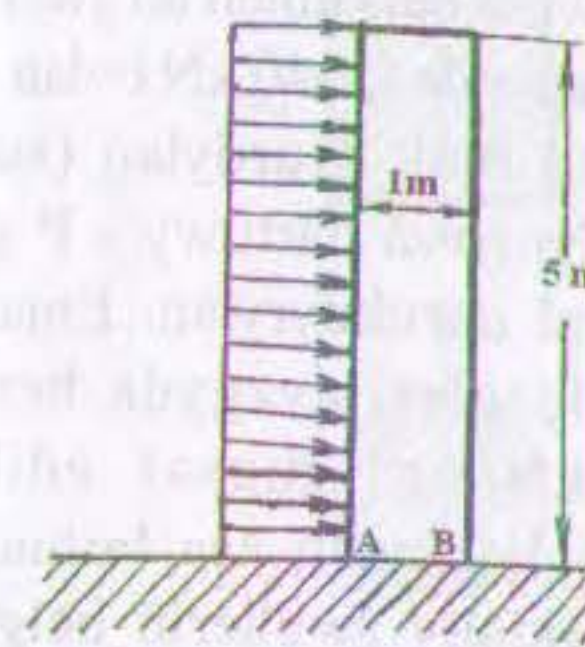
7.7. Uzynlygy 1.6 m , ölçegi $80 \times 80 \times 7\text{ mm}$ bolan ugolok bir tarapy gaty berkidilen balka görnüşinde işleýär; kesigiň egilme merkezinden geçýän bir ýere jemlenen $P = 1\text{ kN}$ güýç balkanyň erkin tarapynda goýlan. Balkanyň howply kesiginde bitarap okuň ýagdaýyny we A, B we C nokatlarda normal dartgynlylyklary kesgitlemeli. Ugologyň iň uly egrelmesiniň ululygyny we ugruny kesgitlemeli.

7.8. Jaýyň üçeginiň gapyrgasynyň ($p = 3,2\text{ kN/m}^2$ wertikal ýüki göterýän bolsa) kesiginiň ölçeglerini iki görnüşde saýlamaly: gönüburçluk $[\sigma] = 1,25\text{ kN/sm}^2$ (agaç) we ikitawra ($[\sigma] = 16\text{ kN/sm}^2$) Gapyrganyň dereg aralygy $\ell = 4\text{ m}$; gapyrgalaryň özara aralygy $a = 1,25\text{ m}$ deň.



7.8-nji surat

7.2. Egilmäniň süýnme we gysma bilen bilelikdäki täsiri

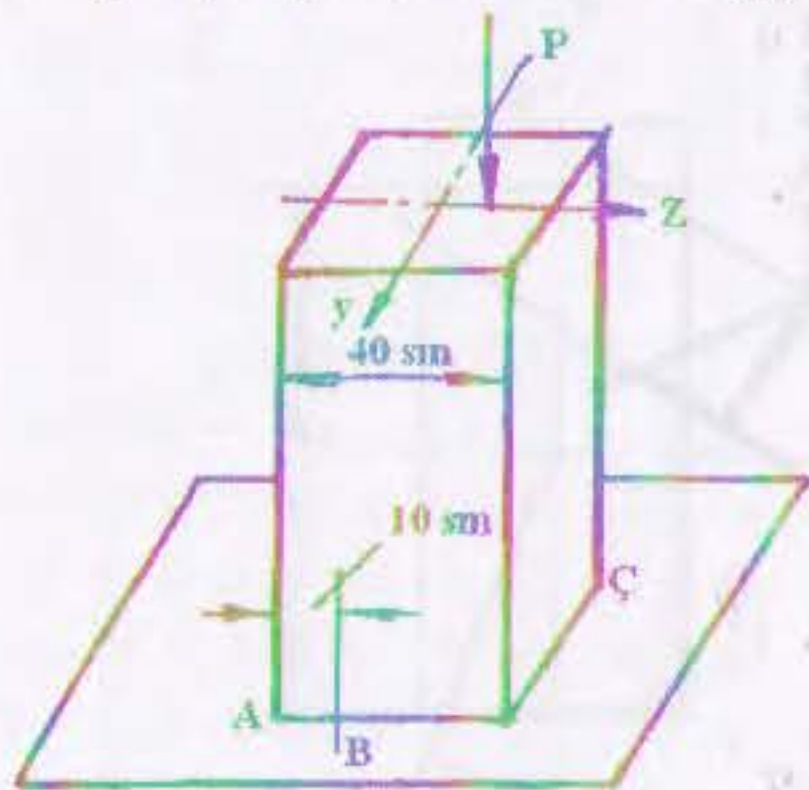


7.9-nji surat

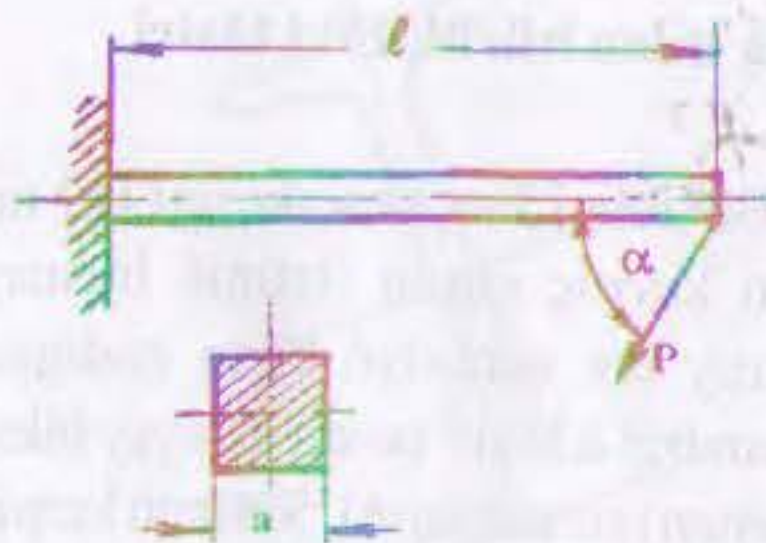
7.9. Beýikligi 5 m , kese-kesigi $1 \times 1\text{ m}^2$ bolan kerpiç sütün özüniň hususy agramy we şemalyň kese endigan ýaýran $0,8\text{ kN/m}^2$ bolan basyşy bilen ýüklenen (surata seret). Sütüniň kerpiç örüminiň udel agramy $1,6$. Sütüniň esasyndaky iň uly we iň kiçi gysylma dartgynlyklaryny kesgitlemeli.

7.10. Kesilen kesigi suratda shematiki görkezilen daşdan edilen söýeg diwary ýeriň gum üýşmegini saklaýar. Örümiň udel agramy 1,8-e deň. Ýeriň basyşy q gorizonta ugrukdyrylan we diwaryň beýikligine üçburçlugaň kanuny boýunça ýaýraýar; diwaryň esasyndaky iň uly basyş $1,5 \text{ kN/m}^2$ deň. Diwaryň esasyndaky iň uly we iň kiçi gysylma dartgynlylyklaryň ululygyny kesgitlemeli.

7.11. Gönüburçly $15 \times 20 \text{ sm}$ kese kesikli ağaç direk baş inersiýa oklaryň her haýsyndan 3 sm uzaklykda ýerleşen N nokatda 90 kN deň gysýan boý güýji bilen ýüklenen. Bitarap okuň ýagdaýyny kesgitlemeli we gönüburçlugaň taraplary boýunça normal dartgynlylygyň ýaýraýşynyň epýuryny gurmaly.



7.12-nji surat

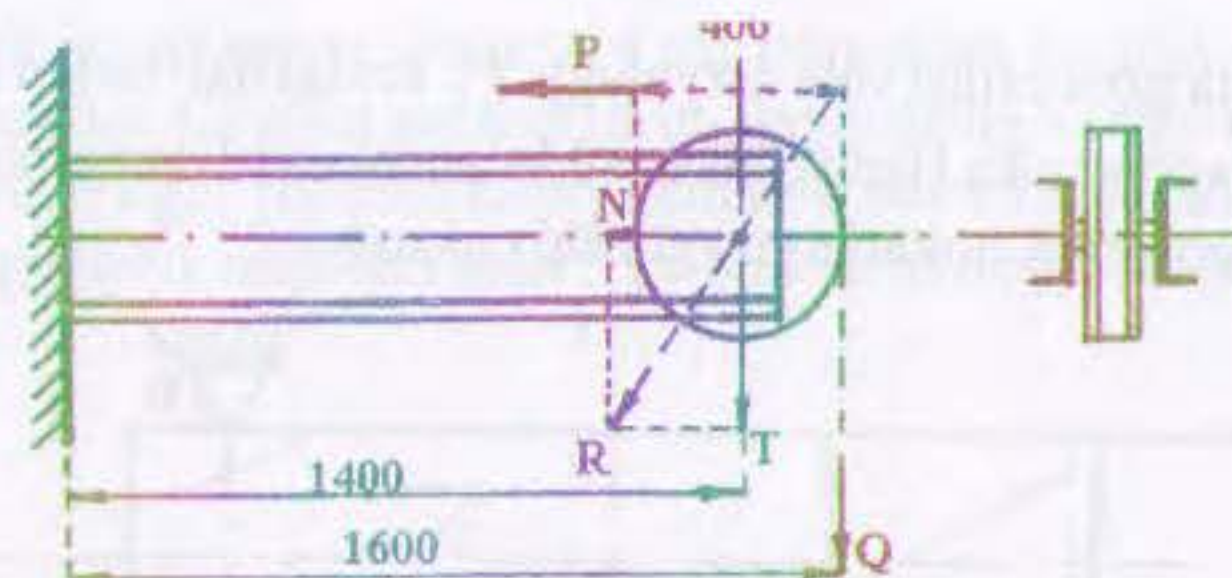


7.13-nji surat

7.12. Gysylan brusuň normal dartgynlylygy A nokatda $0,2 \text{ kN/sm}^2$ -a (süýnme), B nokatda bolsa nola deň (surata seret). C nokatda dartgynlylyk näçä deň?

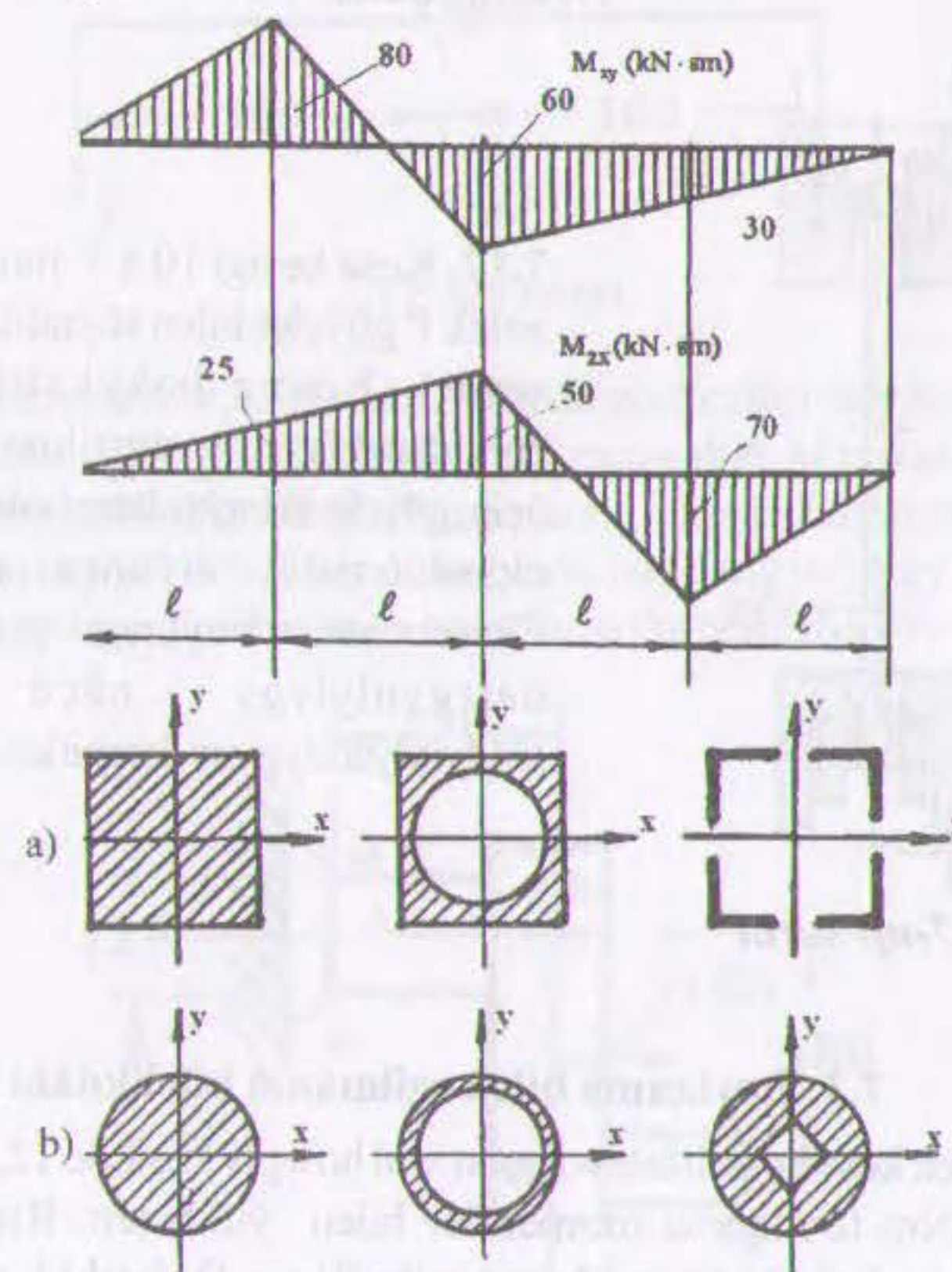
7.13. Kwadrat kesikli (axa) konsol sterženiň okuna α burç boýunça ýapgytlanan P güýç erkin tarapyndan ýüklenen. Sterženiň berkidilen kesiginde iň uly dartgynlylygy kesgitlemeli we α burçuň haýsy bahasynda dartgynlylyk iň uly baha deň bolýar.

7.14. Diwara berkidilen iki şwelleriň erkin tarapynda $Q=40 \text{ kN}$ bolan ýüki galdyryan blok oturdylan (surata seret). Zynjyryň dartuwy - P güýç gorizonta ugrukdyrylan. Enjamyň esasy ölçegleri çyzgyda berlen. $[\sigma]=8 \text{ kN/sm}^2$ rugsat edilyän dartgynlylygyndan aşa bolmadyk ýagdaýyndaky şwelleriň belgisini kesgitlemeli.



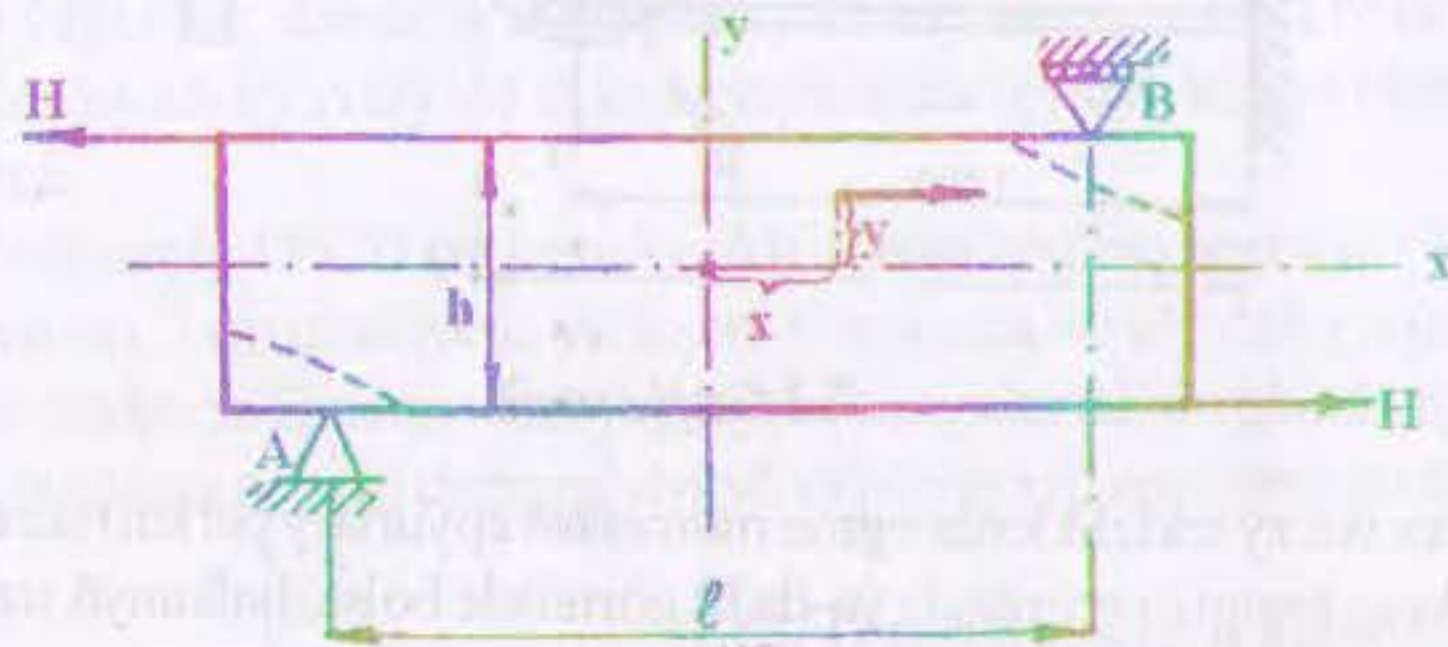
7.14-nji surat

7.15. zx we zy tekizliklerde egme momentiň epýurlary berlen (surata seret). Eger kese kesigi a) görnüşde ýa-da b) görnüşde bolsa, balkanyň uzynlygyna iň uly dartgynlylygyň üýtgeýiş kanunyny kesgitlemeli.



7.15-nji surat

7.16. Suratda görkezilişi ýaly uzynlygy ℓ , kesigi $h \times b$ bolan iki diregde goýlan gönüburçly balka H güýç bilen ýüklenen. Normal dartgynlylygynyň nola deň bolýan geometrik nokatlaryny gözläp tapmaly.



7.16-njy surat



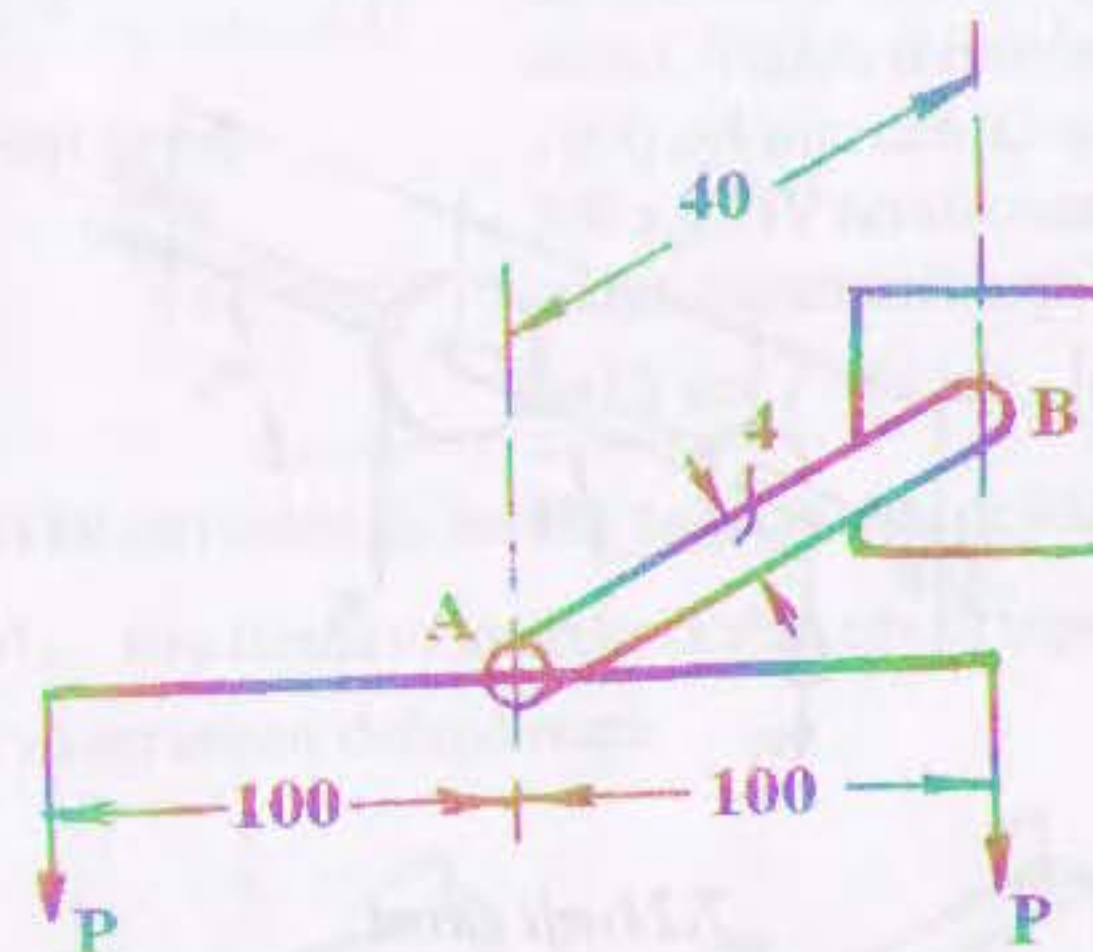
7.17-nji surat

7.17. Kese kesigi 10×5 mm bolan polat zolak P güýçler bilen süýndürilýär (surata seret). Emma hakykatdan gysýan enjamlardaky uly sürtülme bolýandygy üçin, güýçleriň haýsy hem bolsa biri $0,1$ mm ekssentrisitet boýunça täsir edýär. Ekssentrisitet boýunça goýlan güýjüň dartgynlylygy näçe görterim galdyrylýandygyny kesgitlemeli.

7.3. Towlanma bilen egilmäniň bilelikdäki täsiri

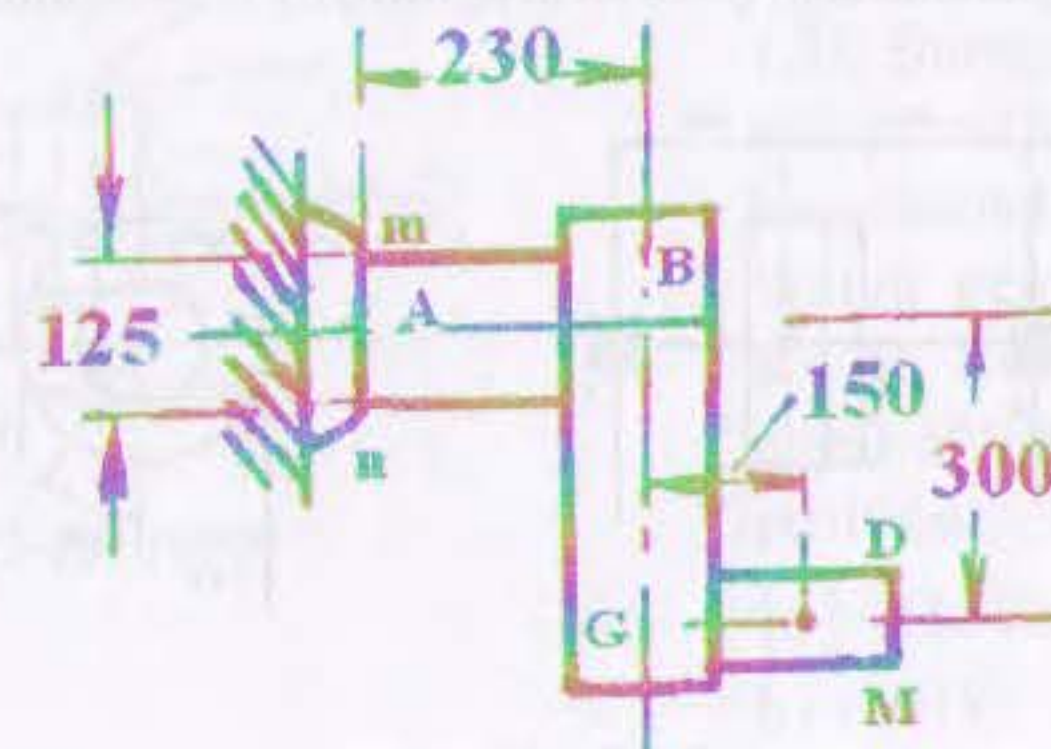
7.18. Tegelek kese kesikli bitewi polat wal howply kesikde $12,5$ kNm egme we $12,5$ kNm towlanma momentler bilen ýüklenen. Rugsat edilyän dartgynlylygy $[\sigma] = 8$ kN/sm² hasap edip III we IV berklik nazaryýetleri boýunça berklik şertinden walyň diametrini kesgitlemeli.

7.19. Uzynlygy 40 sm we diametri 4 sm, birmeňzeş iki güýç $P = 1$ kN bilen ýüklenen, tegelek AB polat sterženiň iň uly hasap dartgynlylygyny kesgitlemeli (surata seret). Eger ýükleriň haýsy hem bolsa birini aýyrsaň, steržendäki hasap dartgynlylyk näçä deň bolar? IV berklik nazaryýetini peýdalanmaly.



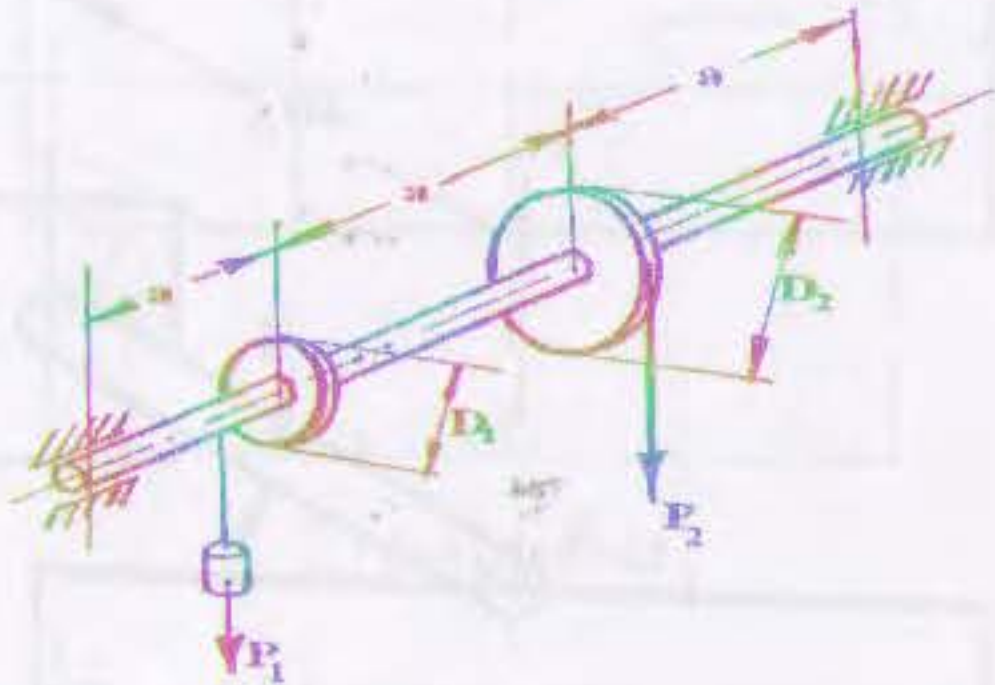
7.19-njy surat

7.20. Polat tirsekli ABCD steržen, suratda görkezilişi ýaly berkidilen. AB bölegiň kese kesigi tegelek, diametri 125 mm-e deň. M nokatda çyzgynyň tekizligine perpendikulýar 20 kN güýç goýlan. Galtaşma dartgynlylygy hasaba almazdan m kesigiň iň howply nokadynda baş dartgynlylygy we II, III we IV berklik nazaryýetleri boýunça hasaplama dartgynlylyklary kesgitlemeli.



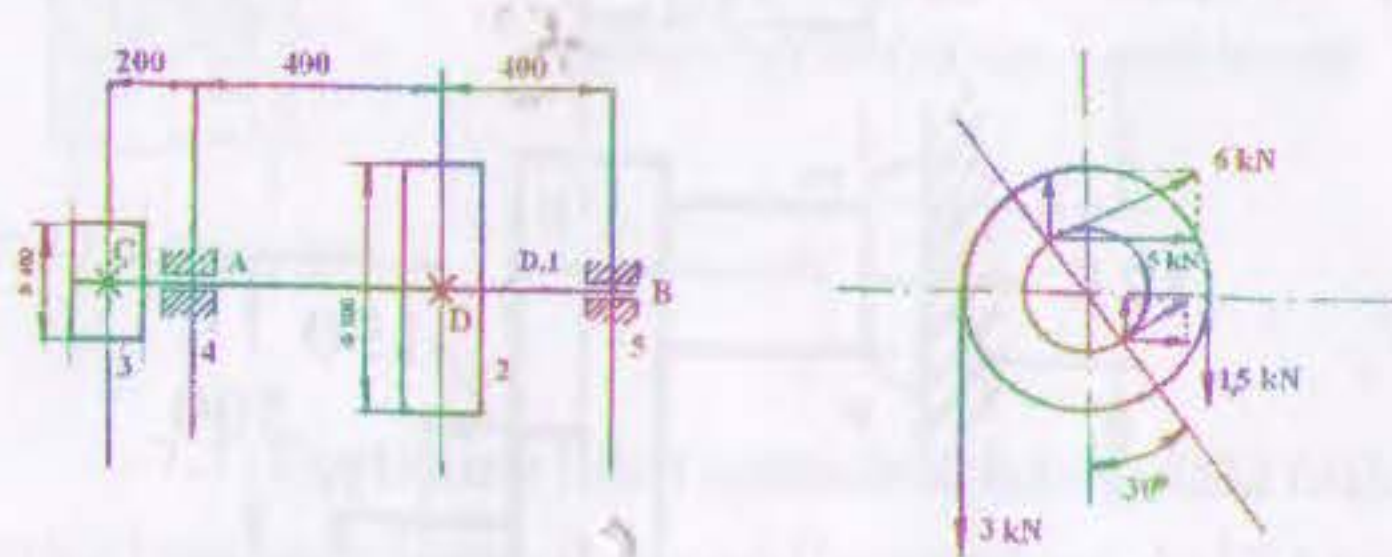
7.20-nji surat

7.21. Diametrleri $D_1=20$ sm we $D_2=50$ sm bolan iki tigr, suratda görkezilişi ýaly wala oturdylan, tigirlere P_1 we P_2 wertikal güýçler täsir edýärler. $P_1=5$ kN we $[\sigma]=10$ kN/sm², $a=120$ sm şertlerde III berklik nazaryýeti boýunça walyň diametrini kesgitlemeli. Podşipniklerdäki sürtülmäni hasaba almaly däl.

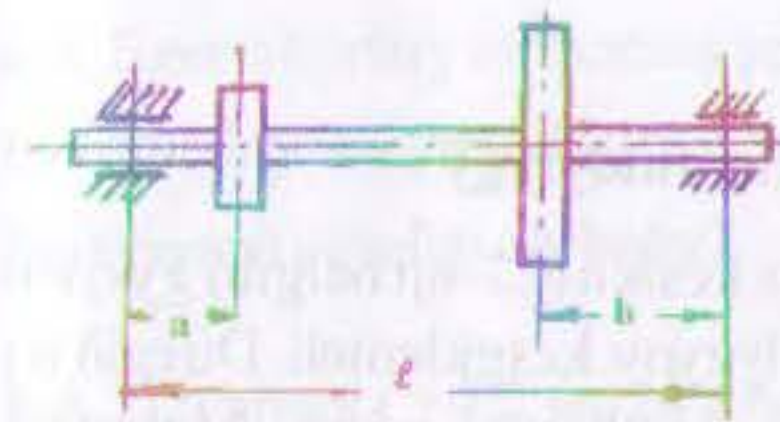


7.21-nji surat

7.22. Waldan-1, şkiwlerden-2 we 3, podşipniklerden-4 we 5 ybarat hereketi geçirijiniň walynyň diametrini kesgitlemeli. Şkiwleriň diametrleri $D_1=800$ mm, $D_2=400$ mm. Çekiniň şahalaryndaky güýçler suratda görkezilen. Walyň materialy üçin egilmede rugsat edilýän normal dartgynlyk $[\sigma]=9$ kN/sm²-a deň. Hasap üçin iň uly galtaşma dartgynlygyň berklik nazaryýetini peýdalanmaly. Şkiwleriň agramyny hasaba almaly däl.



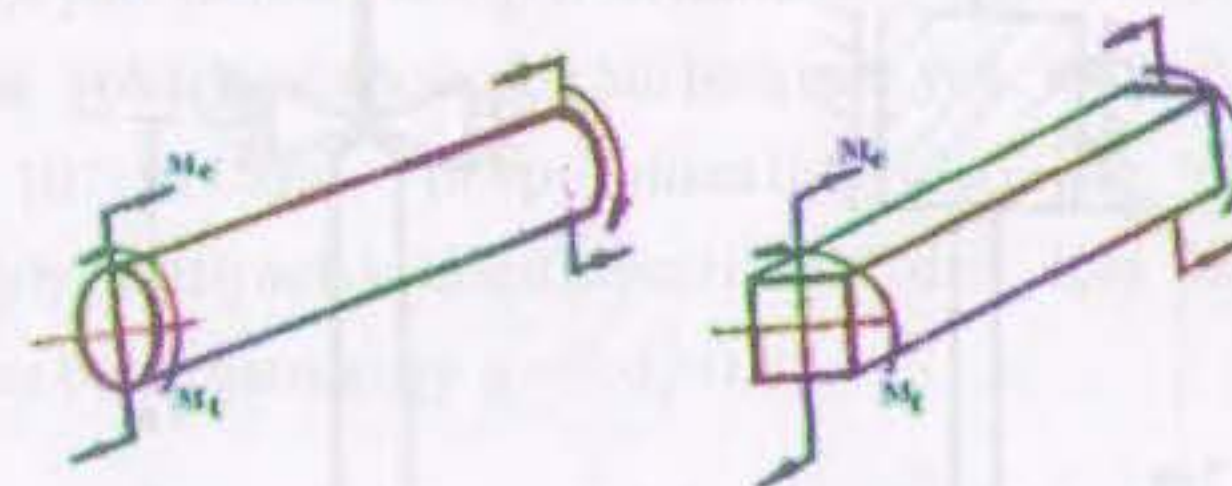
7.22-nji surat



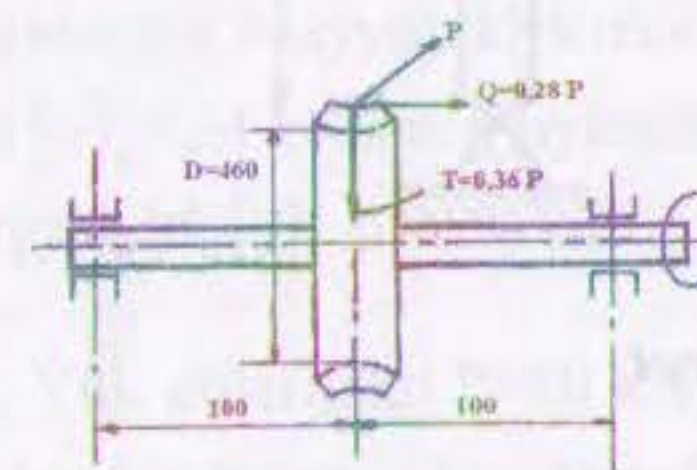
7.23-nji surat

7.23. Radiuslary $r_1=6$ sm we $r_2=12$ sm bolan aýlanýan polat wala iki dişli tigrler oturdylan. Töwerekleýin täsir edýän güýçler wertikal oklara $\alpha_1=45^\circ$ we $\alpha_2=30^\circ$ burç bilen ýapgytlanan (surata seret). Walyň minutdaky aýlaw sany 1000 aýl/min deň. Geçirýän kuwwaty 500 a.g.. IV berklik nazaryýeti boýunça walyň diametrini kesgitlemeli. $a=10$ sm, $b=15$ sm, $l=50$ sm, $[\sigma]=12$ kN/sm².

7.24. Deň berklik şertinden III berklik nazaryýetini peýdalanyp, M_e egme we $M_t = \frac{1}{3} M_e$ towlanma momentleri kabul edýän tegelek we kwadrat kesikli bruslaryň agramyny deňeşdirmeli.



7.24-nji surat



7.25-nji surat

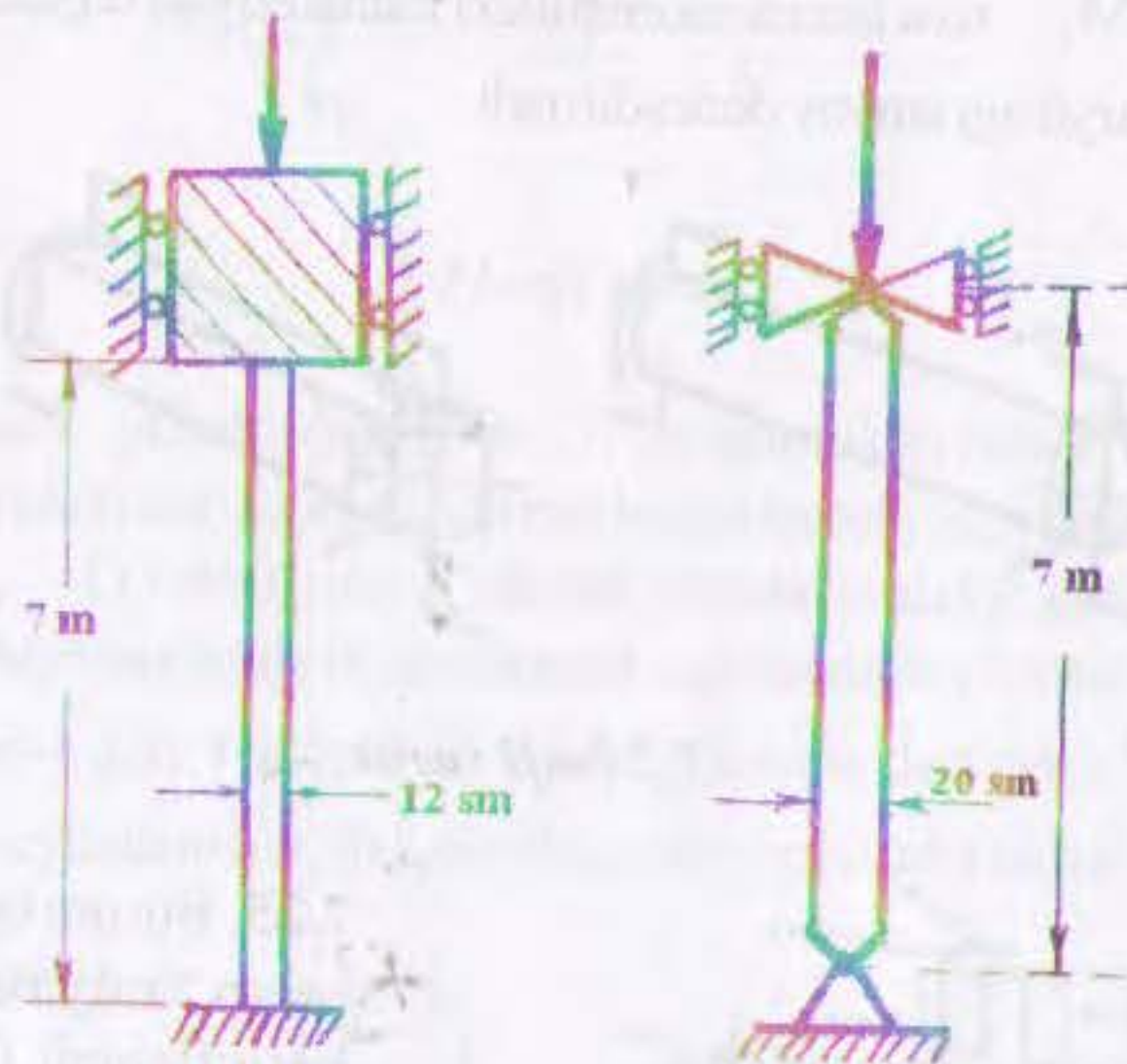
7.25. Burum tigriniň walynyň talap edýän diametrini kesgitlemeli (surata seret). Walyň geçirýän kuwwaty $N=12$ kwt; aýlaw sany $n=80$ aýl/min; wala rugsat edilýän dartgynlyk $[\sigma]=4$ kN/sm². Hasapda IV berklik nazaryýetini peýdalanmaly.

VIII bap

Gysylan sterženleriň durnuklylygy

8.1. Eýleriň formulasyny ulanyp iki tawra kesikli (22-nji belgili) gysylan diregiň kritiki güýjüni we kritiki dartgynlygyny kesgitlemeli. Diregiň iki tarapy hem şarnirli berkidilen. Sütüniň uzynlygy $\ell = 5\text{ m}$. Materialy proporsionallyk çägi $[\sigma]_{ps} = 20\text{ kN/sm}^2$ bolan polat.

8.2. Uzynlygy 7 m, gönüburçly kese kesikli $12 \times 20\text{ sm}^2$ agaç diregiň kritiki güýjüniň we kritiki dartgynlygynyň ululygyny kesgitlemeli. Maýyşgaklyk moduly $E = 0,9 \cdot 10^3\text{ kN/sm}^2$ deň. İn kiçi gatylykdaky tekizlikde diregiň iki tarapy hem berkidilen, oňa perpendikulýar tekizlikde – iki tarapy şarnirli berkidilen (surata seret).



8.2-nji surat

8.3. Eger diregleriň biri tegelek, beýlekisi turba görnüşli, kese kesikleriniň meýdanlary deň ululykda bolsa, Eýleriň formulasyny peýdalanyp, birmeňzeş şertlerde işleýän diregleriň kritiki güýçleriniň gatnaşygyny tapmaly. Turba görnüşli kesigiň diametrleriniň gatnaşygy $d_d : d_i = 1,25$ -e deň.

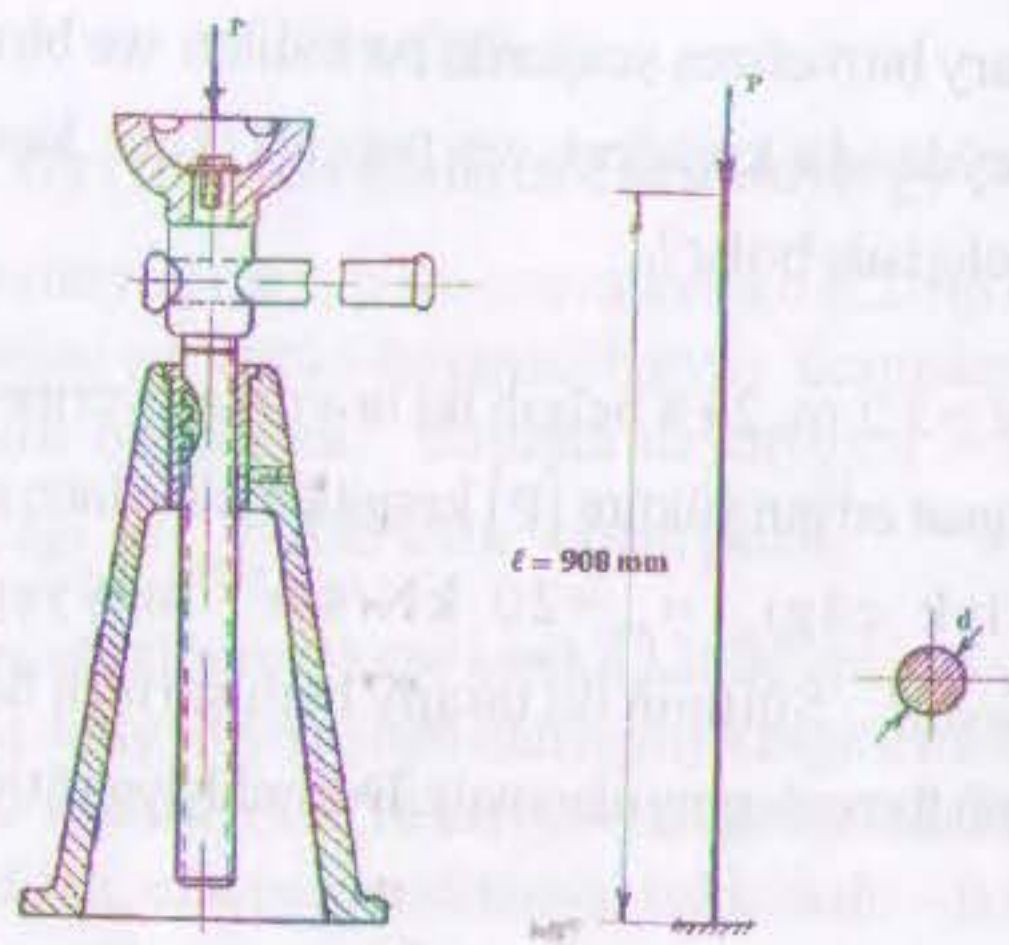
8.4. Eger ahyrlary birmeňzeş şertlerde berkidilen we birmeňzeş ýüklenen bir ululykly meýdanda kwadrat we tegelek kese kesikli sterženleriň haýsysynyň çeyeligi uly bolar?

8.5. Uzynlygy $\ell = 3,2\text{ m}$, 24 a belgili iki tawradan ýerine ýetirilen sütüniň durnuklylyga rugsat edýän ýüküni $[P]$ kesgitlemeli. Materialy – polat 3, onuň proporsionallyk çägi $\sigma_{ps} = 20\text{ kN/sm}^2$, maýyşgaklyk moduly $E = 2 \cdot 10^4\text{ kN/sm}^2$. Sütüniň iki tarapy hem şarnirli berkidilen. Mesele çözüleninde Eýleriň formulasyny ulanmaly. Durnuklylyga ätiýaçlyk koeffisiýenti $n_d = 2,8$ -e deň.

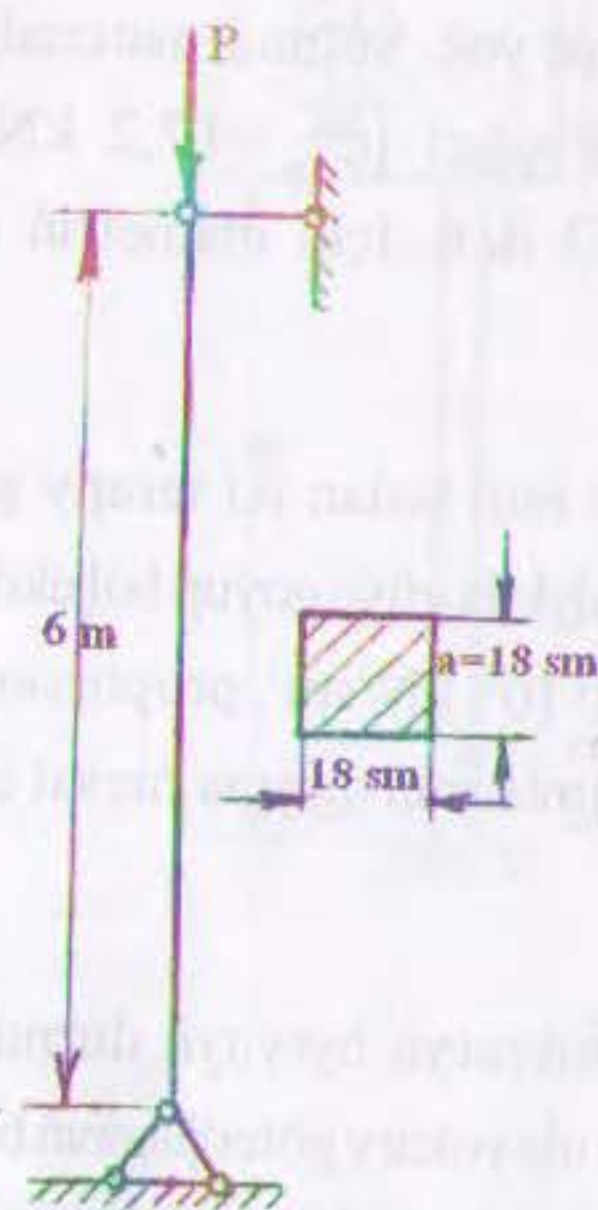
8.6. $[P_d] = 300\text{ kN}$ güýç bilen gysylýan, uzynlygy $\ell = 3,2\text{ m}$ bolan içi boş tegelek çöýun sütüniň kesigini saýlamaly. Sütüniň aşaky tarapy gaty berkidilen, ýokarsynda bolsa hiç hili berkitme ýok. Sütüniň materialy üçin $E = 1,15 \cdot 10^4\text{ kN/sm}^2$, proporsionallyk çägi $[\sigma]_p = 17,2\text{ kN/sm}^2$. Durnuklylyga ätiýaçlyk koeffisiýenti $n_d = 3$ deň. Içki diametriň daşky diametrine bolan gatnaşygy $\alpha = d_i : d_d = 0,85$.

8.7. Uzynlygy $\ell = 2,7\text{ m}$, diametri $d = 200\text{ mm}$ bolan iki tarapy şarnirli berkidilen tegelek kesikli agaç direge näçe ululykda güýç goýup boljakdygyny kesgitlemeli. Maýyşgaklyk moduly $E = 1,1 \cdot 10^3\text{ kN/sm}^2$, proporsionallyk çägi $[\sigma]_p = 2,1\text{ kN/sm}^2$ gysylmada boý süýümleriniň ugruna rugsat edilýän dartgynlylyk $[\sigma] = 0,6\text{ kN/sm}^2$.

8.8. Ýük göterijiligi $P = 50\text{ kN}$ bolan domkratyň hyrynyň durnuklylyk hasabyndan diametrini kesgitlemeli. Ýüküň in uly ýokary göterijiliginiň beýikligi $\ell = 900\text{ mm}$; durnuklylyga ätiýaçlyk koeffisiýenti $n_d = 4,0$. Hyryň materialy polat 30; maýyşgaklyk moduly $E = 2,1 \cdot 10^4\text{ kN/sm}^2$.



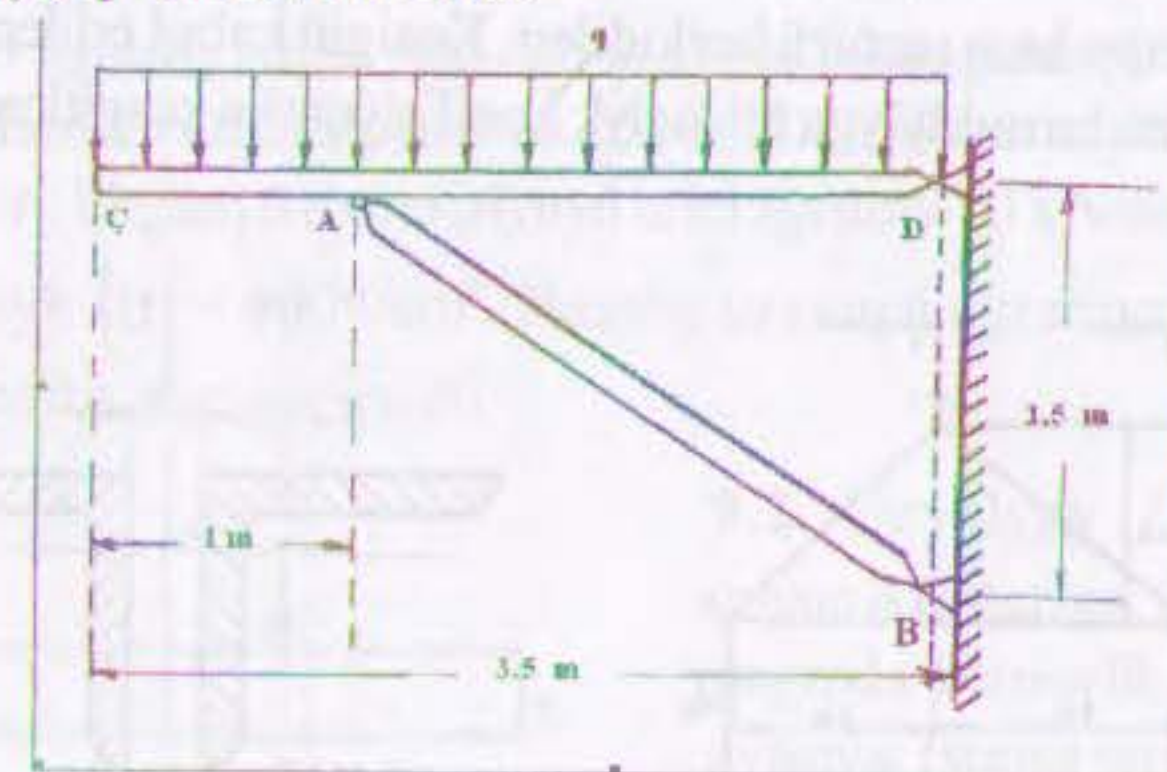
8.8-nji surat



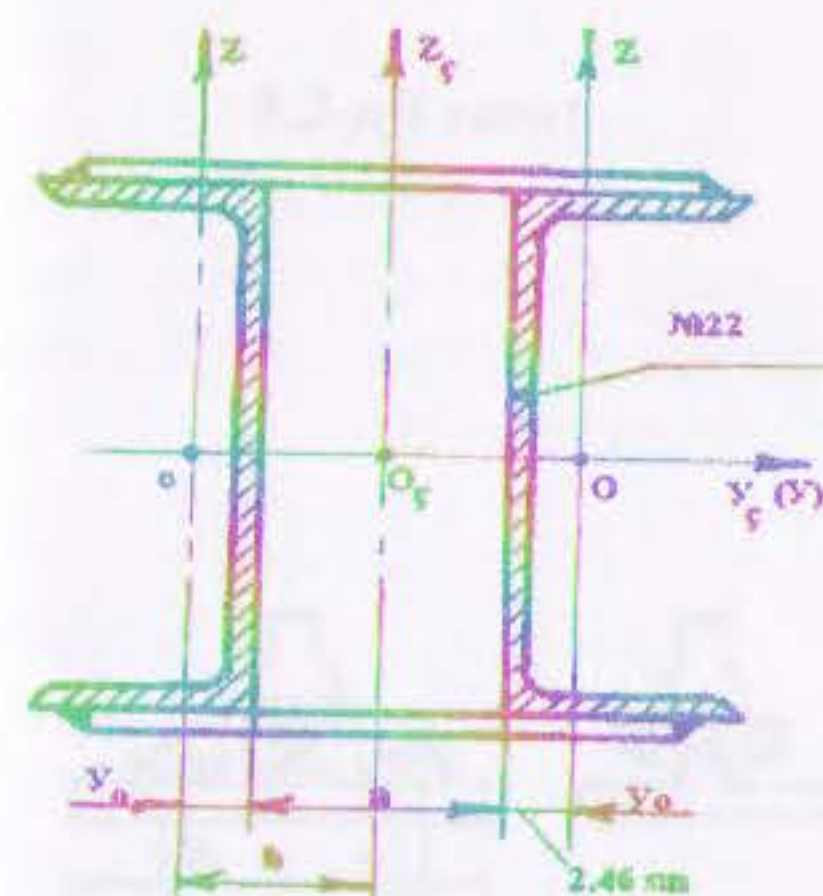
8.9-nji surat

8.9. Beýikligi 6 m kwadrat kesekesikli ağaç diregiň kritiki we rugsat edilyän güýjüni, şonuň ýaly-da esasy rugsat edilyän dartgynlylygy azaldýan koeffisiýenti tapmaly. Diregiň iki tarapy hem şarnirli berkidilen. Kwadratnyň taraplary $a=18$ sm. Ätiýaçlyk koeffisiýenti $n_d=3$. Gysylma rugsat edilyän dartgynlylyk $[\sigma]=1$ kN/sm².

8.10. Esasy rugsat edilyän dartgynlylygy $[\sigma]=1,1$ kN/sm² bolan AB kronşteýniň ağaçdan söýeginiň diametrini kesgitlemeli. Söýeginiň iki tarapyny hem şarnirli berkidilen diýip hasap etmeli. ÇD balka täsir edýän endigan ýaýran güýç $q=60$ kN/m-e deň.



8.10-nji surat



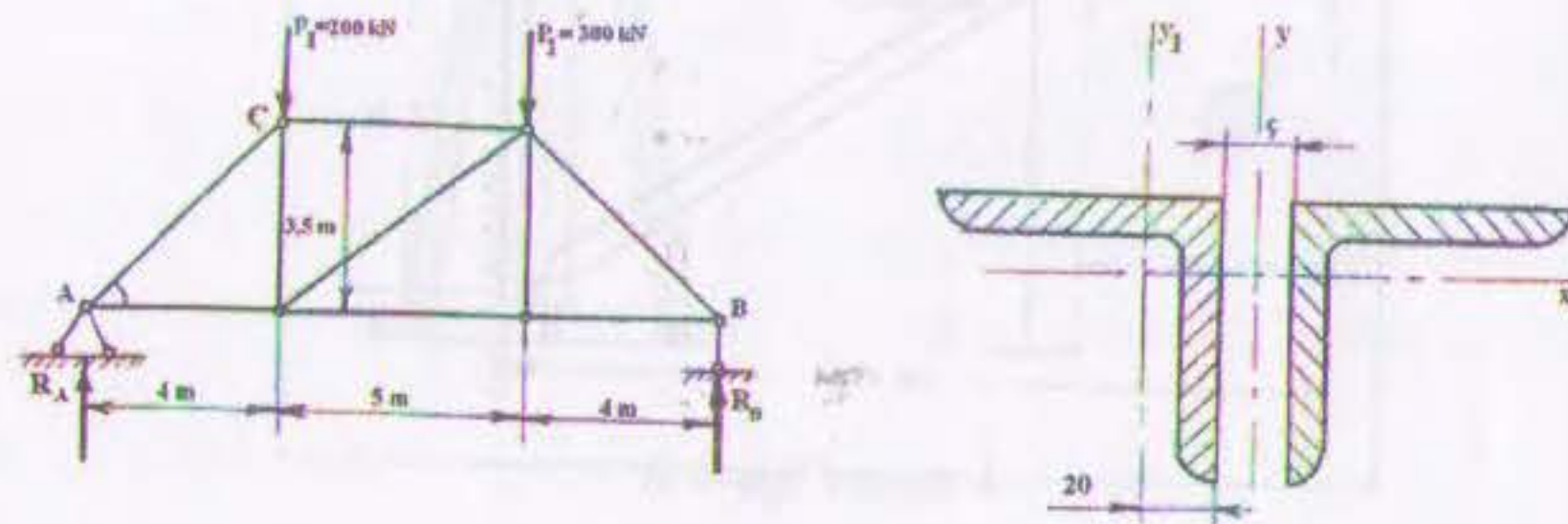
8.11-nji surat

8.11. Uzynlygy $\ell=5$ m bolan sütün 22 a belgili iki şwelleri birikdirýän plankadan ybarat. Şwelleriň materialy polat 3, onuň üçin $[\sigma]=16$ kN/sm². Sütüniň iki tarapy şarnirli berkidilen. Sütüne iň uly rugsat edilyän güýji kesgitlemeli.

$I_{y_c} = I_{z_c}$ şertden şwellerleriň aralygyny kesgitlemeli.

8.12. Eger: a) göwrüm agramy $\gamma=80 \cdot 10^{-6}$ kN/sm³ we maýyşgaklyk moduly $E=2 \cdot 10^4$ kN/sm² bolan polatdan, b) $\gamma=26 \cdot 10^{-6}$ kN/sm³ we $E=0,7 \cdot 10^4$ kN/sm² duraldan, ç) $\gamma=6 \cdot 10^{-6}$ kN/sm³ we $E=1 \cdot 10^3$ kN/sm² ağaçdan ýasalan tegelek kese kesiginiň diametri 10 sm, bir tarapy berkidilen, beýleki tarapy berkitmeden erkin bolan sterženiň hususy agramyndan ýitirýän kritiki uzynlygyny kesgitlemeli.

8.13. Suratda şekillendirilen fermanyň gysylan AÇ elementiniň (surata seret) kesigini saýlamaly. Elementiň kesigi suratda görkezilişi ýaly, iki burçlukdan ybarat we bir steržen ýaly işleýär. Materialy polat 3, $[\sigma] = 16 \text{ kN/sm}^2$. Sterženiň iki tarapy hem şarnirli berkidilen. Kesigiň kabul edilen ölçegleri boýunça sterženiň durnuklylyga ätiýaçlyk koeffisiýentini kesgitlemeli.



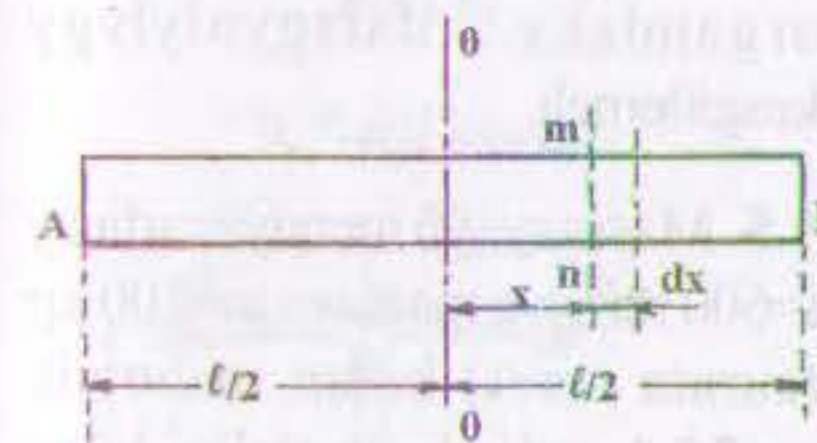
8.13-nji surat

IX bap

Dinamiki we dowamly ýüklenmeler.

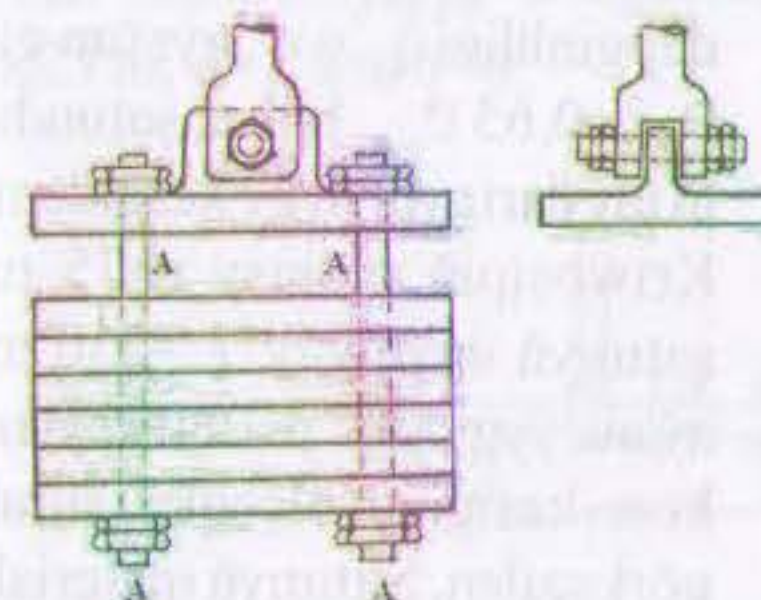
9.1. Inersiýa güýçlerini hasaba almak

9.1. 50 kN agramy bolan ýüki deň tizlenme bilen galdyrýan uzynlygy 60 m urganyň diametrini kesgitlemeli. Birinji üç sekuntda ýük 9 m beýiklige galdyrylýar. Urganyň materialynyň udel agramy 70 kN/m^3 , rugsat edilyän dartgynlyk $[\sigma] = 6 \text{ kN/sm}^2$. Hasaby urganyň agramyny hasaba alman hem-de hasaba alyp geçirmeli.



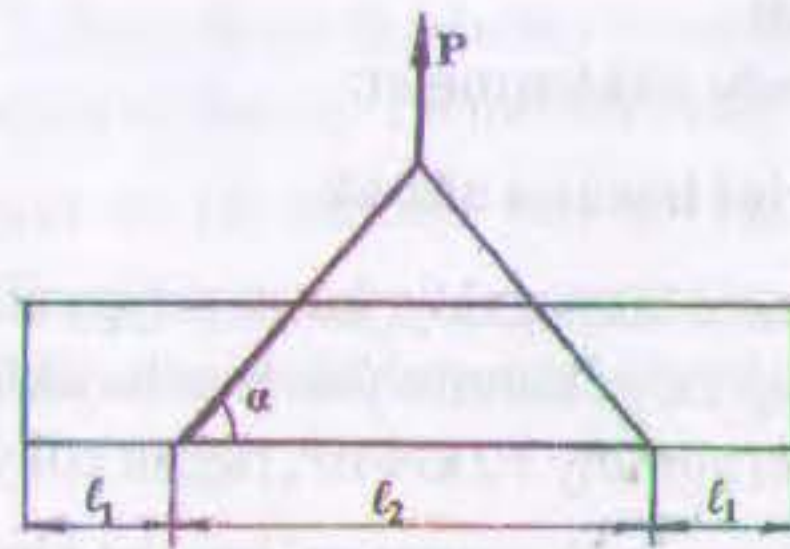
9.2-nji surat

9.2. Uzynlygy $\ell = 1,8 \text{ m}$ bolan çöýun AB steržen, 00 wertikal okuň daşynda hemişelik burç tizligi bilen aýlanýar (surata seret). Eger çöýunüň göwrüm agramy $\gamma = 74 \text{ kN/m}^3$, süýnmä rugsat edilyän dartgynlyk $[\sigma] = 4 \text{ kN/sm}^2$ bolsa, sterženiň aňryçäk minutdaky aýlaw sanyny kesgitlemeli. Eger $E = 1,6 \cdot 10^4 \text{ kN/sm}^2$, aýlaw sany 1000 aýl/min bolsa, sterženiň uzalmasyny kesgitlemeli.

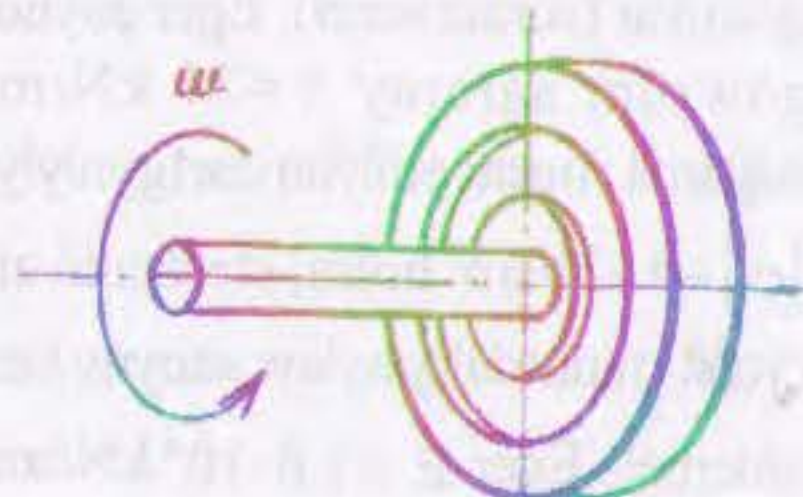


9.3-nji surat

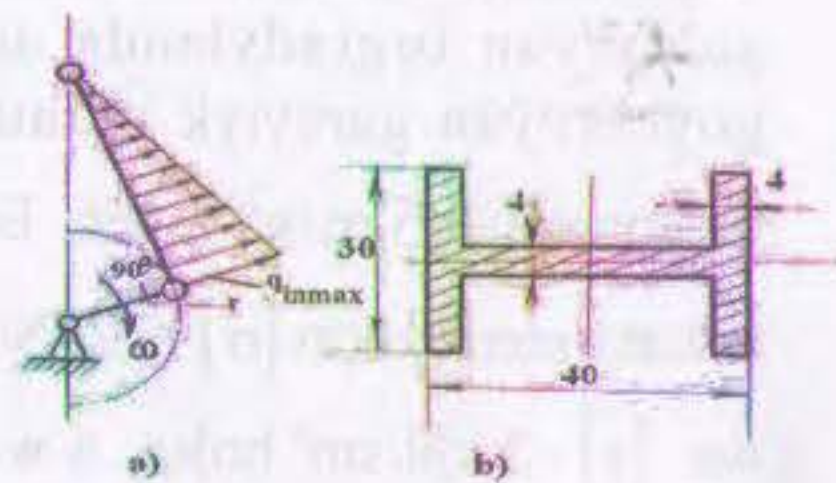
9.3. Göterijiniň garşylyk agramy 42 kN deň (surata seret). Göterijini galdyrýan togtadylanda aşak goýberilýän garşylyk agramyň tizlenmesi $1,5 \text{ m/s}^2$ -a deň. Eger boltuň materialy üçin $[\sigma] = 3,2 \text{ kN/sm}^2$ we $[\tau] = 2 \text{ kN/sm}^2$ bolsa, A we B garşylyk agramynyň boltunyň diametrini kesgitlemeli. Boltlaryň sany A-iki, B-bir.



9.4-nji surat



9.5-nji surat

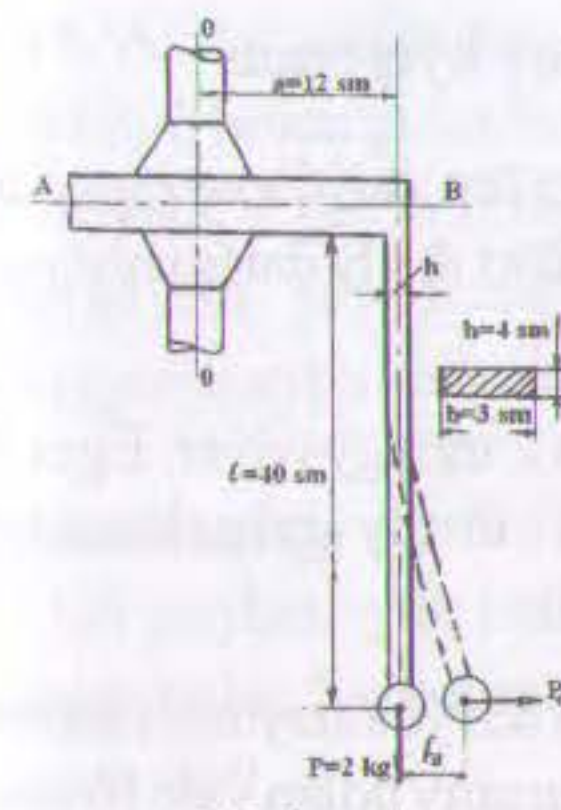


9.6-nji surat

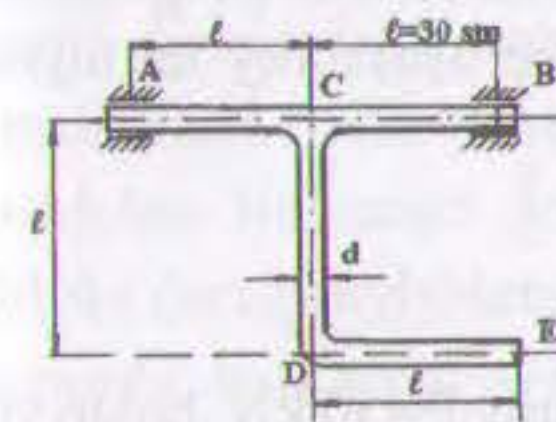
9.4. Tizlenmesi $a=6 \text{ m/s}^2$ bolan beton balka kran bilen ýokary göterilýär (surata seret). Eger balkanyň kese kesigi – taraplary $b=20 \text{ sm}$ bolan kwadrat, betonyň udel agramy $\gamma=24 \text{ kN/m}^3$ bolan balkanyň dartgynlylygyny kesgitlemeli. Polat urganyň kese kesiginiň meýdany $A=1,27 \text{ sm}^2$, $\alpha=45^\circ$, $\ell_1=1 \text{ m}$, $\ell_2=4 \text{ m}$ bolsa, urgandaky dartgynlylygy kesgitlemeli.

9.5. Massasynyň inersiýa radiusy $i=600 \text{ mm}$ we massasy $m=200 \text{ kg}$ (surata seret) bolan mahowik $\omega=75,4 \text{ rad/s}$ burç tizligi bilen aýlanýar. Deňölçegli haýallanýan togtamada mahowik 20 aýlawdan soň durýar. Mahowik oturdylan walyň diametri $d=50 \text{ mm}$ bolsa, walyň iň uly galtaşma dartgynlylygyny kesgitlemeli.

9.6. Şatuny egýän inersiýa güýjüň depginliligi q_m we gysýan güýç $P_{90}^0=0,65 P_{\max}$ bolsa, şatundaky iň uly dartgynlylygy kesgitlemeli. Kriwoşipiň radiusy $r=75 \text{ mm}$, şatunyň uzynlygy $\ell=250 \text{ mm}$, aýlaw ýygylgy $n=2800 \text{ aýl/min}$, kese-kesiginiň ölçegleri suratda görkezilen. Şatunyň materialy – polat 45 $\Gamma 2$, rugsat edilyän dartgynlylyk $[\sigma]=0,25$, $\sigma_b=850 \text{ MPa}$, $P_{\max}=30 \text{ kN}$.

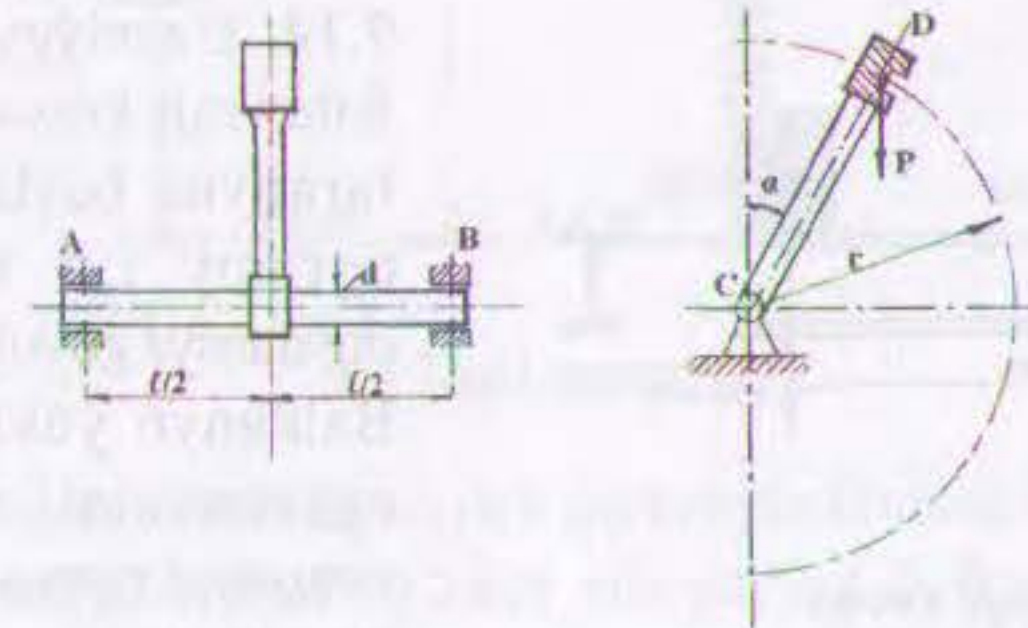


9.7-nji surat



9.8-nji surat

9.9. Nusgany urga synag edýän AB kopýor okuň daşynda aýlanýan ÇD maýatnikden ybarat. Synagdan öň maýatnik suratda görkezilişi ýaly ýagdaýda saklanýar we agram güýjüniň täsirinden aşak gaçmaga mejbur edilyär. Maýatnikiň inersiýa güýjünden AB okda döreyän egilmeden iň uly normal dartgynlylygy kesgitlemeli. Berlen: $P=0,25 \text{ kN}$, $r=0,75 \text{ m}$, $\ell=0,25 \text{ m}$, $d=2 \text{ sm}$, $\alpha=0$.



9.9-nji surat

9.7. Regulýator (sazlaýjy) 00 okuň daşyndan hemişelik burç tizligi bilen aýlanýar (surata seret). Regulatoryň aňryçäk aýlaw sanyny tapmaly we eger $[\sigma]=18 \text{ kN/sm}^2$ bolsa, şol aýlaw sanda BÇ polat sterženiň erkin tarapynyň egrelmesini kesgitlemeli. AB steržen absolýut gaty diýip hasap etmeli. BÇ sterženiň inersiýa güýjüni hasaba almaly däl.

9.8. Tegelek kese kesikli ($d=18 \text{ mm}$) döwürük brus AB okuň daşyndan endigan aýlanýar. Eger $\gamma=78 \text{ kN/m}^3$, $[\sigma]=10 \text{ kN/sm}^2$ bolsa, iň uly rugsat edilyän burç tizligini kesgitlemeli.

9.2. Urguda dartgynlylyk we durkuny üýtgetme

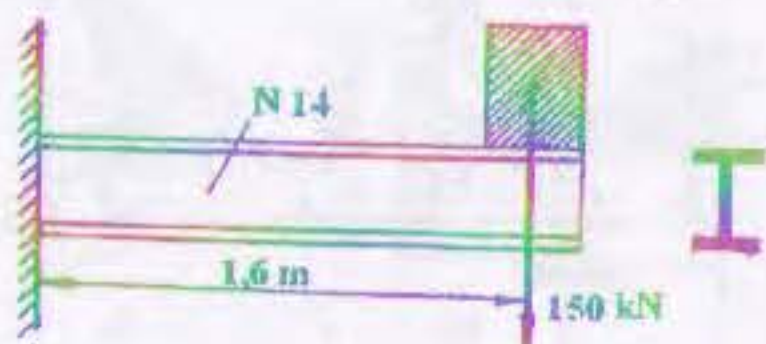
9.10. Diametri 25 mm we uzynlygy 1,5 m polat steržen duýdansyz goýlan hemişelik güýç $P=25$ kN bilen dartylýar. Steržendäki in uly dartgynlylygy we durkuny üýtgetmäni kesgitlemeli.

9.11. Statiki goýlan P güýç bilen wertikal steržen 2 mm gysylýar. Eger P ýük 1 mm beýiklikden gaçýan bolsa, sterženiň in uly gysgalmasyny kesgitlemeli.

9.12. Uzynlygy 5 m bolan tegelek kesikli polat steržen ýokarsyndan asylan we aşaky tarapynda halka çykyntgysy bar. 8 kN agramy bolan ýük 16 mm beýiklikden sterženiň boýuna gaçýar we bu ýüki çykyntgy saklaýar. Rugsat edilýän dartgynlylyk 16 kN/sm^2 bolsa, sterženiň diametrini kesgitlemeli. Urguda dartgynlylygy hasaplamagyň takyk we aşakdaky takmynan

formulasyny $\sigma_d = \sigma_{st} \sqrt{\frac{2H}{\Delta_{st}}}$ peýdalanmaly:

9.13. Polat trosuň (urganyň) bir tarapynda agramy $P=50$ kN bolan ýük berkidilen, beýleki tarapyň lebyodkanyň barabanyňa oralan ýük $v = 1,6$ m/s hemişelik tizlik bilen aşak goýberilýär. Lebyodka birdenkä togtadylanda, ýük şol bada saklanýar. Saklanan pursatda trosuň ýük bilen lebyodkanyň arasyndaky uzynlygy $\ell = 240$ m deň. Trosyň kese kesiginiň meýdany $A=10 \text{ sm}^2$. Trosuň agramyny hasaba alyp we hasaba almazdan, in uly dartgynlylyklary kesgitlemeli.



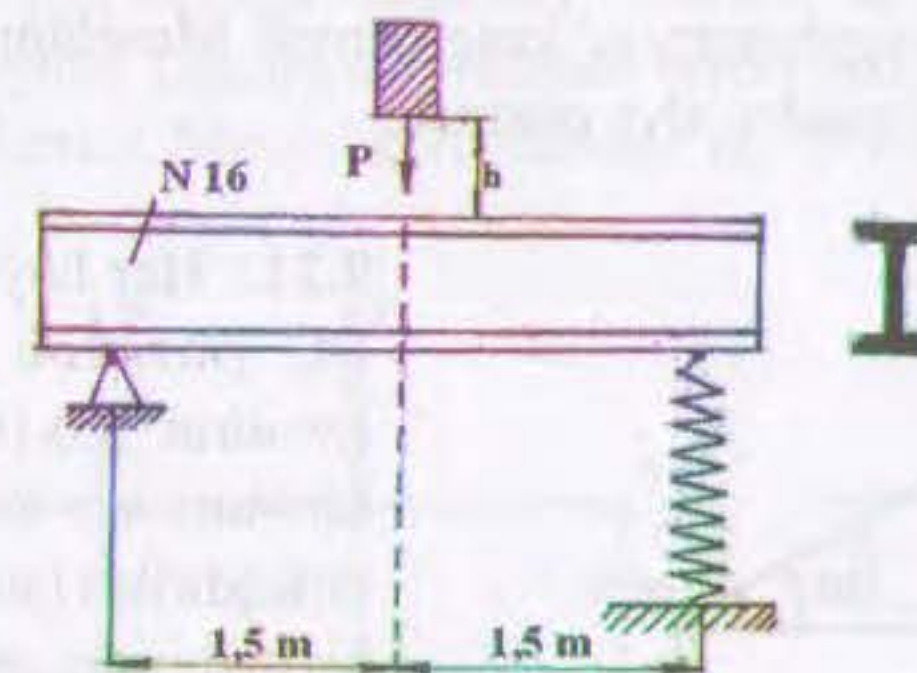
9.14-nji surat

9.14. Uzynlygy $\ell=1,6$ m bolan ikitawraly konsol balkanyň erkin tarapyna başlangyç tizliksiz, agramy 1,5 kN bolan ýük duýdansyz goýulýar (surata seret). Balkanyň ýüküň aşagyndaky egrelmesini we berkidilen tarapyň normal dartgynlylygyny kesgitlemeli.

9.15. Aýlaw tizligi $n=150$ aýl/min, diametri $D=600$ mm we galyňlygy $t=40$ mm bolan polat bitewi disk diametri $d=100$ mm bolan polat walda oturdylan. Eger wal diskden $\ell=2,5$ m uzaklykdaky kesikde birdenkä togtadylsa, towlanmadan walyň kese kesigindäki in uly galtaşma dartgynlylygyny kesgitlemeli. Walyň massasyny hasaba almaly däl.

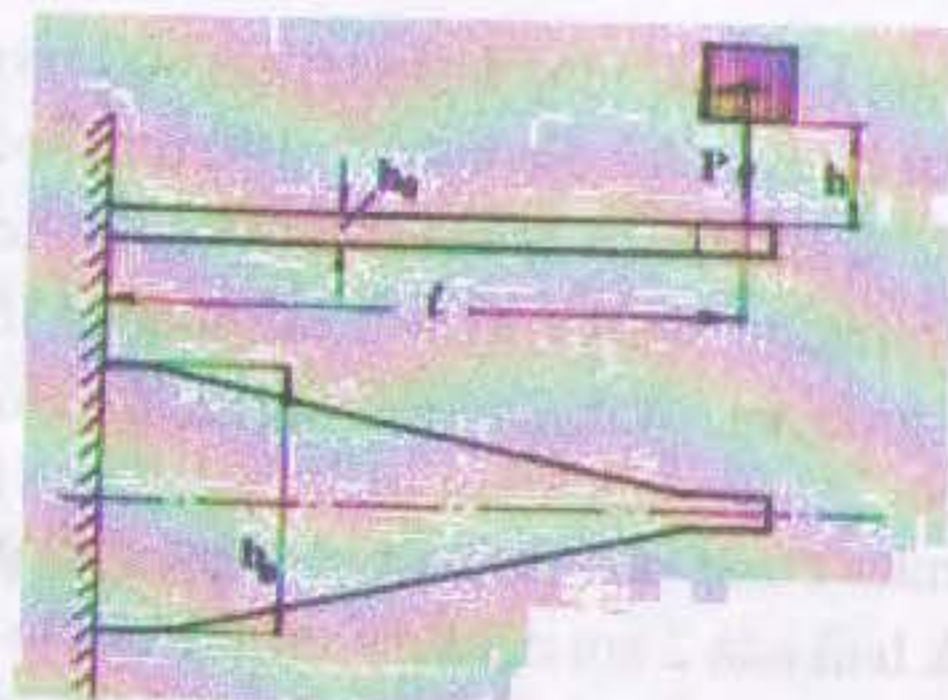
9.16. Ahyrlary şarnirli berkidilen balkanyň direg aralygynyň ortasynda 45 kN goýlan, ýük balkada 2 sm egrelme döredýär. Şu balka 5 kN ýük gaçýan bolsa, 2 sm-den uly bolmadyk egrelme döredýän ýüküň in uly tizligi näçe bolar?

9.17. Uzynlygy 3 m bolan 16-njy belgili ikitawraly balkanyň bir tarapy gaty şarnirli diregde berkidilen. Beýleki tarapy simiň diametri 20 mm, sarymyň orta diametri 10 sm we sarymynyň sany 10-a deň bolan hyr şekilli pružinde oturdylan. Balkanyň $[\sigma]=16 \text{ kN/sm}^2$, pružiniň $[\tau]=20 \text{ kN/sm}^2$ rugsat edilýän dartgynlylyklary bolanda, agramy 2 kN ýük nähili beýiklikden gaçanda balkanyň we pružiniň dartgynlylyklary rugsat edilýän dartgynlylyklardan ýokary bolmaz?



9.17-nji surat

9.18. Hemme kesiklerinde deň garşylyk görkezýän konsolyň erkin tarapyna $h=20$ sm bolan beýiklikden $P=0,2$ kN ýük gaçýar. Balkanyň massasyny hasaba alyp, konsolyň ahryndaky egrelmesini we in uly dartgynlylygyny hasaplamaly.

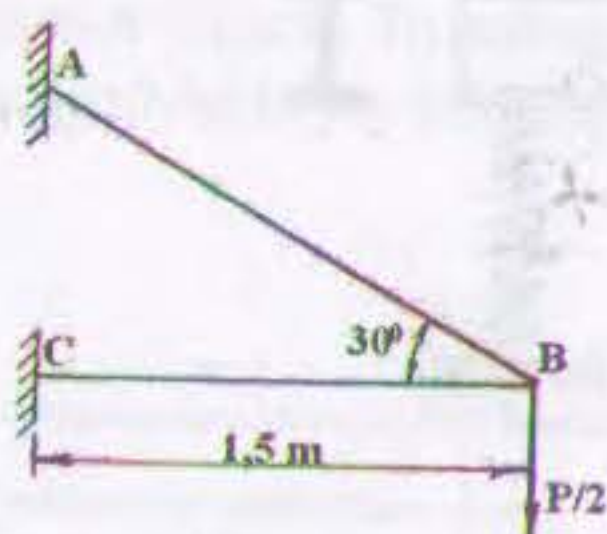


9.18-nji surat

9.19. Eger sterženiň kese kesiginiň meýdanyny iki gezek azaltsaň, h beýiklikden gaçýan ýük sterženi boý urga sezewar edýän bolsa, steržende döreyän dartgynlyk näçe göterim köpeler?

9.3. Yrgyldydan dartgynlyk we durkuny üýtgetme

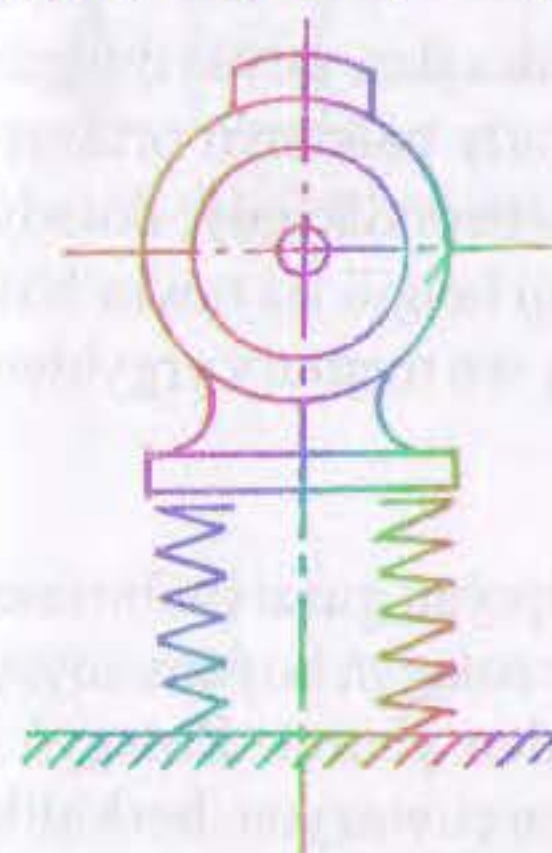
9.20. Uzynlygy 80 sm we diametri 5 sm, 100 kN boýuna gysýan güýç bilen ýüklenen tegelek kesikli polat diregiň boý hususy yrgyldysynyň periodyny t_0 we ýygylgyny ω_0 kesgitlemeli. Meseläni diregiň massasyny hasaba alman we hasaba alyp çözmeli.



9.21-nji surat

9.21. Her haýsy iki agaç AB we BC pürsden ýerine ýetirilen kwadrat $10 \times 10 \text{ sm}^2$ kese kesikli biri-biri we diwar bilen şarnirli birleşdirilen (surata seret) iki ABC kronşteýne agramy $P=100 \text{ kN}$ bolan elektrodwigatel berkidilen. Hususy wertikal yrgyldynyň periodyny we yrgyldynyň ýygylgyny kesgitlemeli. $E=10^3 \text{ kN/sm}^2$.

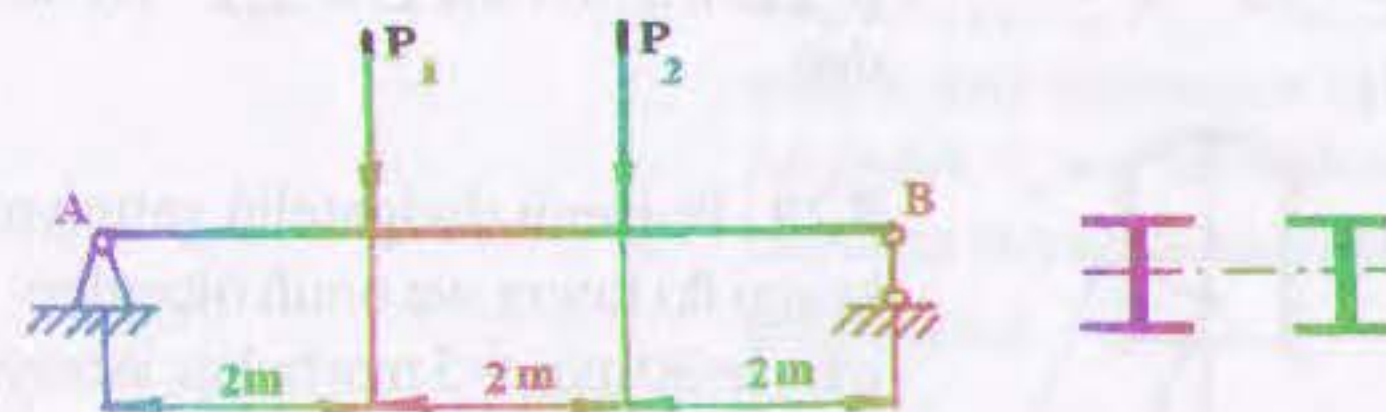
9.22. Kronşteýne berkidilen elektrodwigatel (öňki meselä seret) 1300 aýl/min ýygylgıda aýlanýar. BÇ sterženiň okuna perpendikulýar tekizlikde aýlanýan dwigateliň bölekleriniň doly däl deňagramlaşmagy netijesinde 1,6 kN deň merkezden daşlaşýan inersiýa güýçleri döreyär. Ulgamyň diňe wertikal mejbury yrgyldysyna seredip, kronşteýniň pürslerindäki yrgyldynyň ösme koeffisiýentini, dinamiki koeffisiýentini we iň uly normal dartgynlygynyň ululygyny hasaplamaly. Garşylyk güýçleri hasaba almaly däl.



9.23-nji surat

9.23. Massasy $m=1 \text{ kN}$ bolan elektrodwigatel dört silindrik hyr şekilli pružinde oturdylan. Pružiniň häsiýetnamalary: $d=12 \text{ mm}$, $D=10 \text{ mm}$, sarymyň sany $n=7$ (surata seret). Elektrodwigateliň aýlaw ýygylgyny $n=240 \text{ aýl/min}$. Rotoryň deňagramlaşmadyk massasy $m_0=10 \text{ kg}$, massanyň eksentrisiteti $r=0,02 \text{ m}$ deň. Ulgamy rezonansa barlamaly, iň uly galtaşma dartgynlygy we pružiniň çökmesini kesgitlemeli.

9.24. Uzynlygy $\ell=6 \text{ m}$, inersiýa momenti $I_x=945 \text{ sm}^4$ iki ikitawraly balkada oturdylan iki maşynlar ulgamynyň (surata seret) hususy yrgyldysynyň ýygylgyny kesgitlemeli. Maşynlaryň massasy: $m_1=500 \text{ kg}$, $m_2=1500 \text{ kg}$.

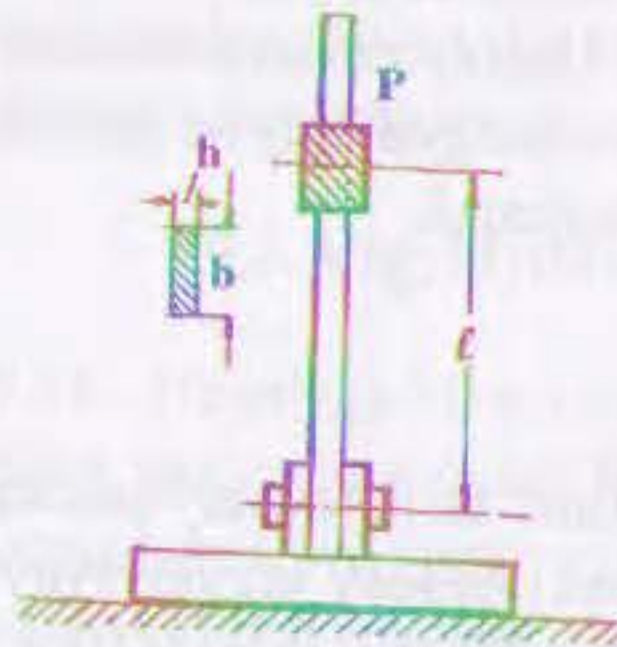


9.24-nji surat

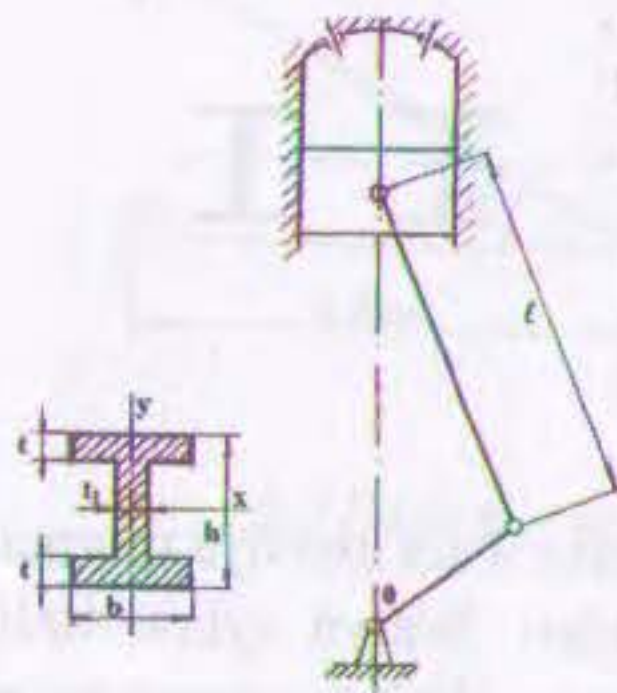
9.25. Uzynlygy $\ell=1,5 \text{ m}$, diametri $d=5 \text{ sm}$ bolan wala inersiýa momenti $I_m=0,31 \text{ kN} \cdot \text{sm} \cdot \text{s}^2$ bolan mahowik oturdylan. Walyň aýlaw tizligi 950 aýl/min-a deň. Waly rezonansa barlamaly. Walyň agramyny we mahowigiň agramynyň döredýän egrelmesini hasaba almaly däl.

9.26. Wagonyň resory sarymyň orta radiusy $R=60$ mm, pružiniň siminiň radiusy $r=15$ mm, sarymyň sany $n=8$ deň bolan sekiz sany silindr görnüşli spiral pružinden durýar; simiň materialynyň süýşmede maýyşgaklyk moduly $G=9,5 \cdot 10^3$ kN/sm², wagonyň gabynyň agramy $Q=50$ kN, peýdaly ýük $S=3,5$ kN. Relsleriň sepgitleriniň arasy $\ell=8$ m. Wagonyň rezonans hadysasynyň boljak hereketiniň kritiki tizligini kesgitlemeli.

9.27. Agramy $Q=25$ kN bolan we $n=540$ aýl/min aýlaw edýän dwigatel, uzynlygy $\ell=3,5$ m deň bolan iki daýanç nokatly balkanyň ortasynda berkidilen. Dwigatel $P_1=P \sin \omega t$ deň bolan wertikal periodiki güýç döredýär. Bu ýerde $P=8$ kN. Eger balkanyň kesigi 27-nji belgili iki tawra bolsa, howply kesikdäki iň uly dinamiki dartgynlygy we mejbury yrgyldynyň amplitudasyny tapmaly. $[\sigma]=13$ kN/sm² deň.



9.28-nji surat

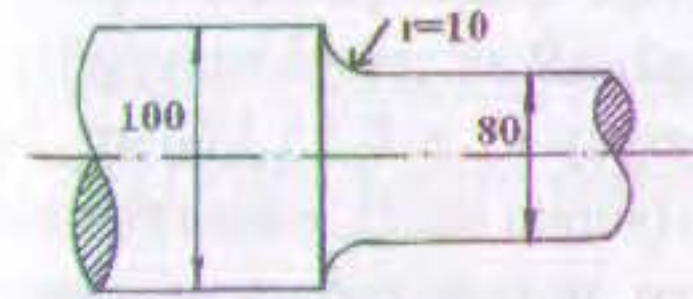


9.29-nji surat

9.28. Titremäni ölçeyän gural (wibrometr) polat zolakdan we zolagyň boýuna süýşýän $P=0,001$ kN ýükden ybarat. Zolagyň bir tarapy abzalyň çarçuwasyna berkidilen. Yrgyldyny ýazmak üçin wibrometr titreyän konstruksiya berkidilýär, ýük bolsa zolak ýük bilen konstruksiya bilen bilelikde güýçli titröp başlar ýaly ℓ aralykda berkidilýär. Eger $\ell=20$ sm bolsa, konstruksiýanyň ýygylgyny kesgitlemeli. Zolagyň Kese kesiginiň ölçegleri: $b=5$ sm, $h=0,3$ sm, $E=2,2 \cdot 10^4$ kN/sm²-a deň.

9.29. Porşenli dwigateliň şatunynyň kese kesigi iki tawra we onuň ölçegleri: $h=50$ mm, $b=30$ mm, $t=5$ mm bolup, inersiya güýjüň täsirinden yranma tekizliginde kese yrgyldy ýagdaýynda bolýar. Şatunyň hususy yrgyldysynyň ýygylgyny we periodyny, şonuň ýaly-da dwigateliň kritiki aýlaw sanyny kesgitlemeli.

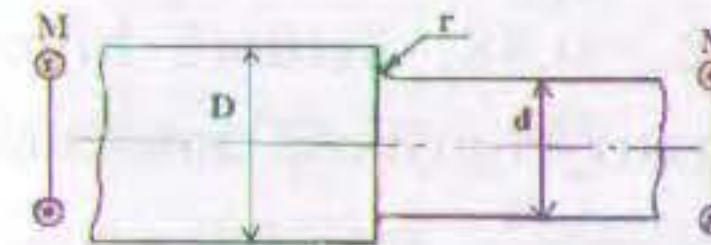
9.4. Dowamly ýüklenmeler



9.30-nji surat

9.30. Aýlanýan tegelek basgançakly wal hemişelik moment M bilen egilýär. Uglerodly polatdan ýasalan walyň berklik çägi $\sigma_b=45$ kN/sm² we egilmede çydamlylyk çägi $\sigma_{-1}^{\ell}=22$ kN/sm² (simmetriýa sikli). Walyň diametrleri $D=100$ mm we $d=80$ mm; galteliň radiusy $r=10$ mm (surata seret).

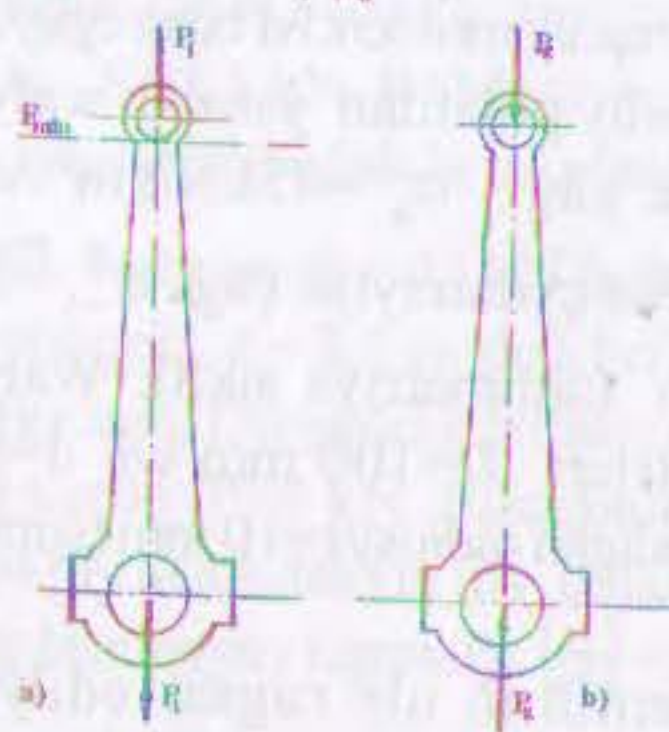
Momentiň iň uly rugsat edilyän ululygyny kesgitlemeli. Şaýyň berkliginiň ätiýaçlyk koeffisiýenti onuň çydamlylyk çäğine bolan gatnaşygy $k=2$.



9.31-nji surat

9.31. $M=0,64$ kN·m moment bilen ýüklenen basgançakly wal (surata seret) hemişelik burç tizligi bilen aýlanýar. Walyň ölçegleri: $D=50$ mm; $d=40$ mm; $r=2$ mm; materialy-legirlenen polat; $\sigma_b=75$ kN/sm²; $\sigma_a=42$ kN/sm²; $\sigma_{-1}=32,5$ kN/sm² walyň üsti ýylmanan (şlifowka). Akyjylyk η_a we döwürme η_d çägi boýunça ätiýaçlyk koeffisiýentlerini kesgitlemeli.

9.32. Üýtgeýän egilme bilen towlanma sezewar bolýan diametleri $d=40$ mm we $D=50$ mm basgançakly walyň berklige ätiýaçlyk koeffisiýentini kesgitlemeli. Galteliň radiusy $r=2$ mm, normal dartgynlylyk $\sigma_{\max}=5$ kN/sm², $\sigma_{\min}=-5$ kN/sm² çenli üýtgeýär, galtaşma dartgynlylyk - $\tau_{\max}=4$ kN/sm², $\tau_{\min}=2$ kN/sm² walyň materialy uglerodly polat $\sigma_b=50$ kN/sm², $\sigma_{-1}=22$ kN/sm², $\tau_{-1}=12$ kN/sm², $\sigma_a=30$ kN/sm², $\sigma_{-1}=18$ kN/sm², $\psi_{\sigma}=0,05$, $\psi_{\tau}=0$.



9.33-nji surat

9.33. Polat 45-den ýasalan awtomobil dwigateliniň şatunynyň statiki we sikl berkliginiň ätiýaçlyk koeffisiýentini kesgitlemeli. Şatun-porşen toparynyň inersiýa güýji P we gazyň basyş güýji P_g , gazyň basyşy $P_z = 0,55 \text{ kN/sm}^2$ bilen ýüklenen (surata seret). Silindriň diametri $D=78 \text{ mm}$, porşen toparynyň massasy $m_p=0,005 \text{ kN}$, şatunynyň ýokarky böleginiň massasy $m_{y.s}=0,002 \text{ kN}$. Kriwoşipiň

radiusy $r=40 \text{ mm}$, $\lambda = \frac{r}{\ell_s} = 0,28$,

áýlaw ýygylgy $n_{\max} = 6000 \text{ aýl/min}$, şatunynyň iň kiçi kesigi suratda görkezilen. Şatunynyň başjagazyndan sterženine geçýän ýeriniň konsentrasiýa koeffisiýenti $K_\sigma=1,27$, masştab faktory ($h=23 \text{ mm}$ üçin), $\varepsilon_\sigma=0,88$, üstüniň hiliniň koeffisiýenti (ýel goýberip tämizlemek) $\beta_\sigma=1,3$.

9.34. Walyň kesigi sponka (pahna) dilkaw bilen gowşadylan we howply kesiginde pulşirleýji sikl boýunça üýtgeýän iň uly towlanma moment $M_l=64 \text{ kN sm}$ we simmetriýa sikli boýunça üýtgeýän egme moment $M_e=80 \text{ kN sm}$ täsir edýär. Walyň diametri $d=50 \text{ mm}$, walyň materialy—polat, onuň mehaniki häsiýetnamalary: $\sigma_{-1} = 28 \text{ kN/sm}^2$, $\sigma_a = 35 \text{ kN/sm}^2$. Howply kesik üçin berklige ätiýaçlyk koeffisiýentini kesgitlemeli.

Jogaplar, görkezmeler, çözüwler

I bap. Süýnme we gysylma

1.1. $P=256 \text{ kN}$. Berklik şertinden $P=[\sigma] \cdot A = 1 \cdot 256 = 256 \text{ kN}$.

1.2. $d=213 \text{ mm}$. Çatyny dartýan güýç

$$P = \sigma \cdot A_\varphi = 10 \cdot \frac{3,14 \cdot 2,5^2}{4} = 49,06 \text{ kN}.$$

Berklik şertinden epenegiň meýdany:

$$A_e = \frac{P_\varphi}{\sigma_e} = \frac{49,06}{0,14} = 350,45 \text{ sm}^2$$

ýa-da $A_e = \frac{\pi}{4}(d^2 - d_\varphi^2)$, onda

$$d^2 = \frac{4A_e}{\pi} + d_\varphi^2 = \frac{4 \cdot 350,45}{3,14} + 2,5^2 = 452,68,$$

$$d = 21,28 \text{ sm} \approx 213 \text{ mm}.$$

1.3. $\sigma = 10 \text{ kN/sm}^2$. Zolagyň gowşadylan kesiginiň meýdany

$$A = 20 \cdot 1 - 3 \cdot 1 \cdot 2 = 14 \text{ sm}^2,$$

$$\text{orta dartgynlylygyň ululygy } \sigma = \frac{P}{A} = \frac{140}{14} = 10 \text{ kN/sm}^2.$$

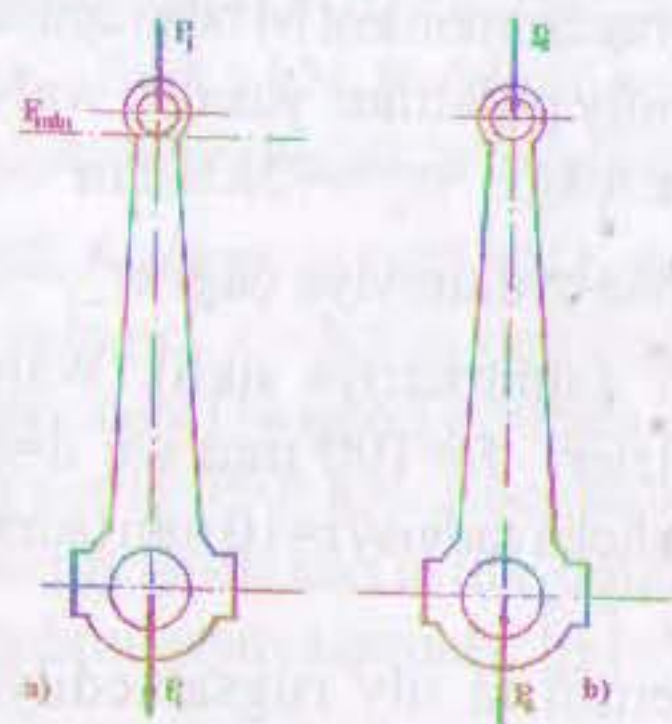
1.4. $a=46 \text{ sm}$. Berklik şertinden $A = \frac{Q}{[\sigma]} = \frac{60}{0,09} = 666,7 \text{ sm}^2$.

Iki tawranyň diwara galtaşýan meýdany $A = b \cdot a$, kesgitlenen sortdan 30 a belgili iki tawra üçin,

$$\text{onda } b \cdot a = 666,7, \quad a = \frac{666,7}{14,5} = 46 \text{ sm}.$$

1.5. $d_p=0,71 \text{ mm}$. Meseläniň şerti boýunça $\Delta \ell_p =$ (ne).

öredýär.



9.33-nji surat

9.33. Polat 45-den ýasalan awtomobil dwigateliniň şatunynyň statiki we sikl berkliginiň ätiýaçlyk koeffisiýentini kesgitlemeli. Şatun-porşen toparynyň inersiýa güýji P we gazyň basyş güýji P_z , gazyň basyşy $P_z = 0,55 \text{ kN/sm}^2$ bilen ýüklenen (surata seret). Silindriň diametri $D=78 \text{ mm}$, porşen toparynyň massasy $m_p=0,005 \text{ kN}$, şatunynyň ýokarky böleginiň massasy $m_{y.s}=0,002 \text{ kN}$. Kriwoşipiň

radiusy $r=40 \text{ mm}$, $\lambda = \frac{r}{\ell_s} = 0,28$,

aýlaw ýygylgy $n_{\max} = 6000 \text{ aýl/min}$, şatunynyň iň kiçi kesigi suratda görkezilen. Şatunynyň başjagazyndan sterženine geçýän ýeriniň konsentrasiýa koeffisiýenti $K_\sigma=1,27$, masştab faktory ($h = 23 \text{ mm}$ üçin), $\varepsilon_\sigma=0,88$, üstüniň hiliniň koeffisiýenti (ýel goýberip tämizlemek) $\beta_\sigma=1,3$.

9.34. Walyň kesigi şponka (pahna) dilkaw bilen gowşadylan we howply kesiginde pulşirleýji sikl boýunça üýtgeýän iň uly towlanma moment $M_t=64 \text{ kN sm}$ we simmetriýa sikli boýunça üýtgeýän egme moment $M_e=80 \text{ kN sm}$ täsir edýär. Walyň diametri $d=50 \text{ mm}$, walyň materialy-polat, onuň mehaniki häsiýetnamalary: $\sigma_{-1} = 28 \text{ kN/sm}^2$, $\sigma_a = 35 \text{ kN/sm}^2$. Howply kesik üçin berklige ätiýaçlyk koeffisiýentini kesgitlemeli.

Jogaplar , görkezmeler, çözüwler

I bap. Süýnme we gysylma

1.1. $P=256 \text{ kN}$. Berklik şertinden $P = [\sigma] \cdot A = 1 \cdot 256 = 256 \text{ kN}$.

1.2. $d=213 \text{ mm}$. Çatyny dartýan güýç

$$P = \sigma \cdot A_\varphi = 10 \cdot \frac{3,14 \cdot 2,5^2}{4} = 49,06 \text{ kN}.$$

Berklik şertinden epenegiň meýdany:

$$A_e = \frac{P_\varphi}{\sigma_e} = \frac{49,06}{0,14} = 350,45 \text{ sm}^2$$

ýa-da $A_e = \frac{\pi}{4} (d^2 - d_\varphi^2)$, onda

$$d^2 = \frac{4A_e}{\pi} + d_\varphi^2 = \frac{4 \cdot 350,45}{3,14} + 2,5^2 = 452,68,$$

$$d = 21,28 \text{ sm} \approx 213 \text{ mm}.$$

1.3. $\sigma = 10 \text{ kN/sm}^2$. Zolagyň gowşadylan kesiginiň meýdany

$$A = 20 \cdot 1 - 3 \cdot 1 \cdot 2 = 14 \text{ sm}^2,$$

$$\text{orta dartgynlylygyň ululygy } \sigma = \frac{P}{A} = \frac{140}{14} = 10 \text{ kN/sm}^2.$$

1.4. $a=46 \text{ sm}$. Berklik şertinden $A = \frac{Q}{[\sigma]} = \frac{60}{0,09} = 666,7 \text{ sm}^2$.

Iki tawranyň diwara galtaşýan meýdany $A = b \cdot a$, $b=14,5 \text{ sm}$ – kesgitlenen sortdan 30 a belgili iki tawra üçin,

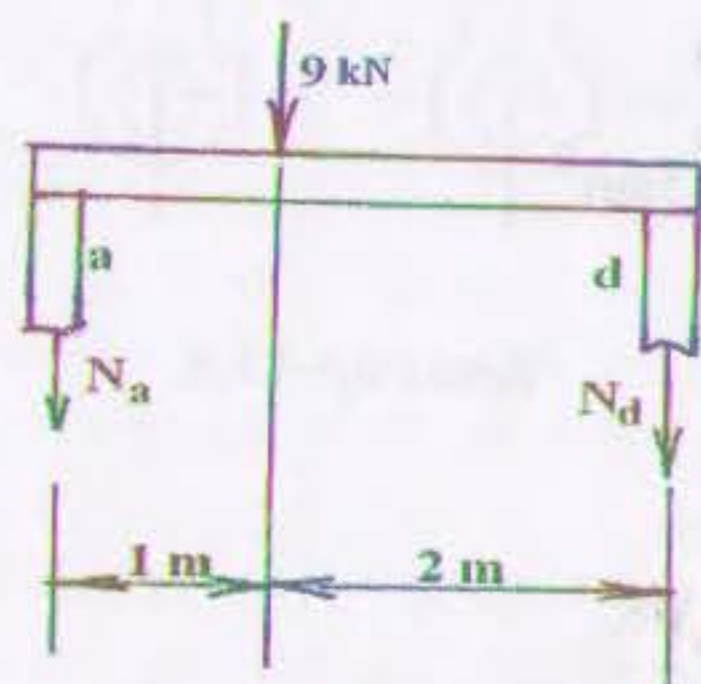
$$\text{onda } b \cdot a = 666,7, \quad a = \frac{666,7}{14,5} = 46 \text{ sm}.$$

1.5. $d_p=0,71 \text{ mm}$. Meseläniň şerti boýunça $\Delta \ell_p = \Delta \ell_m$;

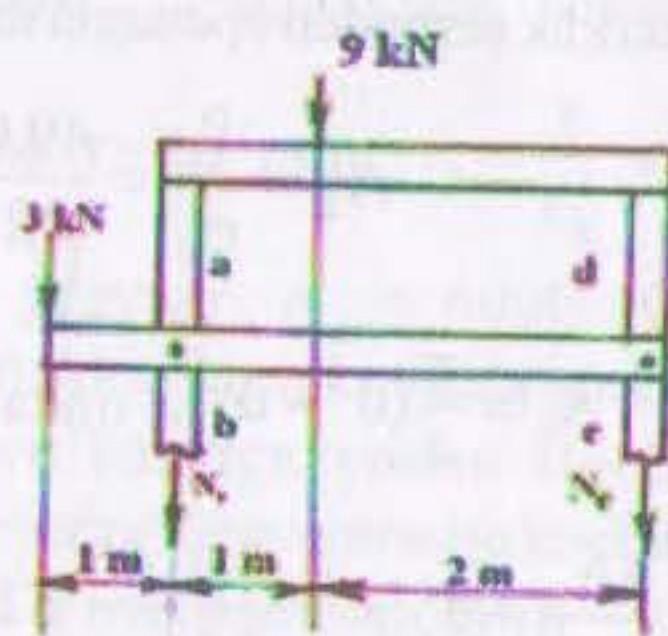
$$\text{onda } d_p = \sqrt{\frac{E_m}{E_p}} \cdot d_m = \sqrt{\frac{10^4}{2 \cdot 10^4}} \cdot 0,1 = 0,071 \text{ sm} = 0,71 \text{ mm}.$$

1.6. $\sigma_a = -0,06 \text{ kN/sm}^2$, $\sigma_b = -0,1 \text{ kN/sm}^2$, $\sigma_c = -0,085 \text{ kN/sm}^2$, $\sigma_e = -0,02 \text{ kN/sm}^2$; $\sigma_f = -0,065 \text{ kN/sm}^2$; $\sigma_d = -0,03 \text{ kN/sm}^2$, Kesmek usulyny ulanyp, ilki direglerdäki içki güýçleri, soň bolsa degişli dartgynlyklaryny kesgitleýäris.

ad kesik



be kesik



$$1) \sum M_a = N_d \cdot 3 + 9 \cdot 1 = 0, \\ N_d = -3 \text{ kN};$$

$$\sigma_d = -\frac{3}{100} = -0,03 \text{ kN/sm}^2;$$

$$2) \sum M_d = -N_a \cdot 3 - 9 \cdot 2 = 0, \\ N_a = -6 \text{ kN},$$

$$\sigma_a = -\frac{6}{100} = -0,06 \text{ kN/sm}^2$$

$$1) \sum M_b = 0, \\ N_e \cdot 3 + 9 \cdot 1 - 3 \cdot 1 = 0,$$

$$N_e = -\frac{6}{3} = -2 \text{ kN},$$

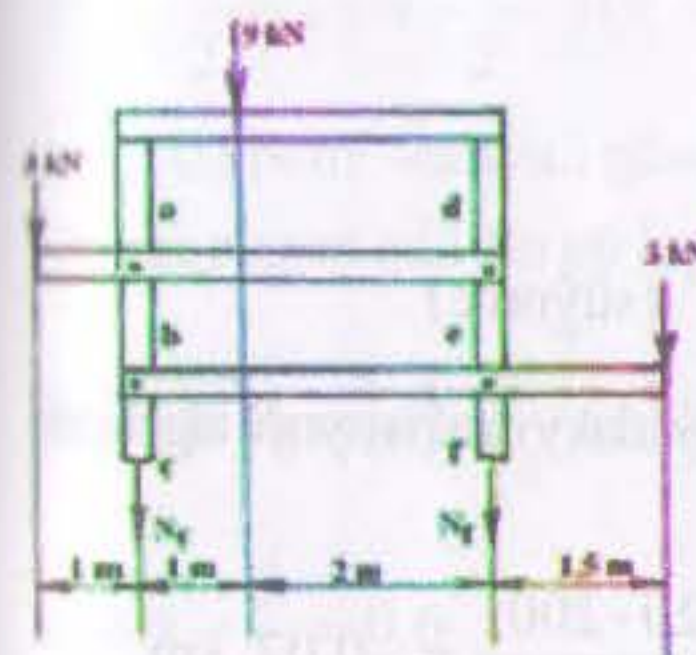
$$\sigma_e = -\frac{2}{100} = -0,02 \text{ kN/sm}^2;$$

$$2) \sum M_e = 0, \\ N_b \cdot 3 + 9 \cdot 2 + 3 \cdot 4 = 0,$$

$$N_b = -\frac{30}{3} = -10 \text{ kN},$$

$$\sigma_b = -\frac{N_b}{100} = -\frac{10}{100} = -0,1 \frac{\text{kN}}{\text{sm}^2}$$

cf kesik



1.6-njy surat

$$1) \sum M_c = 0, \\ N_f \cdot 3 + 9 \cdot 1 - 3 \cdot 1 + 3 \cdot 4,5 = 0,$$

$$N_f = -\frac{19,5}{3} = -6,5 \text{ kN},$$

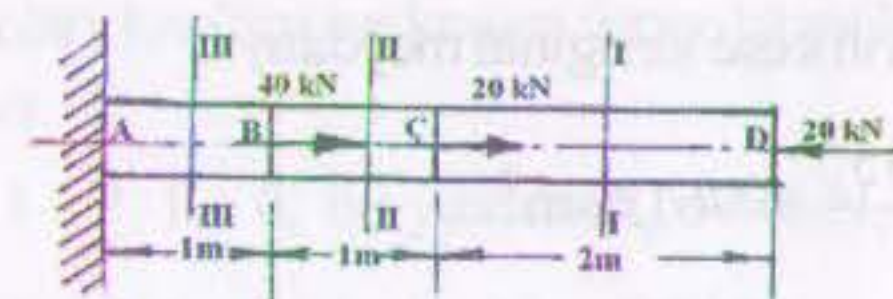
$$\sigma_f = -\frac{6,5}{100} = -0,065 \text{ kN/sm}^2$$

$$2) \sum M_f = 0, \\ N_c \cdot 3 + 9 \cdot 2 + 3 \cdot 4 - 3 \cdot 1,5 = 0$$

$$N_c = -\frac{25,5}{3} = -8,5 \text{ kN},$$

$$\sigma_c = \frac{-8,5}{100} = -0,085 \text{ kN/sm}^2.$$

$$1.7. \sigma_{AB} = 4 \text{ kN/sm}^2, \sigma_{BC} = 0, \sigma_{CD} = -2 \text{ kN/sm}^2, \Delta l = 0.$$



1.7-nji surat

DÇ bölegiň I-I kesiginde N_1 boý güýji döredýär. I-I kesiginiň bölünip alynýan sag böleginiň deňagramlylygyna seredýäris: $\sum X = -N_1 - 20 = 0$, bu ýerden $N_1 = -20 \text{ kN}$ (gysylma). BÇ bölegiň II-II kesigindäki N_2 boý güýji deňagramlylygyň deňlemesinden tapýarys:

$\sum X = -N_2 - 20 + 20 = 0$, bu ýerden $N_2 = 0$. Şonuň ýaly-da BA bölegiň III-III kesiginde $\sum X = -N_3 - 20 + 20 + 40 = 0$, $N_3 = 40 \text{ kN}$ (süýnme). Sterženiň hemme bölekleriniň kese kesiginde normal dartgynlyk döredýär.

$$\text{DÇ böleginde: } \sigma_{\text{CD}} = \frac{N_1}{A} = -\frac{20}{10} = -2 \text{ kN/sm}^2 \text{ (gysylma).}$$

$$\text{ÇB böleginde: } \sigma_{\text{CB}} = \frac{N_2}{A} = -\frac{0}{10} = 0$$

$$\text{BA böleginde: } \sigma_{\text{BA}} = \frac{N_3}{A} = -\frac{40}{10} = 4 \text{ kN/sm}^2 \text{ (süýnme)}$$

Sterženiň doly uzalmasy, onuň her böleginiň aýratynlykdaky uzalmasyňyň algebrailik jemine deň.

$$\text{DÇ bölegiň gysylmasy: } \Delta \ell_{\text{DÇ}} = \frac{N_1 \cdot 200}{EA} = -\frac{20 \cdot 200}{2 \cdot 10^4 \cdot 10} = -0,02 \text{ sm.}$$

ÇB böleginde içki güýç N_2 nola deň, şonuň üçin hem $\Delta \ell_{\text{CB}} = 0$

$$\text{BA bölegindäki uzalma: } \Delta \ell_{\text{BA}} = \frac{N_3 \cdot 100}{EA} = \frac{40 \cdot 100}{2 \cdot 10^4 \cdot 10} = 0,02 \text{ sm.}$$

Sterženiň doly uzalmasy

$$\Delta \ell = \Delta \ell_{\text{DÇ}} + \Delta \ell_{\text{BA}} = -0,02 + 0,02 = 0.$$

1.8. $n=10$ bolt. Silindriň kese kesiginiň meýdany

$$A_s = \frac{\pi D^2}{4} = \frac{3,14 \cdot 35^2}{4} = 961,6 \text{ sm}^2.$$

Gapaga täsir edýän güýç $P = A_s \cdot q = 961,6 \cdot 0,1 = 96,16 \text{ kN}$.

Boltlaryň kese kesiginiň meýdany

$$A = n A_b = n \cdot \frac{\pi d_b^2}{4} = n \cdot \frac{3,14 \cdot 1,8^2}{4} = 2,54n$$

n —berkitmedäki boltlaryň sany

Boltlaryň berklik şerti $\sigma = \frac{P}{A} \leq [\sigma_b]$, onda

$$n = \frac{P}{2,54[\sigma]} = \frac{96,16}{2,54 \cdot 4} = 9,5 \approx 10 \text{ bolt.}$$

1.9. $\ell = 1,88 \text{ m}$. Uzynlygy ℓ deň germewajyň bölegine seredýäris. Bu uzynlyga bir direg düşýär. Seredilýän bölege suwuň gidrostatiki basyşy

$$P = \frac{3 \cdot 3}{2} \gamma \cdot \ell = \frac{3 \cdot 3}{2} \cdot 10 \ell = 45 \ell$$

$\gamma = 10 \text{ kN/m}^3$ —suwuň göwrüm agramy.

Direge rugsat edilýän güýç

$$[P] = [\sigma] A = [\sigma] \cdot \frac{\pi d^2}{4} = 0,2 \cdot \frac{3,14 \cdot 15^2}{4} = 35,33 \text{ kN,}$$

$$\cos \alpha = \frac{3}{5} = 0,6$$

$$\sum M_c = [P] 4 \cos \alpha - P \cdot 1 = 0$$

$$4[P] \cos \alpha = 45 \ell$$

$$\ell = \frac{4[P] \cos \alpha}{45} = \frac{4 \cdot 35,33 \cdot 0,6}{45} = 1,88 \text{ m.}$$

1.10. $\Delta = 0,6 \text{ mm}$. A we B diregleriň içki güýçlerini tapmak üçin hyýaly pikirde olary kesýäris we kesilen ýerine häzirlilikçe bize näbelli güýçleri goýýarys.

$$\sum M_A = N_B \cdot 3 + P \cdot 1 = 0, \text{ bu ýerden } N_B = -40 \text{ kN,}$$

$$\sum M_B = N_A \cdot 3 + P \cdot 1 = 0, \text{ onda } N_A = -80 \text{ kN.}$$

Ortakly steržendäki içki güýçden $N = P = 120 \text{ kN}$ ýüküň asylan nokadynyň aşak ornuny üýtgetmesi

$$\Delta = \Delta \ell_c + \Delta \ell_{\text{dir}},$$

$$\Delta \ell_c = \frac{N_c \ell_c}{E_m A_m} = \frac{120 \cdot 50}{10^4 \cdot 30} = 2 \cdot 10^{-2} \text{ sm} \text{ — ortakly sterženiň uzalmasy.}$$

Gyraky diregleriň gysylmasy.

$$\Delta \ell_A = \frac{N_A \ell_A}{E_p A_p} = \frac{-80 \cdot 100}{2 \cdot 10^4 \cdot 10} = -4 \cdot 10^{-2} \text{ sm,}$$

$$\Delta \ell_B = \frac{N_B \ell_B}{E_a A_a} = \frac{-40 \cdot 100}{10^3 \cdot 100} = -4 \cdot 10^{-2} \text{ sm},$$

Direglerdäki $\Delta \ell_A = \Delta \ell_B$ we bu durkuny üýtgetmeler P güýjüň goýlan nokadyny aşak süýşürýärler, şonuň üçin hem

$$\Delta = 2 \cdot 10^{-2} + 4 \cdot 10^{-2} = 6 \cdot 10^{-2} \text{ sm} = 0,6 \text{ mm}.$$

1.11. $P=33,3 \text{ kN}$. AB dartyjynyň uzynlygy $\ell_{AB} = \sqrt{15^2 + 10^2} = 18,03 \text{ m}$,

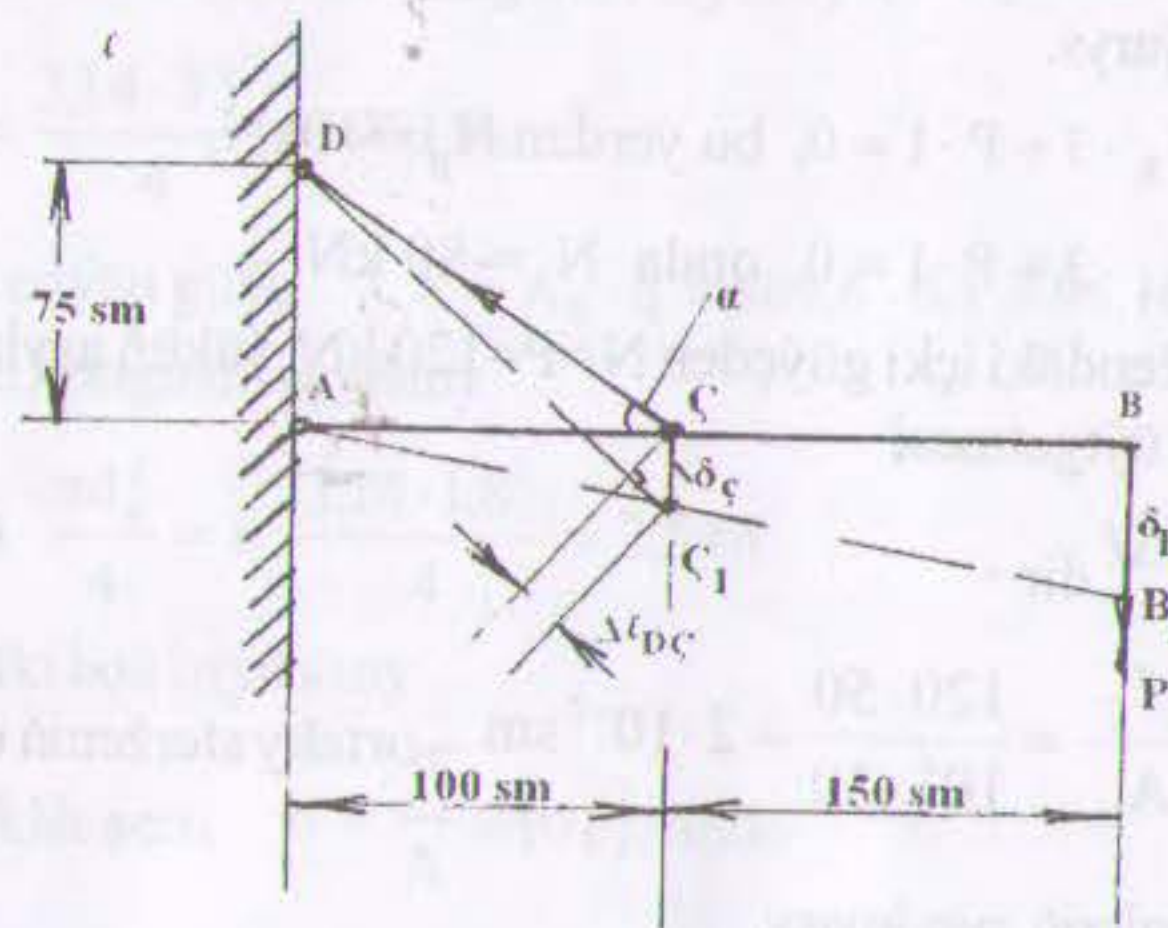
$$\sin \alpha = \frac{10}{18,03} = 0,554, \quad \cos \alpha = \frac{15}{18,03} = 0,832$$

$$\sum M_D = N_{AB} \cdot 10 \cos \alpha - P \cdot 5 = 0, \quad P = \frac{N_{AB} \cdot 10 \cdot \cos \alpha}{5}$$

$$N_{AB} = [\sigma] \cdot A_{AB} = 4 \cdot 5 = 20 \text{ kN},$$

$$\text{onda } P = \frac{20 \cdot 10 \cdot 0,832}{5} = 33,3 \text{ kN}.$$

1.12. $P=12 \text{ kN}$, $\delta_B=4,17 \text{ mm}$. Çyzgydan $\ell_{DC} = \sqrt{100^2 + 75^2} = 125 \text{ sm}$



1.12-nji surat

$$\Delta ACD - \text{den } \sin \alpha = \frac{\ell_{DA}}{\ell_{DC}} = \frac{75}{125} = \frac{3}{5} = 0,6$$

$$\sum M_A = P \cdot 2,5 - N_{DC} \cdot 1,0 \sin \alpha = 0$$

$$P = \frac{N_{DC} \cdot 1 \cdot \sin \alpha}{2,5} \quad (1)$$

Berklik şertinden

$$N_{DC} = [\sigma] \cdot A_{DC} = [\sigma] \cdot \frac{\pi d^2}{4} = 16 \cdot \frac{3,14 \cdot 2^2}{4} = 50,24 \text{ kN}.$$

$$\text{Onda (1) aňlatmadan } P = \frac{50,24 \cdot 1 \cdot 0,6}{2,5} = 12 \text{ kN}$$

çyzgydan

$$\delta_B = 2,5 \delta_C = 2,5 \cdot \frac{\Delta \ell_{DC}}{\sin \alpha} = 2,5 \cdot \frac{N_{DC} \cdot \ell_{DC}}{EA \cdot \sin \alpha} = 2,5 \cdot \frac{50,24 \cdot 125}{2 \cdot 10^4 \cdot 3,14 \cdot 0,6} = 0,417 \text{ sm} = 4,17 \text{ mm}.$$

1.13. $x=0,081 \text{ m}$, $P=414 \text{ kN}$, $\sigma_{AD}=2,347 \text{ kN/sm}^2$, $\sigma_{BE}=1,01 \text{ kN/sm}^2$. Birinji sterženiň uzynlygy

$$\ell_1 = \sqrt{2^2 + 3^2} = \sqrt{13} = 3,6 \text{ m}.$$

$$\sin \alpha = \frac{3}{3,6} = 0,833; \quad \cos \alpha = \frac{2}{3,6} = 0,555$$

$$A_1 = \frac{\pi d^2}{4} = \frac{3,14 \cdot 2,5^2}{4} = 4,9 \text{ sm}^2$$

Ulgamyň deňagramlylygynyň deňlemesi

$$\sum M_B = N_1 (2 + 1,5) \sin \alpha - P \cdot x = 0$$

$$\sum M_A = N_2 3,5 - P (3,5 - x) = 0$$

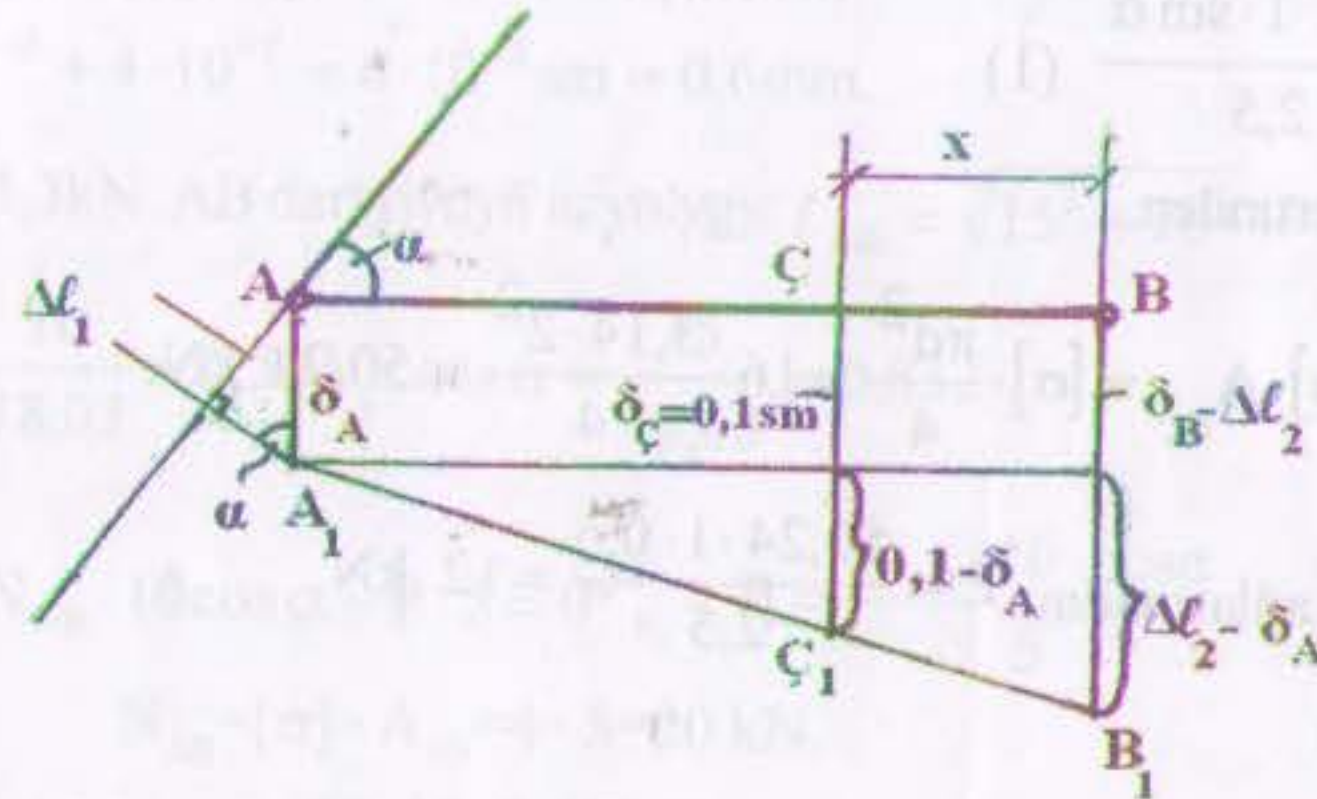
$$\sum Y_i = N_1 \sin \alpha + N_2 - P = 0.$$

$$\text{Bu ýerden } 3,5 N_1 \sin \alpha = P \cdot x, \quad (1)$$

$$3,5 N_2 = P (3,5 - x), \quad (2)$$

$$0,833 N_1 + N_2 = P. \quad (3)$$

Görüşümüz ýaly üç deňlemäniň dört näbellesi bar. Ulgamyň durkuny üýtgeden ýagdaýyna seredýäris.



1.13-nji surat

Meseläniň şertinden $\delta_B = 2\delta_A$, çyzgydan $\delta_A = \frac{\Delta l_1}{\sin \alpha}$, $\delta_B = \Delta l_2$,

$\Delta l_2 = \frac{2\Delta l_1}{\sin \alpha}$ – durkuny üýtgetmäniň bilelikdäki deňlemesi.

Gukun kanunyny ulanyp alarys. $\frac{N_2 \ell_2}{E_2 A_2} = \frac{2 \cdot N_1 \ell_1}{E_1 A_1 \sin \alpha}$, bu ýerden onda

$$N_2 = 35,4 N_1 \quad (4)$$

(4) aňlatmany (3) deňlemä goýup alarys $0,833 N_1 + 35,4 N_1 = P$,

$$N_1 = \frac{P}{36,23}, \quad (1) \text{ aňlatma goýup alarys.}$$

$$3,5 \cdot \frac{P}{36,23} \cdot 0,833 = Px, \text{ bu ýerden } x = 0,081 \text{ m, çyzgydan}$$

$$\frac{0,1 - \delta_A}{3,5 - 0,081} = \frac{\Delta l_2 - \delta_A}{3,5}$$

$$\frac{0,1 - \frac{\Delta l_1}{0,83}}{3,419} = \frac{\Delta l_2 - \frac{\Delta l_1}{0,833}}{3,5} \Rightarrow 3,5 \left(0,1 - \frac{N_1 \ell_1}{E_1 A_1 \sin \alpha} \right) =$$

$$= 3,419 \left(\frac{N_2 \ell_2}{E_2 A_2} - \frac{N_1 \ell_1}{E_1 A_1 \cdot 0,833} \right)$$

Soňky aňlatmany (4) bilen bilelikde işläp alarys $N_2 = 404 \text{ kN}$
(2) deňlemeden $3,5 \cdot 404 = P \cdot 3,419$, bu ýerden $P = 414 \text{ kN}$

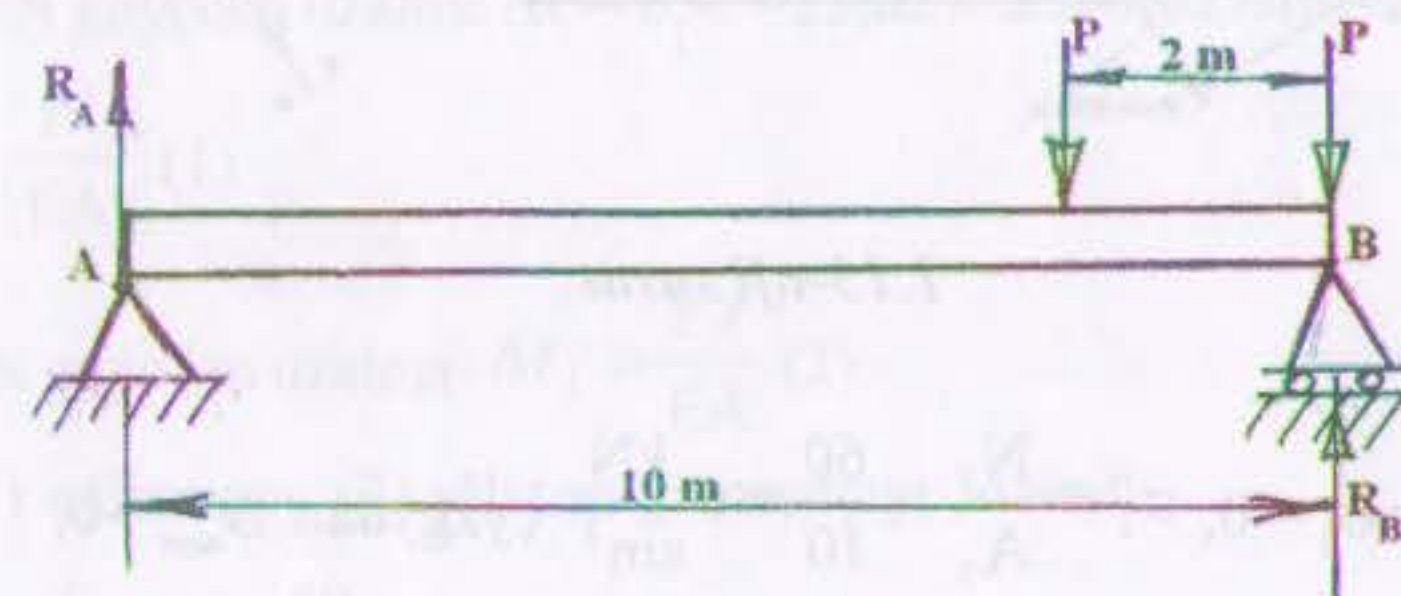
$$(1) \text{ deňlemeden } N_1 = \frac{Px}{3,5 \cdot \sin \alpha} = \frac{414 \cdot 0,081}{3,5 \cdot 0,833} = 11,5 \text{ kN, onda}$$

sterženlerdäki dartgynlylyklar:

$$\sigma_1 = \frac{N_1}{A_1} = \frac{11,5}{4,9} = 2,347 \text{ kN/sm}^2$$

$$\sigma_2 = \frac{N_2}{A_2} = \frac{404}{400} = 1,01 \text{ kN/sm}^2.$$

1.14. Ýüküň in oňaysyz ýagdaýy A ýa-da B direkleriň üstünde goýlan ýagdaýda bolýar.



1.14-nji surat

$$\sum M_A = R_B \cdot 10 - P \cdot 10 - P \cdot 8 = 0$$

$$R_B = \frac{18P}{10} = \frac{18 \cdot 150}{10} = 270 \text{ kN}$$

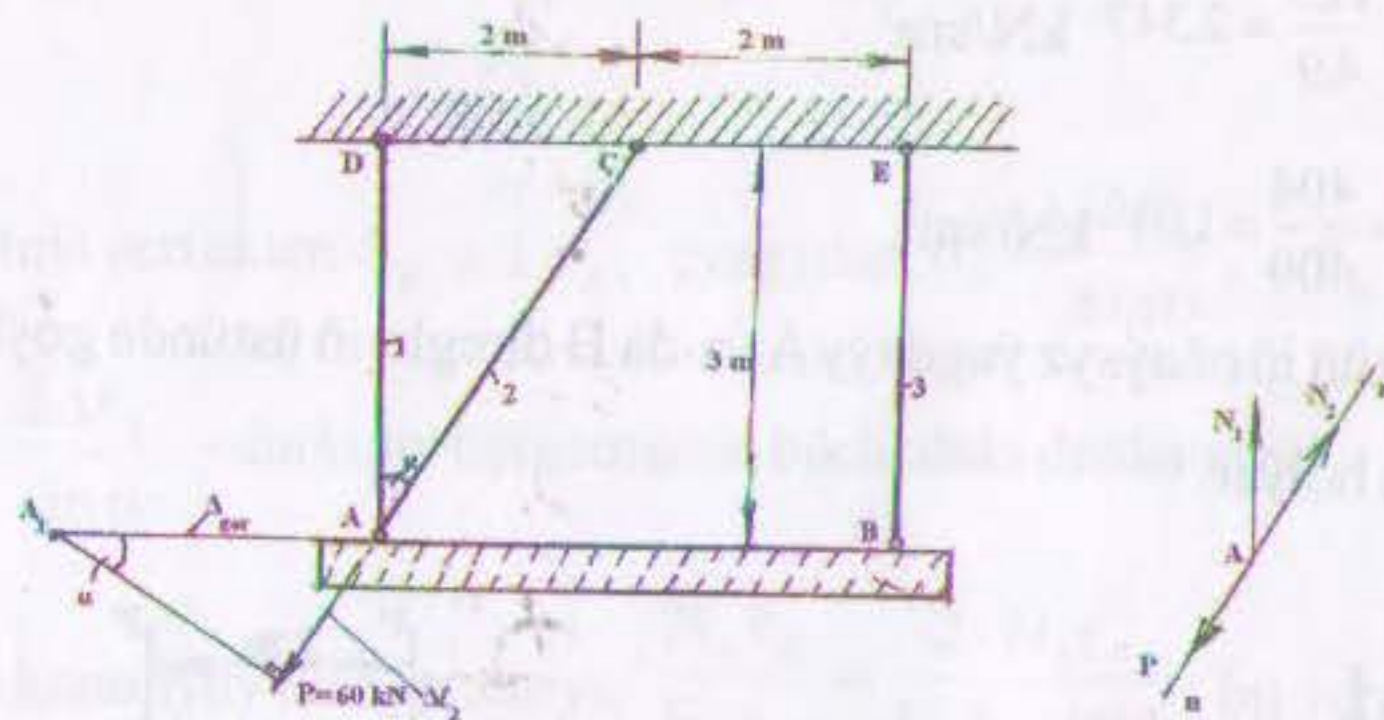
Berklik şertinden $\sigma = \frac{R_B}{A} \leq [\sigma]$ gerek bolan ölçegleri kesgitleýäris:

$$A = \frac{R_B}{[\sigma]} = \frac{270}{0,1} = 2700 \text{ sm}^2, \quad a = \sqrt{A} = \sqrt{2700} = 52 \text{ sm}.$$

Kwadrat kesigiň ölçegleri 52 x 52 sm.

$$1.15. \sigma_1 = \sigma_3 = 0, \quad \sigma_2 = 6 \frac{\text{kN}}{\text{sm}^2}, \quad \Delta_{\text{wert}} = 0, \quad \Delta_{\text{gor}} = 1,946 \text{ mm}.$$

A düwüniň deňagramlylygyna seredýäris. Düwne täsir edýän güýçleri n-n oka proyektirläp alarys $N_2 = P = 60 \text{ kN}$, $N_1 = 0$, $N_3 = 0$.



1.15-nji surat

$$\text{Onda } \sigma_1 = \sigma_3 = 0, \quad \sigma_2 = \frac{N_2}{A_2} = \frac{60}{10} = 6 \frac{\text{kN}}{\text{sm}^2} \text{ çyzgydan } \Delta_{\text{wert}} = 0,$$

$$\Delta_{\text{gor}} = \frac{\Delta \ell_2}{\sin \alpha},$$

$$\ell_2 = \sqrt{3^2 + 2^2} = 3,6 \text{ m}; \quad \Delta \ell_2 = \frac{N_2 \ell_2}{EA_2} = \frac{60 \cdot 360}{2 \cdot 10^4 \cdot 10} = 10,8 \cdot 10^{-2} \text{ sm};$$

$$\sin \alpha = \frac{2}{3,6} = 0,555, \text{ onda } \Delta_{\text{gor}} = \frac{10,8 \cdot 10^{-2}}{0,555} = 0,1946 \text{ sm},$$

$$\Delta_{\text{gor}} = 1,946 \text{ mm}.$$

1.16. $E = 1,15 \cdot 10^4 \text{ kN/sm}^2$. Gukuň kanuny boýunça polat we mis simi täsir edýän güýçler:

$$\text{Polat simi } P = \frac{\Delta \ell E_p A_p}{\ell}, \quad A_p = \frac{\pi d^2}{4} = \frac{3,14 \cdot 0,16^2}{4} = 0,002 \text{ sm}^2$$

Mis simi

$$P_1 = \frac{\Delta \ell_1 E_m A_m}{\ell_1}, \quad A_m = \frac{\pi d_1^2}{4} = \frac{3,14 \cdot 0,32^2}{4} = 0,008 \text{ sm}^2$$

Meseläniň şertine görä, $P = P_1$.

$$\text{onda } \frac{\Delta \ell E_p A_p}{\ell} = \frac{\Delta \ell_1 E_m A_m}{\ell_1}, \text{ bu ýerden}$$

$$E_m = \frac{\Delta \ell E_p A_p \ell_1}{\Delta \ell_1 A_m \ell} = \frac{0,15 \cdot 2 \cdot 10^4 \cdot 0,002 \cdot 300}{0,039 \cdot 0,008 \cdot 180} = 1,15 \cdot 10^4 \text{ kN/sm}^2$$

$$1.17. \ell_1 = 25,0135 \text{ sm}, \quad \ell'_1 = 25,0106 \text{ sm}, \quad E = 1,88 \cdot 10^4 \text{ kN/sm}^2.$$

100 kN güýçden uzalma $\Delta \ell = \ell_1 - \ell'_1 = 25,027 - 25 = 0,027 \text{ sm}$ ýa-da

$$\Delta \ell = \frac{P \ell}{EA} \quad (1)$$

$$50 \text{ kN güýçden uzalma } \Delta \ell_1 = \frac{P_1 \ell}{EA} \quad (2)$$

(1) aňlatmany (2) aňlatma gatnaşdyryp, olaryň

$$\Delta \ell_1 = \frac{P_1}{P} \Delta \ell = \frac{50}{100} \cdot 0,027 = 0,0135 \text{ sm} - \text{bu uzalma bolsa steržene}$$

50 kN güýçden bolýar, $\ell_1 = 25,0135 \text{ sm}$.

(1) aňlatmadan

$$E = \frac{P\ell}{A \cdot \Delta\ell} = \frac{100 \cdot 25 \cdot 4}{3,14 \cdot 2,5^2 \cdot 0,027} = 1,88 \cdot 10^4 \text{ kN/sm}^2 \text{ steržendäki}$$

dartgynlylyk

$\sigma = 8 \text{ kN/sm}^2$ bolanda, uzalmany kesgitleýäris.

$$\Delta\ell_1 = \frac{\sigma\ell}{E} = \frac{8 \cdot 25}{1,88} = 0,0106 \text{ sm},$$

$$\ell_1^1 = \ell_1 + \Delta\ell_1^1 = 25 + 0,0106 = 25,0106 \text{ sm}.$$

1.18. $E = 2,1 \cdot 10^4 \text{ kN/sm}^2$, $\mu = 0,2425$. 5 sm uzynlykda sterženiň uzalmasy 0,004 sm bolsa, Gukuň kanunyny ulanyp, sterženiň materialynyň maýysgaklyk modulyny kesgitleýäris.

$$E = \frac{P\ell_1}{A \cdot \Delta\ell}, \text{ bu ýerde } \ell_1 = 5 \text{ sm}, A = \frac{\pi d^2}{4} = \frac{3,14 \cdot 3,2^2}{4} = 8,04 \text{ sm}^2$$

$$\text{onda } E = \frac{135 \cdot 5}{0,004 \cdot 8,04} = 2,1 \cdot 10^4 \text{ kN/sm}^2.$$

$$\text{Otnositel boý durkuny üýtgetme } \varepsilon = \frac{\Delta\ell}{\ell_1} = \frac{0,004}{5} = 0,0008, \text{ otnositel}$$

$$\text{kese durkuny üýtgetme } \varepsilon^1 = \frac{\Delta d}{d} = \frac{0,00062}{3,2} = 0,000194, \text{ kese}$$

durkuny üýtgetmäniň koeffisiýenti

$$\mu = \left| \frac{\varepsilon^1}{\varepsilon} \right| = \frac{0,000194}{0,0008} = 0,2425.$$

1.19. $\Delta V = 3 \text{ sm}^3$. Sterženiň otnositel göwrümini üýtgetmesi

$$\theta = \frac{\Delta V}{V} = \frac{1-2\mu}{E} \cdot \sigma, \quad \sigma = \frac{P}{A}, \quad V = A\ell$$

onda sterženiň göwrüminiň artmagy

$$\Delta V = V \frac{1-2\mu}{E} \sigma = A\ell \frac{1-2\mu}{E} \cdot \frac{P}{A} = \frac{1-2\mu}{E} P\ell = \frac{1-2-0,25}{2 \cdot 10^4} \cdot 200 \cdot 600 = 3 \text{ sm}^3.$$

$$1,20. 2 \cdot 10^4 \text{ kN/sm}^2.$$

Şaýyň hakyky absolýut uzalmasy

$$\Delta\ell = \frac{\Delta}{K} = \frac{2,5}{500} = 0,005 \text{ sm}.$$

Şaýyň otnositel uzalmasy

$$\varepsilon = \frac{\Delta\ell}{S} = \frac{0,005}{10} = 5 \cdot 10^{-4}.$$

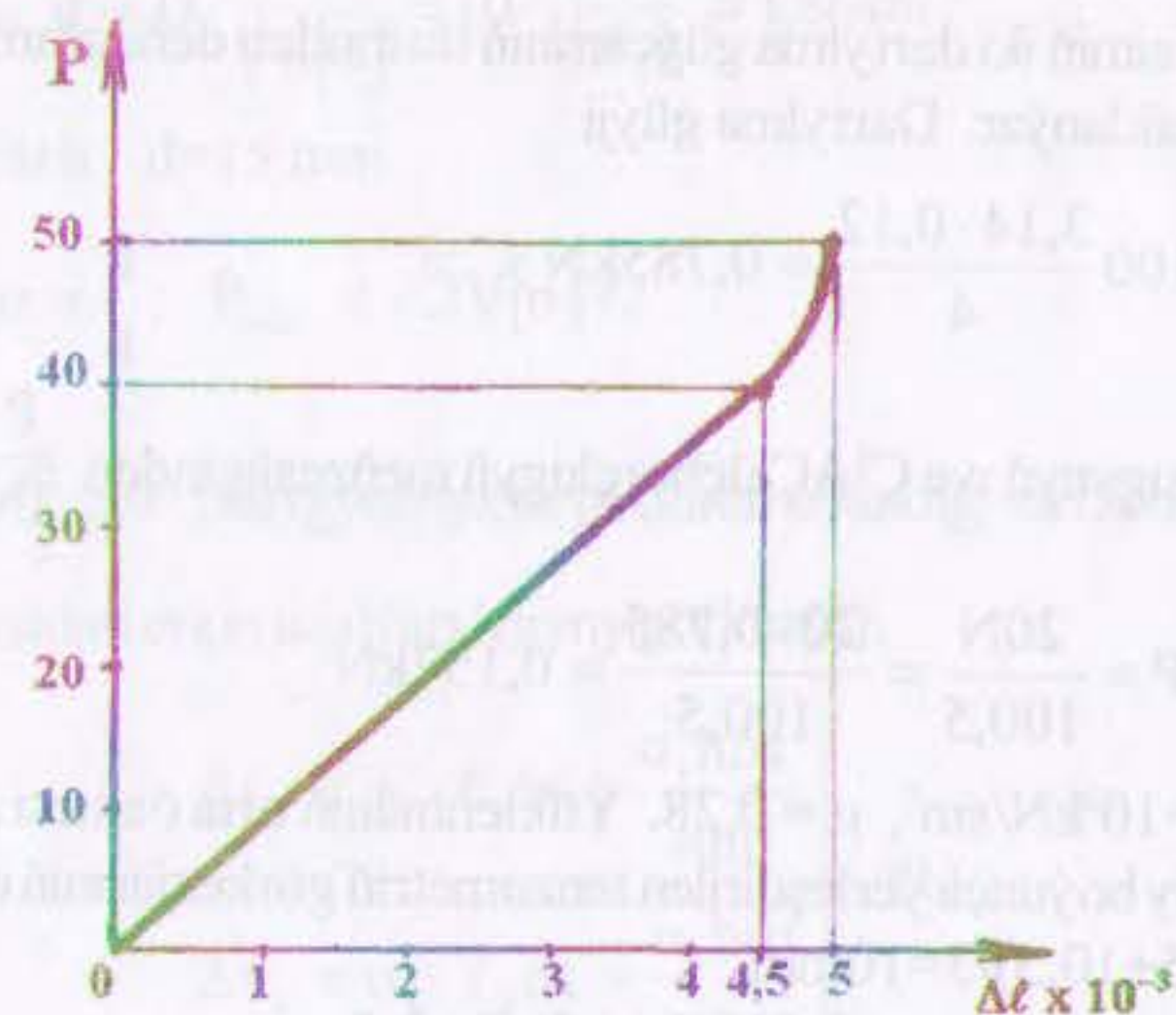
Şaýyň normal dartgynlylygy

$$\sigma = \frac{P}{A} = \frac{100}{10} = 10 \text{ kN/sm}^2.$$

Dartgynlylyk üçin Gukuň kanunynyndan

$$E = \frac{\sigma}{\varepsilon} = \frac{10}{5 \cdot 10^{-4}} = 2 \cdot 10^4 \text{ kN/sm}^2.$$

1.21. $E = 1,78 \cdot 10^3 \text{ kN/sm}^2$. $P-\Delta\ell$ gysma diagrammany gurýarys.



1.21-nji surat

Meseläniň şertine görä, $\sigma=0,4\text{ kN/sm}^2$ bolanda, otnositel durkuny

$$\text{üýtgetme } \varepsilon = \frac{\Delta \ell}{\ell} = \frac{4,5 \cdot 10^{-3}}{20} = 0,225 \cdot 10^{-3},$$

$$\text{onda } E = \frac{\sigma}{\varepsilon} = \frac{0,4}{0,225 \cdot 10^{-3}} = 1,78 \cdot 10^3 \text{ kN/sm}^2.$$

1.22. $\text{ÇÇ}^1=10 \text{ sm}$, $\sigma=100 \text{ kN/sm}^2$, $P=0,157 \text{ kN}$.

Simiň absolýut uzalmasy

$$\Delta \ell = \varepsilon \ell = 0,005 \cdot 200 = 1 \text{ sm}.$$

Onda simiň ortasyndaky Ç nokatdan çep ýa-da sag böleginiň uzynlygy

$$\ell_1 = 100 + \frac{\Delta \ell}{2} = 100 + 0,5 = 100,5 \text{ sm}.$$

AÇÇ¹ üçburçlukdan

$$\text{ÇÇ}^1 = \sqrt{\ell_1^2 - \left(\frac{\ell}{2}\right)^2} = \sqrt{100,5^2 - 100^2} = 10 \text{ sm}.$$

Simdäki dartgynlylyk $\sigma = E\varepsilon = 2 \cdot 10^4 \cdot 0,005 = 100 \text{ kN/sm}^2$.

Ç nokat P we simiň iki dartylma güýçleriniň täsirinden deňagramlylyk ýagdaýynda saklanýar. Dartylma güýji

$$N = \sigma \cdot A = 100 \frac{3,14 \cdot 0,12}{4} = 0,785 \text{ kN}.$$

Güýç üçburçlugynyň we Ç¹AÇ üçburçlugynyň meňzeşliginden $\frac{P}{2N} = \frac{10}{100,5}$

$$\text{bu ýerden, } P = \frac{20N}{100,5} = \frac{20 \cdot 0,785}{100,5} = 0,157 \text{ kN}.$$

1.23. $E = 1,9 \cdot 10^4 \text{ kN/sm}^2$, $\mu = 0,28$. Ýüklenmäniň orta ösmesi $\Delta P = 10 \text{ kN}$, nusganyň boýy boýunça ýerleşdirilen tenzometriň görkezijisiniň orta ösmesi

$$\Delta n_A = (10 + 9,5 + 10,5) / 3 = 10 \text{ mm},$$

$$\text{kese tenzometr üçin } \Delta n_A = (3,5 + 2,5 + 4,5) / 3 = 3,5 \text{ mm}.$$

$$\text{Absolýut uzalma: } \Delta S_A = 10 / 950 = 1,05 \cdot 10^{-2} \text{ mm}$$

$$\Delta S_B = \frac{3,5}{1190} = 2,9 \cdot 10^{-3} \text{ mm}, \text{ bu ýerden}$$

$$E = \frac{\Delta P \cdot S_A}{A \Delta S_A} = \frac{10 \cdot 2}{1 \cdot 0,105 \cdot 10^{-2}} = 1,9 \cdot 10^4 \text{ kN/sm}^2$$

Puassonyň koeffisiýenti

$$\mu = \frac{\varepsilon_B}{\varepsilon_A} = \frac{\Delta S_B / S_B}{\Delta S_A / S_A} = \frac{\Delta S_B}{\Delta S_A} = \frac{0,29 \cdot 10^{-3}}{0,105 \cdot 10^{-2}} = 0,28.$$

1.24. $d=15 \text{ mm}$. Karterden silindri ýolup aýyrjak bolýan güýjiň ululygy

$$P = p \frac{\pi D^2}{4}.$$

Eger şpilkalara ýokarky güýç endigan ýaýran bolsa, rugsat edilyän güýç

$$P = n \frac{\pi d^2}{4} \cdot [\sigma].$$

$$\text{Bu ýerden } d = D \cdot \sqrt{\frac{P}{n[\sigma]}} = 10 \cdot \sqrt{\frac{1}{8 \cdot 6}} = 1,86 \text{ sm};$$

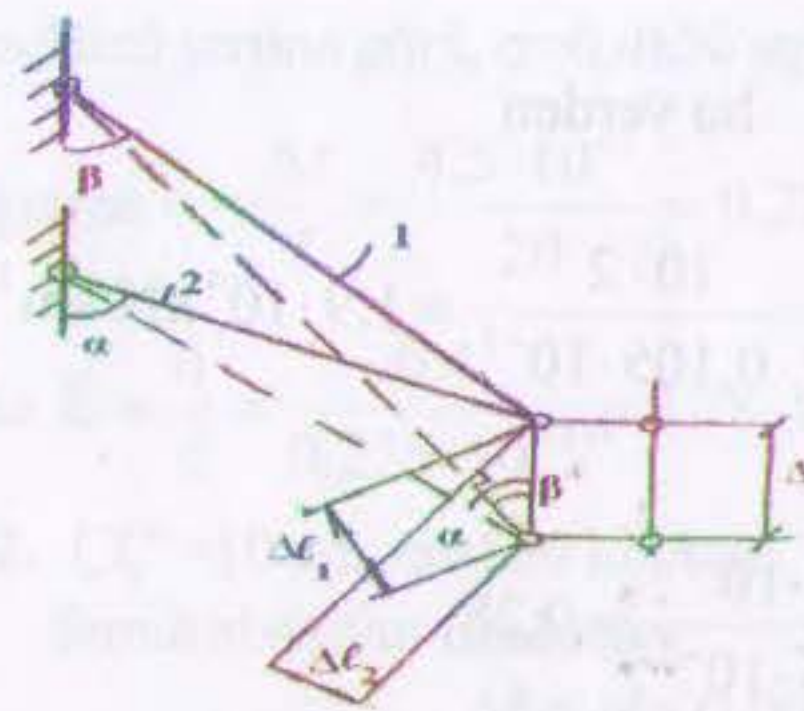
kabul edýäris $d=15 \text{ mm}$

$$1.25. \quad \alpha = \frac{\pi}{4}; \quad P_{\max} = \sqrt{2} V [\sigma] \ell.$$

$$1.26. \quad \beta = \frac{\pi}{2} - \alpha \quad \text{Dartgynlylyklaryň doremeyändigini sterženleriň}$$

gyzdyrylmadan erkin uzalýandygyny görkezýär.

$$\left. \begin{aligned} \Delta \ell_1 &= \alpha_1 \cdot \ell_1 \Delta t = \frac{\alpha_1 h \Delta t}{\sin \beta} \\ \Delta \ell_2 &= \alpha_1 \cdot \ell_2 \Delta t = \frac{\alpha_1 h \Delta t}{\sin \alpha} \end{aligned} \right\} (1),$$



1.26-njy surat

Bu ýerde: $\ell_1 = \frac{h}{\sin\beta}$,

$\ell_2 = \frac{h}{\sin\alpha}$

α_1 -sterženiň materialynyň temperatura koeffisiýenti ölçegleriň üýtgemezlik ýörelgesine esaslanyp, çyzgydan

$\Delta = \frac{\Delta\ell_1}{\cos\beta} = \frac{\Delta\ell_2}{\cos\alpha}, (2)$

Soňky aňlatmany (1) formula goýup alarys:

$$\frac{\alpha_1 h \Delta t}{\sin\beta \cos\beta} = \frac{\alpha_1 h \Delta t}{\sin\alpha \cos\alpha}$$

ýa-da $2\sin\beta\cos\beta = 2\sin\alpha\cos\alpha$, $\sin 2\beta = \sin 2\alpha$

$$\sin 2\beta - \sin 2\alpha = 0 \Rightarrow 2\sin \frac{\beta - \alpha}{2} \cdot \cos \frac{\beta + \alpha}{2} = 0.$$

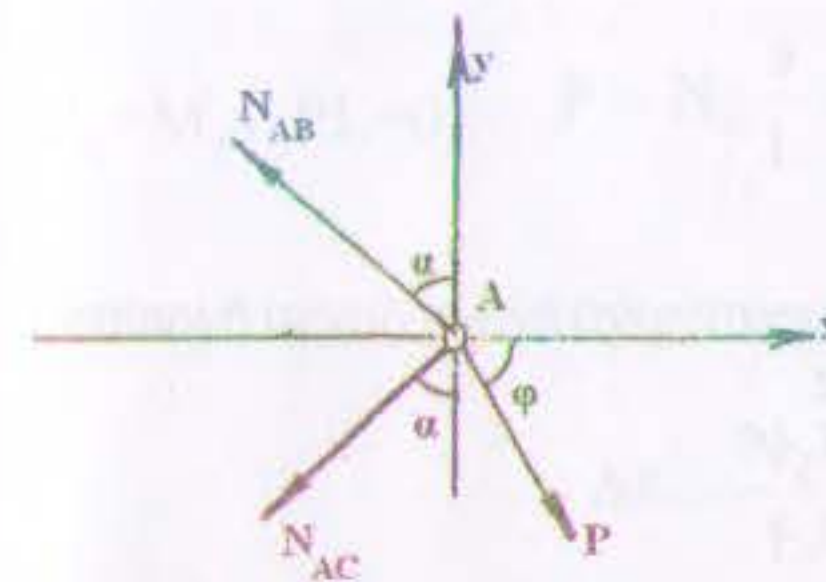
Bu ýerden, $\beta - \alpha = n \cdot 180^\circ$ ($n = 0, 1, 2, 3, \dots$)

$$\beta + \alpha = \frac{\pi}{2} + n \cdot 180^\circ \quad (n = 0, 1, 2, 3, \dots).$$

Çyzgyda α we β burçlar $\frac{\pi}{2}$ -den kiçi (diýmek $n=0$) we meseläniň şerti

boýunça $\alpha \neq \beta$, onda $\beta + \alpha = \frac{\pi}{2}$ ýa-da $\beta = \frac{\pi}{2} - \alpha$.

1.27. $\alpha = \frac{\pi}{4}$. Ilki bilen P güýjüň sterženlerde iň uly güýjüni döredýän φ burçy tapýarys.



1.27-nji surat

$$\begin{aligned} \sum X &= P \cos \varphi - N_{AB} \sin \alpha - N_{AC} \sin \alpha = 0; \\ \sum Y &= P \sin \varphi - N_{AB} \cos \alpha - N_{AC} \cos \alpha = 0. \end{aligned}$$

Bu ýerden

$$N_{AB} = \frac{P}{2} \cdot \frac{\cos \varphi}{\sin \alpha} + \frac{\sin \varphi}{\cos \varphi},$$

$$N_{AC} = \frac{P}{2} \cdot \frac{\cos \varphi + \sin \varphi}{\sin \alpha + \sin \alpha}.$$

Görşümiz ýaly, $N_{AB} > N_{AC}$ we N_{AB} iň uly bahasy $\alpha = \varphi$ bolanda bolýar.

1.28. $\sigma = \left(\frac{R}{r} - 1 \right) E$ Gurşaw bilen tigriň töwerekleriniň uzynlyklarynyň

tapawudy

$$\Delta \ell = 2\pi(R-r) \quad (1)$$

Şeýle-de Gukun kanunyna esaslanyp absolýut uzalma

$$\Delta \ell = \frac{N \ell}{EA} = \frac{N \cdot 2\pi r}{EA} \quad (2)$$

(1) we (2) aňlatmalaryň sag taraplaryny deňläp alarys.

$$2\pi(R-r) = \frac{N 2\pi r}{EA} \Rightarrow N = \left(\frac{R}{r} - 1 \right) EA$$

Gurşawdaky dartgynlylyk $\sigma = \left(\frac{R}{r} - 1 \right) E$.

1.29. $\Delta \ell = 21,6 \cdot 10^{-3}$ sm.



1.29-njy surat

$\Delta ABO \propto \Delta CDO$ alarys

$$\frac{b}{\ell_o} = \frac{3b}{\ell + \ell_o} \Rightarrow \ell_o = \frac{1}{2} \ell.$$

Çyzgydan $\frac{b_z}{z} = \frac{b}{\ell_o}, \quad b_z = \frac{bz}{\ell_o} = \frac{2bz}{\ell}.$

Üýtgeýän kesikli sterženiň uzalmasy

$$\Delta \ell = \int_0^{\ell} \frac{N dz}{EA} = \frac{P}{E} \int_0^{\ell} \frac{dz}{A} = \frac{P}{E} \int_0^{\ell} \frac{\ell dz}{2b \delta z} = \frac{P \ell}{2E \delta b} \ln 3 = \frac{12 \cdot 40}{2 \cdot 0,7 \cdot 10^4 \cdot 2 \cdot 0,8} \ln 3 = 21,6 \cdot 10^{-3} \text{ sm}.$$

$$\ln 3 = 1,0986,$$

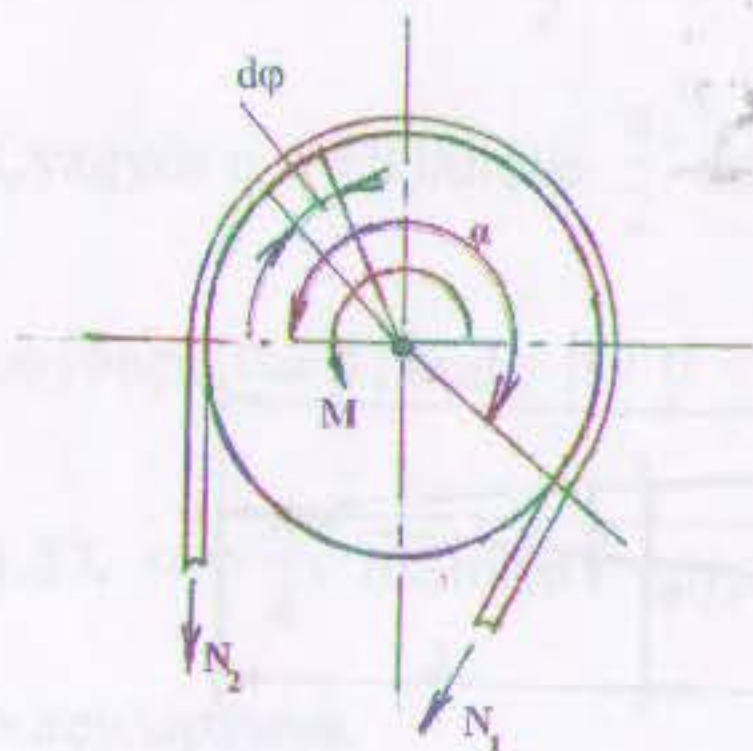
1.30. $K=3,78, A=2,7 \text{ sm}^2$. Gukuň kanunyny ulanyp birdenkä ýüklenmedäki dartgynlylygy kesgitleýäris.

$$\sigma_d = E \varepsilon = 2 \cdot 10^4 \cdot \frac{1}{1800} = 11,1 \text{ kN/sm}^2$$

$$\sigma = \sigma \cdot K_d = \frac{PK_d}{A} \Rightarrow A = \frac{PK_d}{\sigma_d} = \frac{15 \cdot 2}{11,1} = 2,7 \text{ sm}^2.$$

Ätiýaçlyk koeffisiýenti

$$K = \frac{\sigma_b}{\sigma_d} = \frac{42}{11,1} = 3,78.$$



1.31-nji surat

1.31. $P=0,406 \text{ kN}; \delta=3,52 \text{ mm}.$

Lentanyň elementiniň deňagramlylyk şertinden:

$$N - (N + dN) + N f d\varphi = 0$$

$$dN/N = f d\varphi; \quad N = C \ell^{f\varphi} \quad \varphi = 0,$$

$$N = N_2, \quad N_1 = N_2 \ell^{f\varphi}$$

$$\sum M = M + (N_2 - N_1)R = 0,$$

$$M = +(N_1 - N_2)R = N_2 R (1 - \ell^{f\varphi})$$

$$\text{onda } N_2 = M/R(\ell^{f\varphi} - 1);$$

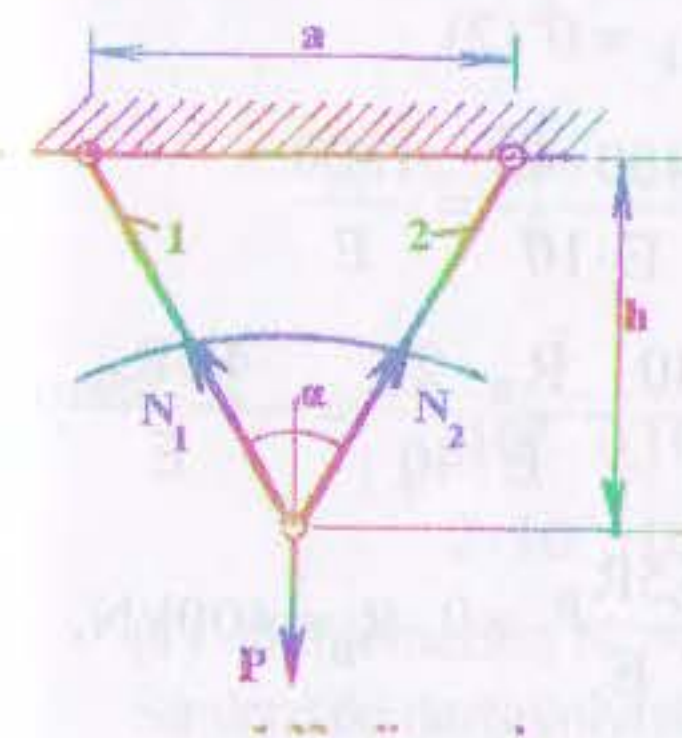
$$M_K = M_2 a - PL = 0, \quad P = N_2 \frac{a}{L} = \frac{a}{L} \cdot \frac{M}{R(e^{f\varphi} - 1)}.$$

Lentanyň uzynlygynyň üýtgetmesi:

$$\Delta \ell = \frac{N_2 \ell_2}{EA} + \int_0^a \frac{N_2 e^{f\varphi} R}{EA} d\varphi$$

$$\delta = \Delta \ell \cdot \frac{L}{a} = 3,52 \text{ mm}.$$

1.32. $h = \frac{a}{2}$



1.32-nji surat

Statikanyň deňlemesinden

$$N_1 = N_2 = \frac{P}{2 \cos \alpha}$$

$$\cos \alpha = \frac{h}{\sqrt{h^2 + \frac{a^2}{4}}}$$

Kesigiň zerur meýdany.

$$A = \frac{N}{[\sigma]} = \frac{P \cdot \sqrt{h^2 + \frac{a^2}{4}}}{2[\sigma] \cdot h}$$

Kesigiň göwrümi

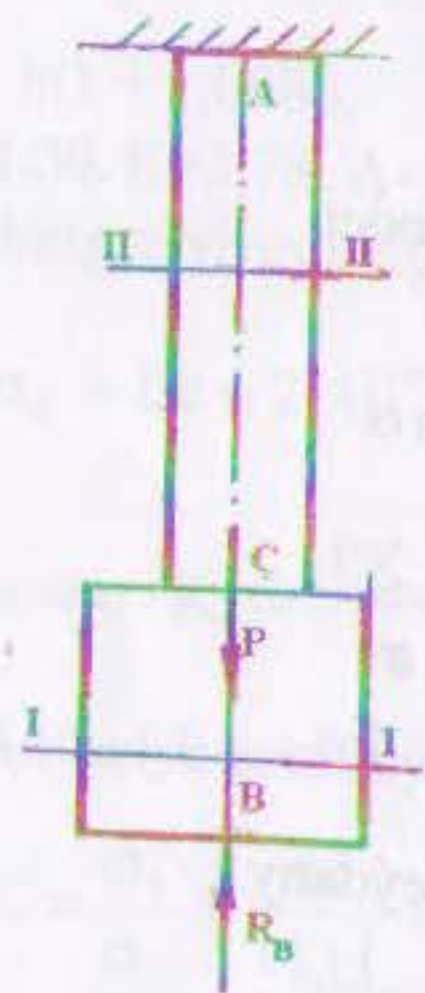
$$V = A \cdot \ell = \frac{P \sqrt{h^2 + \frac{a^2}{4}}}{2[\sigma] \cdot h} \sqrt{h^2 + \frac{a^2}{4}} = \frac{P \left(h^2 + \frac{a^2}{4} \right)}{2[\sigma] \cdot h}.$$

Sterženiň göwrüminden h boýunça ösme alyp we alnan aňlatmany nola deňläp alarys.

$$V^I = \frac{P}{2[\sigma]} \cdot \left(\frac{h^2 + a^2}{h} \right) = 0,$$

Bu ýerden $h = \frac{a}{2}$ ýa-da $\alpha = \frac{\pi}{4}$.

1.33. $\sigma_{yok} = 5 \text{ kN/sm}^2$, $\sigma_{aş} = -10 \text{ kN/sm}^2$,



1.33-nji surat

Deňagramlylygyň deňlemesi

$$\Sigma Y = R_A + R_B - P = 0 \quad (1)$$

Durkuny üýtgetmäniň deňlemesi

$$\Delta \ell = \Delta \ell_{R_B} + \Delta \ell_P = 0 \quad (2)$$

$$\Delta \ell_P = \frac{P \cdot 40}{E \cdot 10} = \frac{450 \cdot 40}{E \cdot 10} = \frac{1800}{E}$$

$$\Delta \ell_{R_B} = \frac{-R_B \cdot 40}{E \cdot 10} - \frac{R_B \cdot 20}{E \cdot 40} = -\frac{4,5R_B}{E}$$

$$\text{Onda } \frac{1800}{E} - \frac{4,5R_B}{E} = 0, R_B = 400 \text{ kN},$$

$$R_A = P - R_B = 450 - 400 = 50 \text{ kN}$$

$$\text{I-I kesikde } N_{aş} = -R_B = -400 \text{ kN}, \quad \sigma_{aş} = \frac{N_{aş}}{40} = -\frac{400}{40} = -10 \text{ kN/sm}^2,$$

$$\text{II-II kesikde } N_{yok} = R_A = 50 \text{ kN},$$

$$\sigma_{yok} = \frac{N_{yok}}{10} = \frac{50}{10} = 5 \text{ kN/sm}^2.$$

1.34. $\sigma_m = 4,6 \text{ kN/sm}^2$; $\sigma_p = 9,29 \text{ kN/sm}^2$.

Deňagramlylygyň deňlemesinden $N_m + N_p = P \quad (1)$

Durkuny üýtgetmäniň deňlemesinden $\varepsilon_m = \varepsilon_p \quad (2)$

$$\text{ýa-da } \frac{N_m}{E_m A_m} = \frac{N_p}{E_p A_p} \Rightarrow N_m = \frac{E_m A_m}{E_p A_p} N_p \quad (3)$$

(3) aňlatmany (1) deňlemä goýup alarys

$$N_p = \frac{P}{1 + \frac{E_m A_m}{E_p A_p}};$$

Bu ýerde $E_m = 10^4 \text{ kN/sm}^2$,
 $E_p = 2 \cdot 10^4 \text{ kN/sm}^2$.

$$A_m = \frac{\pi d_1^2}{4} = \frac{3,14 \cdot 0,5^2}{4} = 0,196 \text{ sm}^2,$$

$$A_p = \frac{\pi d_2^2}{4} \cdot 9 = \frac{3,14 \cdot 0,25^2}{4} \cdot 9 = 0,44 \text{ sm}^2,$$

$$\text{onda } N_p = \frac{5}{1 + \frac{10^4 \cdot 0,196}{2 \cdot 10^4 \cdot 0,44}} = 4,09 \text{ kN}$$

(1) Deňlemeden $N_m = P - N_p = 5 - 4,09 = 0,91 \text{ kN}$

Simlerdäki dartgynlylyklar:

$$\sigma_m = \frac{N_m}{A_m} = \frac{0,91}{0,196} = 4,64 \text{ kN/sm}^2,$$

$$\sigma_p = \frac{N_p}{A_p} = \frac{4,09}{0,44} = 9,29 \text{ kN/sm}^2.$$

1.35. $a = 39 \text{ sm}$, $d = 22 \text{ mm}$.

$$N_b + N_a = P; \quad \frac{N_b}{E_b A_b} = \frac{N_a}{E_a A_a}; \quad \frac{N_b}{E_b A_b} = \frac{N_a}{10 E_b \cdot 0,01 A_b}; \quad N_b = 10 N_a;$$

$$11 N_a = P, \quad N_a = \frac{P}{11} = \frac{1000}{11} = 91 \text{ kN}, \quad N_b = 909 \text{ kN}.$$

$$A_b = \frac{N_b}{[\sigma]_b} = \frac{909}{0,6} = 1516 \text{ sm}^2, \quad a = \sqrt{A_b} = \sqrt{1516} = 39 \text{ sm}.$$

Şerte görä:

$$A_a = 0,01 A_b, \quad A_a = 0,01 \cdot 1516 = 15,16 \text{ sm}^2, \quad A_a^1 = \frac{A_a}{4} = \frac{15,16}{4} = 3,79 \text{ sm}^2$$

$$A_a^1 = \frac{\pi d^2}{4} \Rightarrow d = \sqrt{\frac{4 \cdot A_a^1}{\pi}} = \sqrt{\frac{4 \cdot 3,79}{3,14}} = 2,2 \text{ sm} = 22 \text{ mm}$$

Kabul edýäris: $d=22 \text{ mm}$.

1.36 $A=4,3 \text{ sm}^2$.

Deňagramlylygyň deňlemesi:

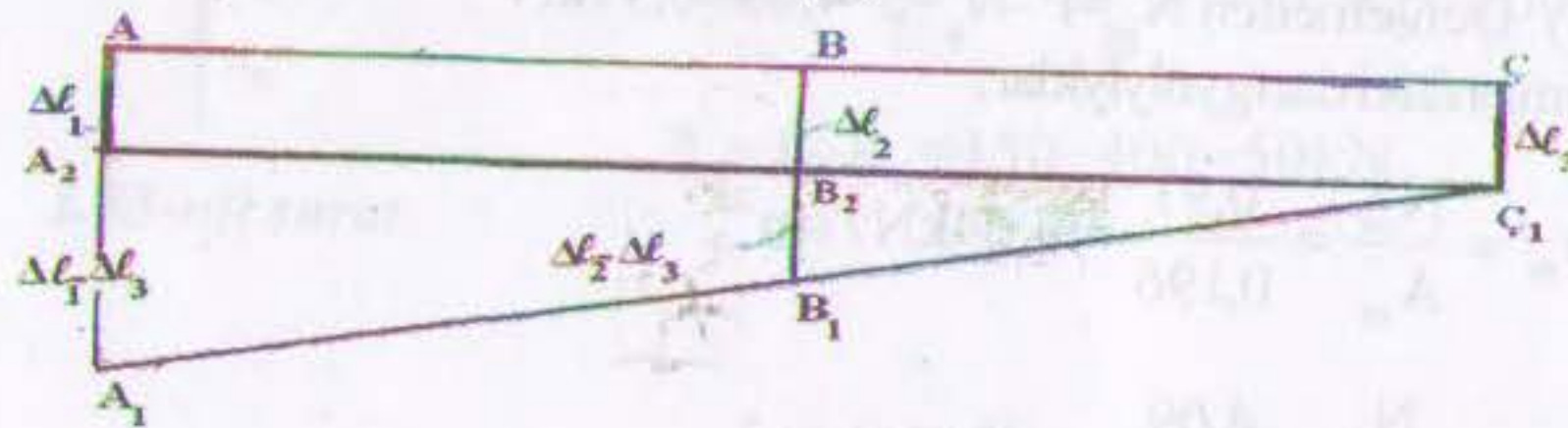
$$1). \Sigma Y = N_1 + N_2 + N_3 - P = 0; \quad \Sigma M_A = N_2 \cdot 1,5 + N_3 \cdot 3 - P \cdot 1,125 = 0.$$

Durkuny üýtgetmäniň deňlemesi:

$$\Delta A_1 A_2 C_1 \propto \Delta B_1 B_2 C_1$$

$$\frac{\Delta l_1 - \Delta l_3}{3} = \frac{\Delta l_2 - \Delta l_3}{1,5}; \quad \Delta l_1 = 2\Delta l_2 - \Delta l_3, \quad (3)$$

$$\text{ýa-da } N = 2N_2 - N_3 \quad (4)$$



1.36-njy surat

(1), (2) we (3) aňlatmalary bilelikde işläp alarys: $N_1=6,97 \text{ kN}$, $N_2=50 \text{ kN}$, $N_3=30,3 \text{ kN}$.

$$A_1 = \frac{N_1}{[\sigma]} = \frac{69,7}{16} = 4,3 \text{ sm}^2, \quad A_2 = \frac{N_2}{[\sigma]} = \frac{50}{16} = 3,125 \text{ sm}^2,$$

$$A_3 = \frac{N_3}{[\sigma]} = \frac{30,3}{16} = 1,89 \text{ sm}^2, \quad \text{kabul edýäris } A=4,3 \text{ sm}^2.$$

$$1.37. \quad N_1 = \frac{2P}{h} \cdot \frac{\zeta b^3}{b^3 + 4\zeta^3}, \quad N_2 = \frac{4P}{h} \cdot \frac{b\zeta^3}{b^3 + 4\zeta^3}.$$

$$\text{Cyzgydan } \sin \alpha = \frac{h}{\zeta}, \quad \sin \beta = \frac{h}{b}.$$

Deňagramlylygyň deňlemesi

$$\Sigma M_A = N_1 \cdot a \sin \alpha + N_2 \cdot 2a \sin \beta - P \cdot 2a = 0. \quad (1)$$

Durkuny üýtgetmäniň bilelikdäki deňlemesi

$$\text{Cyzgydan } \frac{\Delta l_1}{a \sin \alpha} = \frac{\Delta l_2}{2a \sin \beta} \Rightarrow 2\Delta l_1 \sin \beta = \Delta l_2 \sin \alpha \quad (2)$$

$$\text{ýa-da } 2\Delta l_1 \zeta = \Delta l_2 b;$$

$$\text{onda } \frac{2N_1 \ell_1 \zeta}{E_1 A_1} = \frac{2N_2 \ell_2 b}{E_2 A_2} \Rightarrow 2N_1 \zeta^2 = N_2 b^2;$$

$$\text{bu ýerden } N_2 = \frac{2N_1 \zeta^2}{b^2}.$$

Bu aňlatmany (1) deňlemä goýup,

$$N_1 \sin \alpha + \frac{4N_1 \zeta^2}{b^2} \cdot \sin \beta = 2P \Rightarrow N_1 \frac{h}{\zeta} + 4N_1 \frac{\zeta^2}{b^2} \cdot \frac{h}{b} = 2P$$

$$N_1 h b^3 + 4N_1 \zeta^3 h = 2P \cdot \zeta b^3 \text{ alarys.}$$

$$\text{Bu ýerden } N_1 = \frac{2P}{h} \cdot \frac{\zeta b^3}{b^3 + 4\zeta^3}$$

$$\text{onda } N_2 = \frac{4P}{h} \cdot \frac{b\zeta^3}{b^3 + 4\zeta^3}$$

$$1.38. \quad \sigma_1 = 21,05 \text{ kN/sm}^2, \quad \sigma_2 = 4,3 \text{ kN/sm}^2, \quad \sigma_3 = 14,4 \text{ kN/sm}^2.$$

Cyzgydan

$$\sin \alpha = \frac{C_2 C_5}{\delta_y}, \sin \alpha = \frac{C_2 C_6}{\delta_x}, \sin \alpha = \frac{C_2 C_7}{\delta_y}, \sin \alpha = \frac{C_2 C_8}{\delta_x}.$$

Deňagramlylygyň deňlemesi

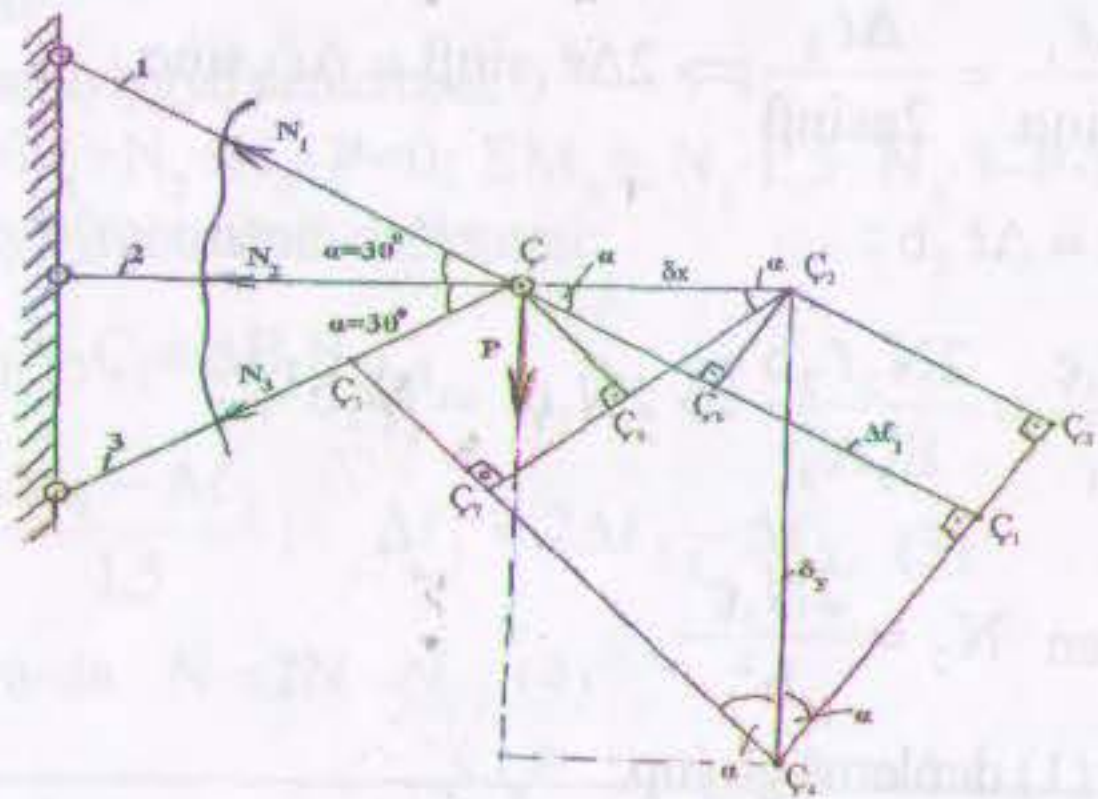
$$1) \Sigma X_i = -N_1 \cos \alpha - N_2 + N_3 \cos \alpha = 0$$

$$0,86 N_2 + N_2 = 0,86 N_3, \quad (1)$$

$$2) \Sigma Y_i = N_1 \sin \alpha + N_3 \sin \alpha - P = 0$$

$$0,5 (N_1 + N_3) = P, \quad (2)$$

Çyzgydan $\ell_1 = \ell_3 = \frac{\ell_2}{\cos \alpha}.$



1.38-nji surat

Durkuny üýtgetmäniň deňlemesi:

Ulgamyň durkuny üýtgeden ýagdaýyna seredip alarys:

$$\begin{cases} \Delta \ell_1 = C_2 C_5 + C_2 C_6 \\ \Delta \ell_3 = C_7 C_2 - C_2 C_8 \end{cases}$$

$$\Delta \ell_2 = C_2 C_2$$

$$C_2 C_5 = \delta_y \sin \alpha, \quad C_2 C_6 = \delta_x \cos \alpha, \quad C_2 C_7 = \delta_y \sin \alpha, \quad C_2 C_8 = \delta_x \cos \alpha,$$

$$\text{Onda} \begin{cases} \Delta \ell_1 = \delta_y \sin \alpha + \delta_x \cos \alpha \\ \Delta \ell_3 = \delta_y \sin \alpha - \delta_x \cos \alpha \end{cases}$$

bu ýerden $\Delta \ell_1 - \Delta \ell_3 = 2 \delta_x \cos \alpha \quad (3)$

$$\frac{N_1 \ell_2}{EA_1 \cos \alpha} - \frac{N_3 \ell_2}{EA_3 \cos \alpha} = 2 \frac{N_2 \ell_2}{EA_2} \cos \alpha$$

$$\frac{N_1}{2 \cdot 0,86} - \frac{N_3}{4 \cdot 0,86} = 2 \frac{N_2}{3} 0,86 \Rightarrow N_2 = N_1 - 0,506 N_3$$

(1) deňleme boýunça $N_1 = 0,73 N_3$

$$(2) \text{ deňleme boýunça } N_3 = \frac{P}{0,866} = \frac{50}{0,866} = 57,7 \text{ kN}$$

$$N_1 = 0,73 \cdot N_3 = 0,73 \cdot 57,7 = 42,1 \text{ kN},$$

$$N_2 = N_1 - 0,506 N_3 = 42,1 - 0,506 \cdot 57,7 = 12,9 \text{ kN},$$

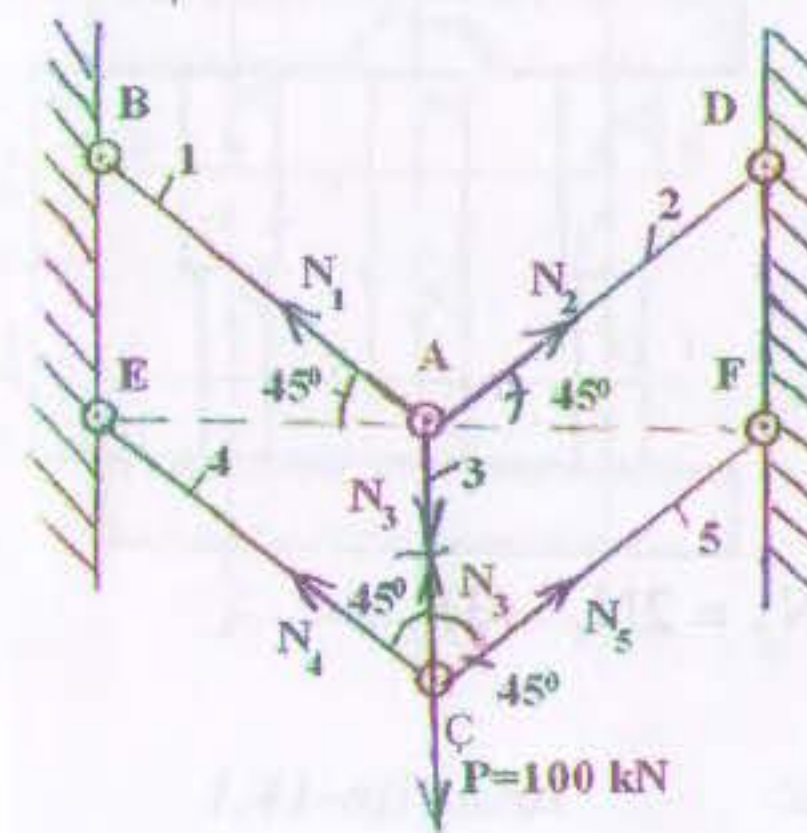
Degişlilikde, sterženiň dartgynlylyklary

$$\sigma_1 = \frac{N_1}{A_1} = \frac{42,1}{2} = 21,05 \text{ kN/sm}^2 \quad (\text{süýnme})$$

$$\sigma_2 = \frac{N_2}{A_2} = \frac{12,9}{3} = 4,3 \text{ kN/sm}^2 \quad (\text{süýnme})$$

$$\sigma_3 = \frac{N_3}{A_3} = \frac{57,7}{4} = 14,4 \text{ kN/sm}^2 \quad (\text{gysylma})$$

1.39. $\Delta \varphi = 0,894 \text{ sm}$



Statikanyň deňlemelerini düzýäris.

A düwün üçin

$$\Sigma X = -N_1 \cos 45^\circ + N_2 \cos 45^\circ = 0,$$

$$N_1 = N_2;$$

$$\Sigma Y = N_1 \sin 45^\circ + N_2 \sin 45^\circ - N_3 = 0,$$

$$2 N_1 \sin 45^\circ = N_3 \Rightarrow N_3 = \sqrt{2} N_1$$

Ç düwün üçin

$$\Sigma X = -N_4 \sin 45^\circ + N_5 \sin 45^\circ = 0,$$

$$\Sigma Y = N_3 + 2N_4 \cos 45^\circ - P = 0,$$

$$N_3 + \sqrt{2}N_4 = P$$

Durkuny üýtgetmäniň bilelikdäki deňlemesi

$$\Delta_C = \Delta_A + \Delta - \ell_C; \quad \Delta_C = \frac{\Delta \ell_4}{\cos 45^\circ}, \quad \Delta_A = \frac{\Delta \ell_1}{\cos 45^\circ}$$

$$\text{onda } \frac{N_4 a \sqrt{2}}{EA \cos \alpha} = \frac{N_1 a \sqrt{2}}{EA \cos \alpha} + \frac{N_3 a \sqrt{2}}{EA}$$

$$\begin{cases} 2N_4 = 2N_1 + N_3 \\ N_3 = \sqrt{2}N_1 \\ N_3 + \sqrt{2}N_4 = P \end{cases}$$

Bu ýerden $N_4 = 44,7 \text{ kN}$
onda

$$\Delta_C = \frac{\Delta \ell_4}{\cos 45^\circ} = \frac{N_4 a \sqrt{2}}{EA \cdot \cos 45^\circ} = \frac{2N_4 a}{EA} = \frac{2 \cdot 44,7 \cdot 100}{2 \cdot 10^4 \cdot 5} = 0,894 \text{ sm}$$

1.40. $[P] = 1250 \text{ kN}$

Deňagramlylygyň deňlemesi

$$\Sigma M_A = N_1 \cdot 2 + N_2 \cdot 4 - P \cdot 2 = 0$$

$$N_1 + 2N_2 = P$$

Durkuny üýtgetmäniň deňlemesi

$$BB_1 = \Delta \ell_1, \quad CC_1 = \Delta \ell_2$$

$$\Delta ABB_1 \propto \Delta ACC_1$$

$$\frac{\Delta \ell_1}{2} = \frac{\Delta \ell_2}{4} \Rightarrow \Delta \ell_2 = 2\Delta \ell_1 \quad (2)$$

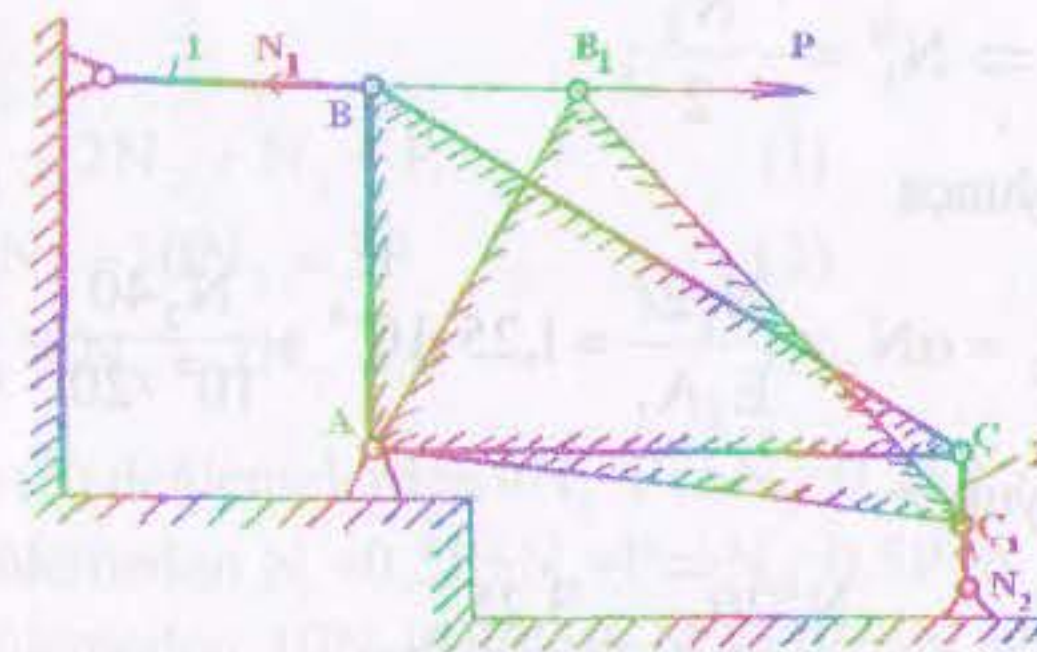
$$\text{Onda } \frac{N_2 \cdot 100}{1,2 \cdot 10^4 \cdot 50} = 2 \frac{N_1 \cdot 200}{2 \cdot 10^4 \cdot 30} \Rightarrow N_2 = 2N_1 \quad (3)$$

(3) aňlatmany (1) deňlemä goýup alarys:

$$N_1 = 0,2 P, \quad N_2 = 0,4 P$$

Sterženlerdäki dartgynlylyklar

$$\sigma_1 = \frac{N_1}{A_1} = \frac{0,2}{30} = 0,00667 P, \quad \sigma_2 = \frac{0,4}{50} = 0,008 P,$$

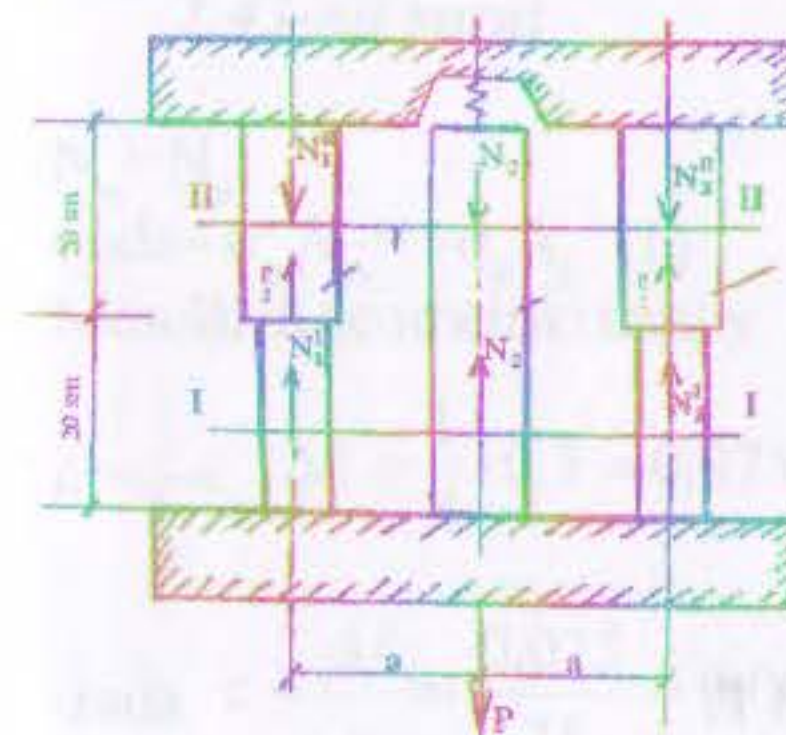


1.40-njy surat

$\sigma_2 > \sigma_1$, şonuň üçin hem çöýün sterženiň berklige çydamlylygyndan rugsat edilyän güýji kesgitleýäris.

$$\sigma_2 = 0,008[P] = [\sigma]_c \Rightarrow [P] = \frac{[\sigma]_c}{0,008} = \frac{10}{0,008} = 1250 \text{ kN}$$

1.41. $\sigma_1^I = -0,9 \text{ kN/sm}^2, \quad \sigma_1 = 10,26 \text{ kN/sm}^2, \quad \sigma_2 = 1,44 \text{ kN/sm}^2.$



1.41-nji surat

Deňagramlylygyň deňlemesi

I-I kesik

$$1) \quad N_1^I + N_2 + N_3^I = P, \quad N_1^I = N_3^I$$

II-II kesik

$$2) \quad N_1^{II} + N_2 + N_3^{II} = 0, \quad N_1^{II} = N_3^{II}$$

Durkuny üýtgetmäniň deňlemesi

$$3) \quad \Delta \ell_2^{II} = \Delta \ell_2 + \alpha N_2 = \Delta \ell_1$$

$$4) \quad \Delta \ell_1 = \Delta \ell_1^{II} + \Delta \ell_1^I, \quad \Delta \ell_2 = \frac{N_2 2\ell}{E_2 A_2}$$

(1) deñleme boýunça

$$2N_1^I + N_2 = P \Rightarrow N_1^I = \frac{P - N_2}{2};$$

(2) deñleme boýunça

$$2N_1^{II} + N_2 = 0 \Rightarrow N_1^{II} = -\frac{N_2}{2};$$

(3) deñleme boýunça

$$\Delta \ell_1 = \alpha N_2 + \Delta \ell_2 = \alpha N_2 + \frac{N_2 2\ell}{E_2 A_2} = 1,25 \cdot 10^{-4} + \frac{N_2 40}{10^4 \cdot 20} = \frac{3,25}{10^4} N_2;$$

(4) deñleme boýunça

$$\Delta \ell_1 = \frac{N_1^{II} 20}{2 \cdot 10^4 \cdot 20} + \frac{N_1^I 20}{2 \cdot 10^4 \cdot 16} = \frac{3,25}{10^4} N_2,$$

$$N_1^{II} + \frac{N_1^I}{1,6} = 3,25 N_2 \Rightarrow \frac{P - N_2}{2} - \frac{N_2}{2 \cdot 1,6} = 3,25 N_2 \Rightarrow N_2 = 28,8 \text{ kN}$$

$$N_1^I = \frac{P - N_2}{2} = \frac{234 - 28,8}{2} = 102,6 \text{ kN},$$

$$N_1^{II} = -\frac{N_2}{2} = -\frac{28,8}{2} = -14,4 \text{ kN}.$$

Değişli dartgynlyklar:

$$\sigma_1^{II} = \frac{N_1^{II}}{A_1^I} = \frac{-14,4}{16} = -0,9 \text{ kN/sm}^2,$$

$$\sigma_1^I = \frac{N_1^I}{A_1} = \frac{102,6}{10} = 10,26 \text{ kN/sm}^2,$$

$$\sigma_2 = \frac{N_2}{A_2} = \frac{28,8}{20} = 1,44 \text{ kN/sm}^2.$$

1.42. $N_1 = 0,4 P$, $N_2 = 0,25 P$, $N_3 = 0,1 P$.

Meseläniň statiki tarapy

1) $\Sigma Y = N_1 + 2N_2 + N_3 - P = 0;$



1.42-nji surat

2) $\Sigma M_V = N_3 \cdot 50 + P15 - N_1 50 = 0.$

Meseläniň geometriki tarapy

$$\Delta \ell_2 = \frac{\Delta \ell_1 + \Delta \ell_3}{2} \Rightarrow 2\Delta \ell_2 = \Delta \ell_1 + \Delta \ell_3,$$

$$2N_2 = N_1 + N_3.$$

Onda

$$\begin{cases} N_1 + 2N_2 + N_3 - P = 0 & (1) \\ 10N_1 - 10N_3 = 3P & (2) \\ N_1 + N_3 - 2N_2 = 0 & (3) \end{cases}$$

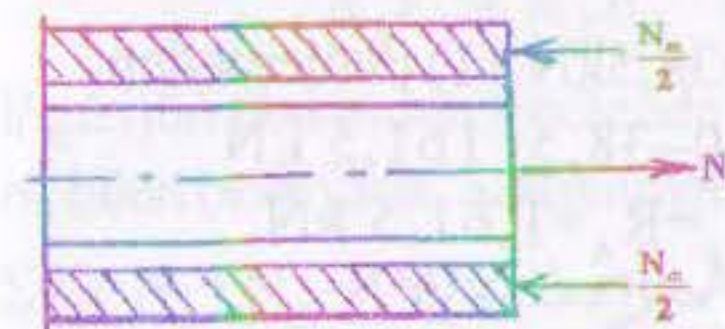
(1) we (3) deñlemelerden $4N_2 = P \Rightarrow N_2 = 0,25P$

(1) deñlemeden $N_1 + 0,5P + N_3 = P \Rightarrow N_3 = 0,5P - N_1$

(2) deñlemeden $10N_1 - 10(0,5P - N_1) = 3P \Rightarrow N_1 = 0,4P$

$$N_3 = 0,5P - N_1 = 0,5P - 0,4P = 0,1P.$$

1.43. $\sigma_p = 12,74 \text{ kN/sm}^2$, $\sigma_m = -3,636 \text{ kN/sm}^2$.



1.43-nji surat

$$A_p = \frac{\pi d_1^2}{4} = \frac{3,14 \cdot 2^2}{4} = 3,14 \text{ sm}^2,$$

$$A_m = \frac{\pi}{4} (d_3^2 - d_2^2) = \frac{3,14}{4} (4,5^2 - 2,5^2) = 1 \text{ sm}^2$$

Meseläniň statiki tarapyna seredyäris.

$$N_m = N_p$$

onda $\sigma_m A_m = -\sigma_p A_p$ (1)

Meseläniň geometriki tarapy

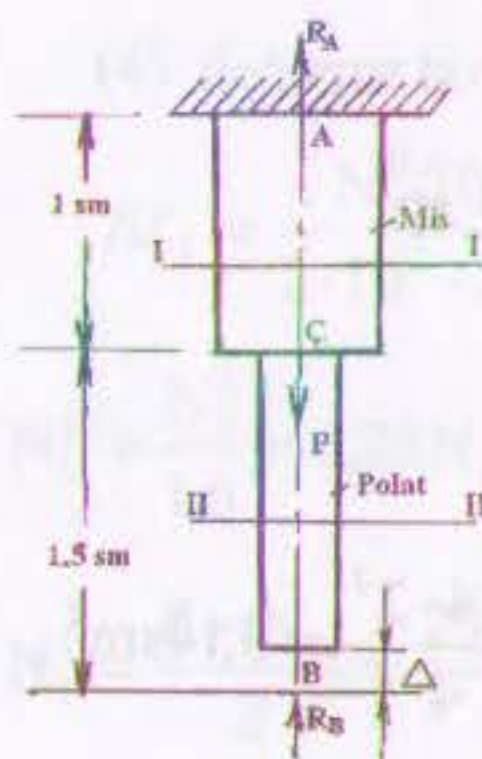
$$\varepsilon = \varepsilon_p - \varepsilon_m; \Delta \ell = \frac{1}{4} \cdot 0,3 = 0,075 \text{ sm},$$

onda $\varepsilon = \frac{\Delta \ell}{\ell} = \frac{0,075}{75} = 0,001$, $\varepsilon_m = \frac{-\sigma_m}{E_m}$, $\varepsilon_p = \frac{\sigma_p}{E_p}$,

$$\begin{cases} \frac{\sigma_p}{E_p} - \frac{\sigma_m}{E_m} = 0,001 \\ -\sigma_m A_m = \sigma_p A_p \end{cases}$$

$$\frac{\sigma_p}{E_p} + \frac{A_p}{A_m} \cdot \frac{\sigma_p}{E_m} = 0,001 \Rightarrow \sigma_p = 12,74 \text{ kN/sm}^2, \sigma_m = -6,636 \text{ kN/sm}^2.$$

1.44. $\sigma_y = 1,07 \text{ kN/sm}^2, \sigma_a = -0,77 \text{ kN/sm}^2.$



1.44-nji surat

Meseläniň statik tarapy.

$$\Sigma Y = R_A + R_B - P = 0 \quad (1)$$

Meseläniň geometrik tarapy

$$\Delta \ell_p - \Delta \ell_{R_B} = \Delta \quad (2)$$

$$\frac{P \cdot 100}{E_y \cdot A_y} - \frac{R_B \cdot 100}{E_y \cdot A_y} - \frac{R_B \cdot 150}{E_a \cdot A_a} = \Delta$$

Bu ýerden $R_B = 38,5 \text{ kN}$ (1) deňlemeden

$$R_A = P - R_B = 200 - 38,5 = 161,5 \text{ kN}$$

$$\text{AÇ bölekde } N_y = R_A = 161,5 \text{ kN}$$

$$\text{BÇ bölekde } N_a = R_B = -38,5$$

Bu böleklerdäki dartgynlylyklar

$$\sigma_y = \frac{N_y}{A_y} = \frac{161,5}{150} = 1,076 \text{ kN/sm}^2,$$

$$\sigma_a = \frac{N_a}{A_a} = -\frac{38,5}{50} = -0,77 \text{ kN/sm}^2.$$

1.45. $\sigma_1 = -0,8 \text{ kN/sm}^2, \sigma_2 = -0,2 \text{ kN/sm}^2.$

Statikanyň deňagramlylygynyň deňlemesi

$$\Sigma Y = 2N_1 + N_2 - P = 0; \quad (1)$$

Durkuny üýtgetmäniň deňlemesi

$$\Delta l_1 - \Delta l_2 = \Delta \quad (2)$$

ýa-da $\frac{N_1 \cdot 350}{1400 \cdot 400} - \frac{N_2 \cdot 350}{1400 \cdot 400} = 0,15 \Rightarrow N_1 - N_2 = 240 \quad (3)$

(3) aňlatmany (1) deňlemä goýup alarys:

$$2N_1 + (N_1 - 240) = 720 \Rightarrow N_1 = 320 \text{ kN}, \quad N_2 = 80 \text{ kN}.$$

Sütünlerdäki dartgynlylyklar:

$$\sigma_1 = \frac{-N_1}{A} = \frac{-320}{400} = -0,8 \text{ kN/sm}^2;$$

$$\sigma_2 = \frac{-N_2}{A} = \frac{-80}{400} = -0,2 \text{ kN/sm}^2.$$

1.46. $\sigma_1^I = -\frac{PA_2}{A_1E_1 + A_2E_2} \cdot \frac{E_1 - mE_2}{mA_1 + A_2},$

$$\sigma_2 = \frac{PA_1}{A_1E_1 + A_2E_2} \cdot \frac{E_1 - mE_2}{mA_1 + A_2}.$$

P güýjüň täsirinden steržende we turbada döreýän dartgynlylyklary σ_1 we σ_2 bilen belleýäris. Statikanyň deňlemesini ýazýarys

$$\Sigma X = N_1 + N_2 - P = 0 \Rightarrow A_1\sigma_1 + A_2\sigma_2 = P. \quad (1)$$

Durkuny üýtgetmäniň deňlemesi

$$\frac{\sigma_1}{E_1} = \frac{\sigma_2}{E_2} \quad (2)$$

Alnan deňlemeleri bilelikde işläp taparys:

$$\sigma_1 = \frac{PE_1}{A_1E_1 + A_2E_2} \text{ we } \sigma_2 = \frac{PE_2}{A_1E_1 + A_2E_2}.$$

P güýç bilen ýüklenmedik ýagdaýynda steržen we turba üçin statika bize aşakdaky deňlemäni berýär.

$$A_1\sigma_1^I + A_2\sigma_2^I = 0, \quad (3)$$

Başga tarapdan meseläniň şertine görä

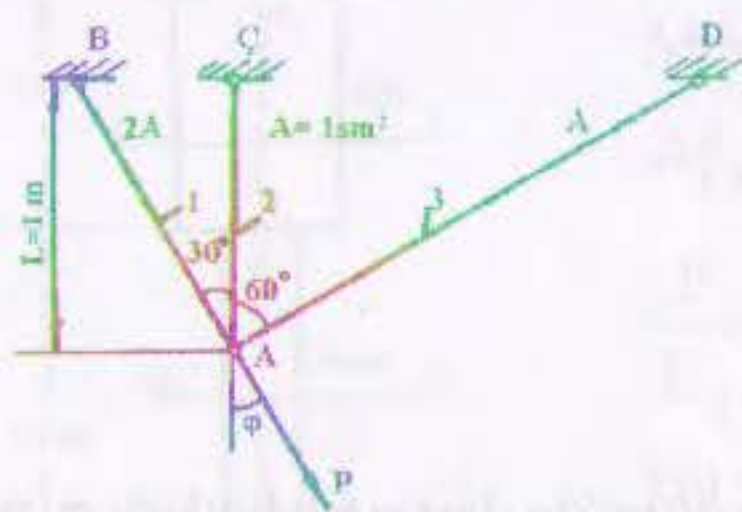
$$\frac{\sigma_1 + \sigma_1^I}{\sigma_2 + \sigma_2^I} = m. \quad (4)$$

Ýokardaky deňlemeleri bilelikde işläp taparys:

$$\sigma_1^I = \frac{PA_2}{A_1E_1 + A_2E_2} \cdot \frac{E_1 - mE_2}{mA_1 + A_2},$$

$$\sigma_2^I = \frac{PA_1}{A_1E_1 + A_2E_2} \cdot \frac{E_1 - mE_2}{mA_1 + A_2}.$$

1.47. $P=24,8\text{kN}$, $\varphi=12,4^\circ$.



1.47-nji surat

$$l_1 = l_2 / \cos 30^\circ, \quad l_3 = l_2 / \cos 60^\circ.$$

Statikanyň deňlemesinden

$$\begin{cases} 0,866N_3 - 0,5N_1 = -P \sin \varphi, \\ N_2 + 0,866N_1 + 0,5N_3 = P \cos \varphi \end{cases} \quad (1).$$

Durkuny üýtgetmäniň deňlemesiinden

$$\Delta l_2 = \Delta = 0,05 \text{ sm}$$

$$\Delta l_1 = \Delta l_2 \cos 30^\circ, \quad \Delta l_3 = \Delta l_2 \cos 60^\circ.$$

Gukuň kanuny ulanyp, soňky aňlatmadan

$$N_1 = \frac{\Delta l_1 EA_1}{l_1}, \quad N_2 = \frac{\Delta l_2 EA_2}{l_2}, \quad N_3 = \frac{\Delta l_3 EA_3}{l_3},$$

Bu ýerden $N_1=14,8 \text{ kN}$, $N_2=10 \text{ kN}$, $N_3=2,5 \text{ kN}$.

Bu bahalary (1) deňlemelere goyup alarys:

$$\begin{cases} 0,866 \cdot 2,5 - 0,5 \cdot 14,8 = -P \sin \varphi \\ 10 + 0,866 \cdot 14,8 + 0,5 \cdot 2,5 = P \cos \varphi \end{cases}$$

Bu ýerden $\varphi=12,4^\circ$, $P=24,8\text{kN}$.

1.48. $\sigma_p = -5\text{kN/sm}^2$, $\sigma_v = -3\text{kN/sm}^2$.

Meseläniň statiki tarapyndan $N_1=N_3$, $2N_1+N_2=P$

Meseläniň geometriki tarapy

$$\Delta l_1 = \Delta l_3, \quad \Delta + \Delta l_2 = \Delta_{pr} + \Delta l_1, \quad \Delta_{pr} = N \cdot \alpha.$$

Soňky deňlemelerdäki durkuny üýtgetmeleri Gukuň kanuny boýunça aňladyp alarys:

$$\Delta + \frac{N_2 l_2}{E_2 A_2} = \Delta_{pr} + \frac{N_1 l_1}{E_1 A_1}, \quad l_1 = 100 \text{ sm}, \quad l_2 = 99,95 \text{ sm}.$$

$$\Delta + \frac{(P - 2N_1) l_2}{E_2 A_2} = \Delta_{pr} + \frac{N_1 l_1}{E_1 A_1} \Rightarrow N_1 = 100 \text{ kN}.$$

Onda $N_2 = P - 2N_1 = 350 - 2 \cdot 100 = 150 \text{ kN}$.

Çetki we ortaky direlgelerdäki dartgynlylyklar

$$\sigma_1 = \sigma_p = -\frac{N_1}{A_1} = -\frac{100}{20} = -5 \text{ kN/sm}^2$$

$$\sigma_2 = \sigma_v = -\frac{N_2}{A_2} = -\frac{150}{50} = -3 \text{ kN/sm}^2$$

1.49. $\sigma_y = -6,66\text{kN/sm}^2$, $\sigma_a = -3,33\text{kN/sm}^2$.

Statikanyň deňlemesinden $R_A = R_B$

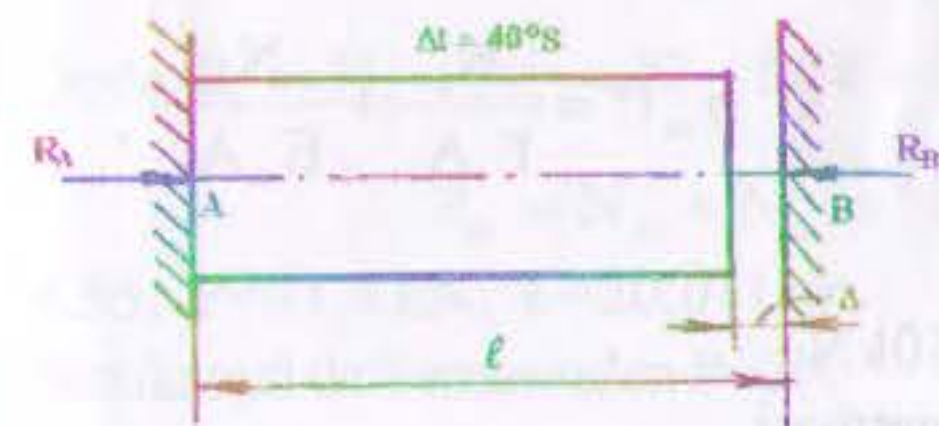
Meseläniň geometrik tarapyndan $\Delta l_1 = \Delta l_{RB}$

$$\text{ýa-da } \alpha \Delta l_1 2a = \frac{R_B a}{EA_1} + \frac{R_B a}{EA_2} \Rightarrow R_B = 33,33 \text{ kN}, \quad R_A = 33,33 \text{ kN}.$$

$$N_a = -R_B = -33,33 \text{ kN}, \quad N_y = -R_A = -33,33 \text{ kN}.$$

$$\text{Onda } \sigma_a = -\frac{N_a}{A_2} = -\frac{-33,33}{10} = -3,33 \text{ kN/sm}^2,$$

$$\sigma_y = -\frac{N_y}{A_1} = -\frac{33,33}{5} = -6,66 \text{ kN/sm}^2$$



1.50-nji surat

1.50. $\sigma = -9,50\text{kN/sm}^2$.

Statikanyň deňlemesi

$$R_A = R_B \quad (1)$$

Durkuny üýtgetmäniň bilelikdäki deňlemesi

$$\Delta \ell_i - \Delta \ell_{R_B} = \Delta \quad (2)$$

$$\alpha \Delta t_i \ell - \frac{R_A \ell}{EA} = \Delta \Rightarrow 1,25 \cdot 10^{-5} \cdot 40 \cdot 200 - \frac{R_A \cdot 200}{2 \cdot 10^4 \cdot A} = 0,005.$$

Bu ýerden $R_A = 9,5A$, $R_A = R_B = 9,5A$ kN, $N = -R_A = -9,5A$.

$$\sigma = \frac{N}{A} = \frac{-9,5A}{A} = -9,5 \text{ kN/sm}^2.$$

1.51. $\Delta = +0,056$ sm (iki sterženiňki).

$$\Delta \ell = \frac{N \ell}{EA} = \frac{\sigma_1 \ell}{E}$$

Temperatura dartgynlylygy $\sigma_t = \pm E \alpha \Delta t$, $\Delta t = -10^\circ \text{S}$ temperatura sterženlerde süýnme dartgynlylyklaryny döredýär, onda

$$\sigma_t = E \alpha \Delta t = 2 \cdot 10^4 \cdot 1,25 \cdot 10^{-5} \cdot 10 = 2,5 \text{ kN/sm}^2,$$

$$\sigma_1^I = \sigma_1 + \sigma_t = 2,5 + 1,5 = 4 \text{ kN/sm}^2,$$

$$\sigma_2^I = \sigma_2 + \sigma_1^I = 8 - 4 = 4 \text{ kN/sm}^2.$$

$$\text{Onda } \Delta_1 = \frac{\sigma_2^I \ell}{E} = \frac{4 \cdot 140}{2 \cdot 10^4} = 0,028 \text{ sm}.$$

Umumy uzalma

$$\Delta = \Delta_1 + \Delta_2 = 0,028 + 0,028 = 0,056 \text{ sm}.$$



1.50-nji surat

Bu ýerden $N_m = N_i = 150 \text{ kN} \Rightarrow P = 150 \text{ kN}$.

Misiň we inwaryň erkin durkuny üýtgetmesi

1.52. $P = 150 \text{ kN}$, $\ell_m = 50,01 \text{ sm}$, $\ell = 49,99 \text{ sm}$.

$$\varepsilon_t = \varepsilon_i + \varepsilon_m \quad (1) \quad N_i = N_m;$$

$$\varepsilon_t = (\alpha_m + \alpha_i)t,$$

$$\alpha_m t^\circ = \frac{N_i}{E_i A_i} + \frac{N_m}{E_m A_m},$$

$$\Delta \ell_m = \frac{N_m \ell_m}{E_m A_m} = \frac{150 \cdot 50}{10^4 \cdot 37,5} = 0,02 \text{ sm},$$

$$\Delta \ell_i = \frac{N_i \ell_i}{E_i A_i} = \frac{150 \cdot 50}{2 \cdot 10^4 \cdot 37,5} = 0,01 \text{ sm}.$$

Onda $\ell_m = 50 + (\Delta \ell_m - \Delta \ell_i) = 50 + (0,02 - 0,01) = 50,01 \text{ sm}$,

$$\ell_i = 50 - (\Delta \ell_m - \Delta \ell_i) = 50 - 0,01 = 49,99 \text{ sm}.$$

1.53. $\sigma = -0,1 \text{ kN/sm}^2$.

Plitada döreyän boý güýji direglerdäki gaýtargylara deň we bu güýji durkuny

üýtgetmäniň deňlemesinden tapýarys. $\Delta \ell_i - \Delta \ell_N = \Delta$ ýa-da $\alpha \Delta t \ell - \frac{N \ell}{EA} = \Delta$.

Bu ýerden $N = \frac{EA(\alpha \Delta t \ell - \Delta)}{\ell}$ – plitanyň bir inindäki güýç, $N = -400 \text{ kN}$.

Plitanyň kesigindäki dartgynlylyk

$$\sigma = \frac{N}{A} = -\frac{400}{100 \cdot 40} = -0,1 \text{ kN/sm}^2.$$

1.54. Temperatura üýtgeýänçä $P_p = 27 \text{ kN}$, $P_m = 18 \text{ kN}$.

Temperatura üýtgände $P_p = 1,26 \text{ kN}$, $P_m = 32,4 \text{ kN}$.

Statikanyň deňlemesi $N_p + N_m = P$ (1).

Durkuny üýtgetmäniň deňlemesi $\varepsilon_p = \varepsilon_m$ (2).

(1) we (2) deňlemäni bilelikde işläp, $N_p = 27 \text{ kN}$, $N_m = 18 \text{ kN}$.

Diregler $\Delta t = 30^\circ \text{S}$ gyzdyrylanda,

$$N_p^I = N_m^I \quad (1) \quad \varepsilon_m^I - \varepsilon_m^N = \varepsilon_p^I + \varepsilon_p^N. \quad (2)$$

Bu deňlemeleri işläp alarys.

$$N_p^I = N_m^I = 14,4 \text{ kN}$$

$$\text{Onda } P_p = N_p - N_p^I = 27 - 14,4 = 12,6 \text{ kN},$$

$$P_m = N_m + N_m^I = 18 + 14,4 = 32,4 \text{ kN}.$$

1.55. $P = 31,4 \text{ kN}$, $\ell = 20,011 \text{ sm}$.

Statikanyň deňlemesinden $P = 2N_b$

$$A_b = \frac{\pi d^2}{4} = \frac{3,14 \cdot 1^2}{4} = 0,785 \text{ sm}^2,$$

$$\Delta \ell = (\ell_2 - \ell_1) = 20,02 - 20 = 0,02 \text{ sm},$$

onda

$$\frac{N_b \ell_1}{E_b A_b} = 0,02 \Rightarrow N_b = \frac{0,02 \cdot E_b \cdot A_b}{\ell_1} = \frac{0,02 \cdot 2 \cdot 10^4 \cdot 0,785}{20} = 15,7 \text{ kN},$$

$$P = 2N_b = 2 \cdot 15,7 = 31,4 \text{ kN}.$$

P güýç aýrylandan soň, boltlardaky dartuw güýçleriniň bir bölegini mis steržen kabul edýär.

Statikanyň deňlemesinden $2N_b = N_m = 31,4 \text{ kN}$.

Durkuny üýtgetmäniň deňlemesi $\varepsilon_m = \varepsilon_b$

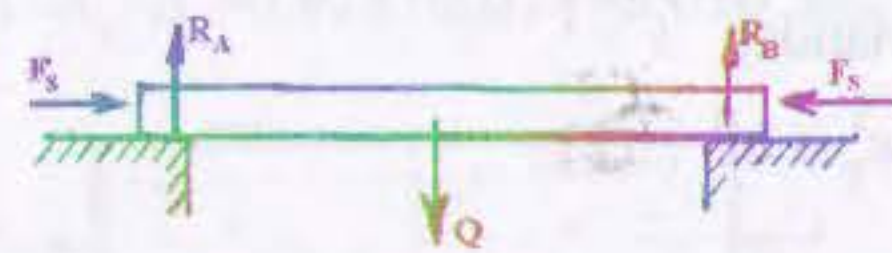
$$\frac{N_m}{E_m A_m} = \frac{N_b}{E_b A_b} \Rightarrow N_m = \frac{E_m A_m}{E_b A_b} N_b,$$

$$\Delta = \Delta \ell_b^1 - \Delta \ell_m^1,$$

onda

$$\Delta = \frac{N_b \cdot \ell_1}{E_b A_b} - \frac{N_m \cdot \ell_2}{E_m A_m} = \frac{15,7 \cdot 20,02}{2 \cdot 10^4 \cdot 0,785} - \frac{31,4 \cdot 20,02}{10^4 \cdot 6} = 0,0095 \text{ sm},$$

$$\ell = \ell_2 - \Delta = 20,02 - 0,0095 = 20,011 \text{ sm}.$$



1.56-njy surat

$$1.56. \Delta t = \pm 2,97^\circ \text{S},$$

$$\sigma = \pm 0,743 \text{ kN/sm}^2$$

$$R_A = R_B = \frac{Q}{2} = \frac{100}{2} = 50 \text{ kN}$$

$$F_s = f \cdot R_A = 0,3 \cdot 50 = 15 \text{ kN},$$

$$\sigma = \Delta t \alpha E = \frac{F_s}{A} \Rightarrow \Delta t = \frac{F_s}{\alpha E A}$$

16-njy belgili iki tawra üçin $A = 20,2 \text{ sm}^2$

$$\text{onda } \Delta t = \pm \frac{15}{20,2 \cdot 1,25 \cdot 10^{-5} \cdot 2 \cdot 10^4} \cong \pm 2,97^\circ \text{S}$$

bu ýerden $\sigma = \alpha \cdot \Delta t \cdot E = \pm 1,25 \cdot 10^{-5} \cdot 12 \cdot 10^4 \cdot 2,97 = \pm 0,743 \text{ kN/sm}^2$

$$1.57. \Delta t = 5^\circ \text{mm}, \sigma_t = 12,5 \text{ kN/sm}^2.$$

Zerur bolan boşlugyň ululygy ($\Delta t = 50^\circ \text{S}$)

$$\Delta t = \alpha \Delta t \ell = 1,25 \cdot 10^{-5} \cdot 50 \cdot 800 = 0,5 \text{ sm}$$

Boşluk bolmadyk ýagdaýynda relsde döreýän gysma dartgynlyk

$$\sigma_t = -\alpha \Delta t E = -1,25 \cdot 10^{-5} \cdot 50 \cdot 2 \cdot 10^4 = -12,5 \text{ kN/sm}^2$$

$$1.58. \ell_1 = 30,062 \text{ m}, \sigma = -41,25 \text{ kN/sm}^2.$$

Polat turbanyň temperaturanyň ýokarlanmagy sebäpli erkin uzynlygyna giňelmegi

$$\Delta \ell_t = \alpha \Delta t \ell = 1,25 \cdot 10^{-5} \cdot 165 \cdot 3000 = 6,2 \text{ sm},$$

$$\text{onda } \ell_1 = \ell + \Delta \ell_t = 30 + 0,062 = 30,062 \text{ m}.$$

Meseläniň ikinji şerti aşakdaky formula bilen tapylýar.

$$\sigma_t = -\alpha \Delta t E = -1,25 \cdot 10^{-5} \cdot 165 \cdot 2 \cdot 10^4 = -41,25 \text{ kN/sm}^2.$$

$$1.59. \text{ a) } \sigma = 18,4 \text{ kN/sm}^2, \text{ b) } \sigma_1 = 0,7 \text{ kN/sm}^2, \text{ ç) } t_2 = 545^\circ \text{S}.$$

a) Halkadaky dartgynlyk

$$\sigma = E \cdot \varepsilon = \alpha_m (t_1 - t_0) E_m = 1,6 \cdot 10^{-5} (135 - 20) \cdot 10^4 = 18,4 \text{ kN/sm}^2.$$

b) Waly we halkany bir wagtda 0°S -a çenli sowadylanda halkada döreýän goşmaça dartgynlyk

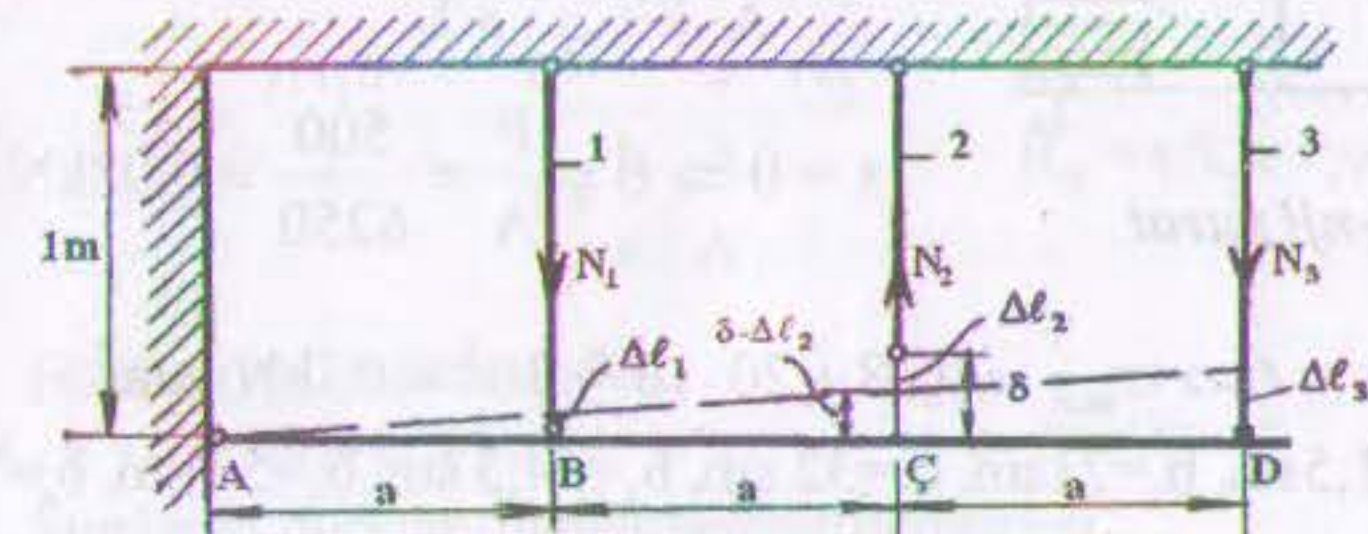
$$\sigma_1 = (\alpha_m - \alpha_p) t_0 E_m = (1,6 \cdot 10^{-5} - 1,25 \cdot 10^{-5}) \cdot 200 \cdot 10^4 = 0,7 \text{ kN/sm}^2.$$

Halkadaky doly dartgynlyk $\sigma = \sigma + \sigma_1 = 19,1 \text{ kN/sm}^2$.

ç) Halkadaky dartgynlyk nola deň bolmak üçin aşakdaky şert ýerine ýetirilmeli

$$\sigma_2 = (\alpha_m - \alpha_p) E_m t_2, \text{ bu ýerden } t_2 = \frac{\sigma_2}{(\alpha_m - \alpha_p) E_m} = 545^\circ \text{S}.$$

$$1.60. \sigma = -143 \text{ kN/sm}^2 \quad \sigma = 715 \text{ kN/sm}^2 \quad \sigma = -429 \text{ kN/sm}^2.$$



1.60-njy surat

Statikanyň deňlemesi $\Sigma M_A = N_1 a - N_2 2a + 3N_3 = 0$ (1)

Durkuny üýtgetmäniň deňlemesi

$$\frac{\Delta \ell_1}{a} = \frac{\delta - \Delta \ell_2}{2a} \text{ we } \frac{\Delta \ell_1}{a} = \frac{\Delta \ell_3}{3a} \Rightarrow 3N_1 = N_3 \quad (2)$$

$$2 \frac{N_1 100}{2 \cdot 10^4 \cdot 20} = 0,05 - \frac{N_2 100}{2 \cdot 10^4 \cdot 20} \Rightarrow N_1 + 0,5N_2 = 100 \quad (3)$$

(1), (2) we (3) deňlemeleri bilelikde işläp alarys:

$N_1 = 28,5 \text{ kN}$, $N_2 = 143 \text{ kN}$, $N_3 = 85,5 \text{ kN}$.

Değişli dartgynlyklary

$$\sigma_1 = \frac{-N_1}{A} = -\frac{28,5}{20} = -1,43 \text{ kN/sm}^2;$$

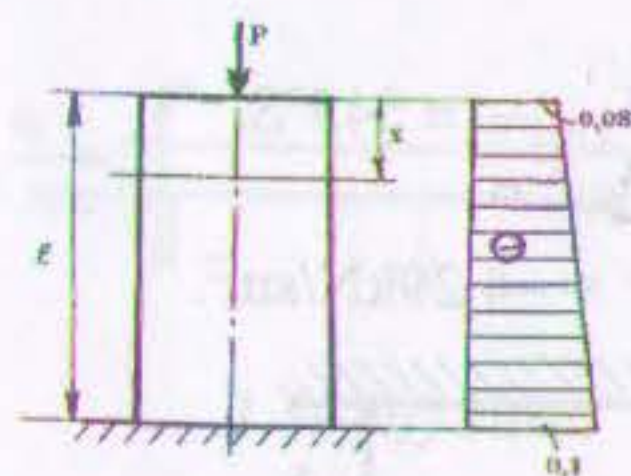
$$\sigma_2 = \frac{N_2}{A} = \frac{143}{20} = 7,15 \text{ kN/sm}^2;$$

$$\sigma_3 = -\frac{N_3}{A} = -\frac{85,5}{20} = -4,29 \text{ kN/sm}^2.$$

1.61. $\sigma = 0,016 \text{ kN/sm}^2$.

$$\sigma = \gamma \ell = 20 \cdot 8 = 160 \text{ kN/m}^2 = 0,016 \text{ kN/sm}^2.$$

1.62. $79 \times 79 \text{ sm}^2$.



1.62-nji surat

$$A = \frac{P}{[\sigma] - \gamma \ell} = \frac{500}{0,1 - 20 \cdot 10^{-6} \cdot 10^3} = 6250 \text{ sm}^2$$

$$a \times a = 79 \times 79 \text{ sm}^2$$

$$\sigma = \frac{P}{A} + \gamma x$$

$$x = 0 \Rightarrow \sigma = \frac{P}{A} = \frac{500}{6250} = 0,08 \text{ kN/sm}^2$$

$$x = \ell \Rightarrow \sigma_{\max} = 0,08 + 20 \cdot 10^{-6} \cdot 10^3 = 0,1 \text{ kN/sm}^2$$

1.63. $b_1 = 11,5 \text{ sm}$, $b_2 = 21 \text{ sm}$, $b_3 = 32 \text{ sm}$, $b_4 = 44,5 \text{ sm}$, $b_5 = 54 \text{ sm}$, $b_6 = 76 \text{ sm}$, $b_7 = 125 \text{ sm}$.

Hasap ýokarky diwardan başlanýar.

$$b_1 = \frac{q_1}{[\sigma] - \gamma \cdot 4} = 11,5 \text{ sm},$$

$$b_2 = \frac{q_1 + q_2 + \gamma b_1 \cdot 4}{[\sigma] - \gamma \cdot 4} = 21 \text{ sm},$$

$$b_3 = \frac{q_1 + 2q_2 + \gamma b_1 \cdot 4 + \gamma b_2 \cdot 4}{[\sigma] - \gamma \cdot 4} = 32 \text{ sm},$$

$$b_4 = \frac{q_1 + 3q_2 + \gamma b_1 \cdot 4 + \gamma b_2 \cdot 4 + \gamma b_3 \cdot 4}{[\sigma] - \gamma \cdot 4} = 44,5 \text{ sm},$$

$$b_5 = \frac{q_1 + 4q_2 + \gamma b_1 \cdot 4 + \gamma b_2 \cdot 4 + \gamma b_3 \cdot 4 + \gamma b_4 \cdot 4}{[\sigma] - \gamma \cdot 4} = 59 \text{ sm},$$

$$b_6 = \frac{q_1 + 5q_2 + \gamma b_1 \cdot 4 + \gamma b_2 \cdot 4 + \gamma b_3 \cdot 4 + \gamma b_4 \cdot 4 + \gamma b_5 \cdot 4}{[\sigma] - \gamma \cdot 4} = 76 \text{ sm},$$

$$b_7 = \frac{q_1 + 5q_2 + q_3 + \gamma \cdot 4(b_1 + b_2 + b_3 + b_4 + b_5 + b_6)}{[\sigma] - \gamma \cdot 4} = 125 \text{ sm}.$$

1.64. $\Delta \ell = 2,8 \text{ mm}$

$$\Delta \ell = \frac{\gamma \ell^2}{2E} = \frac{78 \cdot 10^{-6} \cdot 120^2 \cdot 10^4}{2 \cdot 2 \cdot 10^4} = 0,28 \text{ sm} = 2,8 \text{ mm}.$$

$$1.65. \quad R_A = \frac{\gamma A_1 a}{2} \cdot \frac{1 + \frac{b^2}{a^2} + 2 \frac{b}{a} \frac{A_1}{A_2}}{1 + \frac{b}{a} \frac{A_1}{A_2}}, \quad R_B = \gamma A_1 a + \gamma A_2 b - R_A.$$

Statikanyň deňlemesinden

$$R_A + R_B = \gamma A_1 a + \gamma A_2 b \quad (1)$$

Sterženiň durkuny üýtgetmeginiň deňlemesi

$$\Delta l_{R_A} = \Delta l_Q \quad (2)$$

R_A gaýtargydan sterženiň uzalmasy

$$\Delta l_{R_A} = \frac{R_A a}{EA_1} \left(1 + \frac{b}{a} \cdot \frac{A_1}{A_2} \right).$$

Sterženiň hususy agramyndan gysgalmasy

$$\Delta l_Q = \frac{\gamma a^2}{2E} \left(1 + \left(\frac{b}{a} \right)^2 + 2 \frac{b}{a} \cdot \frac{A_1}{A_2} \right).$$

Soňky aňlatmalary (2) deňlemä goýup alarys:

$$\frac{R_A a}{EA_1} \left(1 + \frac{b}{a} \cdot \frac{A_1}{A_2} \right) = \frac{\gamma a^2}{2E} \left(1 + \left(\frac{b}{a} \right)^2 + 2 \frac{b}{a} \cdot \frac{A_1}{A_2} \right).$$

Bu ýerden
$$R_A = \frac{\gamma A_1 a \left(1 + \frac{b^2}{a^2} + 2 \frac{b}{a} \cdot \frac{A_1}{A_2} \right)}{2 \left(1 + \frac{b}{a} \cdot \frac{A_1}{A_2} \right)}$$

(1) deňlemeden $R_B = \gamma A_1 a + \gamma A_2 b - R_A$.

1.66. $\sigma_b = -0,0187 \text{ kN/sm}^2$, $\sigma_a = -0,28 \text{ kN/sm}^2$.

Sütüniň aşaky kesigi üçin statikanyň deňlemesi

$$N_a + N_b = (\gamma_a A_a + \gamma_b A_b) \ell; \text{ ýöne } N_a = \sigma_a A_a, N_b = \sigma_b A_b,$$

$$A_b = 25 \times 25 = 625 \text{ sm}^2 \quad n = 15 \text{ onda } \sigma_a A_a + \sigma_b A_b = (\gamma_a A_a + \gamma_b A_b) \ell$$

$$A_b = 25 \times 25 = 625 \text{ sm}^2 \quad n = 15 \text{ onda } \sigma_a A_a + \sigma_b A_b = (\gamma_a A_a + \gamma_b A_b) \ell \quad (1)$$

Durkuny üýtgetmäniň bilelikdäki deňlemesi

$$\varepsilon_a = \varepsilon_d, \text{ ýa-da } \frac{\sigma_a}{E_a} = \frac{\sigma_b}{E_b} \Rightarrow \sigma_a = \sigma_b \frac{E_a}{E_b} = n \sigma_b \quad (2)$$

(1) we (2) deňlemeleri bilelikde işläp alarys:

$$\sigma_b = \frac{(\gamma_a A_a + \gamma_b A_b)}{n A_a + A_b} = \frac{(78,5 \cdot 10^{-6} \cdot 19,6 + 25 \cdot 10^{-6} \cdot 625) \cdot 10^3}{15 \cdot 19,6 + 625} =$$

$$= 0,0187 \text{ kN/sm}^2$$

$$\sigma_a = 15 \cdot 0,0187 = 0,28 \text{ kN/sm}^2$$

1.67. $\sigma_{\max} = 8,87 \text{ kN/sm}^2$, $\Delta l = 28,03 \text{ sm}$.

Ştanganyň ýokarky kesigindäki dartgynlyk

$$\sigma = \frac{P}{A_s} + \gamma \ell$$

Toýun ergini hasaba alyp, ştanganyň göwrüm agramyny kesgitleýäris:

$$\gamma = \frac{A_s \gamma_s + A_t \gamma_t}{A_s + A_t} = \frac{136,6 \cdot 78,5 \cdot 10^{-6} + 19,6 \cdot 18 \cdot 10^{-6}}{136,6 + 19,6} = 70,3 \cdot 10^{-6} \text{ kN/sm}^2$$

onda
$$\sigma_{\max} = \frac{50}{136,6} + 70,3 \cdot 10^{-6} \cdot 0,12 \cdot 10^6 = 8,87 \text{ kN/sm}^2.$$

Gukuň kanuny esasynda absolyt durkuny üýtgetme

$$\Delta l = \frac{P \ell}{E_s A_s} + \frac{\gamma \ell^2}{2 E_s} = \frac{50 \cdot 0,12 \cdot 10^{-6}}{2 \cdot 10^4 \cdot 136,6} + \frac{70,3 \cdot 10^{-6} \cdot (0,12 \cdot 10^{-6})}{2 \cdot 2 \cdot 10^4} = 28,03 \text{ sm}$$

1.68. $\alpha = 35^\circ 20'$, $G = 0,19 \text{ kN}$.

Pürsüň deňagramlylygynyň şertinden

$$N_{AD} = \frac{q \ell}{2}, \quad N_{BD} = \frac{q \ell}{2 \sin \alpha}, \quad N_{AC} = \frac{q \ell}{2 \operatorname{tg} \alpha}.$$

Berklik şertinden sterženleriň kese kesiginiň meýdanlaryny kesgitleýäris:

$$A_{AD} = \frac{N_{AD}}{[\sigma]} = \frac{q \ell}{2 [\sigma]}, \quad A_{BD} = \frac{N_{BD}}{[\sigma]} = \frac{q \ell}{2 [\sigma] \cdot \sin \alpha},$$

$$A_{AC} = \frac{N_{AC}}{[\sigma]_s} = \frac{q\ell}{2[\sigma]_s \cdot \operatorname{tg} \alpha}.$$

onda sterženleriň agramlarynyň jemi

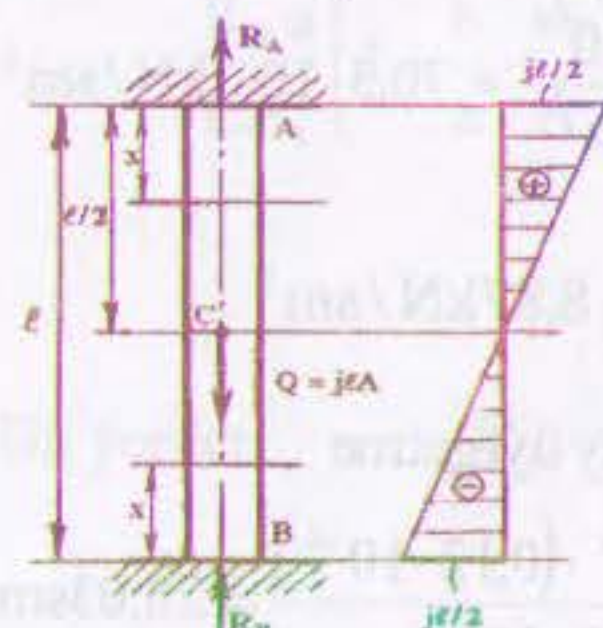
$$G = G_{AD} + G_{BD} + G_{AC} = \frac{\gamma g \ell^2}{2[\sigma]_s} \left(\operatorname{tg} \alpha + \frac{1}{\sin \alpha \cos \alpha} + \frac{[\sigma]_s}{[\sigma]_s g} \right).$$

Soňky aňlatmanyň α görä birinji önümini nola deňläp, in kiçi agramyň şertini tapýarys.

$$3\sin^2 \alpha - 1 = 0 \Rightarrow \alpha = 35^\circ 20'$$

Bu bahany umumy agramynyň aňlatmasyna goýup alarys $G = 0,19 \text{ kN}$.

$$1.69. \sigma_y = \frac{\gamma \ell}{2}, \quad \sigma_a = \frac{\gamma \ell}{2}.$$



1.69-nji surat

$$\sigma_y = \frac{R_A}{A} = \frac{\gamma \ell A}{2A} = \frac{\gamma \ell}{2}$$

Aşakdaky deňlemelerden dartgynlylygyň epýuryny gurýarys:

$$\text{AÇ bölek üçin } \sigma = \frac{R_A}{A} - \gamma x,$$

$$\text{BÇ bölek üçin } \sigma = -\frac{R_B}{A} + \gamma x$$

$$1.70. \Delta \ell = \frac{\gamma \ell^2}{6E}.$$

Statikanyň deňlemesi

$$R_A + R_B - Q = 0 \quad (1)$$

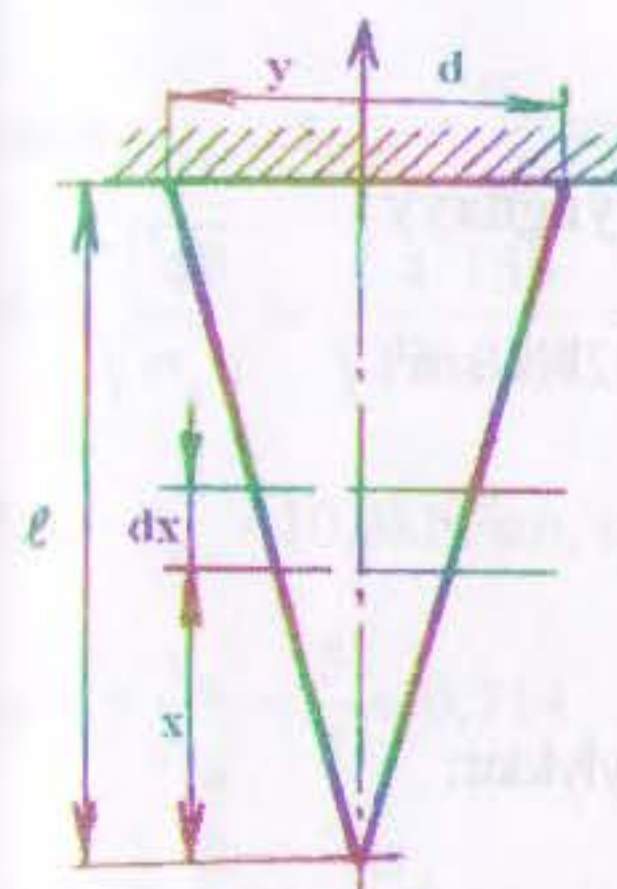
Durkuny üýtgetmäniň deňlemesi

$$\Delta \ell_Q - \Delta \ell_{R_B} = 0 \quad (2)$$

Gukun kanunyny ulanyp

$$\frac{\gamma \ell A \cdot \ell}{2EA} = \frac{R_B \ell}{EA} \Rightarrow R_B = \frac{\gamma \ell A}{2}$$

$$\text{onda } R_A = Q - R_B = \frac{\gamma \ell A}{2}$$

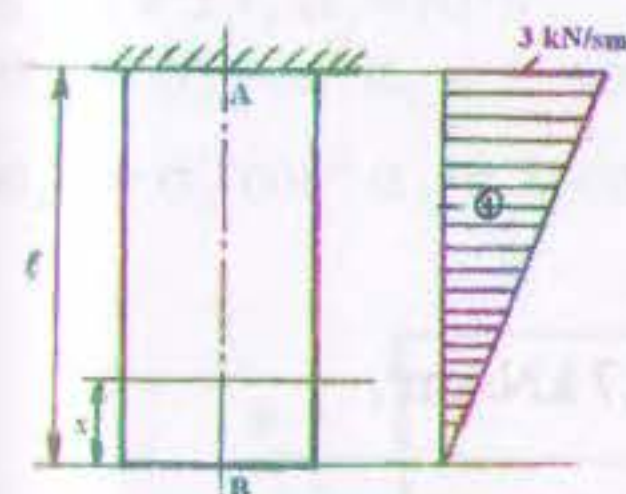


1.70-nji surat

$$\text{we sterženiň doly uzalması } \Delta \ell = \frac{\gamma}{3E} \int_0^\ell x dx = \frac{\gamma \ell^2}{6E}.$$

Bu uzalma prizmatik sterženiň uzalmasınyň üçden birine deň.

$$1.71. \ell = 382 \text{ m}.$$



1.71-nji surat

$$\text{Sterženiň agramy } Q = \frac{\pi d^2}{4} \cdot \frac{\ell}{3} \cdot \gamma$$

Sterženiň aşaky tarapynda x aralykdaky kese kesikdäki dartuw güýji aşaky böleginiň agramyna deň

$$\frac{Qx^3}{\ell^3} = \frac{\pi d^2}{4} \cdot \frac{x^3}{3\ell^2} \cdot \gamma$$

dx uzynlykdaky elemente prizma görnüşinde seredip, elementiniň

$$\text{uzalmasıny alarys: } \Delta dx = \frac{\gamma x^3}{3E} dx$$

Berklik deňlemesinden

$$\ell = \frac{[\sigma]}{\gamma} = \frac{3}{78,5 \cdot 10^{-6}} = 382 \cdot 10^2 \text{ sm}$$

ýa-da $\ell = 382 \text{ m}$.

Dartgynlylygyň epýury

$$\sigma = \gamma x$$

$$x = 0 \Rightarrow \sigma_B = 0$$

$$x = \ell \Rightarrow \sigma_A = \gamma \ell = 78,5 \cdot 10^{-6} \cdot 382 \cdot 10^2 = 3 \text{ kN/sm}^2$$

II bap

Çyzyk we tekiz dartgynlylyk ýagdaýy

2.1. $\sigma_\alpha = 6,63 \text{ kN/sm}^2$, $\tau_\alpha = 3,38 \text{ kN/sm}^2$, $\tau_{\max} = 4,42 \text{ kN/sm}^2$.

Sterženiň kese kesigindäki normal dartgynlylyk:

$$\sigma_o = \frac{4P}{\pi d^2} = \frac{4 \cdot 250}{3,14 \cdot 6^2} = 8,84 \text{ kN/sm}^2.$$

Ýapgyt kesikdäki normal we galtaşma dartgynlylyklar:

$$\sigma_\alpha = \sigma_o \cdot \cos^2 \alpha = 8,84 \cdot \cos^2 30^\circ = 6,63 \text{ kN/sm}^2,$$

$$\tau_\alpha = \frac{\sigma_o}{2} \sin 2\alpha = \frac{8,84}{2} \sin 60^\circ = 3,83 \text{ kN/sm}^2.$$

Iň uly galtaşma dartgynlylyk sterženiň okuna 45° boýunça ýapgytlanan kesikde bolýar.

$$\tau_\alpha = \frac{\sigma_o}{2} = \frac{8,84}{2} = 4,42 \text{ kN/sm}^2.$$

2.2. $\sigma_o = 8,15 \text{ kN/sm}^2$, $p_\alpha = 5,13 \text{ kN/sm}^2$, $\tau_\alpha = 2,075 \text{ kN/sm}^2$.

Kese kesikdäki dartgynlylyk:

$$\sigma_o = \frac{4P}{\pi d^2} = \frac{4 \cdot 350}{3,14 \cdot 7,5^2} = 8,15 \text{ kN/sm}^2.$$

Ýapgyt kesikdäki dartgynlylyklar:

$$\sigma_\alpha = \sigma_o \cdot \cos^2 \alpha = 8,15 \cdot \cos^2 15^\circ = 8,15 \cdot 0,759^2 = 4,7 \text{ kN/sm}^2,$$

$$\tau_\alpha = \frac{\sigma_o}{2} \sin 2\alpha = \frac{8,15}{2} \sin 30^\circ = 2,075 \text{ kN/sm}^2.$$

Doly dartgynlylyk:

$$P_\alpha = \sqrt{\sigma_\alpha^2 + \tau_\alpha^2} = \sqrt{4,7^2 + 2,075^2} = 5,13 \text{ kN/sm}^2.$$

2.3. $d = 4 \text{ sm}$

$\alpha = 45^\circ$ deň bolanda, $\tau_{\max} = 6 \text{ kN/sm}^2$ deň,

onda $\tau_{\max} = \frac{\sigma_o}{2} \Rightarrow \sigma_o = 2\tau_{\max} = 12 \text{ kN/sm}^2$

$$d = \sqrt{\frac{4P}{\sigma_o \pi}} = \sqrt{\frac{4 \cdot 150}{12 \cdot 3,14}} = 4 \text{ sm}.$$

2.4. $\sigma_{\max} = 10,6 \text{ kN/sm}^2$, $\tau_{\max} = 5,01 \text{ kN/sm}^2$.

$$\text{tg} \alpha = \frac{\tau_\alpha}{\sigma_\alpha} = \frac{5}{7} = 0,714, \quad \alpha \approx 35^\circ 30'.$$

onda $\sigma_{\max} = \frac{\sigma_\alpha}{\cos^2 \alpha} = \frac{7}{\cos^2 35^\circ 30'} = \frac{7}{0,814^2} = 10,6 \text{ kN/sm}^2$

we $\tau_{\max} = \frac{\sigma_{\max}}{2} \sin 2\alpha = \frac{10,6}{2} \sin 71^\circ = 5,3 \cdot 0,9455 = 5,01 \text{ kN/sm}^2$

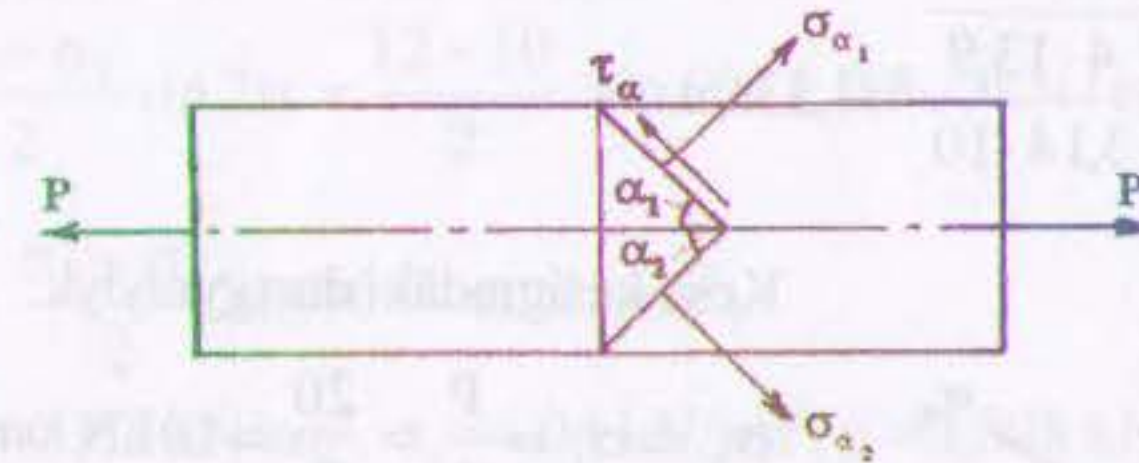
2.5. $\alpha_1 = 19^\circ 55'$, $\alpha_2 = 70^\circ 5'$, $\sigma_{\alpha_1} = 4,42 \text{ kN/sm}^2$, $\sigma_{\alpha_2} = 0,58 \text{ kN/sm}^2$.

$$\sin 2\alpha = \frac{2\tau_\alpha}{\sigma_o} = \frac{2 \cdot 1,6}{5} = 0,64,$$

$$\alpha_1 = 19^\circ 55', \quad \alpha_2 = 70^\circ 5',$$

$$\sigma_{\alpha_1} = \sigma_o \cos^2 \alpha_1 = 5 \cdot \cos^2 19^\circ 55' = 5 \cdot 0,94^2 = 4,42 \text{ kN/sm}^2,$$

$$\sigma_{\alpha_2} = \sigma_o \cos^2 \alpha_2 = 5 \cdot \cos^2 70^\circ 5' = 5 \cdot 0,34^2 = 0,58 \text{ kN/sm}^2.$$



2.5-nji surat

2.6. $q_2 = -4,8 \text{ kN/sm}^2$.

Durkuny üýtgetmäniň deňlemesi $\varepsilon_2 = \frac{1}{E}(\sigma_2 - \mu\sigma_1) = 0$,

Bu ýerden $q_2 = \sigma_2 = \mu\sigma_1 = -0,3 \cdot 16 = -4,8 \text{ kN/sm}^2$.

2.7. $P = 80 \text{ kN}$, $\alpha = 60^\circ$, $\beta = 30^\circ$.

$$\sigma_\alpha = \sigma_0 \cdot \cos^2 \alpha, \sigma_\beta = \sigma_0 \cdot \cos^2 \beta = \sigma_0 \cdot \sin^2 \alpha.$$

Jemlöp alýarys: $\sigma_\alpha + \sigma_\beta = \sigma_0 = 8 \text{ kN/sm}^2$.

Dartyjy güýç

$$P = \sigma_0 \cdot A = 8 \cdot 2 \cdot 5 = 80 \text{ kN/sm}^2.$$

$$\tan^2 \alpha = \frac{\sigma_\alpha}{\tau_\alpha} = \frac{6}{2} = 3 \Rightarrow \alpha = 60^\circ \text{ we } \beta = 30^\circ.$$

2.8. $d_1 = 13,33 \text{ mm}$

$$\varepsilon_x = \varepsilon_y = 0; \sigma_x = \sigma_y - \text{simmetriýa şertinden,}$$

$$\text{Onda } \varepsilon_x = \varepsilon_y = \frac{1}{E} [\sigma_x - \mu(\sigma_z + \sigma_y)] = 0,$$

$$\sigma_x(1-\mu) = \sigma_z \mu \Rightarrow \sigma_x = \mu \sigma_z / (1-\mu),$$

$$\sigma_z = \frac{-P}{a^2} = \frac{100}{60^2} = -0,028 \text{ kN/sm}^2,$$

$$\sigma_x = \frac{-0,4 \cdot 0,028}{(1-0,4)} = -0,0185 \text{ kN/sm}^2.$$

Boltlara täsir edýän güýç

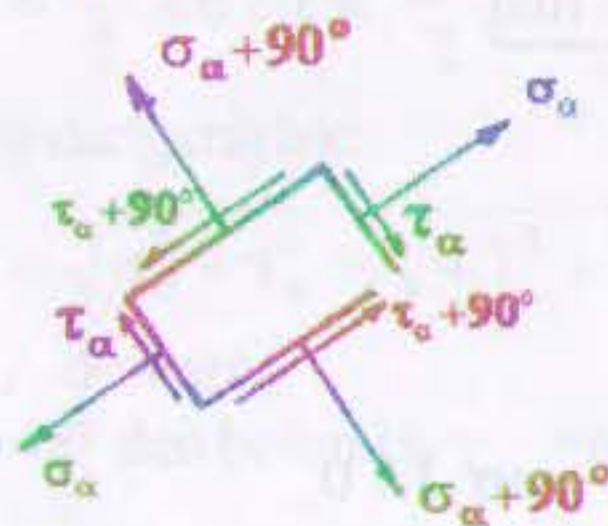
$$Q = a \cdot \ell(\sigma_x) = 60 \cdot 100 \cdot 0,0185 = 111 \text{ kN}.$$

Bir bolta düşýän güýç $Q_b = Q/8 = 13,9 \text{ kN}$.

Berklik şertinden boltuň kesiginiň diametri

$$d = \sqrt{\frac{4Q_b}{\pi[\sigma_s]}} = \sqrt{\frac{4 \cdot 13,9}{3,14 \cdot 10^7}} = 1,33 \text{ sm}.$$

2.9. $\mu = 2,272$.



2.9-njy surat

Kese kesigindäki dartgynlylyk

$$\sigma_x = \sigma_1 = \frac{P}{A} = \frac{20}{2} = 10 \text{ kN/sm}^2,$$

$\alpha = 30^\circ$ burç boýunça ýapgytlanan elementiň granlaryndaky dartgynlylyklar

$$\sigma_\alpha = \sigma_1 \cos^2 \alpha = 7,5 \text{ kN/sm}^2;$$

$$\sigma_{\alpha+90^\circ} = \sigma_1 \sin^2 \alpha = 2,5 \text{ kN/sm}^2.$$

Tenzometriň bazasynyň ugruna çyzyk durkuny üýtgetmäni kesgitlemek üçin aşakdaky aňlatmany düzýäris.

$$\varepsilon_\alpha = \frac{1}{E} (\sigma_\alpha - \mu \sigma_{\alpha+90^\circ}); \quad \varepsilon_\alpha = \frac{\Delta}{SK} = \frac{6,5}{20 \cdot 1000} = 3,25 \cdot 10^{-4}.$$

$$\text{Onda } \mu = \frac{\sigma_\alpha - E \varepsilon_\alpha}{\sigma_{\alpha+90^\circ}} = \frac{7,5 - 2,1 \cdot 10^4 \cdot 3,25 \cdot 10^{-4}}{2,5} = 0,272.$$

2.10. $\sigma_{\max} = 13,24 \text{ kN/sm}^2$, $\sigma_{\min} = 4,76 \text{ kN/sm}^2$, $\alpha_1 = 67,5^\circ$, $\alpha_2 = -22,5^\circ$.

Baş dartgynlylyklar

$$\sigma_{\max/\min} = \frac{\sigma_\alpha + \sigma_\beta}{2} \pm \frac{1}{2} \sqrt{(\sigma_\alpha - \sigma_\beta)^2 + 4\tau^2}.$$

Bu ýerden $\sigma_{\max} = 13,24 \text{ kN/sm}^2$, $\sigma_{\min} = 4,76 \text{ kN/sm}^2$.

Baş meýdançanyň ugry

$$\tan 2\alpha = -\frac{2\tau}{\sigma_\alpha - \sigma_\beta} = -\frac{2 \cdot 3}{12 - 6} = -1$$

$$2\alpha_1 = 135^\circ \Rightarrow \alpha_1 = 67^\circ 30', \quad 2\alpha_2 = -45^\circ, \quad \alpha_2 = -22^\circ 30'.$$

2.11. $\sigma_\alpha = 11,5 \text{ kN/sm}^2$, $\tau_\alpha = 0,5\sqrt{3} \text{ kN/sm}^2$, $\tau_{\alpha(\max)} = 1 \text{ kN/sm}^2$.

Tekiz dartgynlylyk ýagdaý üçin

$$\sigma_\alpha = \sigma_1 \cos^2 \alpha + \sigma_2 \sin^2 \alpha = 12 \cos^2 30^\circ + 10 \sin^2 30^\circ = 11,5 \text{ kN/sm}^2,$$

$$\tau_\alpha = \frac{\sigma_1 - \sigma_2}{2} \sin 2\alpha = \frac{12 - 10}{2} \cdot \sin 60^\circ = 0,5\sqrt{3} \text{ kN/sm}^2$$

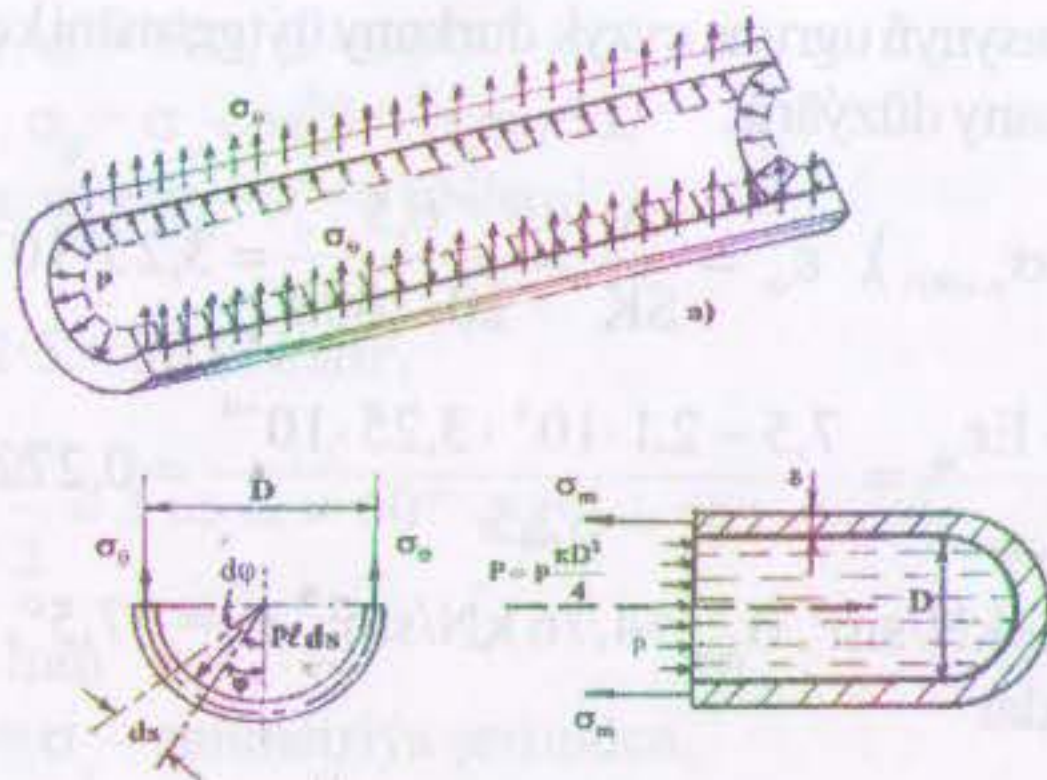
$$\tau_{\alpha(\max)} = \frac{\sigma_1 - \sigma_2}{2} \sin 90^\circ = 1 \text{ kN/sm}^2.$$

2.12. $\sigma_1 = 8,08 \text{ kN/sm}^2$, $\sigma_2 = 4,04 \text{ kN/sm}^2$, $p = 0,808 \text{ kN/sm}^2$.

Belleýäris: σ_θ – töwerekleýin dartgynlylyk, σ_m – meridional dartgynlylyk

Hemme güýçleri σ_θ ugruna proyektirläp alarys:

$$2\sigma_\theta \ell \delta = 2 \int_0^{\pi/2} p \ell \frac{D}{2} \cos \varphi d\varphi \Rightarrow \sigma_\theta = \frac{pD}{2\delta}$$



2.12-nji surat

σ_m ugruna proyektirlap alarys: $\sigma_m \pi D \delta = p \frac{\pi D^2}{4} \Rightarrow \sigma_m = \frac{pD}{4\delta}$

onda $\sigma_1 = \sigma_\theta = \frac{pD}{2\delta}$, $\sigma_2 = \sigma_m = \frac{pD}{4\delta}$, $\sigma_3 = 0$.

σ_1 we σ_2 Gukun baýlaşdyrylan kanuny esasynda tapýarys

$$\varepsilon_1 = \frac{1}{E}(\sigma_1 - \mu\sigma_2), \quad \varepsilon_2 = \frac{1}{E}(\sigma_2 - \mu\sigma_1).$$

Bu aňlatmalardan: $\sigma_1 = \frac{E(\varepsilon_1 + \mu\varepsilon_2)}{1 - \mu^2} = 8,08 \text{ kN/sm}^2$,

$$\sigma_2 = \frac{E(\varepsilon_2 + \mu\varepsilon_1)}{1 - \mu^2} = 4,04 \text{ kN/sm}^2.$$

Onda $p = \frac{\sigma_1 \cdot 2\delta}{D} = 0,808 \text{ kN/sm}^2$.

2.13. Meseläniň şertine görä $\sigma_x = \sigma_y = \sigma$ we süýnme iki tarapa hem birmeňzeş bolýar

$$\Delta b_x = \Delta b_y = \varepsilon b = \frac{b}{E}(\sigma_x - \mu\sigma_y) = \frac{\sigma b}{E}(1 - \mu) \quad (1)$$

Maýýşgaklyk moduly $E = \frac{\sigma_y}{\varepsilon} = \frac{\sigma \cdot b}{\Delta b} \quad (2)$

(2) aňlatmany (1) aňlatma goýup alarys:

$$\Delta b_x = \Delta b_y = \Delta b(1 - \mu) = 0,56 \text{ mm}.$$

Ikinji ýagdaýda σ_x gysýan dartgynlylyk bolany üçin, diňe alamaty üýtgeýär we (1) aňlatmany ulanyp alarys.

$$\Delta b_y = \Delta b(1 + \mu) = 1,04 \text{ mm (süýnme),}$$

$$\Delta b_x = -\Delta b(1 + \mu) = -1,04 \text{ mm (gysylma).}$$

$$2.14. \quad \tau_{zy} = \frac{P}{A} \operatorname{tg} \alpha; \quad \sigma_z = -\frac{P}{A} \operatorname{tg}^2 \alpha.$$

III bap

Süýşme we towlanma

3.1. Dört berçin.

Kesme şertinden berçinleriň sany

$$n \geq \frac{4P}{\pi d^2 \cdot [\tau] \cdot m} = \frac{4 \cdot 180}{3,14 \cdot 2^2 \cdot 10 \cdot 2} = 2,86 \approx 3$$

Ýemşermä şertinden

$$n \geq \frac{P}{d \cdot \delta [\sigma]_y} = \frac{180}{2 \cdot 1 \cdot 28} = 3,2 \approx 4$$

$n = 4$ kabul edýäris.

3.2. $\tau_k = 9,55 \text{ kN/sm}^2$, $\sigma_y = 25 \text{ N/sm}^2$, $\sigma_u = 9,09 \text{ kN/sm}^2$.

$$\tau_k = \frac{4P}{n \cdot \pi d^2 \cdot m} = \frac{4 \cdot 120}{2 \cdot 3,14 \cdot 2^2 \cdot 2} = 9,55 \text{ kN/sm}^2,$$

bu ýerde $n=2$ —berçinleriň sany, $m=2$ —kesme sany

$$\sigma_y = \frac{P}{n \cdot \delta \cdot d} = \frac{120}{2 \cdot 1,2 \cdot 2} = 25 \text{ kN/sm}^2,$$

Listiň dartgynlylygy

$$\sigma_t = \frac{P}{(b \cdot \delta - 2d \cdot \delta)} = \frac{120}{(15 - 4) \cdot 1,2} = 9,09 \text{ kN/sm}^2.$$

Urnanyň dartgynlylygy

$$\sigma_u = \frac{P}{(b - 2d) \cdot 2 \cdot \delta_1} = \frac{120}{(15 - 2 \cdot 2) \cdot 2 \cdot 0,6} = 9,09 \text{ kN/sm}^2.$$

3.3. $P = 250 \text{ kN}$.

$$P_k \leq \frac{n \cdot \pi d^2 \cdot m [\tau]_k}{4} = \frac{3 \cdot 3,14 \cdot 2,6^2 \cdot 2 \cdot 10}{4} = 318,4 \text{ kN}$$

$$P_y \leq \delta d [\sigma]_y \cdot n = 2 \cdot 2,6 \cdot 28 \cdot 3 = 436,8 \text{ kN},$$

$$P_l \leq (b-d) \delta [\sigma]_s = (13-2,6) \cdot 2 \cdot 16 = 364,8 \text{ kN},$$

$$P_{II} \leq (b-n \cdot d) \delta [\sigma]_s = (13-2 \cdot 2,6) \cdot 2 \cdot 16 = 249,6 \text{ kN}.$$

3.4. $n=4$, $d=1 \text{ sm}$.

$d=2t=1 \text{ sm}$ kabul edýäris.

Kesmä berklik şertinden

$$n \geq \frac{4P}{\pi d^2 [\tau]_k} = \frac{4 \cdot 30}{3,14 \cdot 1^2 \cdot 10} \geq 3,8,$$

Ýemşermä berklik şertinden

$$n \geq \frac{P}{dt [\sigma]_y} = \frac{30}{1 \cdot 0,5 \cdot 26} \geq 2,3,$$

$n=4$ berçin kabul edýäris.

Zolagyň gowşak kesiginde listiň üzülmä berkligini barlaýarys,

$$\sigma_{uz} = \frac{P}{(b-d) \cdot t} = \frac{30}{(5-1) \cdot 0,5} = 15 < 16 \text{ kN/sm}^2.$$

3.5. $d=1,6 \text{ sm}$, $n=4$ (bir tarapynda), $\ell=22 \text{ sm}$. Kesmä we ýemşermä berklik şertinden berçinleriň sanyny tapýarys ($d=2t$ kabul edýäris).

$$n_k = \frac{4P}{[\tau]_k \cdot \pi d^2} = \frac{4 \cdot 30}{10 \cdot 3,14 \cdot 1,6^2} = 3,8 \approx 4$$

$$n_{yem} = \frac{P}{d \cdot \delta [\sigma]_y} = \frac{80}{1,6 \cdot 0,8 \cdot 26} = 2,4$$

$n=4$ berçin kabul edýäris.

3.6. $\tau_k = 7,17 \text{ kN/sm}^2$, $\sigma_y = 11,25 \text{ N/sm}^2$, $\sigma_s = 4,09 \text{ kN/sm}^2$.

$$P = \frac{q \cdot Da}{2} = \frac{4 \cdot 150 \cdot 7,5}{2} = 2250 \text{ kg} = 22,5 \text{ kN}.$$

Gazandan iki berçinlemäniň ädimine deň bolan elementi kesip alýarys (surata seret). Dartgynlylyklary kesgitleýäris:

$$\tau_k = \frac{4P}{\pi d^2} = \frac{4 \cdot 22,5}{3,14 \cdot 2^2} = 7,17 \text{ kN/sm}^2,$$

$$\sigma_y = \frac{P}{dt} = \frac{22,5}{2 \cdot 1} = 11,25 \text{ kN/sm}^2,$$

$$\sigma_s = \frac{P}{(a-d)t} = \frac{22,5}{(7,5-2) \cdot 1} = 4,09 \text{ kN/sm}^2.$$

Kesilmä hasap dartgynlyk rugsat edilyän dartgynlyga in golaýy, şonuň üçin hem rugsat edilyän basyşy galtaşma dartgynlygyň üstünden kesgitleýäris. τ basyşa göni proporsional, onda rugsat edilyän basyş

$$[q] = q \frac{[\tau]_k}{\tau_k} = 4 \cdot \frac{7,2}{7,17} = 4,02 \text{ atm}.$$

3.7. $P=30,8 \text{ kN}$.

Turbanyň berklik şertinden syndyrma güýjüň ululygyny kesgitleýäris.

$$P_s = [\sigma]_s \cdot \left[\frac{\pi}{4} (D^2 - d^2) - d_b \cdot t \cdot n \right] = 40 \left[\frac{3,14}{4} (3^2 - 2,8^2) - 0,35 \cdot 0,1 \cdot 4 \right] = 30,8 \text{ kN}$$

Berçinlemäniň berklik şertlerinden syndyrma güýjüň ululygyny kesgitleýäris:

$$P_k = \frac{\pi d^2}{4} [\tau]_k \cdot n = \frac{3,14 \cdot 0,35^2}{4} \cdot 22 \cdot 20 = 42,25 \text{ kN}.$$

$$P_y = dt[\sigma]_y \cdot n = 0,35 \cdot 0,1 \cdot 52 \cdot 20 = 36,4 \text{ kN}.$$

Kabul edýäris $P_s=30,8 \text{ kN}$.

3.8. $\tau=5,57 \text{ kN/sm}^2$, $\sigma_y=10,93 \text{ kN/sm}^2$.

Galtaşma dartgynlyk

$$\tau = \frac{4P}{\pi d^2 \cdot n} = \frac{4 \cdot 52,5}{3,14 \cdot 2^2 \cdot 3} = 5,57 \text{ kN/sm}^2.$$

Normal dartgynlyk

$$\sigma_y = \frac{P}{dt \cdot n} = \frac{52,5}{2 \cdot 0,8 \cdot 3} = 10,93 \text{ kN/sm}^2.$$

3.9. $n=36$ berçin.

Kesilmä berklik şertinden

$$n = \frac{4P}{\pi d^2 \cdot [\tau]_k} = \frac{4 \cdot 785}{3,14 \cdot 2^2 \cdot 7} = 35,6 \approx 36 \text{ sany},$$

$$\text{Bu ýerde } P = q \frac{\pi D^2}{4} = 10 \cdot 0,785 \cdot 10^4 = 785 \text{ kN}.$$

Ýenjilme şertinden

$$n = \frac{P}{dt[\sigma]_y} = \frac{785}{2 \cdot 1 \cdot 16} = 24,5 \approx 25 \text{ sany}.$$

Kabul edýäris $n=36$ berçin.

3.10. $\tau=7,64 \text{ kN/sm}^2$, $\sigma_y=17,14 \text{ kN/sm}^2$.

$$\tau = \frac{4P}{\pi d^2 \cdot n} = 7,64 \text{ kN/sm}^2,$$

$$\sigma_y = \frac{P}{d \cdot t_{\min} \cdot n} = 17,14 \text{ kN/sm}^2.$$

3.11. $\tau_k=2,29 \text{ kN/sm}^2$.

$$\varepsilon_m = \varepsilon_p(1) \Rightarrow \alpha_m \Delta t - \frac{N}{E_m A_m} = \alpha_p \Delta t + \frac{N}{E_p A_p}, \quad (2)$$

$$A_p = \frac{\pi}{4} (D^2 - d^2) = \frac{3,14}{4} (6^2 - 4^2) = 15,7 \text{ sm}^2,$$

$$A_m = \frac{\pi d^2}{4} = \frac{3,14 \cdot 4^2}{4} = 12,56 \text{ sm}^2.$$

(2) aňlatmadan

$$N = \frac{\Delta t \cdot A_m E_p A_p (\alpha_m \alpha_p)}{2A_p + A_m} = 14,35 \text{ kN},$$

$$\tau = \frac{4P}{\pi d^2 \cdot m} = \frac{4 \cdot 14,35}{3,14 \cdot 2^2 \cdot 2} = 2,29 \text{ kN/sm}^2,$$

$m=2$ – kesme meýdanynyň sany.

3.12. $d=5 \text{ sm}$.

Kesilme şertinden

$$d = \sqrt{\frac{4P}{\pi[\tau] \cdot n}} = \sqrt{\frac{4 \cdot 200}{3,14 \cdot 8 \cdot 2}} = 3,99 \text{ sm}.$$

Ýenijilme şertinden

$$d = \frac{P}{\tau[\sigma]} = \frac{200}{2 \cdot 20} = 5 \text{ sm}.$$

Kabul edýäris $d = 5 \text{ sm}$.

3.13. $d_1 = 18,7 \text{ sm}$, $\tau = 5 \text{ kN/sm}^2$.

Bolty gysýan güýjüň ululygy

$$P = \sigma_g \cdot A_b = 10 \cdot \frac{3,14 \cdot 10^2}{4} = 785 \text{ kN}.$$

Ýemşerme dartgynlykdan

$$\sigma_y = \frac{4P}{\pi(d_1^2 - d^2)},$$

$$\text{Bu ýerden } d_1 = \sqrt{\frac{4P + \pi d^2 \sigma_y}{\pi \sigma_y}} = \sqrt{\frac{4 \cdot 785 + 3,14 \cdot 10^2 \cdot 4}{3,14 \cdot 4}} = 18,7 \text{ sm}.$$

Galtaşma dartgynlyk

$$\tau = \frac{P}{\pi d t} = \frac{785}{3,14 \cdot 10 \cdot 5} = 5 \text{ kN/sm}^2.$$

3.14. $P = 44,8 \text{ kN}$, $\sigma = 0,56 \text{ kN/sm}^2$.

Üzüji güýç

$$P = [\sigma] \cdot A = 5,6 \cdot 2 \cdot 4 = 44,8 \text{ kN/sm}^2.$$

Nusganyň kellesinde döreyän owranma dartgynlygy

$$\sigma = \frac{P}{A_{\text{öwr}}} = \frac{44,8}{2 \cdot 10 \cdot 4} = 0,56 \text{ kN/sm}^2.$$

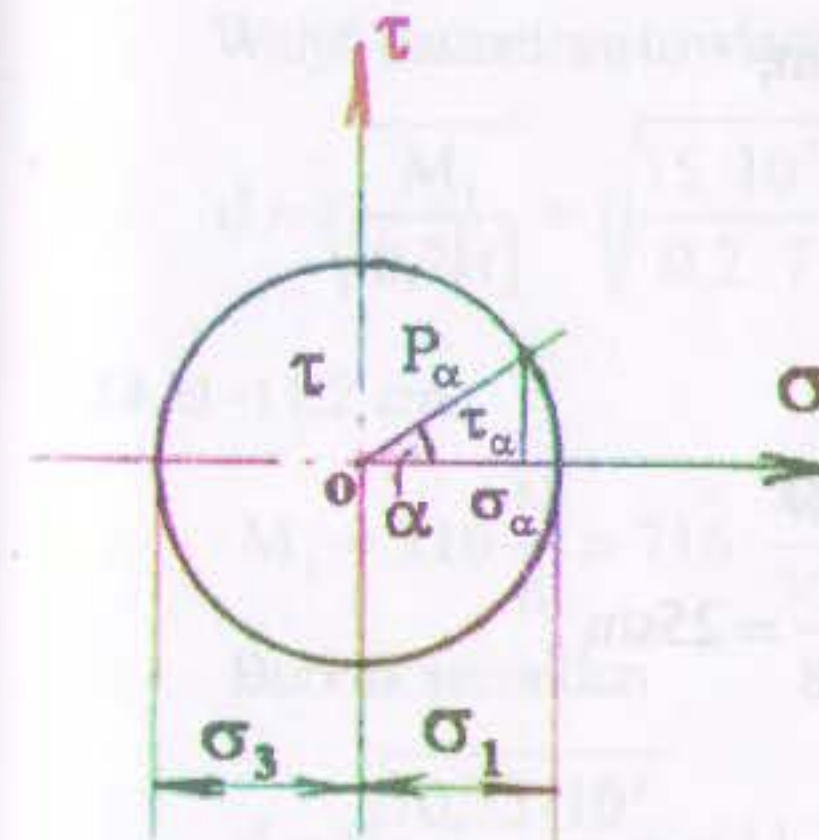
3.15. $h = 6 \text{ sm}$, $\ell = 36 \text{ sm}$.

Ýenijilmä berklik şertinden

$$t \geq \frac{P \cos \alpha}{b[\sigma]_y} \geq \frac{20 \cdot 0,866}{6 \cdot 5} \geq 5,77 \text{ sm} \approx 6 \text{ sm}.$$

Owranma berklik şertinden

$$\ell \geq \frac{N \cos \alpha}{b[\tau]} \geq \frac{20 \cdot 0,866}{6 \cdot 0,08} = 36 \text{ sm}.$$



3.16-njy surat

3.16. $\sigma_\alpha = 4,33 \text{ kN/sm}^2$,

$\tau_\alpha = 2,5 \text{ kN/sm}^2$,

$p_\alpha = 5 \text{ kN/sm}^2$.

Çyzgydan

$\tau_\alpha = 2,5 \text{ kN/sm}^2$, $\sigma_\alpha = 4,33 \text{ kN/sm}^2$.

$$p_\alpha = \sqrt{\sigma_\alpha^2 + \tau_\alpha^2} = \sqrt{4,33^2 + 2,5^2} = 5 \text{ kN/sm}^2$$

3.17. $\Delta S = 0,25 \text{ mm}$, $\gamma = 0,00125$.

Süýşmede Gukuň kanunyny ulanyp alarys:

$$\gamma = \frac{\tau}{G} = \frac{10}{8 \cdot 10^3} = 0,00125.$$

$$\text{Absolýut süýşme } \Delta S = \gamma \cdot S = 0,00125 \cdot 200 = 0,25 \text{ mm}.$$

3.18. $\gamma = 0,00065 \text{ rad}$.

Süýşme burçuň üýtgemeginiň ululygy

$$\gamma = \frac{\sigma}{E} (1 + \mu) \sin 2\alpha = \frac{12}{2 \cdot 10^4} (1 + 0,25) \cdot \sin 60^\circ = 0,00065 \text{ rad}.$$

3.19. $\ell_1 = 9,88 \text{ sm}$, $\ell_2 = 3,92 \text{ sm}$.

Tikiniň umumy uzynlygy

$$\ell = \ell_1 + \ell_2 = \frac{P}{0,7t[\tau_e]} = \frac{6^2}{0,7 \cdot 0,8 \cdot 8} = 13,8 \text{ sm.}$$

Başga tarapdan

$$\frac{\ell_2}{\ell_1} = \frac{z_o}{h - z_o} = \frac{2,27}{8 - 2,27} = 0,396, \ell_2 = 0,396\ell_1, z_o = 2,27 \text{ sm} - \text{tablisadan}$$

alýarys

$$\text{onda } \ell_1 + 0,396\ell_1 = 13,8 \Rightarrow \ell_1 = 9,88 \text{ sm,}$$

$$\ell_2 = 0,396 \cdot 9,88 = 3,92 \text{ sm.}$$

3.20. $x = 7,5 \text{ sm.}$

Liste rugsat edilyän güýç

$$P \leq [\sigma] \cdot A_t = 14 \cdot 10 \cdot 1 = 140 \text{ kN.}$$

Kebşirleme tikiniň umumy uzynlygy

$$\ell = 2x + 10 = \frac{P}{0,7 \cdot 1 \cdot [\tau]} = \frac{140}{0,7 \cdot 8} = 25 \text{ sm,}$$

Bu ýerden $x = 7,5 \text{ sm.}$

3.21. $b = 7,2 \text{ sm, } \sigma_{\text{tik}} = 7,7 \text{ kN/sm}^2, \tau_{\text{tik}} = 7,7 \text{ kN/sm}^2.$

Zolagyň zerur bolan inini süýnmä berklik şertinden tapýarys:

$$b \geq \frac{P}{t[\sigma]} = \frac{100}{1 \cdot 14} \Rightarrow b \geq 7,14 \approx 7,2 \text{ sm.}$$

Gyýa tikiniň uzynlygy

$$\ell_{\text{tik}} = \frac{b}{\sin 45^\circ} - 1 = \frac{7,2}{0,707} - 1 = 9,2 \text{ sm.}$$

Tikiniň berkligini barlaýarys

$$\sigma_{\text{tik}} = \frac{10}{9,2 \cdot 1} \cdot 0,707 = 0,77 < 10 \text{ kN/sm}^2,$$

$$\tau_{\text{tik}} = \frac{10}{9,2 \cdot 1} \cdot 0,707 = 0,77 < 8 \text{ kN/sm}^2.$$

3.22. Berklik şerti kanagatlandyrylýar. Şwelleriň üzülmä berkligini barlaýarys.

$$\sigma_s = \frac{P}{A} = \frac{800}{55,9} = 14,3 < 16 \text{ kN/sm}^2,$$

Tikiniň kesilmä berkligini barlaýarys.

$$\tau_k = \frac{P}{1,4 \cdot 60 + 2 \cdot 20} = 6,45 < 8 \text{ kN/sm}^2.$$

3.23. $d = 10,3 \text{ sm}$

Walyň diametrini tovlanma berklik şertinden tapýarys:

$$d = \sqrt[3]{\frac{M_t}{0,2[\tau]}} = \sqrt[3]{\frac{15 \cdot 10^2}{0,2 \cdot 7}} = 10,3 \text{ sm.}$$

3.24. $d = 11,2 \text{ sm.}$

$$M_t = 716 \frac{\text{N}}{\text{n}} = 716 \cdot \frac{450}{300} = 1075 \text{ kgm} = 10,75 \text{ kNm,}$$

Berklik şertinden

$$d = \sqrt[3]{\frac{10,75 \cdot 10^2}{0,2 \cdot 4}} = 11,2 \text{ sm.}$$

Gatylyk şertinden

$$d = \sqrt[4]{\frac{M_t \ell}{G \cdot 0,1 \cdot [\varphi]}} = \sqrt[4]{\frac{10,75 \cdot 10^2 \cdot 2 \cdot 10^2}{8 \cdot 10^3 \cdot 0,1 \cdot 0,01744}} = 11,54 \text{ sm.}$$

$d = 11,2 \text{ sm}$ kabul edýäris.

3.25. $Q_p = 1,75 Q_a.$

$$\varphi_p = \varphi_a \Rightarrow \frac{1}{G_p I_p} = \frac{1}{G_a I_a}, Q_p = \gamma_p A_p \ell_p, Q_a = \gamma_a A_a \ell_a,$$

$$\frac{Q_p}{Q_a} = \frac{d_p^2 \gamma_p}{d_a^2 \gamma_a}, G_p 0,1 d_p^4 = G_a 0,1 d_a^4 \Rightarrow \frac{d_p}{d_a} = \sqrt[4]{\frac{G_a}{G_p}};$$

$$\frac{Q_p}{Q_a} = \sqrt{\frac{G_a}{G_p} \cdot \frac{\gamma_p}{\gamma_a}} = \sqrt{\frac{2,7 \cdot 10^3}{8 \cdot 10^3} \cdot \frac{78,5}{26}} = 1,75.$$

3.26. Eger $M_t > 23,6 \text{ kNm}$ – rugsat edilyän dartgynlylyk boýunça,
 $M_t < 23,6 \text{ kNm}$ – rugsat edilyän towlanma burçy boýunça.

$$\tau = \frac{M_t}{I} \cdot \frac{d}{2} \leq [\tau] \Rightarrow M_t = \frac{[\tau] \cdot I \cdot 2}{d} - \text{berklik şertinden}$$

$$M_t = \frac{\varphi G I}{\ell} - \text{gatylyk şertinden}$$

$$\frac{\varphi G I}{\ell} = \frac{[\tau] I \cdot 2}{d} \Rightarrow d = 11,46 \text{ sm.}$$

$$M_t \geq \frac{[\tau] \cdot \pi d^4 \cdot 2}{32 \cdot d} = 8 \cdot 0,196 \cdot d^3 = 2,6 \text{ kNm.}$$

3.27. $\tau = 4,66 \text{ kN/sm}^2$.

$$\tau = \frac{\varphi \pi G d}{180 \cdot \ell \cdot 2} = \frac{4 \cdot 3,14 \cdot 8 \cdot 10^3 \cdot 10}{180 \cdot 600 \cdot 2} = 4,66 \text{ kN/sm}^2.$$

3.28. $\tau = 6 \text{ kN/sm}^2$.

$$\tau = \frac{M_t}{W_p} \Rightarrow M_t = 71620 \frac{\text{N}}{\text{n}};$$

$$W_p = \frac{\pi d^3}{16} = \frac{\pi}{16} \cdot 2,5^3 \cdot 40 \cdot \frac{\text{N}}{\text{n}} = 119,3 \frac{\text{N}}{\text{n}};$$

$$\tau = \frac{71620 \frac{\text{N}}{\text{n}}}{119,3 \frac{\text{N}}{\text{n}}} = 600 \text{ kg/sm}^2 = 6 \text{ kN/sm}^2$$

3.29. $\tau_A = 5,3 \text{ kN/sm}^2$, $\tau_B = 2,05 \text{ kN/sm}^2$.



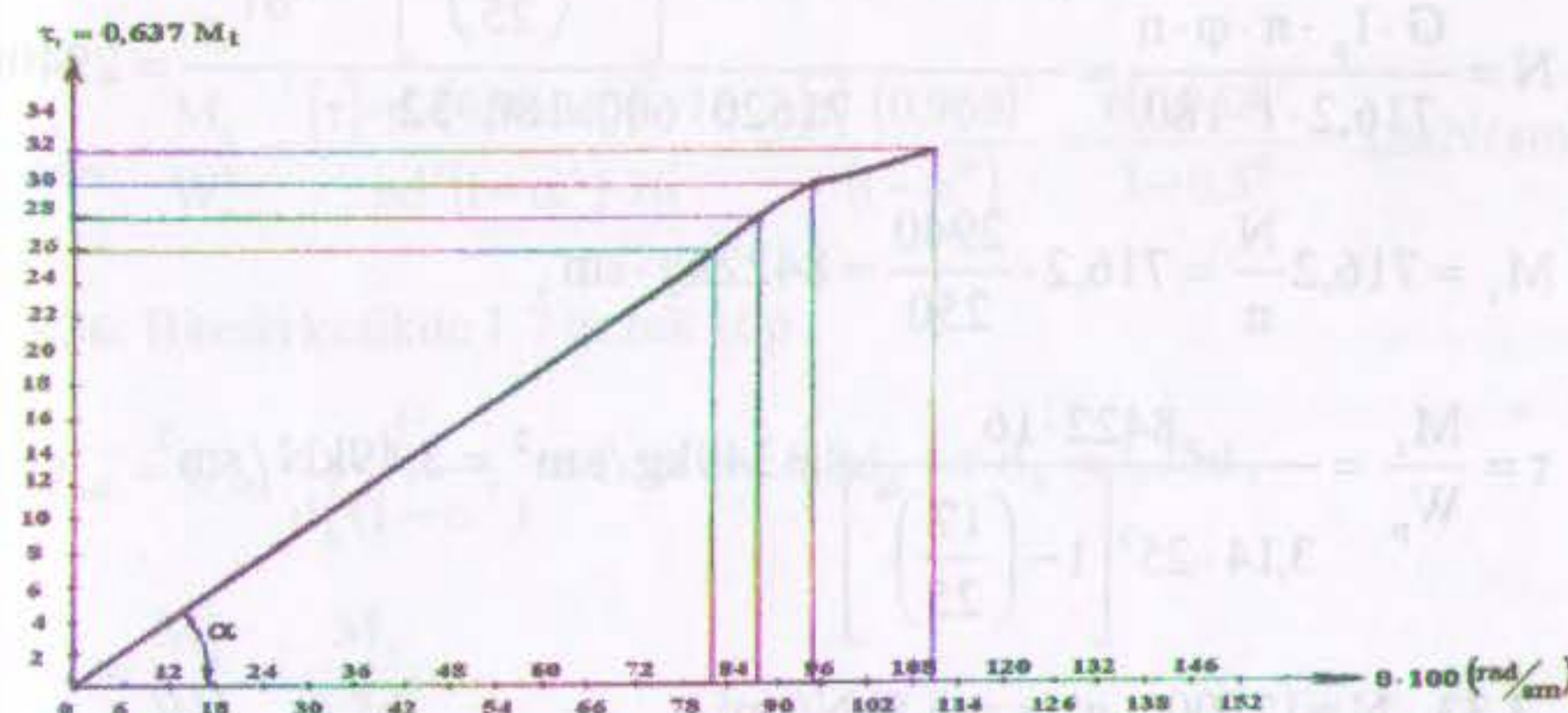
3.29-njy surat

$$M_{AA} = 1,3 \text{ kN m}$$

$$M_{BB} = 1,7 \text{ kN m}$$

$$\tau_{AA} = \frac{16 M_{AA}}{\pi d_A^3} = 5,3 \text{ kN/sm}^2, \quad \tau_{BB} = \frac{16 M_{BB}}{\pi d_B^3} = 2,05 \text{ kN/sm}^2.$$

3.30. $\tau_t = 0,637 M_t$, $\tau_t = \frac{M_t}{W_p} = \frac{16 M_t}{\pi d^3} = \frac{16}{3,14 \cdot 8} M_t = 0,637 M_t$.



3.30-njy surat

$$\theta = \frac{\varphi}{\ell} = \frac{1}{20} \cdot \varphi = 0,05 \text{ rad/sm};$$

$$G = \frac{\tau}{\gamma} = \text{tg} \alpha; \quad \gamma = \frac{d\varphi}{dx} \rho.$$

3.31. $E = 2,16 \cdot 10^4 \text{ kN/sm}^2$; $G = 8,16 \cdot 10^3 \text{ kN/sm}^2$; $\mu = 0,32$.

$$E = \frac{4P\ell}{\pi d^2 \cdot \Delta\ell} = \frac{4 \cdot 60 \cdot 20}{3,14 \cdot 2,5^2 \cdot 0,0113} = 2,16 \cdot 10^4 \text{ kN/sm}^2;$$

$$G = \frac{32M_t \ell \cdot 180}{\pi d^4 \cdot \varphi \pi} = \frac{32 \cdot 20 \cdot 10 \cdot 180}{3,14 \cdot 2,5^4 \cdot 0,55 \cdot 3,14} = 8,16 \cdot 10^3 \text{ kN/sm}^2;$$

$$\mu = \frac{E}{2G} - 1 = \frac{2,16 \cdot 10^4}{2 \cdot 8,16 \cdot 10^3} - 1 = 0,32.$$

3.32. $N = 2940 \text{ a.g.}, \tau = 3,49 \text{ kN/sm}^2.$

$$N = \frac{M_t n}{7,162}; \quad \varphi = \frac{M_t \ell \cdot 180}{G \cdot I_p \cdot \pi} (\text{grad}); \quad M_t = \frac{G \cdot I_p \cdot \pi \cdot \varphi}{\ell \cdot 180};$$

$$N = \frac{G \cdot I_p \cdot \pi \cdot \varphi \cdot n}{716,2 \cdot \ell \cdot 180} = \frac{8 \cdot 10^5 \cdot 3,14^2 \cdot 25^4 \left[1 - \left(\frac{17}{25} \right)^4 \right] \cdot 1,2 \cdot 250}{71620 \cdot 600 \cdot 180 \cdot 32} = 2940 \text{ a.g.}$$

$$M_t = 716,2 \frac{N}{n} = 716,2 \cdot \frac{2940}{250} = 8422 \text{ kg} \cdot \text{sm},$$

$$\tau = \frac{M_t}{W_p} = \frac{8422 \cdot 16}{3,14 \cdot 25^3 \left[1 - \left(\frac{17}{25} \right)^4 \right]} = 349 \text{ kg/sm}^2 = 3,49 \text{ kN/sm}^2$$

3.33. $N = 12500 \text{ a.g.}, \tau = 6,8 \text{ kN/sm}^2.$

$$\tau_{\max} = 2\varepsilon G = 2 \cdot 10^4 \cdot 4,25 \cdot 8 \cdot 10^3 = 6,8 \text{ kN/sm}^2$$

$$N = \frac{\tau_{\max} \cdot W_p \cdot n}{71620} = \frac{680 \cdot 3,14 \cdot 40^3 \cdot \left[1 - \left(\frac{24}{40} \right)^4 \right] \cdot 120}{71620 \cdot 16} = 12500 \text{ a.g.}$$

3.34 $d_h = 42 \text{ sm}; Q_b/Q_h = 1,41.$

$$[\tau]_b = [\tau]_h \Rightarrow \frac{16M_t}{\pi d_b^3} = \frac{16M_t}{\pi d_h^3 (1 - \alpha^4)},$$

Bu yerden $d_h = 42 \text{ sm}$ içi boş walyň daşky diametri.

$$\frac{Q_b}{Q_h} = \frac{A_b \cdot \ell \cdot \gamma}{A_h \cdot \ell \cdot \gamma} = \frac{\pi d^2 \cdot 4}{4\pi d_h^2 (1 - \alpha^2)} = \frac{40^2}{42^2 (1 - 0,6^2)} = 1,41.$$

3.35. $\tau_{\max}^h = 5,8 \text{ kN/sm}^2.$

$$Q_h = 0,8Q_b \Rightarrow \frac{Q_b}{Q_h} = 1,25 = \frac{d^2}{d_h^2 (1 - \alpha^2)},$$

$$d = d_h \sqrt{(1 - \alpha^2) \cdot 1,25} = 0,968 d_h,$$

$$M_t = [\tau] \frac{\pi d^3}{16},$$

$$\tau_{\max}^h = \frac{M_t}{W_p^h} = \frac{[\tau] \cdot \pi \cdot (0,968 d_h)^3 \cdot 16}{\pi d^3 (1 - \alpha^4) \cdot 16} = \frac{[\tau] \cdot (0,968)^3}{(1 - \alpha^4)} = \frac{6(0,968)^3}{1 - 0,5^4} = 5,8 \text{ kN/sm}^2.$$

3.36. Bitewi kesikde 1,7 gezek köp.

$$Q_{\text{hal}} = Q_{\text{bit}} \frac{d^2}{d_h^2 (1 - \alpha^2)} = 1 \Rightarrow d = 0,8 d_h \Rightarrow d_h = 1,25 d,$$

$$\tau_b = \frac{M_t}{W_p^b} = \frac{M_t}{0,2 d^3},$$

$$\tau_h = \frac{M_t}{0,2 d_h^3 (1 - \alpha^4)} = \frac{M_t}{0,2 (1,25 d)^3 (1 - 0,6^4)} = \frac{M_t}{0,2 \cdot 1,7 d^3},$$

$$\frac{\tau_b}{\tau_h} = \frac{M_t \cdot 0,2 \cdot 1,7 d^3}{0,2 d^3 M_t} = 1,7 \text{ gezek.}$$

3.37. $D = 9,04 \text{ sm}, d = 7,24 \text{ sm}.$

$$W_p = \frac{\pi D^3}{16} (1 - \alpha^4), \quad I_p = \frac{\pi}{32} (1 - \alpha^4) \Rightarrow \frac{I_p}{W_p} = \frac{D}{2}.$$

Berklik şertinden

$$W_p = \frac{M_t}{[\tau]}.$$

Gatylyk şertinden

$$I_p = \frac{M_t \ell \cdot 180}{G \varphi \cdot \pi},$$

$$\text{onda } \frac{I_p}{W_p} = \frac{180 \ell [\tau]}{G \varphi \pi} = \frac{D}{2},$$

$$\text{bu ýerden } D = \frac{2 \cdot 180 \cdot \ell [\tau]}{G \varphi \pi} = 9,04 \text{ sm}$$

Başga tarapdan

$$W_p = \frac{M_t}{[\tau]} = \frac{\pi D^3}{16} (1 - \alpha^4),$$

bu ýerden $\alpha = 0,8$.

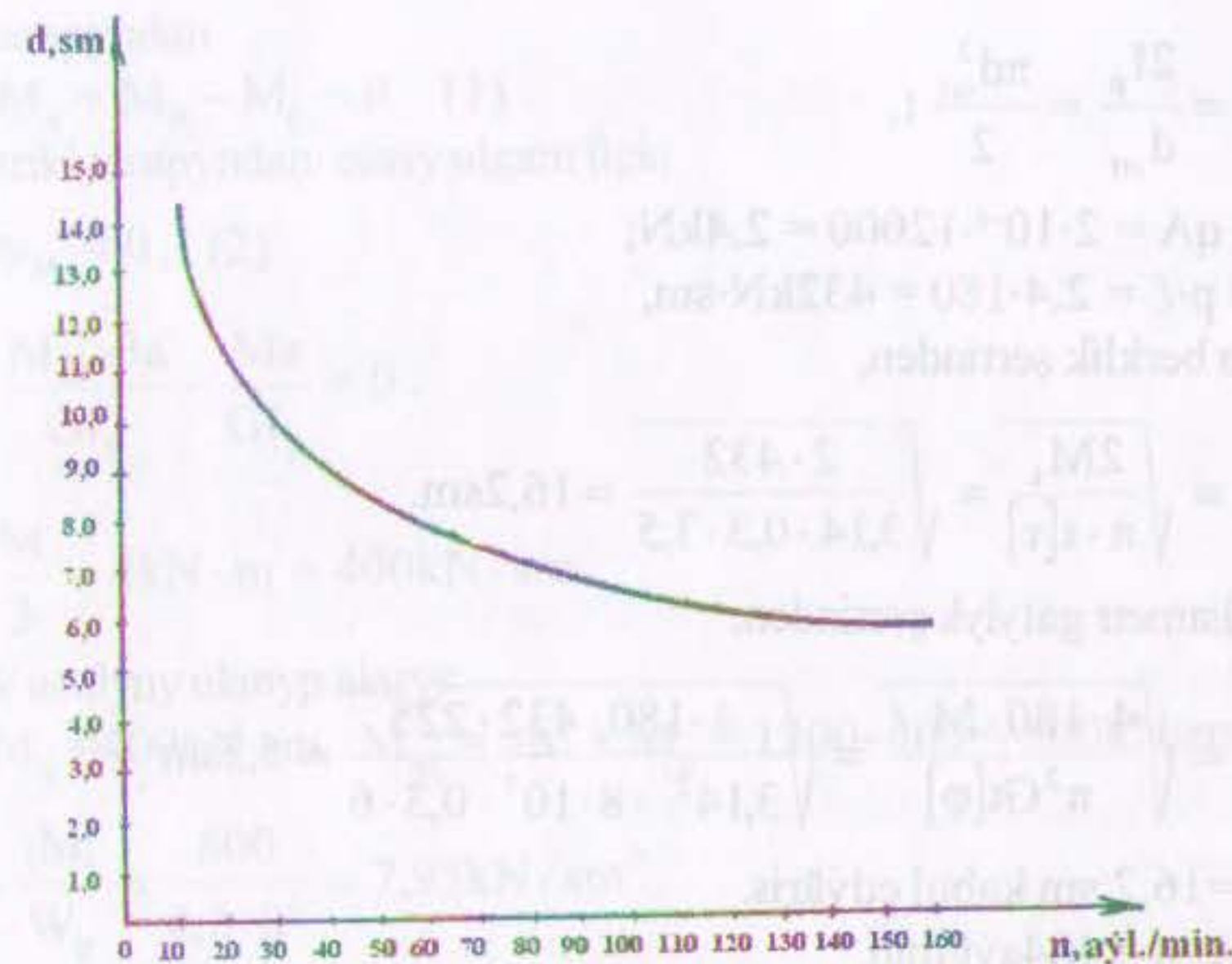
Onda $d = \alpha D = 0,8 \cdot 9,04 \approx 7,24 \text{ sm}$.

$$\mathbf{3.38.} \quad d = \frac{31,2}{\sqrt[3]{n}}.$$

Berklik şertinden

$$d = \sqrt{\frac{16 \cdot M_t}{\pi [\tau]}}, \quad M_t = 71620 \frac{N}{n},$$

$$\text{onda } d = \sqrt[3]{\frac{16 \cdot 71620 \cdot N}{\pi n [\tau]}} = \sqrt[3]{\frac{16 \cdot 71620 \cdot 50}{3,14 \cdot n \cdot 600}} = \frac{31,2}{\sqrt[3]{n}}.$$



3.38-nji surat

3.39. $\varphi = 0,016 \text{ rad}$, $t = 0,318 \text{ sm}$.

Ýuka diwarly sterženlerde galtaşma dartgynlylyk, diwaryň galyňlygyndaky orta bahasyna deň diýip kabul edýäris:

$$\tau = \frac{M_t d_{\text{ort}}}{2 I_p}$$

$$I_p = \int_A \rho^2 dA = \pi d_{\text{ort}} \cdot t \cdot \frac{d_{\text{ort}}^2}{4} = \frac{\pi d_{\text{ort}}^3}{4} \cdot t,$$

$$\text{onda } \tau = \frac{2 M_t}{\pi d_{\text{ort}}^2 \cdot t} \leq [\tau]$$

$$\text{bu ýerden } t = \frac{2 M_t}{\pi d_{\text{ort}}^2 [\tau]} = \frac{2 \cdot 625}{\pi \cdot 12,5^2 \cdot 8} = \frac{1}{\pi} = 0,318 \text{ sm}$$

Towlanma burçuny adaty formuladan tapýarys:

$$\varphi = \frac{M_t \ell}{G I_p} = \frac{4 M_t \ell}{G \pi d_{\text{ort}}^3 \cdot t} = \frac{4 \cdot 625 \cdot 100}{810^3 \cdot 3,14 \cdot 12,5^3 \cdot 0,318} = 0,016 \text{ rad}.$$

3.40. $d_{\text{ort}} = 16,2 \text{ sm}$.

$$W_p = \frac{2I_p}{d_{ort}} = \frac{\pi d_{ort}^2}{2} t,$$

$$p = qA = 2 \cdot 10^{-4} \cdot 12000 = 2,4 \text{ kN};$$

$$M = p \cdot \ell = 2,4 \cdot 180 = 432 \text{ kN} \cdot \text{sm},$$

onda berklik şertinden,

$$d_{ort} = \sqrt{\frac{2M_t}{\pi \cdot t[\tau]}} = \sqrt{\frac{2 \cdot 432}{3,14 \cdot 0,3 \cdot 3,5}} = 16,2 \text{ sm}.$$

Bu diametr gatylyk şertinden,

$$d_{ort}^1 = \sqrt[3]{\frac{4 \cdot 180 \cdot M_t \ell}{\pi^2 G t [\varphi]}} = \sqrt[3]{\frac{4 \cdot 180 \cdot 432 \cdot 225}{3,14^2 \cdot 8 \cdot 10^3 \cdot 0,3 \cdot 6}} = 5,3 \text{ sm},$$

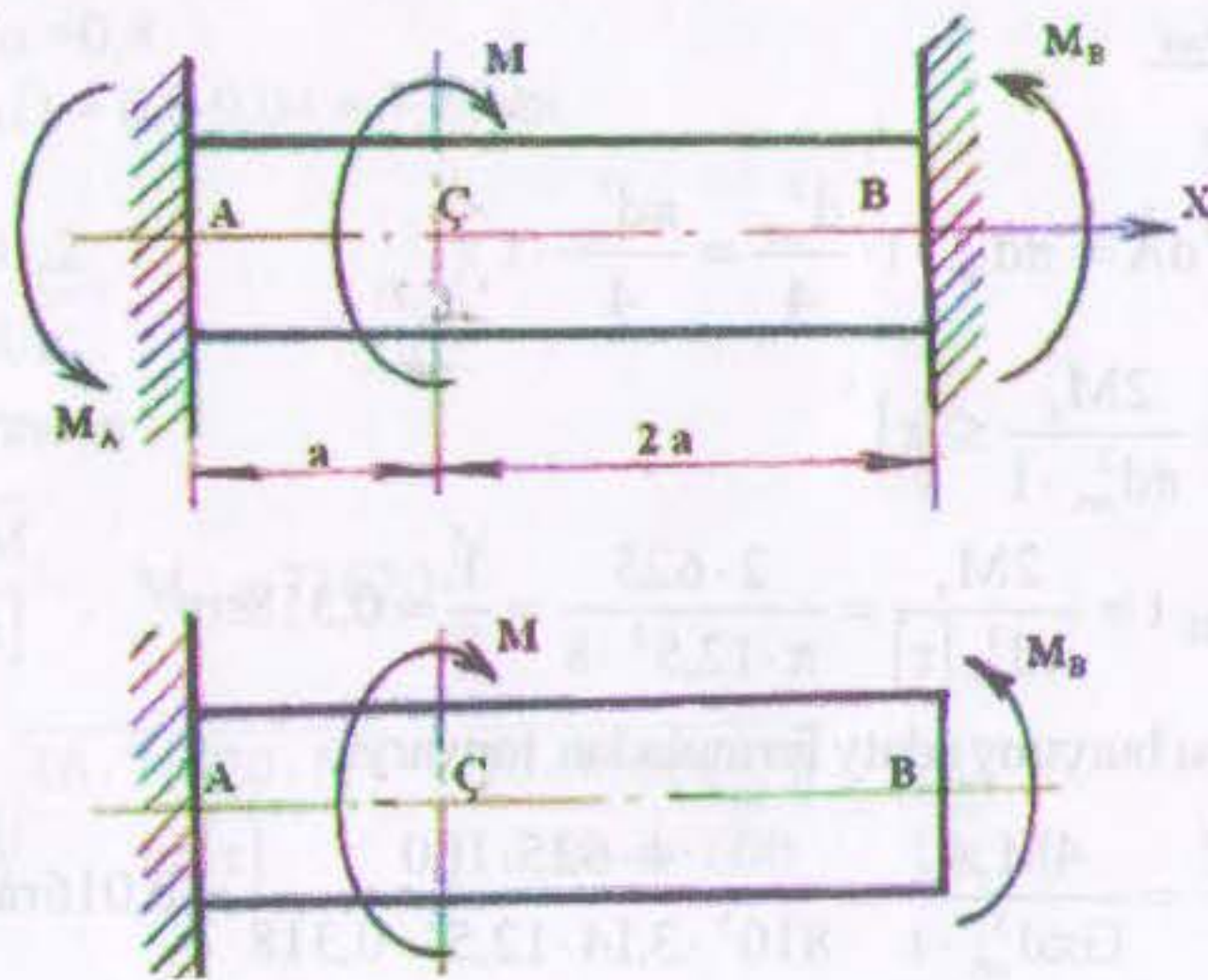
$d_{ort} = 16,2 \text{ sm}$ kabul edýäris.

$$3.41. n = 404 \text{ aýl/min}.$$

Gatylyk şertinden walyň aýlaw tizligini tapýarys:

$$n = \frac{71620 \cdot N \cdot 4 \cdot 180 \cdot \ell}{G t \pi^2 d_{ort}^3 [\varphi]} = \frac{71620 \cdot 50 \cdot 4 \cdot 180 \cdot 370}{8 \cdot 10^3 \cdot 0,3 \cdot 3,14^2 \cdot 10^3 \cdot 1} = 404 \text{ aýl/min}$$

$$3.42. \tau = 7,95 \text{ kN/sm}^2.$$



3.42-nji surat

Statiki tarapyndan

$$\Sigma M_x = M_A + M_B - M_C = 0 \quad (1)$$

Geometriki tarapyndan esasy ulgam üçin

$$\varphi_{M_B} + \varphi_M = 0, \quad (2)$$

$$\varphi_{M_B} = \frac{M_B \cdot 3a}{GI_p} - \frac{Ma}{GI_p} = 0;$$

$$M_B = \frac{M}{3} = 4 \text{ kN} \cdot \text{m} = 400 \text{ kN} \cdot \text{sm}.$$

Kesmek usulyny ulanyp alarys:

$$M_{CB} = M_B = 400 \text{ kN} \cdot \text{sm}, \quad M_{AC} = -M + M_B = 1200 - 400 = 800 \text{ kN} \cdot \text{sm};$$

$$\tau_{\max} = \frac{|M|}{W_p} = \frac{800}{0,2 \cdot 8^3} = 7,95 \text{ kN/sm}^2.$$

$$3.43. \tau_p = 2,5 \text{ kN/sm}^2, \quad \tau_m = 1,15 \text{ kN/sm}^2, \quad M_p = 0,718 \text{ kNm}, \\ M_m = 0,282 \text{ kNm}, \quad \varphi = 1,353^\circ.$$

Statikanyň deňlemesi:

$$M_p + M_m = M \quad (1)$$

Durkuny üýtgetmäniň deňlemesi:

$$\theta_m = \theta_p \quad (2)$$

Gukuň kanuny esasynda:

$$\frac{M_m}{G_m I_p^m} = \frac{M_p}{G_p I_p^p} \Rightarrow M_p = \frac{G_p I_p^p}{G_m I_p^m} \cdot M_m \quad (3)$$

$$(3) \text{ we } (1) \text{ aňlatmalardan } M_m = \frac{M}{1 + \frac{G_p I_p^p}{G_m I_p^m}} = 0,282 \text{ kN} \cdot \text{m} \text{ onda}$$

$$M_p = M - M_m = 0,718 \text{ kNm}$$

$$I_p^p = 0,1 \cdot d_p^4 (1 - \alpha_p^4) = 114 \text{ sm}^4, \quad d_p = 7,5 + 2t, \quad \alpha_p = \frac{7,5}{d_p};$$

$$I_p^m = 0,1 \cdot d_m^4 (1 - \alpha_m^4) = 90 \text{ sm}^4, \quad d_m = 7,5, \quad \alpha_m = \frac{d_m - 7,5}{d_m};$$

$$\tau_m = \frac{M_m}{W_p^m} = 1,15 \text{ kN/sm}^2, \quad \tau_p = \frac{M_p}{W_p^p} = 2,5 \text{ kN/sm}^2,$$

$$\varphi = \frac{M_t^p \ell}{G_p I_p} = \frac{71,8 \cdot 300}{810^3 \cdot 114} = 0,0236 \text{ rad} = 0,0236 \cdot \frac{180}{3,14} = 1,353^\circ.$$

$$3.44. \tau_\varphi = 3,07 \text{ kN/sm}^2, \quad \tau_s = 3,07 \text{ kN/sm}^2, \quad \varphi = 0,33^\circ.$$

Statikanyň adaty deňlemesinden

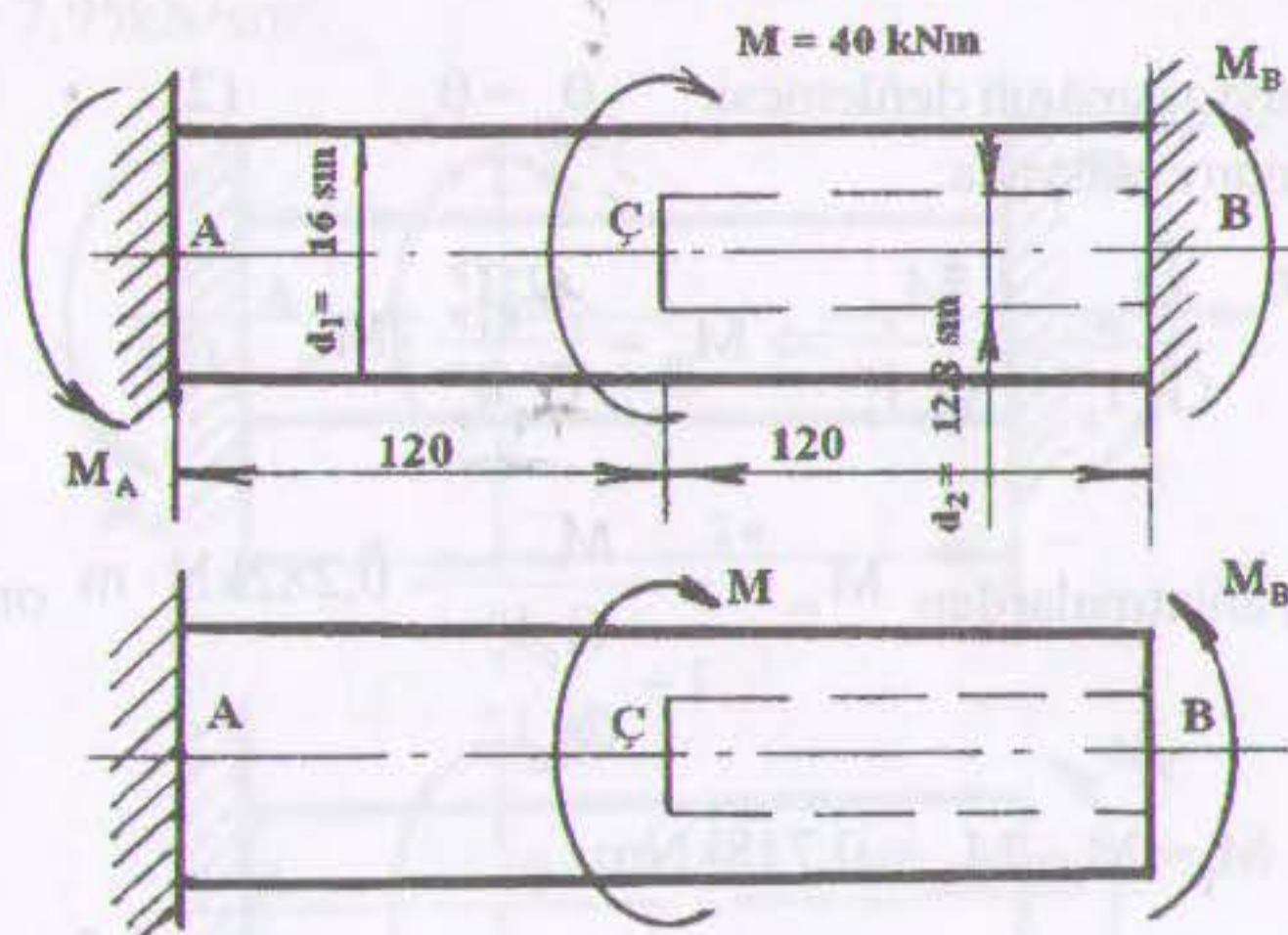
$$M_A + M_B = M. \quad (1)$$

Durkuny üýtgetmäniň deňlemesinden

$$\varphi_B = \varphi_M + \varphi_{MB} = 0,$$

$$I_{p1} = 0,1 \cdot 16^4 = 6553 \text{ sm}^4,$$

$$I_{p2} = 0,1 \cdot 16^4 \left[1 - \left(\frac{12,8}{16} \right)^4 \right] = 3866 \text{ sm}^4.$$



3.44-nji surat

$$\varphi_A = \frac{M \cdot 120}{G I_{p1}} - \frac{M_B \cdot 120}{G I_{p1}} - \frac{M_B \cdot 120}{G I_{p2}} = 0;$$

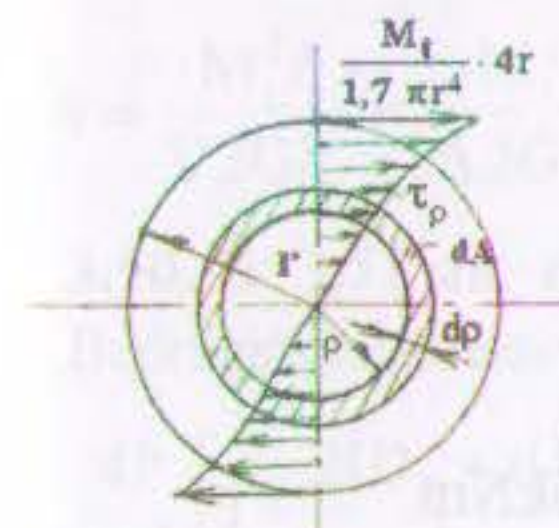
$$M_B = 13,84 \text{ kNm}, \quad M_A = 25,16 \text{ kNm};$$

$$\tau_\varphi = \frac{M_A}{I_{p1}} \cdot \frac{d_1}{2} = \frac{2516}{6553} \cdot 8 = 3,07 \text{ kN/sm}^2;$$

$$\tau_s = \frac{M_B}{I_{p2}} \cdot \frac{d_1}{2} = \frac{1484}{3866} \cdot 8 = 3,07 \text{ kN/sm}^2;$$

$$\varphi_\varphi = \frac{M_A \cdot 120}{G I_{p1}} = \frac{2516 \cdot 120}{8 \cdot 10^3 \cdot 6553} = 0,0058 \text{ rad} = 0,33^\circ.$$

$$3.45. \tau = \frac{M_t}{1,7 \pi r^4} \left(1 + \frac{3\rho}{r} \right) \rho.$$



3.45-nji surat

$$\gamma_p = \gamma \frac{\rho}{r} \text{ — bu ýerde, } \gamma_p \text{ — } \rho \text{ daşlykdaky}$$

süýşme burçy,

γ — daşky gatlakdaky süýşme burçy,

$$\text{onda, } \tau_p = G_p \gamma_p = G \left(1 + \frac{3\rho}{r} \cdot \frac{\gamma_p}{r} \right).$$

Statikanyň deňlemesinden

$$M_t = \int_A \tau_p \rho \cdot dA = \int_0^r \tau_p \cdot \rho (2\pi \rho d\rho) = 2\pi \int_0^r \tau_p \rho^2 d\rho,$$

τ_p — nyň bahasyny goýup we integrirläp alarys:

$$M_t = \frac{2\pi \gamma G}{r} \int_0^r \left(1 + \frac{3\rho}{r} \right) \rho^3 d\rho = \frac{1,7 \pi \lambda G r^4}{r},$$

$$\text{ýa-da } \frac{G \gamma}{r} = \frac{M_t}{1,7 \pi r^4}, \quad \text{onda } \tau = \frac{M_t}{1,7 \pi r^4} \left(1 + \frac{3\rho}{r} \right) \rho \text{ bolar.}$$

$$3.46. A = \frac{\pi D^3}{32a}.$$

$$N = E\alpha\Delta t A, \quad N_{BD} = N_{AC}.$$

$$M = N_{BD} \cdot a + N_{AC} \cdot a = N \cdot 2a,$$

$$\tau = \frac{M}{W_p} = \frac{2a \cdot E\alpha\Delta t A \cdot 16}{\pi D^3}; \quad \tau = \sigma = E\alpha\Delta t,$$

$$\text{onda } A = \frac{\pi D^3}{32a}.$$

$$3.47. M_t = 2,45 \text{ kNm}.$$

$$\sigma_1 = -\sigma_2 = \tau,$$

$$\varepsilon = \frac{1}{E}(\sigma_1 - \mu\sigma_2) = \frac{\tau}{E}(1 + \mu)$$

$$E = 2G(1 + \mu),$$

$$\text{onda } \varepsilon = \frac{\tau}{2G} \Rightarrow \tau = 2G\varepsilon.$$

$$\tau = \frac{M_t}{W_p} = \frac{16M_t}{\pi d^3}; \quad \frac{16M_t}{\pi d^3} = 2G\varepsilon,$$

$$M_t = \frac{G\varepsilon\pi d^3}{8} = \frac{8 \cdot 10^3 \cdot 6,5 \cdot 10^{-4} \cdot 3,14 \cdot 5^3}{8} = 2,55 \text{ kNm}$$

$$\tau = \frac{E \cdot \varepsilon}{1 + \mu} = \frac{2 \cdot 10^4 \cdot 6,5 \cdot 10^{-4}}{1 + 0,3} = 10 \text{ kN/sm}^2.$$

$$3.48. \tau_{\max} = 2,93 \text{ kN/sm}^2, \quad n = 7 \text{ sarym}.$$

Pružiniň iň uly dartgynlygy

$$\tau_{\max} = \frac{P}{A} + \frac{M_t}{W_p} = \frac{8\rho D}{\pi d^3} \left(1 + \frac{d}{2D} \right) = 2,93 \text{ kN/sm}^2.$$

Pružiniň çökmesi

$$\lambda = \frac{8\rho D^3 n}{Gd^4},$$

$$\text{Bu ýerden } n = \frac{\lambda Gd^4}{8\rho D^3} = 6,46 \approx 7 \text{ sarym}.$$

$$3.49. P = 0,0489 \text{ kN}, \quad \lambda = 25,46 \text{ sm}, \quad a = 23 \cdot 10^{-4} \text{ kN/sm}^2.$$

Pružiniň berklilik şertinden

$$P = \frac{\pi d^3 [\tau]}{8D \left(1 + \frac{d}{2D} \right)} = 0,0489 \text{ kN}$$

Pružiniň süýnmesi

$$\lambda = \frac{8\rho D^3 n}{Gd^4} = 25,46 \text{ sm}.$$

Durkuny üýtgemäniň iň uly udel potensial energiýasy

$$a = \frac{M_t^2 \ell}{V 2GI_p} = \frac{M_t^2}{A 2GI_p} = \frac{P^2 D^2}{4A 2GI_p} = 23 \cdot 10^{-4} \text{ kNsm/sm}^3.$$

$$3.50. d = 3,51 \text{ sm}, \quad n = 5 \text{ sarym}.$$

Berkligiň deňlemesini ýazýarys:

$$\frac{4P}{\pi d^2} \left[1 + \frac{2(D_0 + d)}{d} \right] \leq [\tau].$$

Bu deňlemäni özgerdip, aşakdaky aňlatmany alarys.

$$d^2 = \frac{8\rho D_0}{\pi[\tau]d} + \frac{3\rho}{\pi[\tau]}$$

San bahalaryny goýup alarys:

$$d^2 = \frac{40,64}{d} + 0,764.$$

Bu deňlemäni seçmek ýoly bilen çözmek amatly bolýar.

$$\text{Eger: } d = 4 \text{ sm} \quad 16 > 10,92$$

$$d = 3,6 \text{ sm} \quad 12,96 > 12,05$$

$$\begin{aligned} d &= 3,5 \text{ sm} & 12,25 < 12,37 \\ d &= 3,51 \text{ sm} & 12,32 \approx 12,34 \\ d &= 3,51 \text{ sm} & \text{kabul edýäris.} \end{aligned}$$

Sarymyň sany

$$n = \frac{\lambda G d^4}{8 P D_0^3} = \frac{2 \cdot 8 \cdot 10^3 \cdot 3,51^4}{8 \cdot 6 \cdot 21,75^2} = 4,92 \approx 5 \text{ sarym.}$$

$$3.51. R_A = 0,6 \text{ kN}, R_B = 1 \text{ kN}, \tau_{\max} = 6,45 \text{ kN/sm}^2, \lambda_c = 3,265 \text{ sm.}$$

Statikanyň deňlemesi:

$$R_A + R_B - P = 0 \quad (1).$$

Durkuny üýtgetmäniň deňlemesi

$$\lambda_1 = \lambda_2 \quad (2)$$

$$\lambda_1 = \frac{8 R_A D^3 m}{G d^4}, \quad \lambda_2 = \frac{8 R_B D^3 n}{G d^4}.$$

$$\text{Bu ýerden } R_A = \frac{n}{m} R_B.$$

$$\text{Onda } R_A = 0,6 \text{ kN}, R_B = 1 \text{ kN.}$$

Pružindäki iň uly dartgynlylyk

$$\tau_{\max} = \frac{8 R_B D k}{\pi d^3} = \frac{8 \cdot 1 \cdot 24 \cdot 1,12}{3,14 \cdot 2,2^3} = 6,45 \text{ kN/sm}^2.$$

$$\text{Bu ýerde } k = \frac{4 \frac{D}{d} + 2}{4 \frac{D}{d} - 3} = 1,12.$$

Ç nokadyň ornuny üýtgetmesi

$$\lambda = \frac{8 R_A D^3 m}{G D^4} = \frac{8 \cdot 0,6 \cdot 24^3 \cdot 10}{8 \cdot 10^3 \cdot 2,24} = 3,265 \text{ sm.}$$

$$3.52. \tau_{\max} = 2,38 \text{ kN/sm}^2, \lambda = 6,5 \text{ sm}, U = 9,7 \text{ joul.}$$

Iň uly galtaşma dartgynlylyk

$$\tau_{\max} = \frac{2 P R}{\pi r^3} \left(1 + \frac{r}{2 R} \right) = \frac{2 \cdot 0,3 \cdot 12}{3,14 \cdot 1^3} \left(1 + \frac{1}{2 \cdot 12} \right) = 2,38 \text{ kN/sm}^2.$$

Pružiniň uzalmasy

$$\lambda = \frac{4 P R^3}{G r^4} = \frac{4 \cdot 0,3 \cdot 12^3 \cdot 25}{8 \cdot 10^3 \cdot 1^4} = 6,5 \text{ sm.}$$

Potensial energiýany aşakdaky formula boýunça kesgitleýäris.

$$U = \frac{\pi R^3 n P^2}{G I_p} = \frac{3,14 \cdot (12 \cdot 10^{-2})^3 \cdot 25 \cdot 300^2 \cdot 2}{80 \cdot 10^9 \cdot 3,14 (1 \cdot 10^{-2})^4} = 9,7 \text{ joul.}$$

$$3.53. \tau_{\max 1} = 5,8 \text{ kN/sm}^2, \tau_{\max 2} = 11,6 \text{ kN/sm}^2, \lambda = 6 \text{ sm.}$$

Birinji pružini δ ululyga çenli gysýan güýji tapýarys.

$$P_0 = \frac{\delta G d_1^4}{8 D_1^3 n_1} = 0,534 \text{ kN} < P = 1,2 \text{ kN.}$$

Şonuň üçin hem $P = 1,2 \text{ kN}$ güýjüň täsirinden iki pružin ýüklenen; şonuň ýaly-da

$$\lambda_1 = \delta + \lambda_2.$$

Plita üçin deňagramlylygyň deňlemesi

$$P_1 + P_2 = P = 1,2 \quad (1);$$

$$\frac{8 P_1 D_1^3 n_1}{G d_1^4} = \delta + \frac{8 P_2 D_2^3 n_2}{G d_2^4} \quad (2);$$

(1) we (2) aňlatmalary bilelikde işläp alarys $P_1 = 0,8 \text{ kN}$, $P_2 = 0,4 \text{ kN}$.

Pružinlerdäki galtaşma dartgynlylyklar

$$\tau_{\max} = \frac{8 P_1 D_1 k_1}{\pi d_1^3} = \frac{8 \cdot 0,8 \cdot 20 \cdot 1,14}{3,14 \cdot 2^3} = 5,8 \text{ kN/sm}^2.$$

$$k_1 = \frac{4 \cdot \frac{20}{2} + 2}{4 \cdot \frac{20}{2} - 3} = 1,14 = k_2;$$

$$\tau_{\max 2} = \frac{8 P_2 D_2 k_2}{\pi d_2^3} = \frac{8 \cdot 0,4 \cdot 10 \cdot 1,14}{3,14 \cdot 1^3} = 11,6 \text{ kN/sm}^2.$$

Plitanyň ornuny üýtgetmesi birinji pružiniň çökmesine deň

$$\lambda_1 = \frac{8P_1 D_1^3 n_1}{G d_1^4} = \frac{8 \cdot 0,8 \cdot 20^3 \cdot 15}{8 \cdot 10^3 \cdot 2^4} = 6 \text{ sm.}$$

3.54. $d_1 = 1,02 \text{ sm}$, $d_2 = 0,907 \text{ sm}$, $d_3 = 0,944 \text{ sm}$.

Mesele iki gezek statiki kesgitlenmeýän statikanyň deňlemesi

$$\Sigma M_A = Q_1 a + Q_2 2a + Q_3 3a = P \cdot 3a,$$

$$Q_1 + 2Q_2 + 3Q_3 = 3P = 12 \text{ kN.} \quad (1)$$

Ornuny üýtgetmäniň deňlemesi, çyzgydan

$$\lambda_1 : \lambda_2 : \lambda_3 = 1 : 2 : 3$$

ýa-da $\frac{8Q_1 D_1^3 n}{G d_1^4} : \frac{8Q_2 D_2^3 n}{G d_2^4} : \frac{8Q_3 D_3^3 n}{G d_3^4} = 1 : 2 : 3.$

Bu ýerden $\frac{27Q_1}{d_1^4} = \frac{64Q_2}{2d_2^4} = \frac{125Q_3}{3d_3^4}, \quad (2)$

Pružinleriň deňberklik şertinden

$$\tau_{1\max} = \tau_{2\max} = \tau_{3\max} = [\tau],$$

ýa-da $\frac{8Q_1 D_1}{\pi d_1^3} = \frac{8Q_2 D_2}{\pi d_2^3} = \frac{8Q_3 D_3}{\pi d_3^3}.$

Bu ýerden $\frac{3Q_1}{d_1^3} = \frac{4Q_2}{d_2^3} = \frac{5Q_3}{\pi d_3^3} \quad (3)$

(1), (2), (3) aňlatmalary işläp alarys

$$Q_1 = 1,9Q_2 = 2,1Q_3,$$

$$Q_1 = 3,45 \text{ kN.}$$

Onda $d_1 = \sqrt[3]{\frac{8Q_1 D_1}{\pi[\tau]}} = \sqrt[3]{\frac{8 \cdot 3,45 \cdot 6}{3,14 \cdot 50}} = 1,02 \text{ sm},$

$$d_2 = \frac{8}{9} d_1 = 0,907 \text{ sm}, \quad d_3 = \frac{25}{27} d_1 = 0,944 \text{ sm}.$$

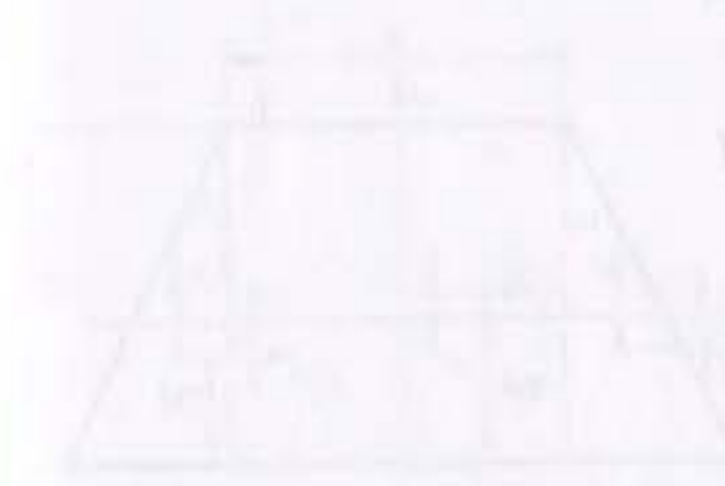
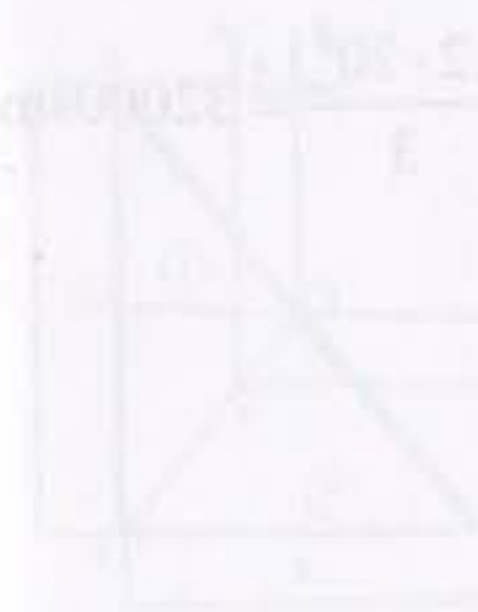
3.55. $d = 3 \text{ mm}$, $\lambda = 17 \text{ mm}$.

Pružiniň siminiň diametri

$$d_1 = \sqrt[3]{\frac{8PD}{\pi[\tau]}} = \sqrt[3]{\frac{8 \cdot 0,15 \cdot 2}{3,14 \cdot 40}} = 0,267 \text{ sm} \approx 3 \text{ mm}.$$

Pružini gysmasynyň ululygy

$$\lambda = \frac{8PD^3 n}{G d^4} = \frac{8 \cdot 0,15 \cdot 2^3 \cdot 6}{4,2 \cdot 10^3 \cdot 0,3^4} = 1,7 \text{ sm}.$$



IV bap

Tekiz kesiklerin geometriki häsiýetleri

4.1. $I_{y_1} = 32000 \text{sm}^4$, $I_{y_1 z_1} = 14400 \text{sm}^4$.

Parallel oklara görä inersiýa momentlerin formulasyňy peýdalanýarys.

$$I_{y_1} = I_y + \left(\frac{h}{2}\right)^2 \cdot A = \frac{bh^3}{12} + \frac{bh^3}{4} = \frac{bh^3}{3} = \frac{12 \cdot 20^3}{3} = 32000 \text{sm}^4,$$

$$I_{y_1 z_1} = A \left(\frac{h}{2}\right) \left(\frac{b}{2}\right) = \frac{b^2 h^2}{4} = \frac{20^2 \cdot 12^2}{4} = 14400 \text{sm}^4.$$

4.2. $I_{y_1} = 4860 \text{sm}^4$.

$\triangle ABC = \triangle DEF$

onda $I_{y_1} = \frac{bh^3}{12} + \left(\frac{h}{2}\right)^2 \cdot A = \frac{bh^3}{3} = \frac{20 \cdot 9^3}{3} = 4860 \text{sm}^4$.



4.2-nji surat

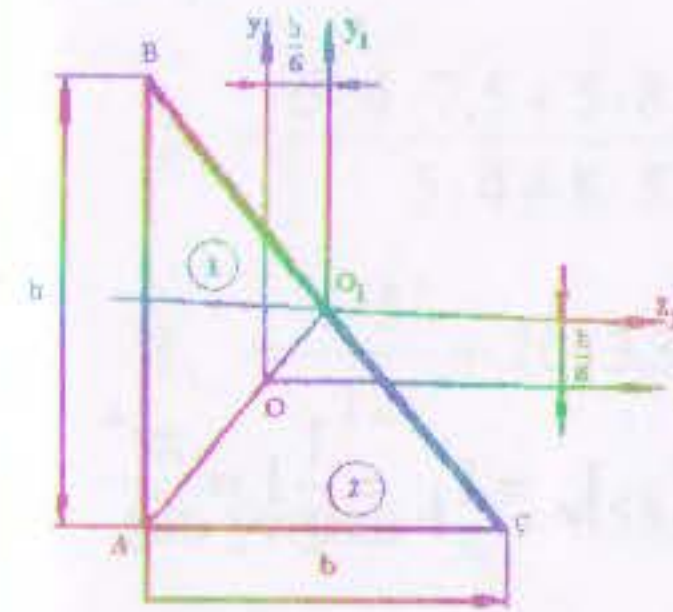
4.3. $I_{y_1} = \frac{bh^3}{4}$, $I_y = \frac{bh^3}{36}$.

$$b_z = b \frac{z}{h}, \quad dA = b_z \cdot dz = b \frac{z}{h} dz,$$

Onda $I_{y_1} = \int_0^h z^2 dA = \int_0^h z^2 b \cdot \frac{z}{h} dz = \frac{bh^3}{4};$

$$I_y = \frac{bh^3}{4} - \left(\frac{2h}{3}\right)^2 \cdot \left(\frac{b}{2}\right) \cdot h = \frac{bh^3}{36}.$$

4.4. $I_{yz} = -\frac{b^2 h^2}{72}$, $I_{AC} = \frac{bh^3}{12}$.



4.4-nji surat

AO kesim ABC üçburçlugyň medianasy. z_1 ok ABO üçburçlugyň simmetriýa oky bolany üçin,

$$I_{(z_1 y_1)_1} = 0, \text{ Şonuň ýaly-da } I_{(z_1 y_1)_2} = 0,$$

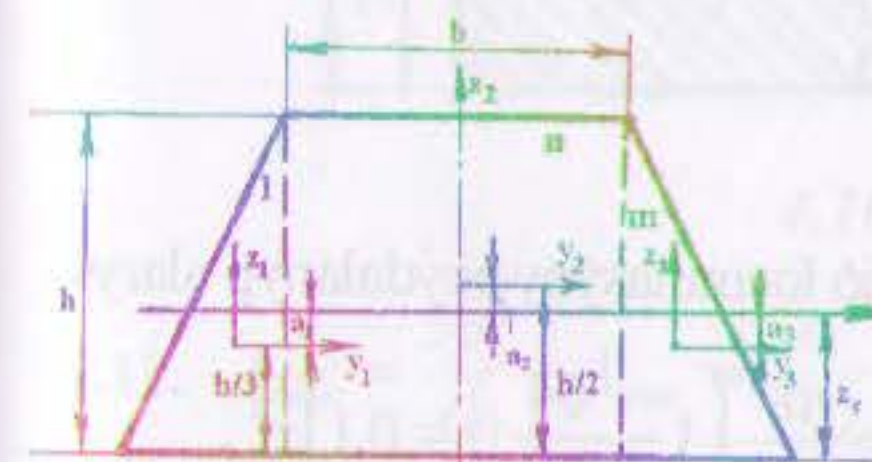
$$\text{onda } I_{z_1 y_1} = I_{(z_1 y_1)_1} + I_{(z_1 y_1)_2} = 0.$$

Parallel oklaryň baglanyşygyndan

$$I_{z_1 y_1} = I_{zy} + A \left(-\frac{h}{6}\right) \left(-\frac{b}{6}\right) = 0$$

Bu ýerden $I_{zy} = -A \frac{hb}{36} = -\frac{bh}{2} \cdot \frac{bh}{36} = -\frac{b^2 h^2}{72},$

$$I_{AC} = I_z + A \left(\frac{h}{2}\right)^2 = \frac{bh^3}{36} + \frac{bh}{2} \cdot \frac{h^2}{9} = \frac{bh^3}{12}$$



4.5-nji surat

4.5. $I_y = \frac{13bh^3}{108}$.

Adaty usul bilen $z_c = \frac{4}{9}h,$

$$a_1 = a_3 = -\frac{h}{9}, \quad a_2 = \frac{h}{18}.$$

Onda $I_y = 2 \frac{bh^3}{72} + \frac{bh}{2} \left(-\frac{h}{9}\right)^2 + \frac{bh^3}{12} + bh \left(\frac{h}{18}\right)^2 = \frac{13bh^3}{108}.$

$$4.6. I_y = 3167 \text{sm}^4.$$

$$I_y = I_y^{\text{gön}} - I_y^{\text{kw}} = 3167 \text{sm}^4.$$

4.7. Meýdan 38,6% köpelyär, inersiýa momenti 4,3% azalýar.

$$I_y^o = 46150 \text{sm}^4, I_y^{oo} = 44187,5 \text{sm}^4, A^o = 406 \text{sm}^2, A^{oo} = 563 \text{sm}^2.$$

$$\frac{A^{oo}}{A^o} = \frac{563}{406} = 1,386 \Rightarrow 38,6\% \text{ köpelyär}$$

$$\frac{I_y^{oo}}{I_y^o} = \frac{44187,5}{46150} = 0,957 \Rightarrow 4,3\% \text{ azalýar.}$$

$$4.8. z_c = \frac{4r}{3\pi}; I_y = \frac{\pi r^4}{8} \left(1 - \frac{64}{9\pi^2}\right) \approx 0,11r^4; I_z = I_{y_1} = \frac{1}{2} I = \frac{\pi r^4}{8}.$$

$$z_c = \frac{S_{y_1}}{A} \Rightarrow S_{y_1} = \int_A y_1 dA = \int_0^r b_y \cdot y_1 dy, A = 0,5\pi r^2,$$

$$b_y = 2r \sin \varphi, y_1 = r \cos \varphi, dy_1 = -r \sin \varphi d\varphi.$$

$$\text{Onda } S_{y_1} = -2r^3 \int_{\frac{\pi}{2}}^0 \sin \varphi \cos \varphi d\varphi = 2r^3 \frac{\sin^3 \varphi}{3} \Big|_0^{\frac{\pi}{2}} = \frac{2}{3} r^3,$$

$$z_c = \frac{\frac{2}{3} r^3}{0,5\pi r^2} = \frac{4r}{3\pi}.$$

Parallel oklara görä inersiýa momentleriň formulasyny peýdalanyp alarys:

$$I_y = I_{y_1} - A \cdot z_c^2 = \frac{\pi r^4}{8} - \frac{\pi r^2}{4} \cdot \frac{16r^2}{9\pi^2} = \frac{\pi r^4}{9} \left(1 - \frac{64}{9\pi^2}\right) \approx 0,11r^4.$$

Bu ýerde $I_{y_1} = \frac{\pi r^4}{8}$ — ýarym töweregiň oka görä inersiýa momenti

Beýleki baş oka görä inersiýa momenti,

$$I_{z_c} = 0,5 \cdot \frac{\pi r^4}{4} = \frac{\pi r^4}{8} \approx 0,39r^4.$$

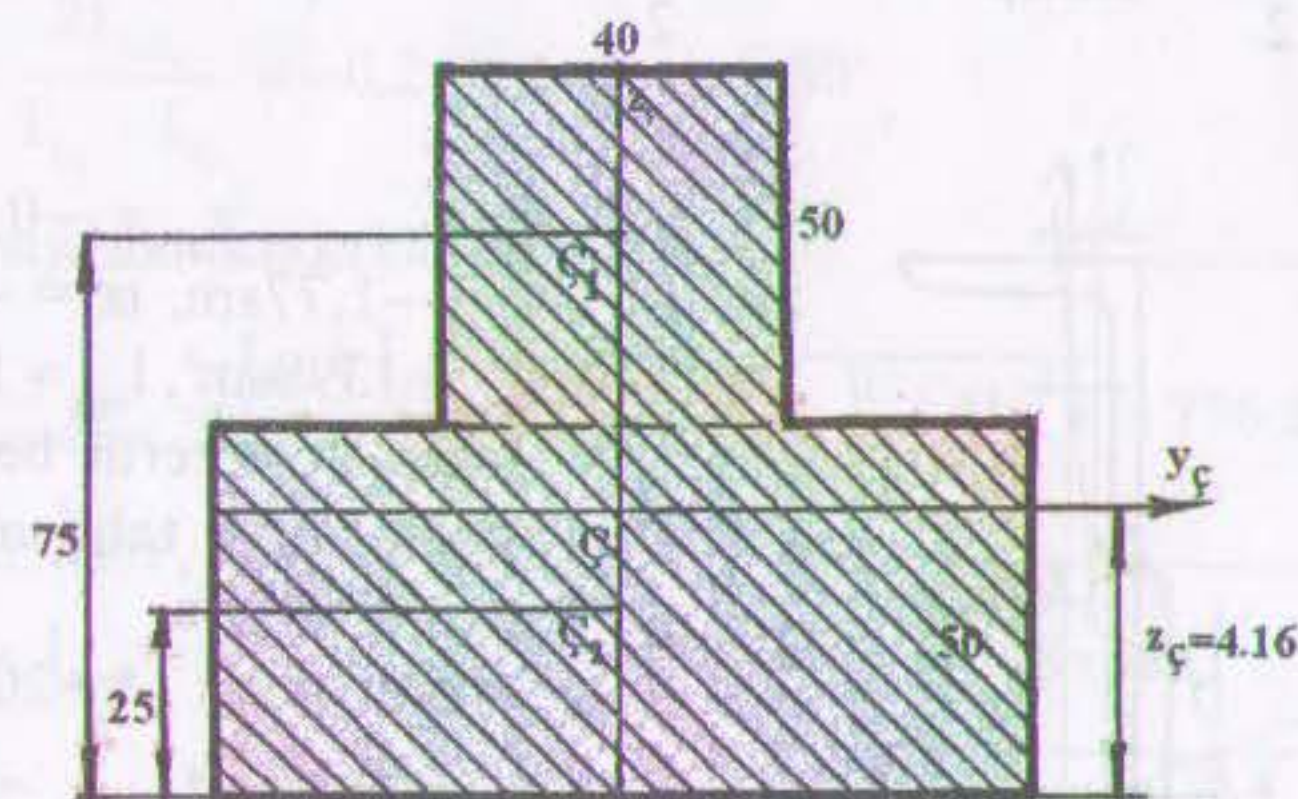
$$4.9. I_y = \frac{ab^3}{12} + \frac{\pi b^4}{64}, I_z = \frac{ab}{12} (a^2 + 2b^2) + \frac{\pi b^4}{64} (b^2 + 4a^2).$$

$$4.10. I_{y_c} = 458 \text{sm}^4.$$

$$z_c = \frac{5 \cdot 4 \cdot 7,5 + 5 \cdot 8 \cdot 2,5}{5 \cdot 4 + 8 \cdot 5} = 4,16 \text{sm},$$

$$I_{y_c} = \frac{4 \cdot 5^3}{12} + 20 \cdot 3,34^2 + \frac{8 \cdot 5^3}{12} + 40(1,66)^2.$$

Bu ýerden $I_{y_c} = 458 \text{sm}^4.$



4.10-njy surat

$$4.11. I_{\max} = \frac{5b^4}{64}; I_{\min} = \frac{7b^4}{192}; I_{z_c y_c} = -0,022b^4.$$

$$z_c = y_c = \frac{\frac{b \cdot b}{2} \cdot \frac{b}{4} + \frac{b \cdot b}{2} \cdot \frac{3}{4} \cdot \frac{b}{4}}{\frac{b \cdot b}{2} + \frac{b \cdot b}{2}} = \frac{5b}{12};$$

$$I_{z_0} = I_{y_0} = \frac{b^4}{16 \cdot 12} + \frac{b}{2} \cdot \frac{b}{2} \cdot \left(-\frac{b}{6}\right)^2 + b \cdot \frac{b}{2} \cdot \left(\frac{b}{12}\right)^2 + \frac{b \cdot b^3}{8 \cdot 12} = \frac{5b^4}{192},$$

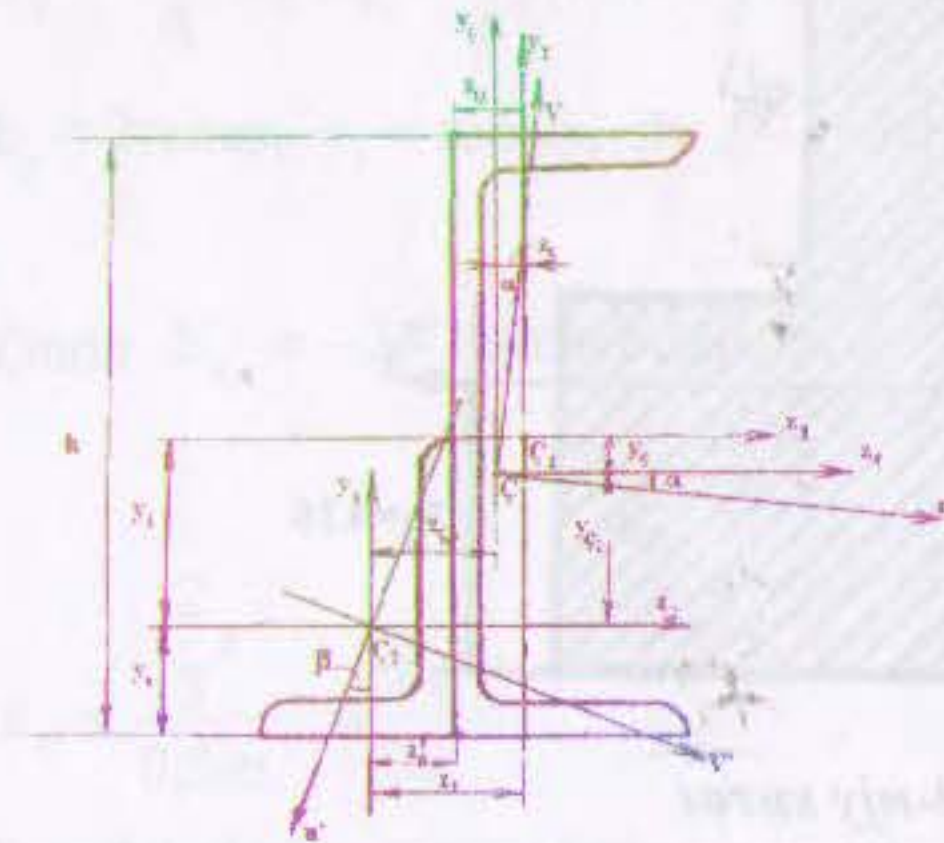
$$I_{z_0 y_0} = b \cdot \frac{b}{2} \cdot \left(\frac{b}{12}\right) \left(-\frac{b}{6}\right) + \frac{b}{2} \cdot \frac{b}{2} (0,334b) (-0,166b) = -0,02b^4,$$

$$\operatorname{tg} 2\alpha = -\frac{I_{z_0 y_0}}{I_{z_0} - I_{y_0}} = +\infty \Rightarrow \alpha = +45^\circ,$$

$$I_{\max(\min)} = \frac{I_{z_0} + I_{y_0}}{2} \pm \frac{1}{2} \sqrt{(I_{z_0} - I_{y_0})^2 + 4I_{z_0 y_0}^2},$$

Bu ýerden $I_{\max} = 0,077b^4$, $I_{\min} = 0,037b^4$.

$$I_{z_0 y_0} = \frac{I_{\max} - I_{\min}}{2} \sin 2\beta = \frac{0,077b^4 - 0,037b^4}{2} \sin(-90^\circ) = -0,02b^4.$$



4.12-nji surat

Burçluk üçin: $A_b = 8,54 \text{ sm}^2$, $I_{z_2} = 70,6 \text{ sm}^4$, $I_{y_2} = 21,2 \text{ sm}^4$, $I_{v_1} = 79,1 \text{ sm}^4$,

$$I_{u_1} = 12,2 \text{ sm}^4,$$

$$\operatorname{tg} \beta = 0,384, z_0^1 = 1,28 \text{ sm}, y_0 = 2,95 \text{ sm}.$$

Şwelleriň merkezi okuna görä kesigiň agyrlýk merkezini kesgitleýäris:

$$z_0 = \frac{A_s \cdot 0 + A_b \cdot z_1}{A_s + A_b} = -0,94 \text{ sm},$$

$$y_0 = \frac{A_s \cdot 0 + A_b \cdot y_1}{A_s + A_b} = -1,77 \text{ sm}.$$

Baş inersiýa okuň yagdaýyny kesgitleýäris:

$$I_{z_0} = I_{z_1} + A_s \cdot y_0^2 + I_{z_2} + A_b \cdot y_{01}^2 = 1382 \text{ sm}^4,$$

$$I_{y_0} = I_{y_1} + A_s \cdot z_0^2 + I_{y_2} + A_b \cdot z_{01}^2 = 170 \text{ sm}^4,$$

$$I_{z_0 y_0} = A_s \cdot z_0 y_0 + \frac{I_{v_1} - I_{u_1}}{2} \cdot \sin 2\beta + A_b \cdot y_{01} \cdot z_{01} = 140 \text{ sm}^4,$$

$$\operatorname{tg} 2\alpha = \frac{2I_{z_0 y_0}}{I_{y_0} - I_{z_0}} = -0,231 \Rightarrow \alpha = -6^\circ 30'.$$

Baş inersiýa momentlerini kesgitleýäris.

$$I_{u,v} = I_{\max(\min)} = \frac{I_{z_0} + I_{y_0}}{2} \pm \frac{1}{2} \sqrt{(I_{z_0} - I_{y_0})^2 + 4I_{z_0 y_0}^2} = 776 \pm 622,$$

$$I_{\max} = 1398 \text{ sm}^4, I_{\min} = 154 \text{ sm}^4.$$

$$\text{Barlagy: } I_{\max} + I_{\min} = I_{z_0} + I_{y_0}; 1382 + 170 = 1398 + 154$$

$$1552 = 1552$$

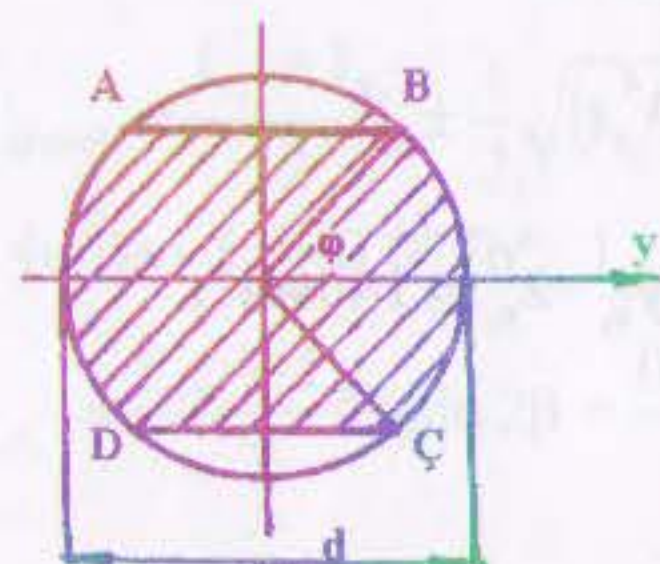
$$\begin{aligned} I_{u,v} &= \frac{I_{z_0} + I_{y_0}}{2} \cdot \sin 2\beta + I_{z_0 y_0} \cdot \cos 2\alpha = \\ &= \frac{1382 - 170}{2} \cdot \sin(-13^\circ) + 140 \cdot \cos(-13^\circ) = 0. \end{aligned}$$

Ýokardaky hasaplar dogry ýerine ýetirilen.

$$4.13. I_y = \frac{d^4}{32} \left(\varphi - \frac{\sin 4\varphi}{4} \right).$$

$$I_y = 2 \frac{b \left(\frac{h}{2} \right)^3}{4} + 2 \cdot \frac{d\varphi}{128} (2\varphi - \sin 2\varphi); \quad b = d \cos \varphi, \quad h = d \sin \varphi.$$

Onda



4.13-nji surat

$$\begin{aligned} I_y &= \frac{d^4 \sin^3 \varphi \cos \varphi}{16} + \frac{d^4 (2\varphi - \sin 2\varphi)}{64} = \\ &= \frac{d^4}{32} \left[\varphi - (0,5 \sin 2\varphi - 2 \sin^3 \varphi \cos \varphi) \right] = \\ &= \frac{d^4}{32} \left[\varphi - \frac{1}{2} (\sin 2\varphi - 4 \cos \varphi \sin^3 \varphi) \right] = \\ &= \frac{d^4}{32} \left[\varphi - \frac{1}{2} (\sin 2\varphi - 2 \cdot 2 \sin \varphi \cos^2 \varphi \sin^2 \varphi) \right] = \\ &= \frac{d^4}{32} \left(\varphi - \frac{\sin 4\varphi}{4} \right). \end{aligned}$$

$$4.14. W_y = \frac{b}{6} (d^2 - b^2), \quad b = \frac{d}{\sqrt{3}} = 0,577d; \quad h = \frac{d\sqrt{2}}{\sqrt{3}} = 0,816d.$$

$$W_y = \frac{bh^2}{6}; \quad d^2 = h^2 + b^2 \Rightarrow h^2 = d^2 - b^2, \quad W_y = \frac{b(d^2 - b^2)}{6},$$

$$W'_y = \left[\frac{b(d^2 - b^2)}{6} \right]' = \frac{d^2 - 3b^2}{6},$$

bu ýerden $b = \frac{d}{\sqrt{3}}$, onda $h = \frac{d\sqrt{2}}{\sqrt{3}}$.

$$4.15. \alpha = 25^\circ, I_{\max} = 1,73 \text{ sm}^4, I_{\min} = 0,43 \text{ sm}^4.$$

Merkezi inersiýa momentlerini integrirlap tapýarys.

Çyzgydan $b_y = \frac{2}{3}(3a - y),$

$$dA = \frac{2}{3}(3a - y)dy,$$

$$I_z = \int_0^{3a} y^2 \cdot \frac{2}{3}(3a - y)dy = 4,5a^4,$$

$$I_{z_c} = I_z - A \cdot \left(\frac{3a}{3} \right)^2 = 4,5a^4 - \frac{3a \cdot 2a}{2} \left(\frac{3a}{3} \right)^2 = \frac{3a^4}{2},$$

$$I_{y_c} = I_y - A \cdot \left(\frac{2a}{3} \right)^2 = \frac{3a \cdot (2a)^3}{12} - \frac{3a \cdot 2a}{2} \left(\frac{2a}{3} \right)^2 = \frac{2a^4}{3},$$

$$I_{z_c y_c} = I_{zy} - A \cdot \left(\frac{3a}{3} \right) \left(\frac{2a}{3} \right) = \frac{(3a)^2 \cdot (2a)^2}{24} - \frac{3a \cdot 2a}{2} \cdot \frac{2}{3} a^2 = -\frac{a^4}{2}.$$

Baş okuň ugruny kesgitleýäris:

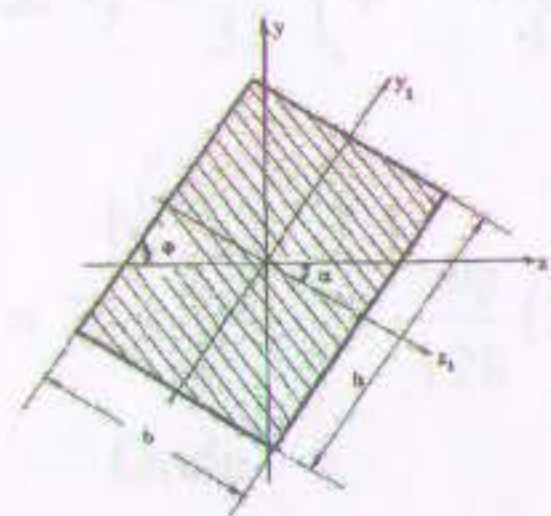
$$\text{tg } \alpha = \frac{2I_{z_c y_c}}{I_{z_c} - I_{y_c}} = \frac{2 \left(-\frac{a^4}{2} \right)}{\frac{3}{2} a^4 - \frac{2}{3} a^4} = 1,2.$$

Bu ýerden $\alpha = 25^\circ$.

Baş inersiýa momentleri:

$$\begin{aligned} I_{\max(\min)} &= \frac{1}{2} \left[I_{z_c} + I_{y_c} \pm \sqrt{(I_{z_c} - I_{y_c})^2 + 4I_{z_c y_c}^2} \right] = \\ &= \frac{1}{2} \left[\frac{3}{2} a^4 + \frac{2}{3} a^4 \pm \sqrt{\left(\frac{3}{2} a^4 - \frac{2}{3} a^4 \right)^2 + 4 \left(-\frac{a^4}{2} \right)^2} \right], \end{aligned}$$

Bu ýerden $I_{\max} = 1,73 \text{ sm}^4, I_{\min} = 0,43 \text{ sm}^4.$



4.16-njy surat

$$4.16. I_{zy} = \frac{bh^3}{12} (h^2 - b^2) \sin \alpha \cos \alpha,$$

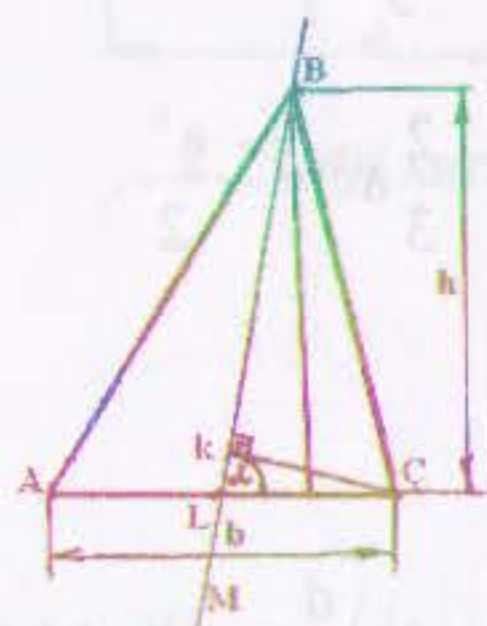
$$I_{z_1} = \frac{bh^3}{12}, I_{y_1} = \frac{b^3h}{12}, I_{z_1y_1} = 0,$$

$$\alpha = 90^\circ - \varphi$$

$$I_{zy} = \frac{I_{z_1} - I_{y_1}}{2} \sin 2\alpha + I_{z_1y_1} \cos 2\alpha =$$

$$= \frac{\frac{bh^3}{12} - \frac{b^3h}{12}}{2} \sin 2\alpha =$$

$$= \frac{hb}{12} (h^2 - b^2) \sin \alpha \cos \alpha.$$



4.17-nji surat

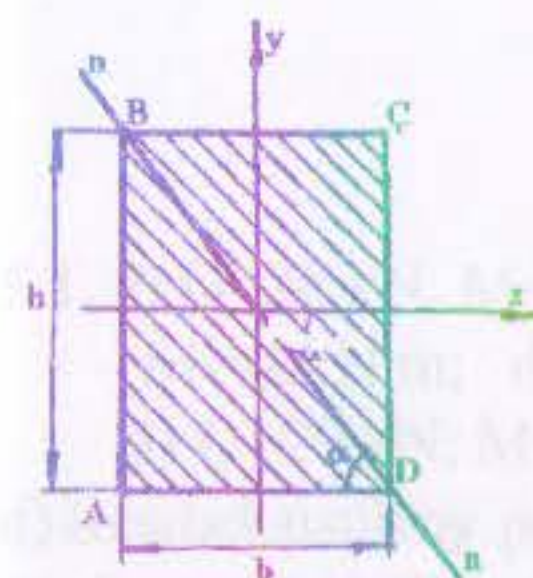
$$4.17. I_x = \frac{hb^3 \cdot \sin^2 \alpha}{48}.$$

BM - mediana

$$\sin \alpha = \frac{KC}{b}, \quad KC = \frac{b}{2} \sin \alpha,$$

$$BL = \frac{h}{\sin \alpha}, \quad I_x = \frac{hb^3}{12},$$

$$I_x = 2 \left[\frac{h}{\sin \alpha} \cdot \frac{\left(\frac{b}{2} \sin \alpha \right)^3}{12} \right] = \frac{2hb^3 \sin^2 \alpha}{8 \cdot 2} = \frac{hb^3 \sin^2 \alpha}{48}$$



4.18-nji surat

$$4.18. I_n = \frac{b^3h^3}{6(h^2 + b^2)}.$$

$$\cos \alpha = \frac{b}{\sqrt{b^2 + h^2}}, \quad \sin \alpha = -\frac{h}{\sqrt{b^2 + h^2}},$$

$$I_n = I_z \cos^2 \alpha + I_y \sin^2 \alpha =$$

$$= \frac{bh^3}{12} \cos^2 \alpha + \frac{b^3h}{12} \sin^2 \alpha =$$

$$= \frac{b^3h^3}{6(h^2 + b^2)}.$$

$$4.19. u = \frac{a}{9\sqrt{2}}; \quad W_z^{\max} = \frac{64\sqrt{2}}{729} a^3; \quad \frac{W_z^{\max}}{W_z} = \frac{256}{243}.$$

Ştrihlenen meýdanyň garşylyk momenti:

$$W_z = \frac{2u(2y)^2}{6} + \frac{(y\sqrt{2})^4}{12y}.$$

$$\text{Çyzgydan } u = \frac{a}{\sqrt{2}} - y;$$

özürtmeden soň:

$$W_z = \frac{2\sqrt{2}}{3} ay^2 - y^3,$$

$$W'_z = \frac{4\sqrt{2}}{3} ay - 3y^2 = 0.$$

$$\text{Bu ýerden: } y = \frac{4\sqrt{2} \cdot a}{9}.$$

$$W_z^{\max} = \frac{2\sqrt{2}}{3} a \left(\frac{4\sqrt{2}}{9} a \right)^2 - \left(\frac{4\sqrt{2}}{9} a \right)^3 = \frac{64\sqrt{2}}{729} a^3,$$

$$W_z = \frac{a^3}{6\sqrt{2}},$$

$$\text{Onda: } \frac{W_z^{\max}}{W_z} = \frac{64\sqrt{2}a^3 6\sqrt{2}}{729a^3} = \frac{256}{243}.$$

$$4.20. \frac{h}{b} = \sqrt{3}, \quad \frac{h}{b} = \sqrt{2}.$$

$$\text{Rombuň dörtten bir bölegi üçin - } I_z^1 = \frac{bh^3}{12},$$

$$\text{Onda: } I_z = \frac{bh^3}{3}; \quad W_z = \frac{I_z}{h} = \frac{bh^2}{3}.$$

$$\text{Çyzgydan } h^2 = a^2 - b^2$$

$$W_z = \frac{b(a^2 - b^2)}{3} \text{ we } \frac{dW_z}{db} = 0,$$

$$W_z' = \left[\frac{b(a^2 - b^2)}{3} \right]' = \frac{a^2 - 3b^2}{3} = 0 \Rightarrow a = b\sqrt{3}.$$

$$\text{Onda: } h = b\sqrt{2} - \text{garşylyk momenti iň uly.}$$

$$\text{Çyzgydan: } b = \sqrt{a^2 - h^2}, \quad I_z = \frac{\sqrt{a^2 - h^2} \cdot h^3}{3} \text{ we } \frac{dI_z}{dh} = 0.$$

$$I_z^1 = \left(\frac{\sqrt{a^2 - h^2} \cdot h^3}{3} \right)' = -h^4 + 3h^2(a^2 - h^2) = 0,$$

$$a = \frac{2h}{\sqrt{3}}, \quad b^2 = a^2 - h^2 = \frac{4h^2}{3} - h^2 = \frac{h^2}{3},$$

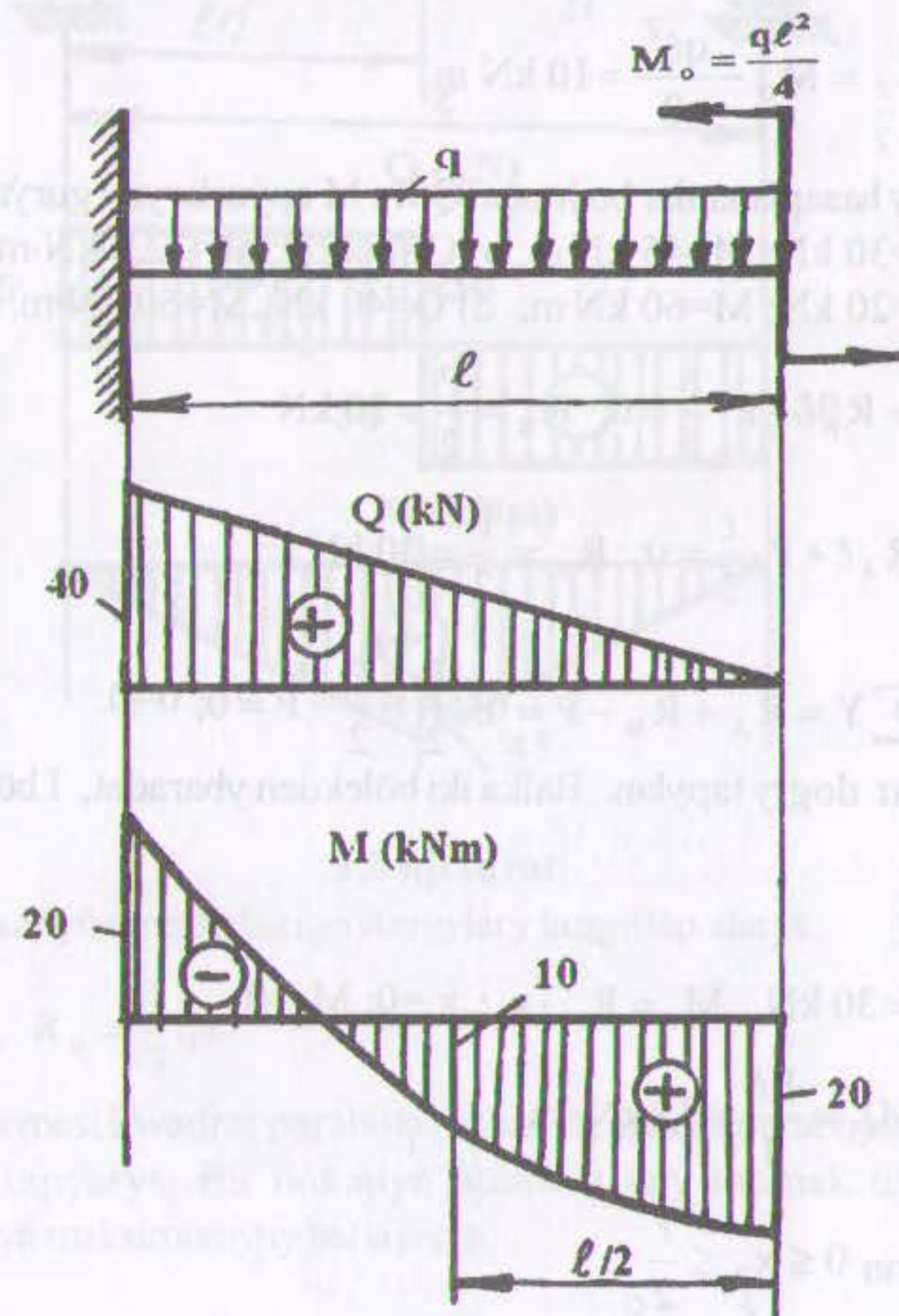
$$\frac{h}{b} = \sqrt{3} - \text{inersiya momenti iň uly.}$$

V bap

Tekiz egilme

- 5.1. a) $Q=20 \text{ kN}$; $M=40 \text{ kN}\cdot\text{m}$; b) $Q=0$; $M=40 \text{ kN}\cdot\text{m}$; c) $Q=40 \text{ kN}$; $M=40 \text{ kN}\cdot\text{m}$; d) $Q=40 \text{ kN}$; $M=20 \text{ kN}\cdot\text{m}$; g) $Q=40$; $M=20 \text{ kN}\cdot\text{m}$; ä) $Q=20 \text{ kN}$; $M=20 \text{ kN}\cdot\text{m}$.

d) Kesmek usulyny peýdalanyň, balkanyň içki güýçleriniň aňlatmalaryny ýazýarys, häsiýetli kesiklerde bahasyny kesgitleýäris we olaryň epýurlaryny gurýarys.



5.1-nji surat

I-I kesik üçün

$$Q_1 = qx, M_1 = M_0 - q \frac{x_1^2}{2} \text{ bu ýerde } 0 \leq x_1 \leq \ell$$

$$\text{Eger } x_1 = 0 \Rightarrow Q_B = 0, M_B = M_0 = 20 \text{ kN m},$$

$$\text{Eger } x_1 = \ell \Rightarrow Q_A = 40 \text{ kN}, M_A = -40 \text{ kN m}.$$

Egme momentiň aňlatmasyndan onuň parabolanyň çyzygy boýunça üýtgeýändigini anyklap, egme momentiň aralyk bahasyny hasaplaýarys.

$$x_1 = \frac{\ell}{2}, M_{\frac{\ell}{2}} = M_0 - \frac{q\ell^2}{8} = 10 \text{ kN m}$$

Ýokardaky hasaplananlar boýunça Q we M epýurlaryny gurýarys.

5.2. a) $Q=30 \text{ kN}$; $M=45 \text{ kN}\cdot\text{m}$; b) $Q=30 \text{ kN}$; $M=22,5 \text{ kN}\cdot\text{m}$;

ç) $Q=20 \text{ kN}$; $M=60 \text{ kN}\cdot\text{m}$; d) $Q=40 \text{ kN}$; $M=60 \text{ kN}\cdot\text{m}$.

$$\text{a) } \sum M_A = R_B \ell - P \cdot \frac{\ell}{2} = 0; R_B = \frac{P}{2} = 30 \text{ kN}$$

$$\sum M_B = R_A \ell + P \cdot \frac{\ell}{2} = 0; R_A = \frac{P}{2} = 30 \text{ kN}.$$

$$\text{Barlagy: } \sum Y = R_A + R_B - P = 0; \frac{P}{2} + \frac{P}{2} - P = 0; 0=0.$$

Gaýtargylar dogry tapylan. Balka iki bölekden ybaradat, I bölek üçün

$$0 \leq x_1 \leq \frac{\ell}{2}$$

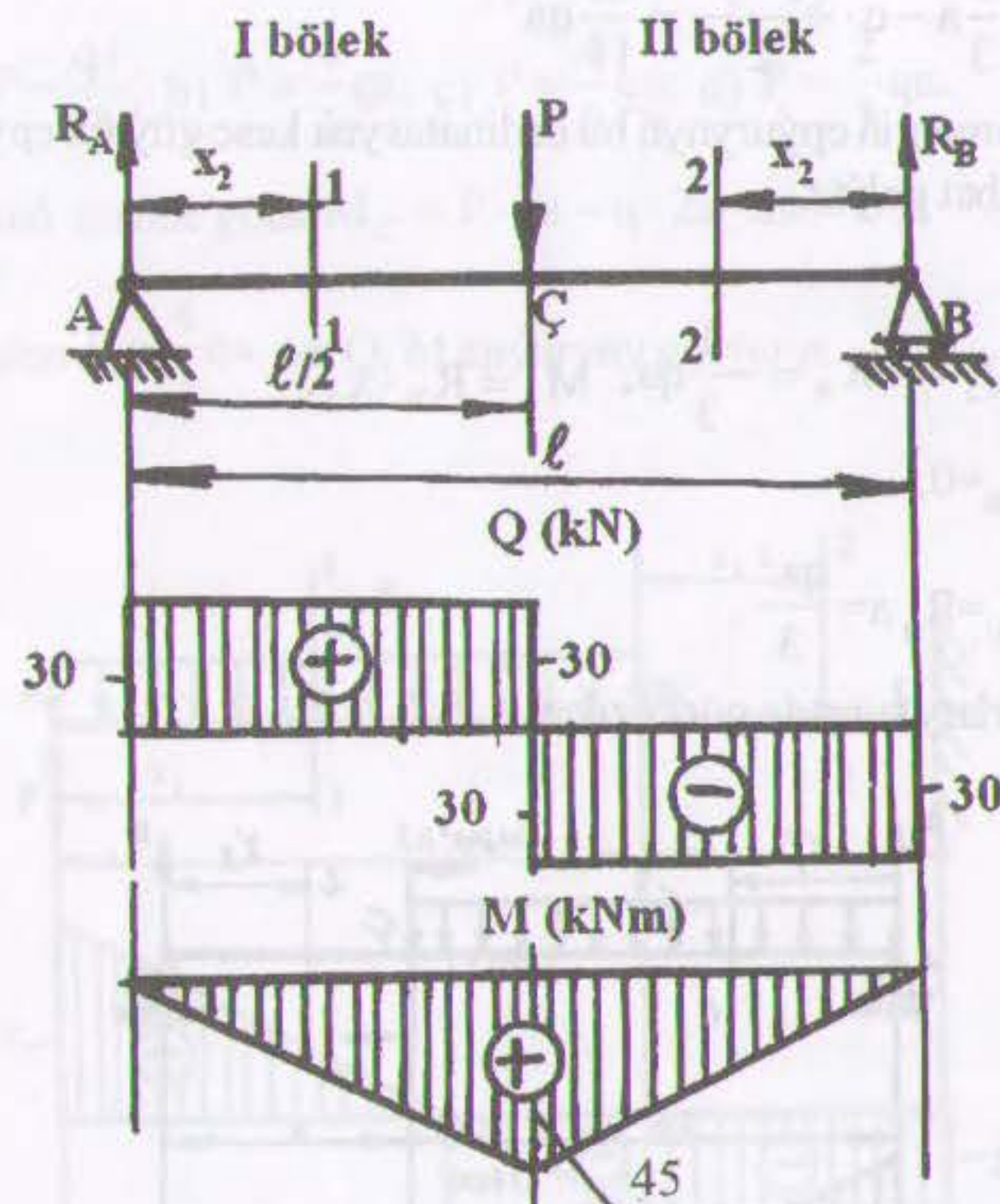
$$Q_1 = R_A = 30 \text{ kN}, M_1 = R_A \cdot x_1; x_1=0; M_A=0$$

$$x_1 = \frac{\ell}{2}, M_{\frac{\ell}{2}} = \frac{P\ell}{4} = 45 \text{ kN}\cdot\text{m}.$$

$$\text{II bölek üçün } 0 \leq x_2 \leq \frac{\ell}{2}$$

$$Q_2 = -R_B = -30 \text{ kN}, M_2 = R_B \cdot x_2; x_1=0, M_B=0; x_2 = \frac{\ell}{2},$$

$$M_{\frac{\ell}{2}} = \frac{P\ell}{4} = 45 \text{ kN}\cdot\text{m}$$



5.2-nji surat

5.3. f) Balkanyň diregindäki gaýtargylary kesgitläp alarys:

$$R_A = \frac{5}{3} qa, R_B = \frac{1}{3} qa.$$

M_1 -iň deňlemesi kwadrat parabola, şonuň üçin hem parabolanyň üçünji nokadyny tapýarys. Bu nokadyň abssissasyny tapmak üçin M_1 -iň aňlatmasynyň maksimumyny barlaýarys.

$$\frac{dM_1}{dx_1} = Q_1 = R_A - qx_1 = 0 \text{ bu ýerden } x_{\max} = \frac{R_A}{q} = \frac{5}{3} a,$$

x_{\max} bahasyny M_1 goýup alarys.

$$M_{\max} = \frac{5qa}{3} \cdot \frac{5}{3}a - q \cdot \frac{\left(\frac{5}{3}a\right)^2}{2} = \frac{25}{18}qa^2.$$

Egme momentin epýurynyň bu ordinatasyna kese güýjün epýurynyň nol nokady gabat gelýär.

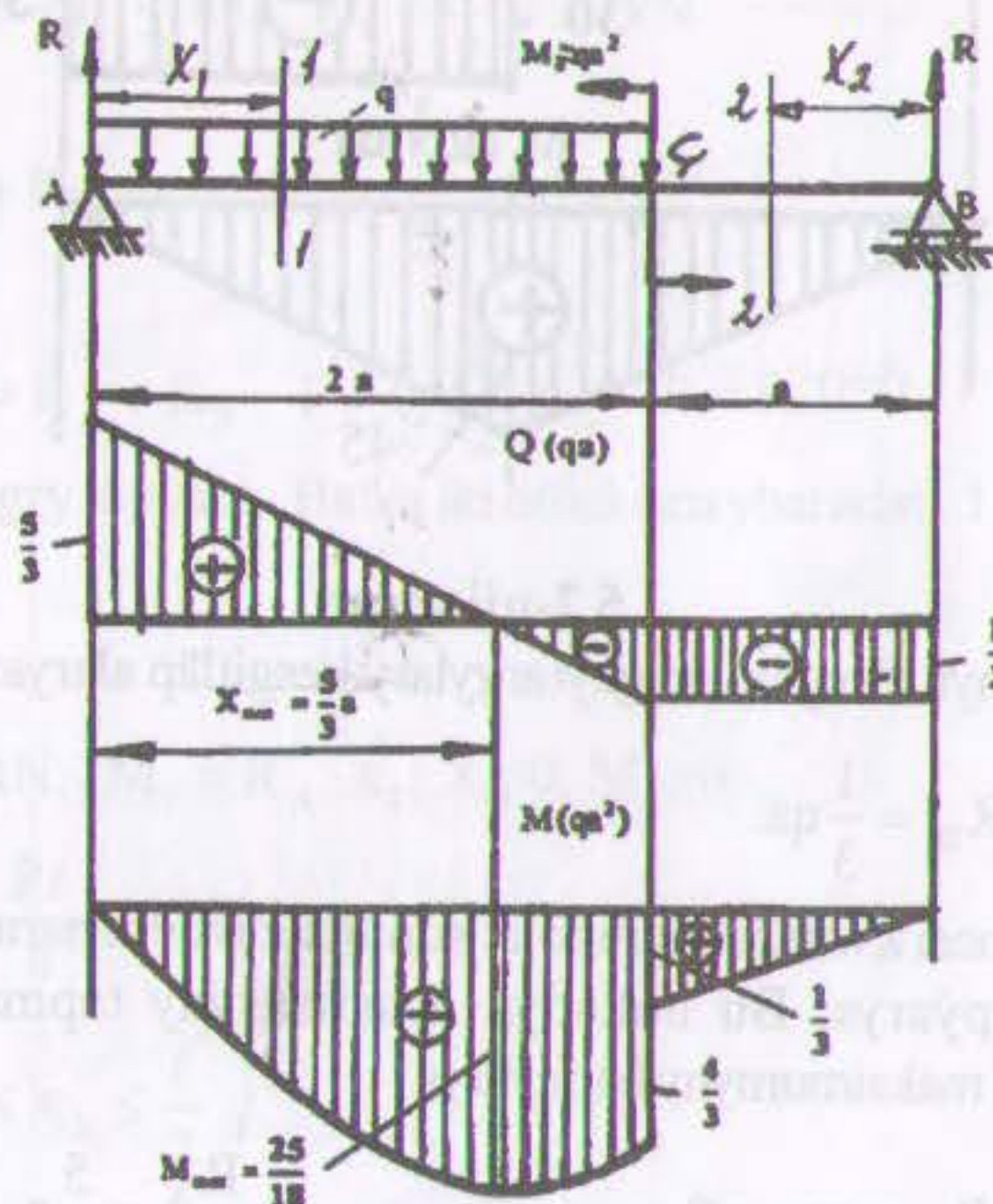
II bölek üçin

$$0 \leq x_2 \leq a, \quad Q_2 = -R_B = -\frac{1}{3}qa, \quad M_2 = R_B \cdot x_2,$$

Eger $x_2=0$, $M_B=0$,

$$\text{Eger } x_2=a, \quad M_C=R_B \cdot a = \frac{qa^2}{3},$$

Q we M epýurlary suratda görkezilen.



5.3-nji surat

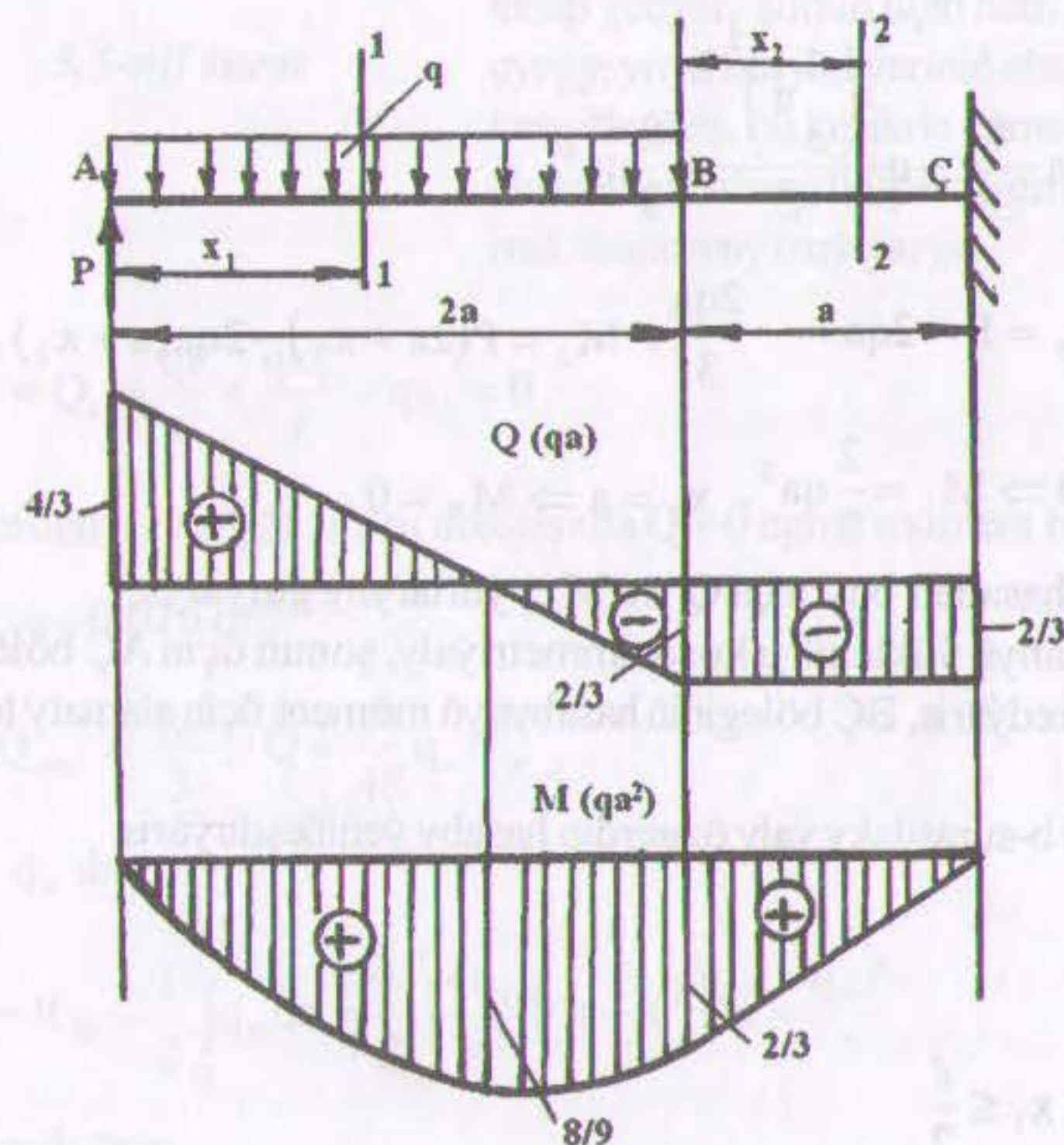
Epýurlardan görünýär Q we M absolýut maksimal bahalary:

$$Q_{\max} = \frac{5}{3}ga, \quad M_{\max} = \frac{25}{18}qa^2$$

$$5.4. \text{ a) } P = \frac{q\ell}{2}; \text{ b) } P = \frac{4}{3}qa; \text{ c) } P = \frac{4}{9}qa; \text{ d) } P = \frac{2}{3}qa.$$

Meseläniň şertine görä $M_C = P \cdot 3a - q \cdot 2a \cdot 2a = 0$.

Bu ýerden $P = \frac{4}{3}qa$ we Q, M epýuryny gurýarys.



5.4-nji surat

I bölek: $Q_1 = P - qx_1$, $0 \leq x_1 \leq 2a$ $M_1 = Px_1 - q \frac{x_1^2}{2}$;

Eger $x_1 = 0 \Rightarrow Q_A = P = \frac{4}{3}qa$, $M_A = 0$

$x_1 = 2a \Rightarrow Q_B = \frac{2}{3}qa$, $M_B = \frac{2}{3}qa^2$

M_1 maksimumyny tapýarys.

$$\frac{dM_1}{dx_1} = P - qx_1 = 0 \Rightarrow x_{\max} = \frac{4}{3}a$$

$$M_{\max} = \frac{4}{3}qa \cdot \frac{4}{3}a - q \cdot \frac{\left(\frac{4}{3}a\right)^2}{2} = \frac{8}{9}qa^2$$

II bölek: $Q_2 = P - 2qa = -\frac{2qa}{3}$, $M_2 = P(2a + x_2) - 2qa(a + x_2)$

Eger $x_2 = 0 \Rightarrow M_2 = \frac{2}{3}qa^2$, $x_2 = a \Rightarrow M_B = 0$.

Ýokardaky hasaplar boýunça Q we M epýurlaryny gurýarys.

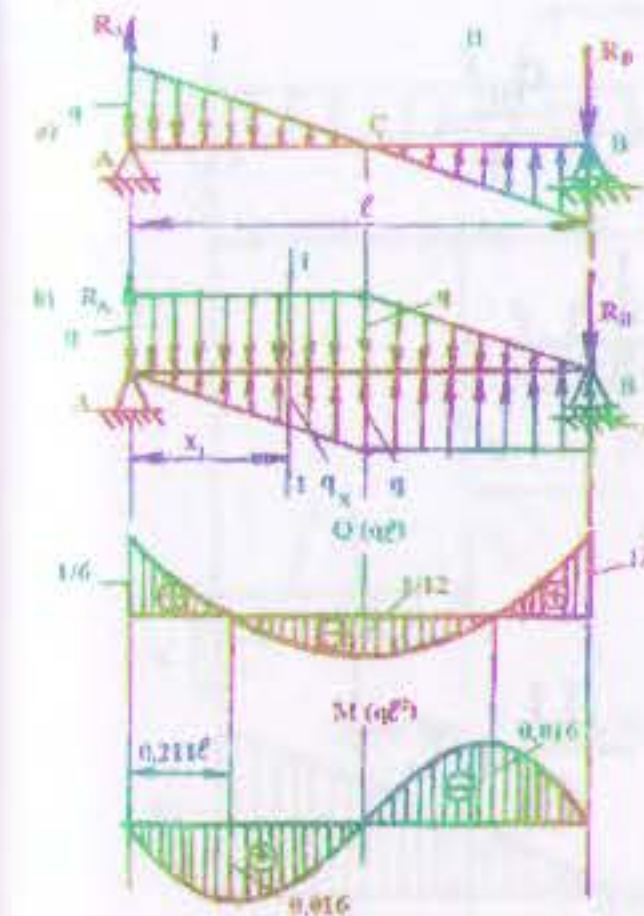
5.5. e) Balkanyň ýüklenilişi kososimetriýaly, şonuň üçin AÇ böleginiň hasabyna seredýäris, BÇ böleginiň hasabynyň moment üçin alamaty tersine bolýar.

Berlen güýji b-suratdaky ýaly özgerdip hasaby ýenilleşdirýäris.

$$q_x = q \frac{2x}{\ell}$$

I bölek: $0 \leq x_1 \leq \frac{\ell}{2}$

$$Q_1 = R_A + q \cdot \frac{x_1}{\ell} \cdot \frac{x_1}{2} - qx_1 = \frac{q\ell}{6} + \frac{qx_1^2}{\ell} - qx_1$$



5.5-nji surat

$$M_1 = \frac{q\ell}{6} \cdot x_1 + \frac{qx_1^3}{3\ell} - q \frac{x_1^2}{2}$$

Eger $x_1 = 0 \Rightarrow Q_A = \frac{q\ell}{6}$, $M_A = 0$

$$x_1 = \frac{\ell}{2} \Rightarrow Q_C = \frac{q\ell}{6} + \frac{q\ell}{4} - q \frac{\ell}{2} = -\frac{1}{12}q\ell$$

$$M_C = \frac{q\ell}{6} \cdot \frac{\ell}{2} + \frac{q\ell^3}{24\ell} - \frac{q\ell^2}{8} = 0$$

Kese güýjüň epýury, epýuryň bazasyny kesip geçýär, şonuň üçin hem epýuryň çyzgysynyň kesýän ýeriniň absissasyny kesgitleýäris, bu kesikde egme momentiniň ekstremal bahasy bolýar. Egme momentiniň maksimumyny barlaýarys:

$$\frac{dM_1}{dx_1} = Q_1 = \frac{q\ell}{6} + \frac{qx_1^2}{\ell} - qx_1 = 0.$$

Bu ýerden $x_1 = 0,211\ell$, şu absissada $Q_1 = 0$ egme moment bolsa,

$$M_{\max} = -0,016 q\ell^2$$

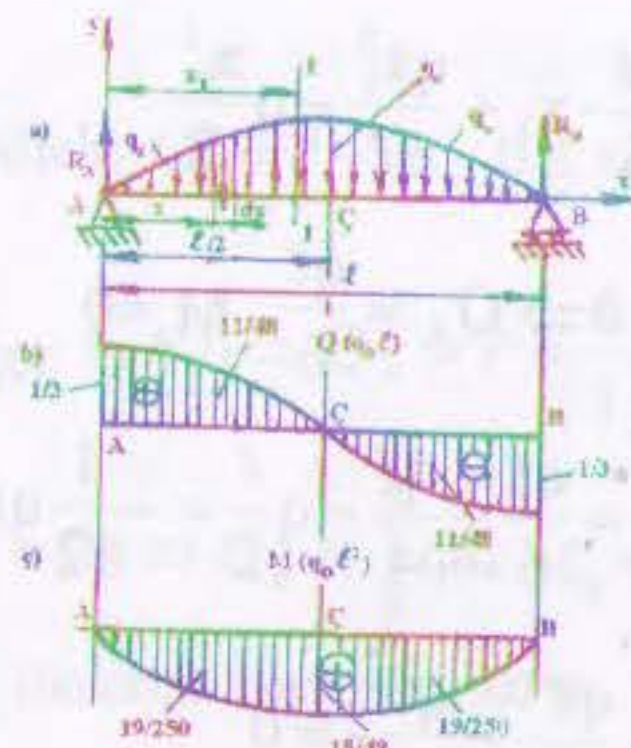
$$\mathbf{5.6.} \quad Q_{\max} = \frac{q_0\ell}{3}; \quad Q = \frac{5}{48}q_0\ell^2.$$

$$d\omega = q_x dx$$

$$R_A = R_B = \frac{1}{2} \int_0^{\ell} q_x dx = \frac{1}{2} \int_0^{\ell} \frac{4q_0}{\ell^2} (\ell x - x^2) dx = \frac{q_0\ell}{3}$$

1-1 kesik üçin

$$Q_x = \frac{q_0\ell}{3} - \int_0^x \frac{4q_0}{\ell^2} (\ell x - x^2) dx = \frac{q_0\ell}{3} - \frac{4q_0}{\ell^2} \left(\frac{\ell x^2}{2} - \frac{x^3}{3} \right)$$



5.6-njy surat

$$\text{Eger } x = 0 \Rightarrow Q_A = \frac{q_0 l}{3},$$

$$x = \frac{l}{4} \Rightarrow Q_{\frac{l}{4}} = \frac{11}{48} q_0 l,$$

$$x = \frac{l}{2} \Rightarrow Q_C = 0$$

$$x = \frac{3l}{4} \Rightarrow Q_{\frac{3l}{4}} = -\frac{11}{48} q_0 l,$$

$$x = l \Rightarrow Q_B = -\frac{q_0 l}{3}.$$

Q_x epýury b suratda görkezilen.

M_x aňlatmasyny ýazmak üçin balkany çep diregden x_1 aralykda kesýäris we 1-1 kesik üçin egme momentiň deňlemesini düzýäris.

$$M_{x_1} = \frac{q_0 l}{3} x_1 - \int_0^{x_1} \frac{4q_0}{l^2} (lx - x^2) dx \cdot (x_1 - x) = \frac{q_0 l}{3} x_1 - \frac{q_0}{3l^2} (2lx_1^3 - x_1^4)$$

$$\text{Eger: } x_1 = 0 \Rightarrow M_A = 0, \quad x_1 = \frac{l}{4} \Rightarrow M_{\frac{l}{4}} = \frac{19}{256} q_0 l^2,$$

$$x_1 = \frac{l}{2} \Rightarrow M_C = \frac{5}{48} q_0 l^2, \quad x_1 = \frac{3}{4} l \Rightarrow M_{\frac{3l}{4}} = \frac{19}{256} q_0 l^2$$

$$x_1 = l \Rightarrow M_B = 0$$

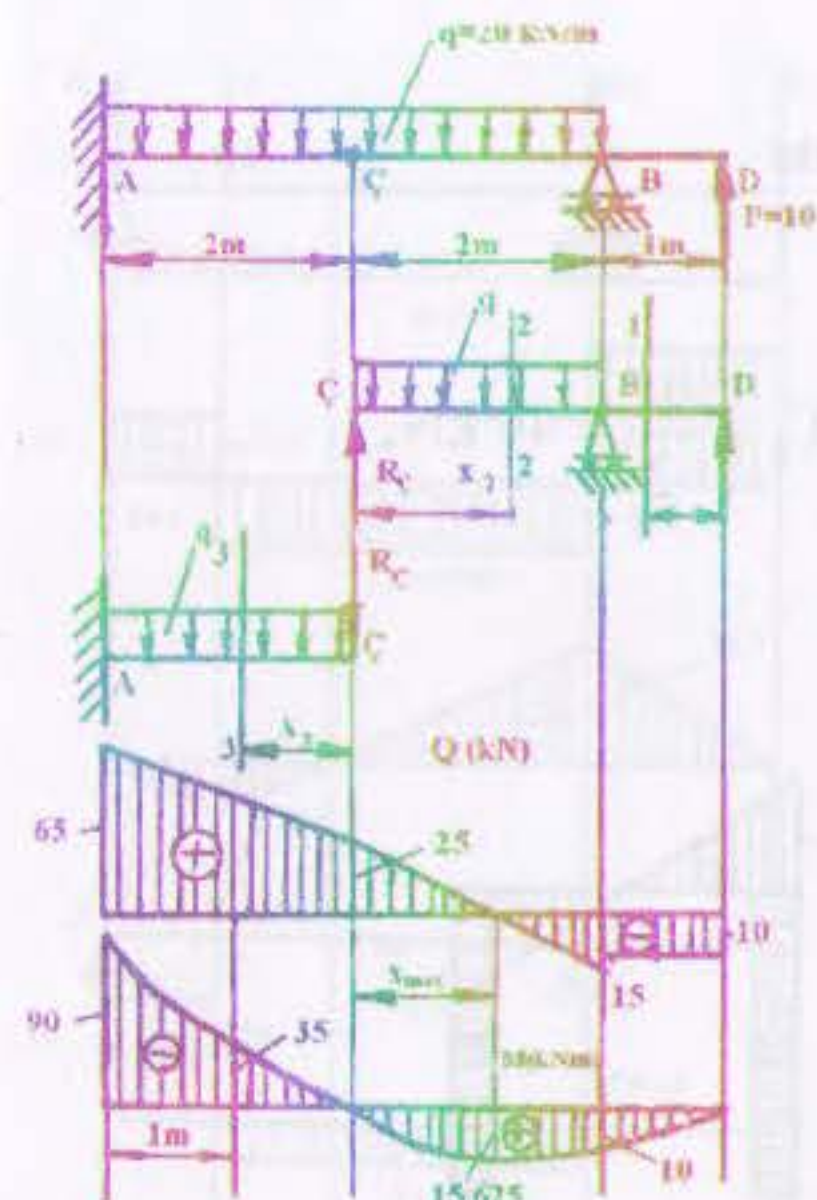
5.7. a) $M=80 \text{ kN m}$; $Q=20 \text{ kN}$; b) $M=-90 \text{ kN m}$; $Q=65 \text{ kN}$;

d) $M=-20 \text{ kN m}$; $Q=30 \text{ kN}$; g) $M=70 \text{ kN m}$; $Q=-66,2 \text{ kN}$.

b) B nokada görä sag balka täsir edýän güýçlerden momentiň deňlemesini düzýäris.

$$\sum M_B = P \cdot 1 + q \cdot \frac{2^2}{2} - R_C \cdot 2 = 0,$$

$$R_C = 25 \text{ kN}$$



5.7-nji surat

Ýokarky balkanyň hasaby

1-1 kesik üçin $0 \leq x_1 \leq 1 \text{ m}$.

$$Q_1 = -P = 10 \text{ kN}$$

$$M_1 = P x_1, \quad x_1 = 0 \Rightarrow M_D = 0$$

$$x_1 = 1 \text{ m} \Rightarrow M_B = 10 \text{ kN m}$$

2-2 kesik üçin $0 \leq x_2 \leq 2 \text{ m}$.

$$Q_2 = R_C - q x_2$$

$$M_2 = R_C \cdot x_2 - q \frac{x_2^2}{2}$$

$$x_2 = 0 \Rightarrow Q_C = R_C = 25 \text{ kN},$$

$$M_C = 0$$

$$x_2 = 2 \text{ m}; \quad Q_B = -15 \text{ kN}, \quad M_B = 10 \text{ kN m}$$

M_2 maksimumyny barlaýarys.

$$\frac{dM_2}{dx_2} = Q_2 = R_C - q x_2 =$$

$$= 0 \Rightarrow x_{\max} = x_2 = \frac{R_C}{q} = 1,25 \text{ m}$$

$$\text{onda } M_{\max} = R_C x_{\max} - q \frac{x_{\max}^2}{2} = 15,625 \text{ kN} \cdot \text{m}$$

Esasy balkanyň hasaby

3-3 kesik üçin $0 \leq x_2 \leq 2 \text{ m}$

$$Q_C = R_C + q x_2, \quad M_B = -R_C x_3 - q \frac{x_3^2}{2}$$

$$x_2 = 0 \Rightarrow Q_C = R_C = 25 \text{ kN}, \quad M_C = 0$$

$$x_2 = 2 \text{ m} \Rightarrow Q_A = R_C + q \cdot 2 = 25 + 40 = 65 \text{ kN}$$

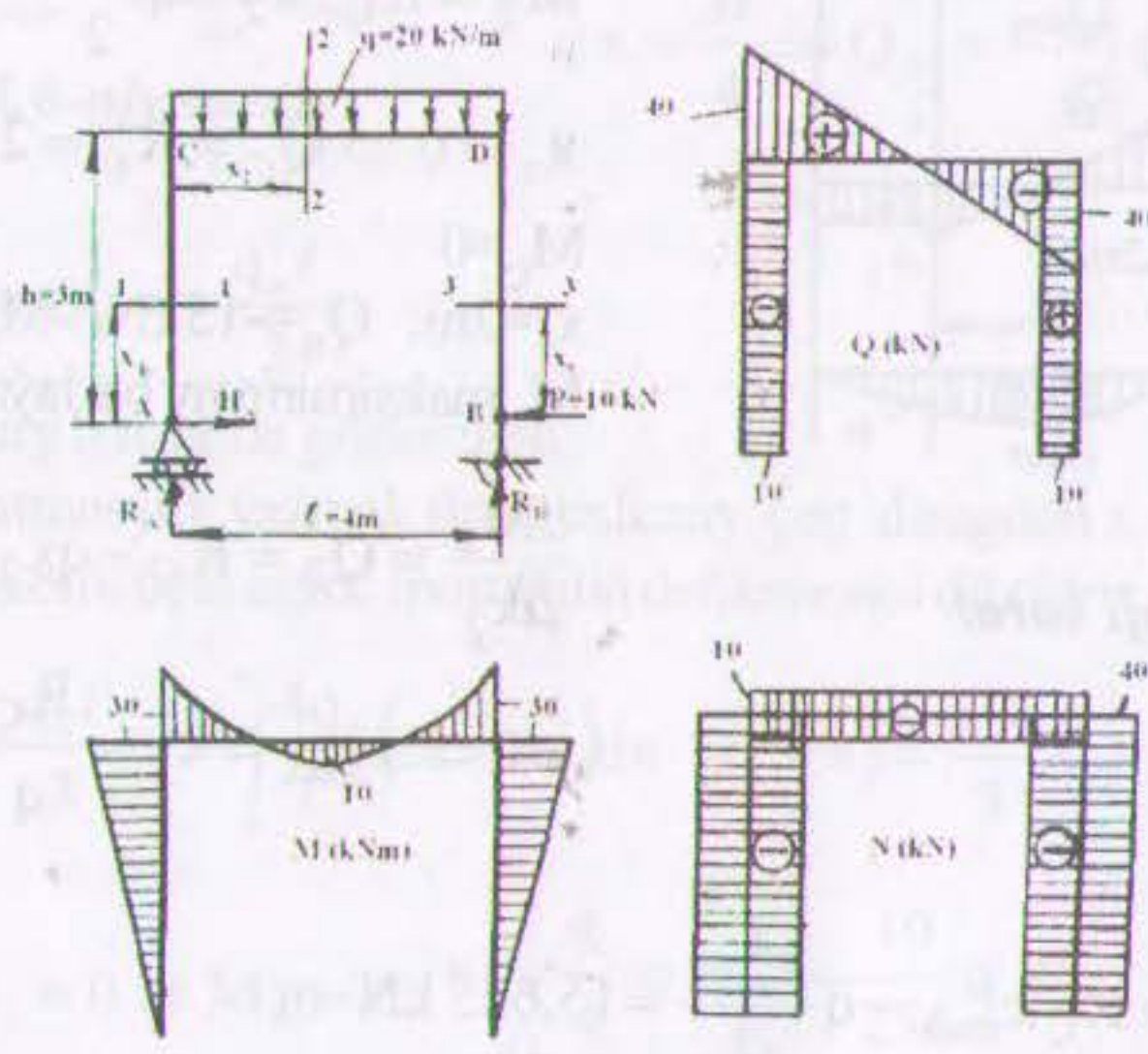
$$M_A = -25 \cdot 2 - 20 \cdot \frac{2^2}{2} = 90 \text{ kN m}$$

$$x_2 = 1 \text{ m}, M_3 = -25 \cdot 1 - 20 \cdot \frac{1^2}{2} = 35 \text{ kN m}.$$

Q we M epýurlary suratda görkezilen.

5.8. a) statikanyň deňlemesinden $R_A = R_B = \frac{q\ell}{2} = 40 \text{ kN}$,

$$H_A = P = 10 \text{ kN}, q = 20 \text{ kN/m}.$$



5.8-nji surat

AÇ direk $Q_{AC} = -H_A = -10 \text{ kN}$, $M_1 = -H_A x_1$,

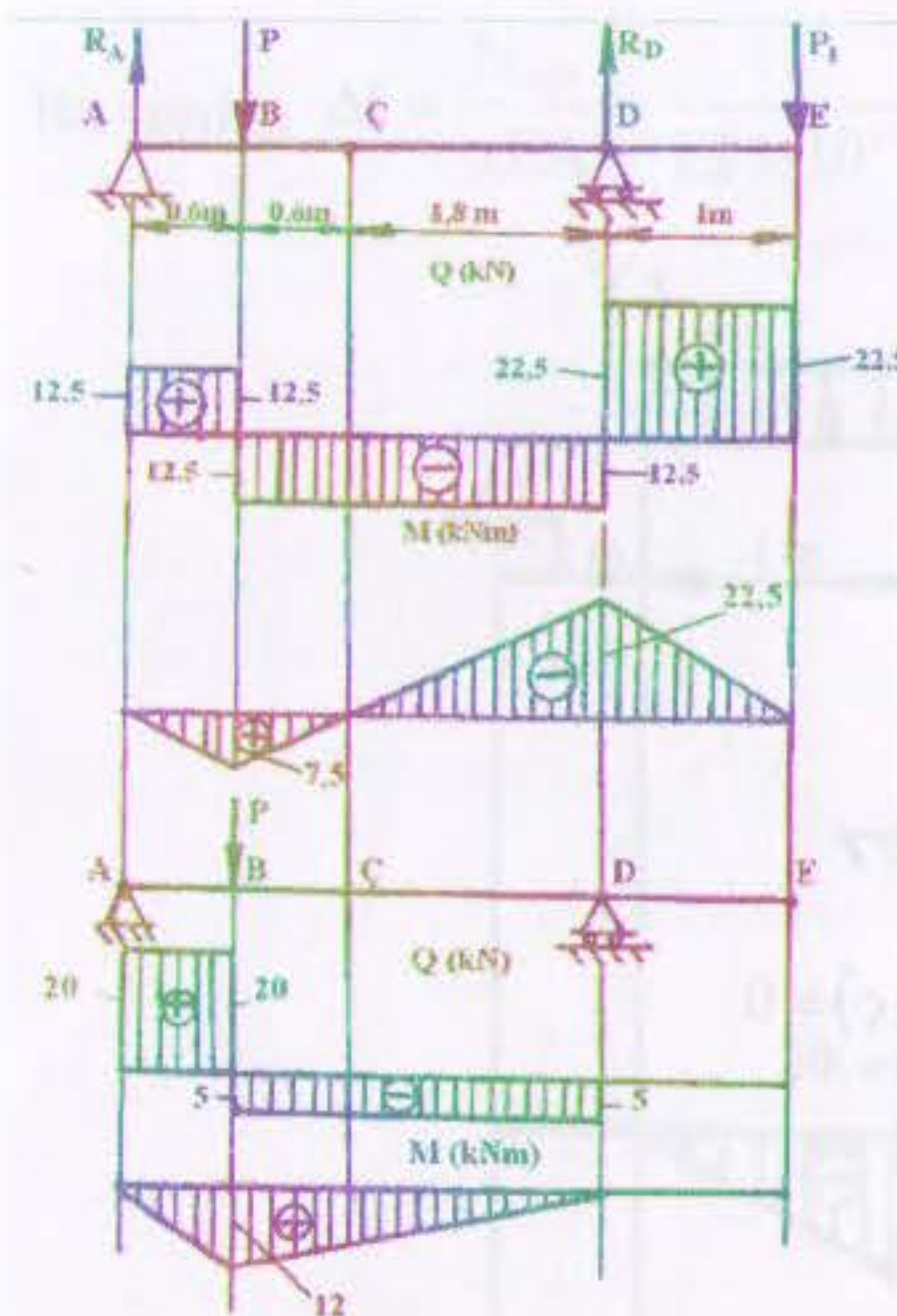
$$N_{AC} = -R_A = -40 \text{ kN}$$

ÇD rigel $Q_2 = R_A - qx_2$, $M_2 = R_A x_2 - q \frac{x_2^2}{2}$,

$$N_{CD} = -H_A = -10 \text{ kN}$$

BD direk $Q_{BD} = P = 10 \text{ kN}$, $M_3 = -P x_3$, $N_{BD} = -R_B = -40 \text{ kN}$

Q, M, N epýurlary suratda görkezilen.



5.9-nji surat

5.9. $P_1 = 22,5 \text{ kN}$. Statikanyň deňlemesinden

$$R_A = \frac{4}{5} \cdot P - \frac{P_1}{3}.$$

Onda

$$M_C = R_A \cdot 1,2 - P \cdot 0,6 =$$

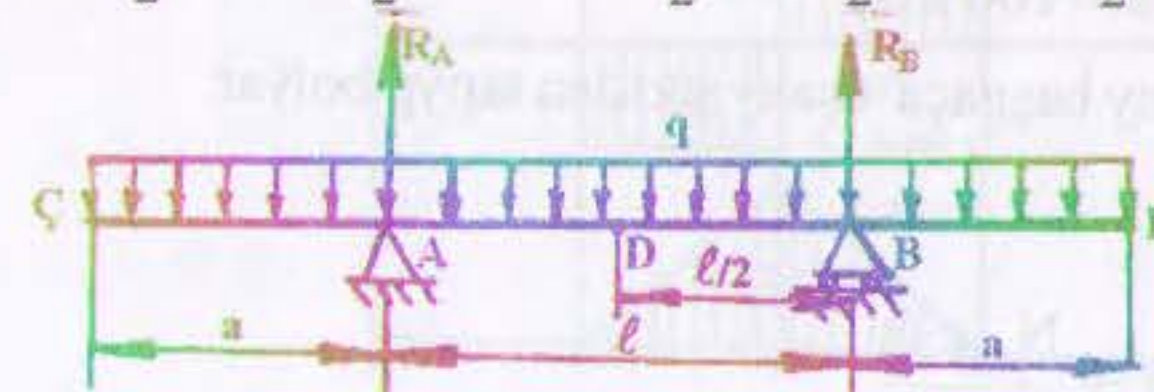
$$= \left(\frac{4P}{5} - \frac{P_1}{3} \right) \cdot 1,2 - P \cdot 0,6 = 0$$

Bu ýerden $P_1 = 22,5 \text{ kN}$
Q we M epýurlary, E
noktdaky güýjüň ululygy
hasaba alnyp we hasaba
almazdan suratda görkezilen.

5.10. $a = \frac{\ell}{2}$; $a = \frac{\sqrt{2}\ell}{4}$.

1) $R_A = R_B = \frac{q(\ell + 2a)}{2}$,

$$M_D = R_A \cdot \frac{\ell}{2} - q \frac{\left(a + \frac{\ell}{2}\right)^2}{2} = \frac{q(1 + 2a)}{2} \cdot \frac{\ell}{2} - q \frac{\left(a + \frac{\ell}{2}\right)^2}{2} = 0$$



5.10-nji surat

Bu ýerden $a = \frac{\ell}{2}$

$$2) M_A = M_D \Rightarrow q \frac{a^2}{2} = \frac{q(\ell + 2a)}{2} \cdot \frac{\ell}{2} - q \frac{\left(a + \frac{\ell}{2}\right)^2}{2}$$

Bu ýerden $a = \frac{\sqrt{2}\ell}{4}$

$$5.11. x = \frac{\ell}{2} - \frac{\zeta}{4}$$

$$\sum M_B = R_A \ell - P(\ell - x) - P(\ell - x - \zeta) = 0$$

$$R_A = 2P - 2P \frac{x}{\ell} - P \frac{\zeta}{\ell}$$

$$M_x = R_A x = 2Px - 2P \frac{x^2}{\ell} - P \frac{\zeta}{\ell} x$$

$$\frac{dM_x}{dx} = 2P - 2P \frac{x}{\ell} - P \frac{\zeta}{\ell} = 0$$

Bu ýerden $x = \frac{\ell}{2} - \frac{\zeta}{4}$

$$5.12. \Delta t = 16^\circ \text{S}$$

Meseläniň şertine görä $R_A = R_B = 0$, onda ÇA steržene düşýän güýç hemme ýüki kabul edýär.

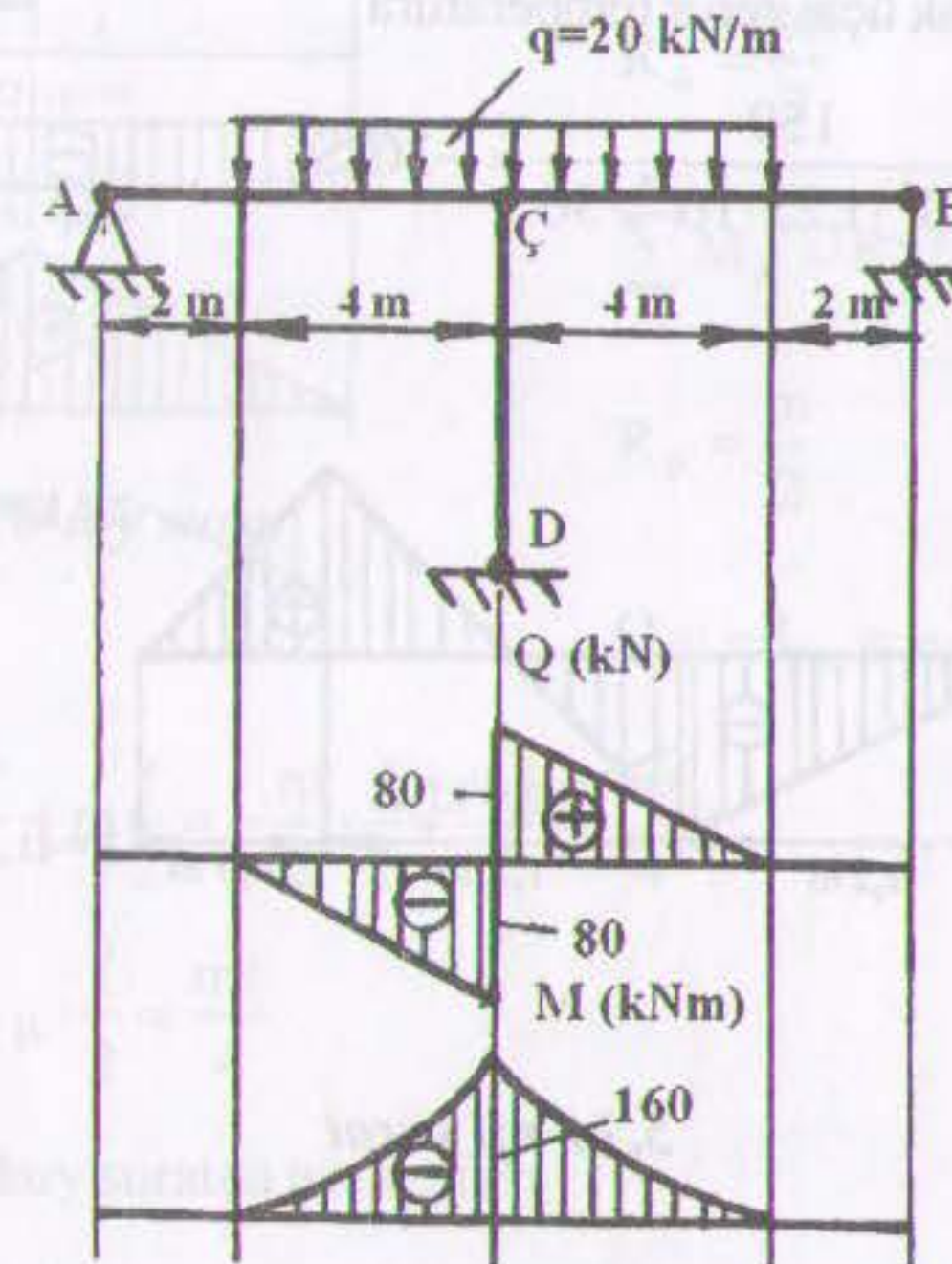
$$N_{CD} = q \cdot 8 = 20 \cdot 8 = 160 \text{ kN}$$

Bu güýjüň ululygyny başgaça aşaky şertden tapyp bolýar.

$$\Delta \ell_t = \Delta \ell_{N_{CD}}$$

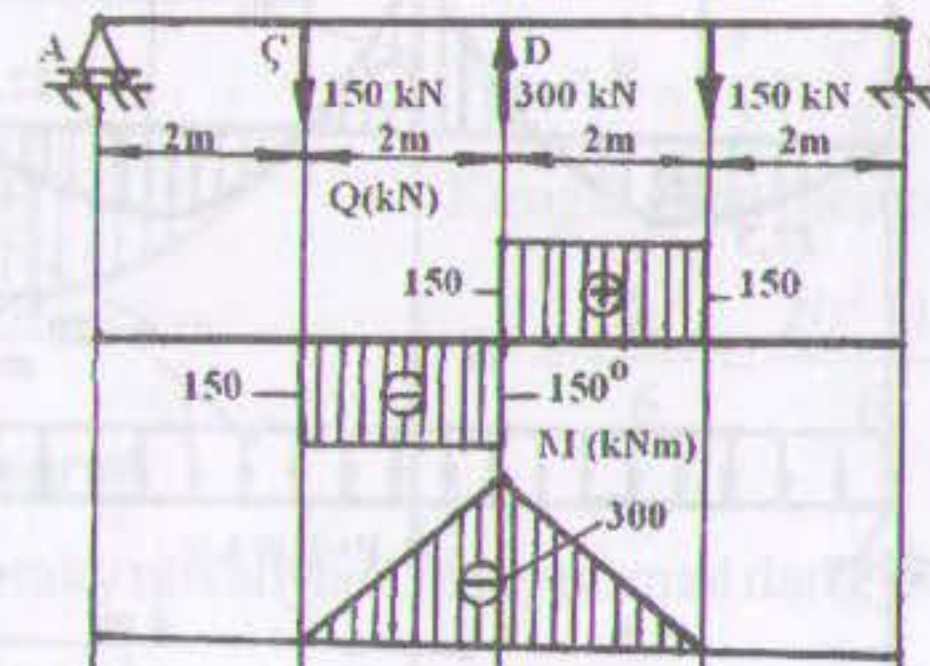
$$\text{Ýa-da } \alpha \cdot \ell_{CD} \cdot \Delta t = \frac{N_{CD} \cdot h}{EA}$$

$$\text{Bu ýerden } \Delta t = \frac{N_{CD}}{\alpha EA} = \frac{160}{1,25 \cdot 10^{-5} \cdot 2 \cdot 10^4 \cdot 40} = 16^\circ \text{S}$$



5.12-nji surat

$$5.13. \Delta t = -20^\circ \text{S}$$



5.13-nji surat

Her direge düşýän güýç

$$N_{CC_1} = N_{DD_1} = 150 \text{ kN}$$

Diregleri sowatmak üçin zerur temperatura

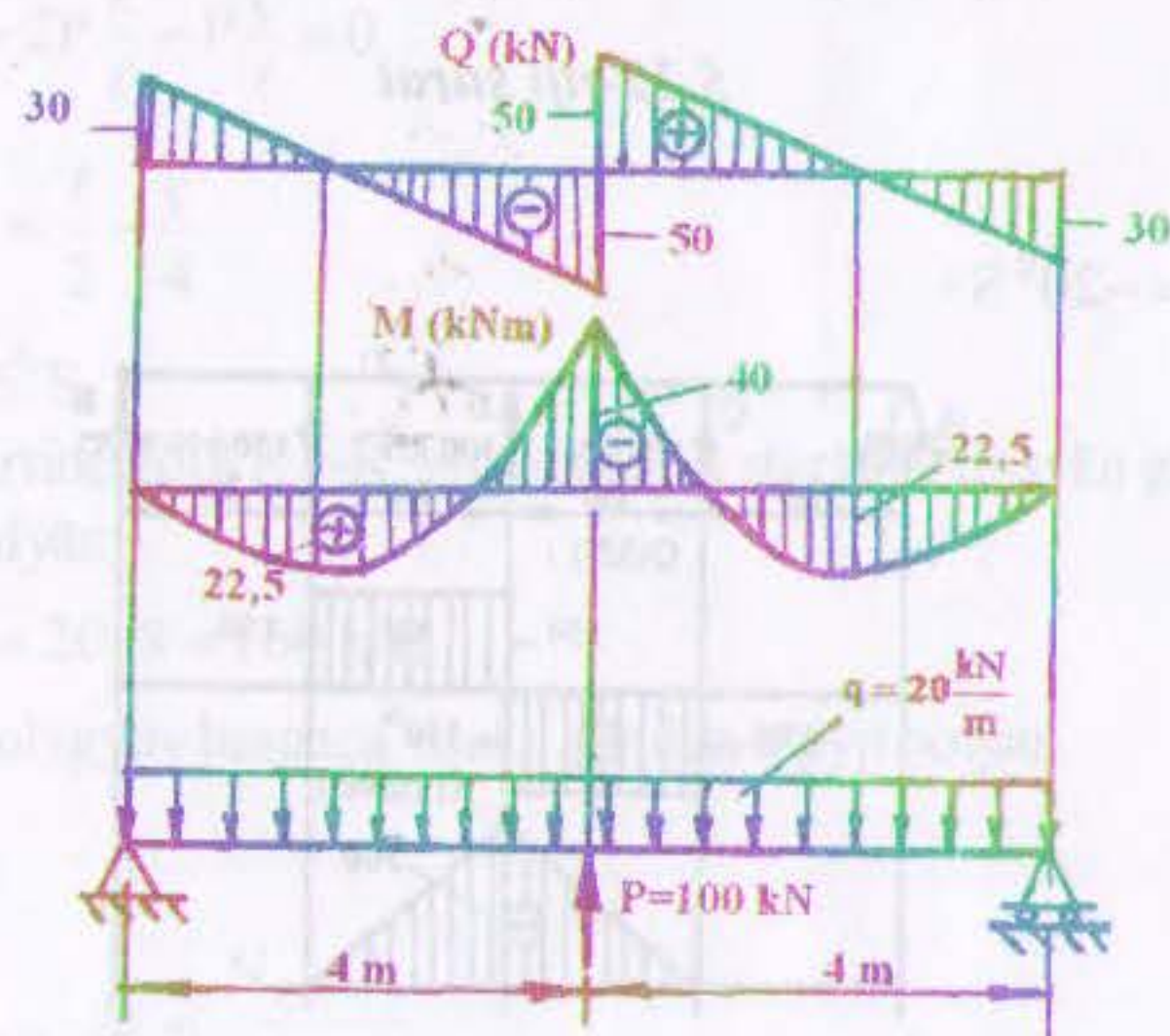
$$\Delta t = \frac{N_{CC_1}}{E\alpha A} = \frac{150}{2 \cdot 10^4 \cdot 1,25 \cdot 10^{-5} \cdot 30} = -20^\circ \text{S.}$$

5.14.

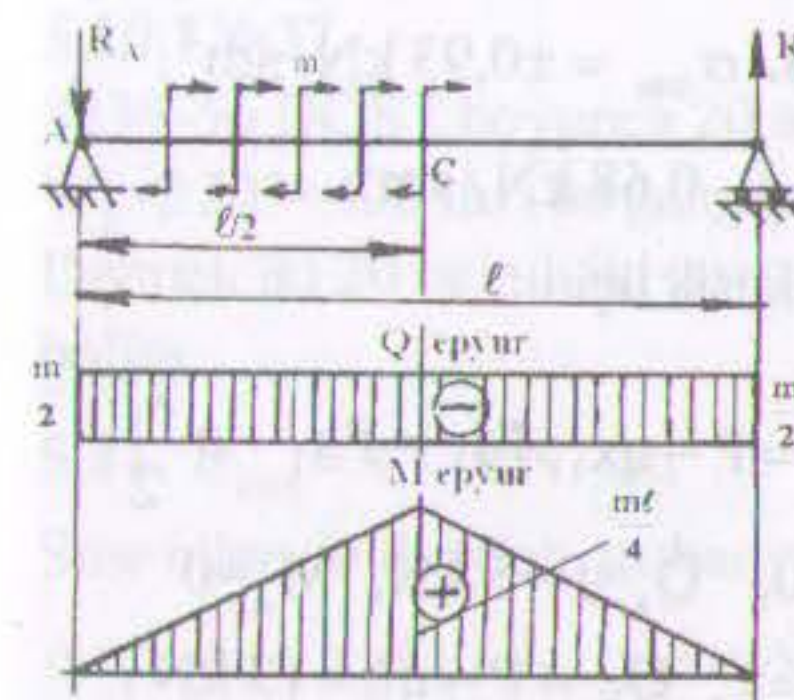


5.14-nji surat

5.15. ç)



5.15-nji surat



5.16-nji surat

$$5.16. \sum M_B = R_A \cdot l - \frac{m \cdot l}{2} = 0,$$

$$R_A = \frac{m}{2}$$

$$\sum M_A = R_B \cdot l - \frac{m \cdot l}{2} = 0,$$

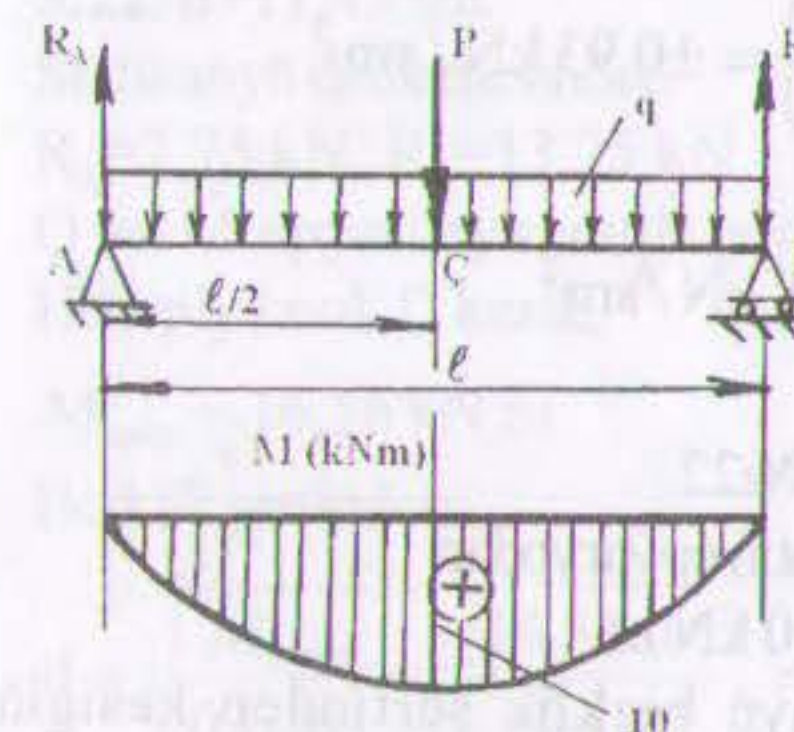
$$R_B = \frac{m}{2}$$

$$Q = -R_A = -\frac{m}{2}$$

$$M_C = -R_A \cdot \frac{l}{2} + m \cdot \frac{l}{2} = -\frac{m}{2} \cdot \frac{l}{2} + \frac{m \cdot l}{2} = \frac{m \cdot l}{4}$$

$$\text{ýa-da } M_C = R_B \cdot \frac{l}{2} = \frac{m \cdot l}{4}$$

Q we M epýurlary suratda görkezilen



5.17-nji surat

Howply kesigiň gyraky nokadynda iň uly normal dartgynlylyk

$$\sigma_{\max} = \frac{M_{\max}}{W} = \frac{10 \cdot 10^2}{800} = 1,25 \text{ kN/sm}^2$$

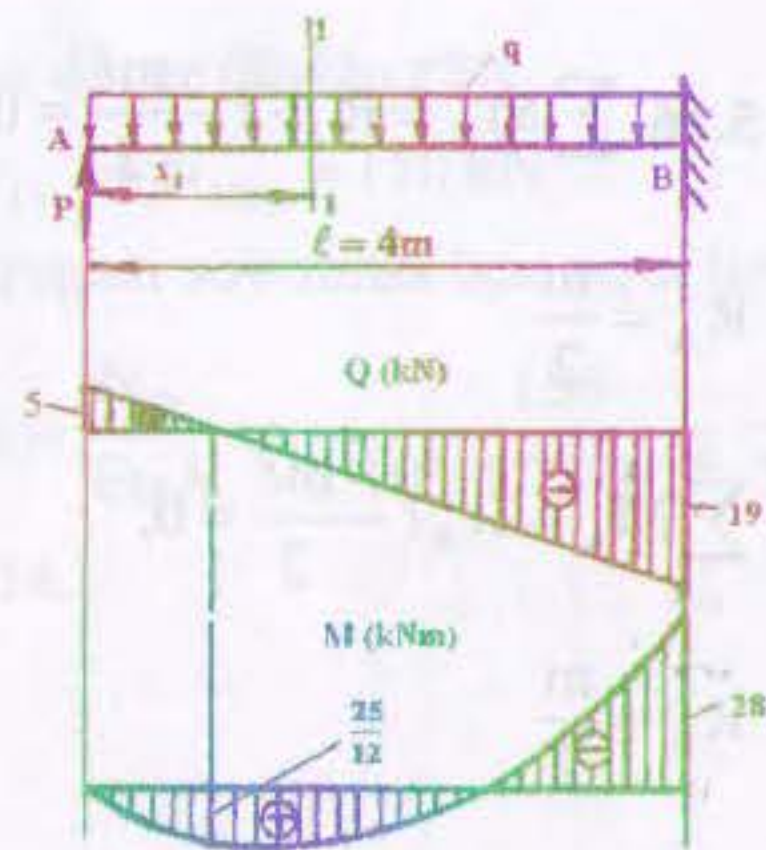
$$5.17. \sigma_{\max} = 1,25 \text{ kN/sm}^2.$$

$$R_A = R_B = \frac{P}{2} + \frac{q \cdot l}{2} = 9 \text{ kN}$$

$$M_C = R_A \cdot \frac{l}{2} - \frac{q \cdot l^2}{8} = 18 - 8 = 10 \text{ kNm}$$

Kesigiň garşylyk momenti

$$W = \frac{bh^2}{6} = \frac{20^2 \cdot 12}{6} = 800 \text{ sm}^3$$



5.18-nji surat

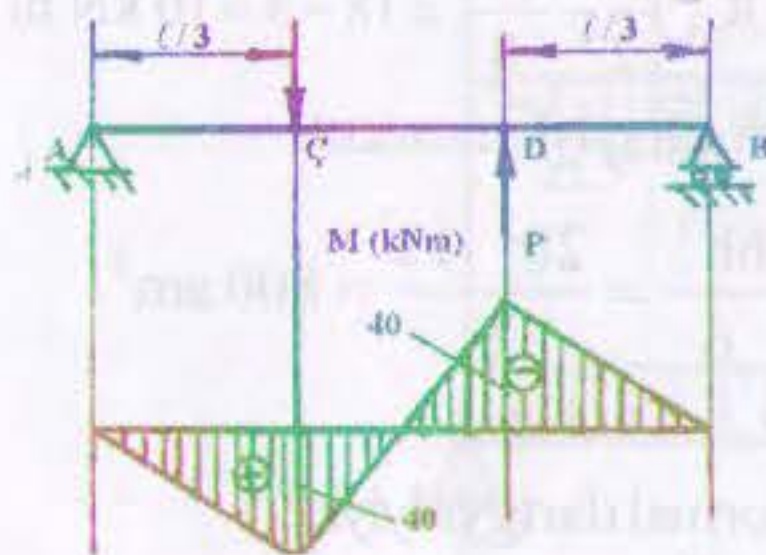
$$\frac{dM_1}{dx_1} = P - qx_1 = 0, \quad x_1 = x_{\max} = \frac{5}{6} \text{ m}$$

$$M_{\max} = P \cdot \frac{5}{6} - q \cdot \frac{5^2}{6^2 \cdot 2} = \frac{25}{12} \text{ kN m}$$

Howply kesigi we $M_B = -28 \text{ kN m}$

$$\sigma_{\max} = \frac{M_B}{I_z} \cdot y_{\max} = \frac{12 \cdot M_B}{bh^3} \left(\pm \frac{h}{2} \right) = \pm 0,93 \text{ kN / sm}^2$$

$$\sigma_c = \frac{M_B}{I_z} \cdot y_c = \frac{12 \cdot M_B}{bh^3} (-y_c) = -0,68 \text{ kN / sm}^2$$



5.19-njy surat

$$5.18. \sigma_{\max} = \pm 0,93 \text{ kN / sm}^2,$$

$$\sigma_c = -0,68 \text{ kN / sm}^2,$$

1-1 kesik üçin

$$Q_1 = P - qx_1, \quad M_1 = Px_1 - q \frac{x_1^2}{2}$$

$$x_1 = 0, \quad Q_A = P = 5 \text{ kN}, \quad M_A = 0$$

$$x_1 = \ell, \quad Q_B = P - q\ell = 19 \text{ kN},$$

$$M_B = P\ell - q \frac{\ell^2}{2} = -28 \text{ kN m}$$

5.19. I №22.

Momentin epýuryndan

$$M_{\max} = 40 \text{ kN m.}$$

Balkanyň berklik şertinden kesigiň garşylyk momenti

$$W_z = \frac{M_{\max}}{[\sigma]} = \frac{40 \cdot 10^2}{16} = 250 \text{ sm}^3.$$

Tablisadan I № 22 kabul edýäris.

5.20. I №27

8239-56 DÖST boýunça 20 a belgili iki iki tawranyň garşylyk momenti $W_z = 2 \cdot 203 = 406 \text{ sm}^3$, bu garşylyk moment 27a belgili ikitawra gabat gelyär. Diýmek iki 20 belgili iki tawrany bir 27a belgili iki tawra bilen çalşyryp bolýar.

$$5.21. \sigma_{\max} = 4,12 \text{ kN / sm}^2.$$

Suw bilen doldurylan turbanyň 1 m uzynlygyna getirilen hususy agramy $q = \gamma_1 A_1 + \gamma_2 A_2$; γ_1, γ_2 - çoýun turbanyň we suwuň udel agramlary, A_1, A_2 - turbanyň diwarynyň kese kesiginiň we suw bilen doldurylan meýdanlary. Iki direkli balkanyň endigan ýaýran q ýükden in uly egme momenti

$$M_{\max} = \frac{q\ell^2}{8}, \text{ onda}$$

$$\sigma_{\max} = \frac{q\ell^2}{8 \cdot W_z} = \frac{\gamma_1 \cdot 0,785 D^2 (1 - \alpha^2) + \gamma_2 \cdot 0,785 \cdot d^2}{8 \cdot 0,1 d^3 (1 - \alpha^4)} = 4,12 \frac{\text{kN}}{\text{sm}^2}.$$

Bu ýerde $d = D - 2t$, $\alpha = \frac{d}{D}$, t - turbanyň diwarynyň galyňlygy.

5.22. $d = 11,45 \text{ sm}$.

Statikanyň deňlemesinden

$$R_A = 7,75 \text{ kN}, \quad R_B = 13,25 \text{ kN.}$$

Q we M epýurlary suratda görkezilen
Howply kesik D kesik,

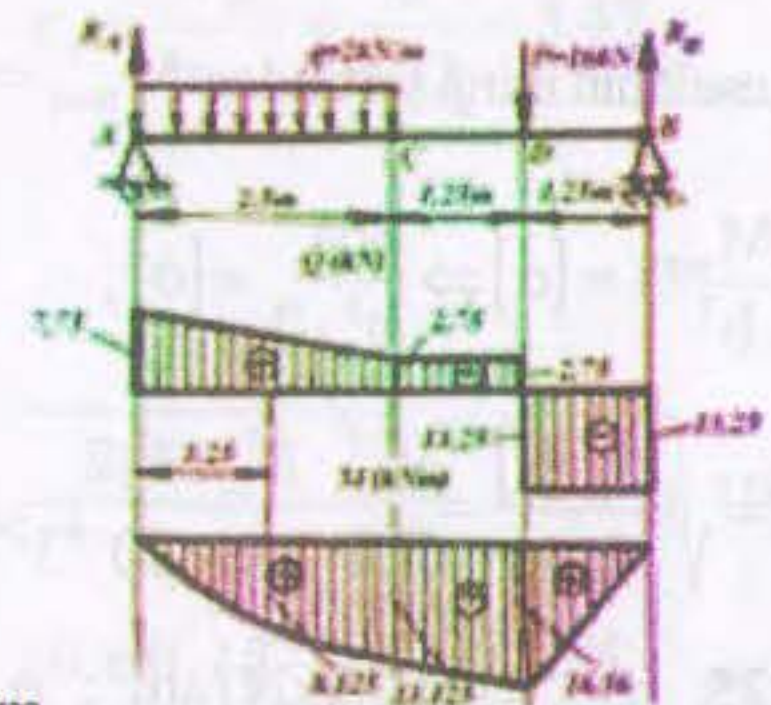
$$M_{\max} = 16,56 \text{ kN m}$$

Berklik şertinden

$$d = \sqrt[3]{\frac{M_{\max}}{0,1 \cdot [\sigma]}} = \sqrt[3]{\frac{16,56 \cdot 10^2}{0,1 \cdot 11}} = 11,45 \text{ sm}$$

5.23. $P_2 = 11,80 \text{ kN}$.

$$A_1 = A_2 \Rightarrow \frac{\pi d^2}{4} = b^2 \Rightarrow d = \frac{2b}{\sqrt{\pi}},$$



5.22-nji surat

$$W_1 = \frac{\pi d^3}{32} = \frac{\pi 8b^3}{32\pi\sqrt{\pi}} = \frac{b^3}{4\sqrt{\pi}}, \quad W_2 = \frac{b^3}{6},$$

$$\frac{M_2}{M_1} = \frac{W_2}{W_1} \Rightarrow \frac{P_2 \ell \cdot 4}{4 \cdot P_1 \ell} = \frac{W_2}{W_1} \Rightarrow \frac{P_2}{P_1} = \frac{b^3 \cdot 4\sqrt{\pi}}{6 \cdot b^3} = 1,18,$$

Bu ýerden kwadrat kesikli balkanyň howpsuz ýüki

$$P_2 = P_1 \cdot 1,18 = 11,80 \text{ kN m}.$$

5.24. 1) $\sigma_{\max} = 28,26 \text{ kN/sm}^2$; 2) $a = 4,22 \text{ m}$.

Meseläniň birinji şertinden $M_{\max} = \frac{q\ell^2}{8}$; $q = \gamma A$.

$$\begin{aligned} \text{Onda } \sigma_{\max} \frac{M_{\max}}{W_Z} &= \frac{\sigma \gamma A \ell^2}{8 \cdot b^3} = \frac{6\gamma b^2 \ell^2}{8b^3} = \frac{6\gamma \ell^2}{8b} = \\ &= \frac{6 \cdot 78,5 \cdot 10^{-6} \cdot 12^2 \cdot 10^4}{8 \cdot 3} = 28,26 \text{ kN/sm}^2. \end{aligned}$$

Meseläniň ikinji şertinden $M_{\max} = \frac{qa^2}{2}$.

$$\frac{6M_{\max}}{b^3} = [\sigma] \Rightarrow \frac{6qa^2}{b^3 \cdot 2} = [\sigma],$$

$$a = \sqrt{\frac{2b^3[\sigma]}{6\gamma A}} = \sqrt{\frac{3^3 \cdot 14 \cdot 2}{6 \cdot 78,5 \cdot 10^{-6} \cdot 3^2}} = 422 \text{ sm} = 4,22 \text{ m}.$$

5.25. $\sigma_{\max} = 0,576 \text{ kN/sm}^2$; $\sigma_{\min} = -1,73 \text{ kN/sm}^2$, $n_2 = 3,47$.

Balkanyň maksimal egme momenti

$$M_{\max} = \frac{P\ell}{4} = \frac{8 \cdot 3,6}{4} = 7,2 \text{ kN m}.$$

$$z_{\zeta} = \frac{75 \cdot 2,5 + 75 \cdot 7,5}{15 \cdot 5 + 15 \cdot 5} = 5 \text{ sm},$$

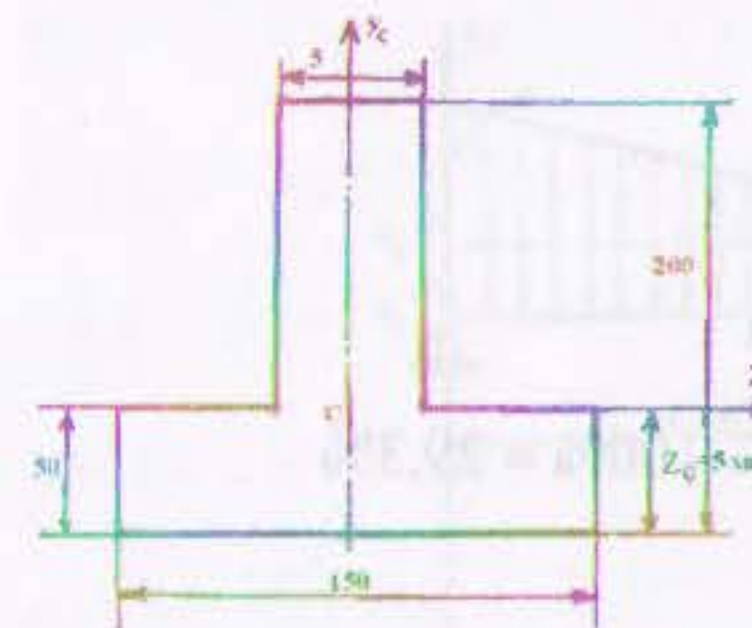
$$\begin{aligned} I_{z_{\zeta}} &= \frac{5^3 \cdot 15}{12} + 15 \cdot 5(-2,5^2) + \frac{15^3 \cdot 5}{12} + 15 \cdot 5 \cdot 7,5^2 = \\ &= 156,25 + 468,75 + 1406,25 + 4216,5 = 6247,75 \text{ sm}^4. \end{aligned}$$

Iň uly süýnme dartgynlyk

$$\sigma_{\max} = \frac{M_{\max}}{I_{z_{\zeta}}} \cdot y_1 = \frac{7,2 \cdot 10^2}{6247,75} \cdot 5 \cong 5,576 \text{ kN/sm}^2.$$

Iň uly gysylma dartgynlyk

$$\sigma_{\min} = \frac{M_{\max}}{I_{z_{\zeta}}} \cdot y_2 = \frac{7,2 \cdot 10^2}{6247,75} \cdot (-15) = -1,73 \text{ kN/sm}^2$$



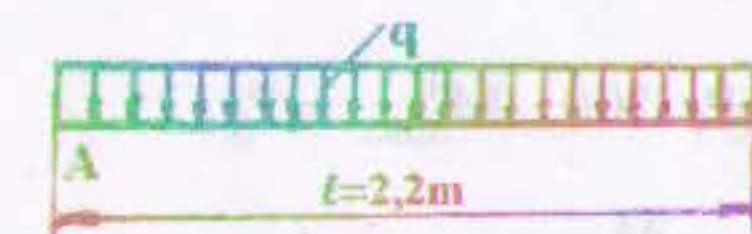
5.25-nji surat

Proporsionallyk çägendäki ätiýaçlyk koeffisiýentleri

$$n_1 = \frac{\sigma_{p\zeta}}{\sigma_{\max}} = \frac{3}{0,576} = 5,2,$$

$$n_2 = \frac{\sigma_{p\zeta}}{\sigma_{\min}} = \frac{6}{1,73} = 3,47$$

5.26.



5.26-njy surat

$$M_{\max} = \frac{q\ell^2}{2} = \frac{q \cdot 220^2}{2} = 2,42q \cdot 10^4$$

$$z_{\zeta} = \frac{20 \cdot 30 \cdot 15 - 15 \cdot 18 \cdot 12,5}{20 \cdot 30 - 15 \cdot 18} = 17 \text{ sm}$$

$$\begin{aligned} I_{z_{\zeta}} &= \frac{20 \cdot 30^3}{12} + 20 \cdot 30 \cdot (-2)^2 - \frac{18 \cdot 15^3}{12} - \\ &- 18 \cdot 15 \cdot (-4,5)^2 = 36870 \text{ sm}^4 \end{aligned}$$

Berklik şertinden
Süýnme

$$\frac{M_{\max}}{I_{z_{\varphi}}} \cdot y_1 = [\sigma]_s \Rightarrow q = \frac{[\sigma]_s \cdot I_{z_{\varphi}}}{10^4 \cdot 2,42 \cdot y_1} = \frac{1,2 \cdot 36870}{2,42 \cdot 13 \cdot 10^4} = 1,41 \frac{\text{kN}}{\text{sm}}$$

Gysylma

$$\frac{M_{\max}}{I_{z_{\varphi}}} \cdot y_2 = [\sigma]_g \Rightarrow q = \frac{[\sigma]_g \cdot I_{z_{\varphi}}}{2,42 \cdot 10^4 \cdot y_2} = \frac{5 \cdot 36870}{2,42 \cdot 10^4 \cdot 17} = 0,448 \frac{\text{kN}}{\text{sm}}$$

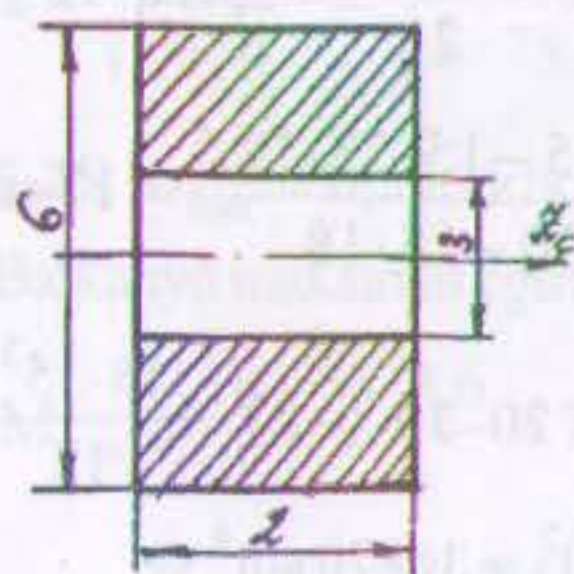
$$I_{z_1} = I_{z_2} = \frac{a^4}{12}; \quad y_1 = \frac{a}{\sqrt{2}}; \quad M_{\max_1} = M_{\max_2},$$

$$\sigma_1 = \frac{M_{\max_1}}{I_{z_1}} \cdot y_1, \quad \sigma_2 = \frac{M_{\max_2}}{I_{z_2}} \cdot y_2$$

$$\frac{\sigma_2 - \sigma_1}{\sigma_2} \cdot 100\% = \frac{y_2 \cdot y_1}{y_2} \cdot 100\% = \frac{\sqrt{2} - 2}{a} \cdot 100\% = 29,3\%$$

5.28. $P_1 = 1,47 \text{ kN}$, $P_2 = 5,88 \text{ kN}$.

$$I_{z_{\varphi}} = 2(I_Z + A \cdot y^2) = 2\left(\frac{2 \cdot 1,5^3}{12} + 2 \cdot 1,5 \cdot 2,25^2\right) = 31,5 \text{ sm}^4,$$



5.28-nji surat

$$M_{\max}^I = P_1 \cdot 100, \quad M_{\max}^{II} = P_2 \cdot 25,$$

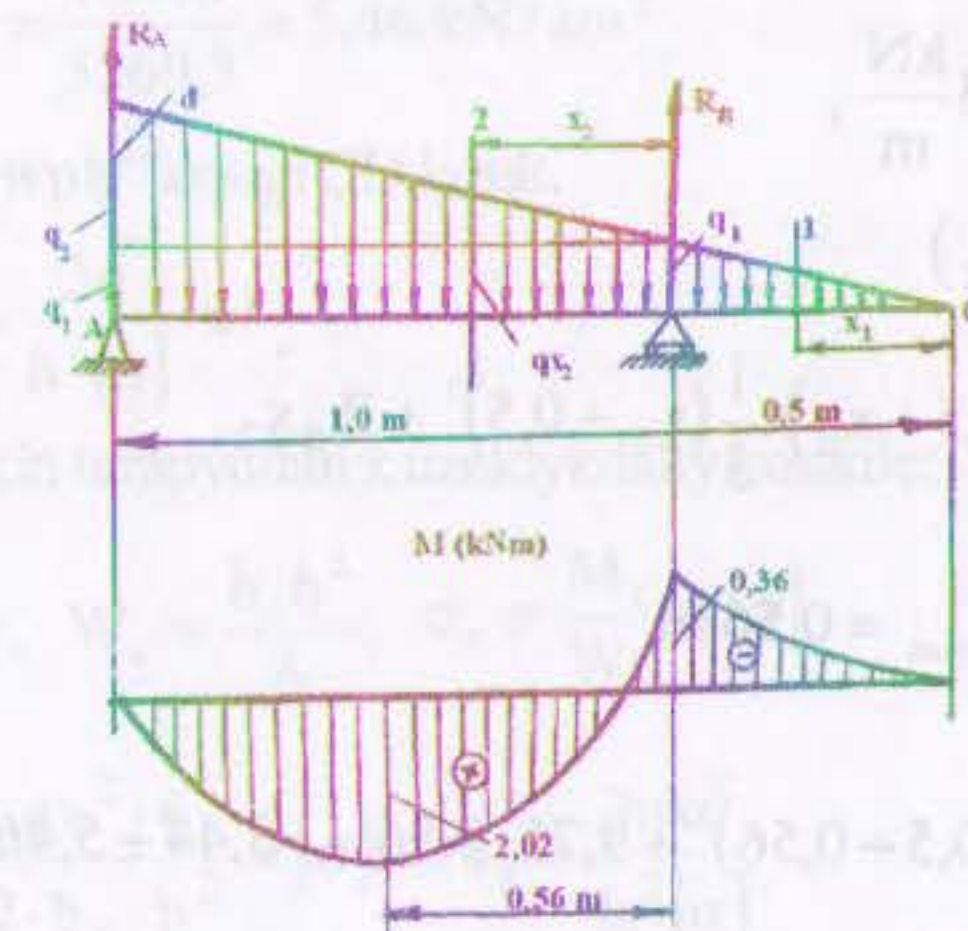
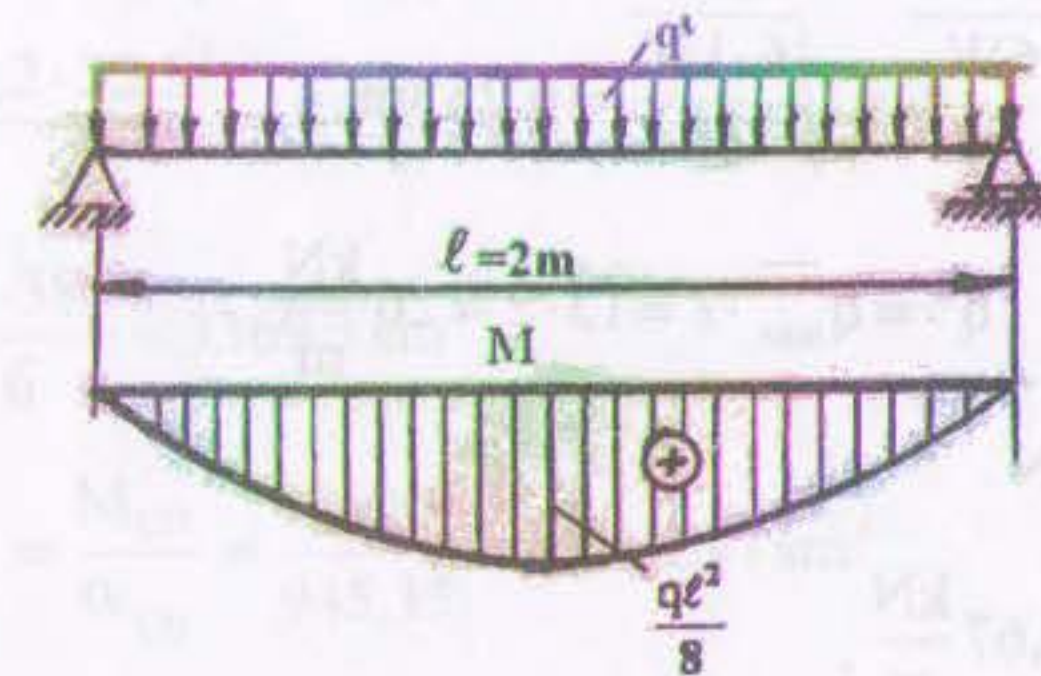
$$\sigma = \frac{M_{\max}}{I_{z_{\varphi}}} \cdot y \leq [\sigma].$$

$$\text{Onda } P_1 = \frac{I_{z_{\varphi}} \cdot [\sigma]}{y \cdot 100} = \frac{31,5 \cdot 14}{3 \cdot 100} = 1,47 \text{ kN},$$

$$P_2 = \frac{I_{z_{\varphi}} [\sigma]}{y \cdot 25} = \frac{31,5 \cdot 14}{3 \cdot 25} = 5,88 \text{ kN}.$$

5.29. Direg üçin $16 \times 16 \text{ sm}^2$, örtük üçin $t = 6,25 \text{ sm}$.

$$q^t = q_{\max} \cdot b = 0,0013 \cdot 20 = 0,026 \text{ kN/sm}.$$



5.29-njy mesele

Tagtanyň galyňlygyny kesgitleýäris:

$$M_{\max} = \frac{q^t \cdot l^2}{8} = \frac{0,026 \cdot 200^2}{8} = 130 \text{ kN} \cdot \text{sm}.$$

$$\text{Berklik şertinden } \sigma_{\max} = \frac{M_{\max}}{W_z} \leq [\sigma].$$

Bu yerden $W_z = \frac{M_{\max}}{[\sigma]} = \frac{130}{1} = 130 \text{ sm}^3$,

$$W_z = \frac{bt^2}{6} \Rightarrow t = \sqrt{\frac{6W_z}{b}} = \sqrt{\frac{6 \cdot 130}{20}} = 6,25 \text{ sm}.$$

$$q^d = q_{\max} \cdot \ell = 13 \cdot 2 = 26 \frac{\text{kN}}{\text{m}}.$$

$$R_A = R_B = 9,75 \text{ kN}.$$

$$\frac{q_1}{0,5} = \frac{q^d}{1,5} \rightarrow q_1 = 8,67 \frac{\text{kN}}{\text{m}},$$

$$q_2 = q^d - q_1 = 17,33 \frac{\text{kN}}{\text{m}},$$

$$q_{x_2} = 17,34(0,5 + x_2)$$

$$M_{x_2} = -\frac{1}{2} \cdot 17,34(0,5 + x_2) \cdot \frac{1}{3}(x_2 + 0,5)^2 + R_B x_2,$$

$$\frac{dM_2}{dx_2} = 0 \Rightarrow x_2 = x_{\max} = 0,56 \text{ m},$$

$$M_{\max} = -\frac{1}{6} \cdot 17,34(0,5 + 0,56)^3 + 9,75 \cdot 0,56 = -3,44 + 5,46 = 2,02 \text{ kN} \cdot \text{m}$$

5.30. $b = \frac{BX}{\ell}.$

$$b_x = B \frac{x}{\ell}, \frac{1}{\rho} = \frac{M}{EI_z}, M = Px, I_z = \frac{b_x h^3}{12} = \frac{bxh^3}{12\ell},$$

$$\frac{1}{\rho} = \frac{Px}{B} \cdot \frac{12\ell}{xh^3E} = \frac{P}{EB} \cdot \frac{12\ell}{h^3} \rightarrow \text{hemişelik}$$

Onda $\rho = \text{hemişelik}$, diymek: $b = \frac{BX}{\ell}.$

5.31. $\sigma_{CD} = 8,04 \text{ kN/sm}^2.$

$$M_{CD} = -P \cdot 95 = -7600 \text{ kN} \cdot \text{sm}, M_{AB} = -P \cdot 230 = -18400 \text{ kN} \cdot \text{sm},$$

$$W_{CD} = \frac{11,2 \cdot 22,5^2}{6} = 945,35 \text{ sm}^3,$$

$$W_{AB} = \frac{14 \cdot 38^2}{6} = 3369,3 \text{ sm}^3.$$

Onda $\sigma_{CD} = \frac{M_{CD}}{W_{CD}} = \frac{7600}{945,35} = 8,04 \text{ kN/sm}^2,$

$$\sigma_{AB} = \frac{M_{AB}}{W_{AB}} = \frac{18400}{3369,3} = 5,46 \text{ kN/sm}^2.$$

Ryçagyn „howply“ kesigi CD kesik.

5.32. $b_x = \frac{3q}{h^2[\sigma]} \cdot x^2.$

Balkanyň erkin tarapyndan x uzaklykdaky kesikde:

$$M_x = -\frac{qx^2}{2}, W_x = \frac{b_x h^2}{6}, \sigma_x = \frac{M_x}{W_x} \leq [\sigma]$$

Bu yerden $\frac{qx^2 \cdot 6}{2 \cdot b_x \cdot h^2} = [\sigma] \Rightarrow b_x = \frac{3qx^2}{h^2[\sigma]}.$

5.33. $I_x = 6000 \text{ sm}^4.$

$$\sigma_{\text{gys}} = E \varepsilon_1 = E \cdot \frac{\Delta n_1}{\ell \cdot k} = -1,2 \cdot 10^4 \cdot \frac{1,5}{2 \cdot 1000} = -9 \text{ kN/sm}^2,$$

$$\sigma_{\text{süýnme}} = E \cdot \varepsilon_2 = E \cdot \frac{\Delta n_2}{\ell \cdot k} = 1,2 \cdot 10^4 \cdot \frac{0,5}{2 \cdot 1000} = 3 \text{ kN/sm}^2,$$

$$M_{\max} = P \cdot a = 50 \cdot 60 = 3000 \text{ kN} \cdot \text{sm},$$

$$\frac{h - y_c}{15} = \frac{y_c}{5} \quad y_c = \frac{h}{4}, \quad y_{gys} = 18 \text{ sm}, \quad y_{süýnme} = 6 \text{ sm}.$$

Gysylma berklik şertinden $I_x = \frac{M_{\max}}{\sigma_{gys}} \cdot y_g = \frac{3000}{9} \cdot 18 = 6000 \text{ sm}^4$

Süýnmeden $I_x = \frac{M_{\max}}{\sigma_{süýnme}} \cdot y_s = \frac{3000 \cdot 6}{3} = 6000 \text{ sm}^4$

5.34. $M = \frac{2}{3} \cdot \frac{\ell b h}{1 - \mu} \cdot \frac{\Delta B}{B}$

Balkanyň ýüklenmesinden $Q = \frac{M}{\ell}$,

Žurawskiniň formulasyndan $\tau = \frac{3}{2} \cdot \frac{Q}{bh} = \frac{3}{2} \cdot \frac{M}{\ell b h}$. (1)

Tenzometr 45° boýunça goýlan we bu kesikde $\sigma_1 = \tau = -\sigma_3$.

Gukuň kanunyna laýyklykda

$$\varepsilon = \frac{1}{E} (\sigma_1 - \mu \sigma_3) = \frac{\tau}{E} (1 + \mu), \text{ bu ýerde } \varepsilon = \frac{\Delta B}{B}.$$

Onda $\tau = \frac{E \Delta B}{(1 + \mu) B}$ (2)

(1) we (2) aňlatmalaryň sag tarapyňy deňläp alarys:

$$M = \frac{2}{3} \cdot \frac{E \ell b h}{1 + \mu} \cdot \frac{\Delta B}{B}$$

5.35. $\sigma = 2,71 \text{ kN/sm}^2$.

Sapfa düşýän güýç $R_s = \frac{G}{2} = \frac{430}{2} = 215 \text{ kN}$.

Sapfanyň boýnundaky egme moment

$$M_{\max} = R_s \cdot 0,34 = 215 \cdot 0,34 = 73,1 \text{ kN m},$$

Sapfanyň boýnundaky dartgynlyk

$$\sigma_{\max} = \frac{M_{\max}}{W_z} = \frac{M_{\max}}{0,1 d_s^3} = \frac{73,1 \cdot 10^2}{0,1 \cdot 30^3} = 2,71 \text{ kN/sm}^2.$$

5.36. I №14.

Balka düşýän ýük $G = \frac{2}{3} \ell b h \gamma$,

$$\frac{dy}{dx} = \frac{4h}{\ell^2} (\ell - 2x),$$

Eger $x = 0 \Rightarrow \frac{dy}{dx} = \text{tg} \alpha = \frac{4h}{\ell}$, $\alpha = 60^\circ$, $h = 0,43 \ell$.

Balkany basýan diwaryň böleginiň agramy

$$G = \frac{2}{3} \cdot 0,43 \ell^2 B \gamma.$$

Iň uly egme moment balkanyň ortasynda bolýar.

$$M_{\max} = \frac{G}{2} \left(\frac{\ell}{2} - \frac{3}{16} \ell \right) = \frac{5 G \ell}{32},$$

$$W_z = \frac{M_{\max}}{2[\sigma]} = \frac{5 G \ell}{2 \cdot 32[\sigma]} = \frac{4,3}{48} \cdot \frac{\ell^3 b \gamma}{2 \cdot [\sigma]} = 86 \text{ sm}^3,$$

Tablisadan $W_z = 81,7 \text{ sm}^3$ I №14.

5.37. $\sigma_A = -0,73 \text{ kN/sm}^2$, $\sigma_B = 6,68 \text{ kN/sm}^2$.

Polat listi ekwivalent agaç bilen çalşyryars, şonuň üçin listiň inini $n=20$ esse ulaldýars, ýagny $B_{ekw} = nb = 20 b$.

Ekwiwalent kesigiň agyrylyk merkezini tapýars.

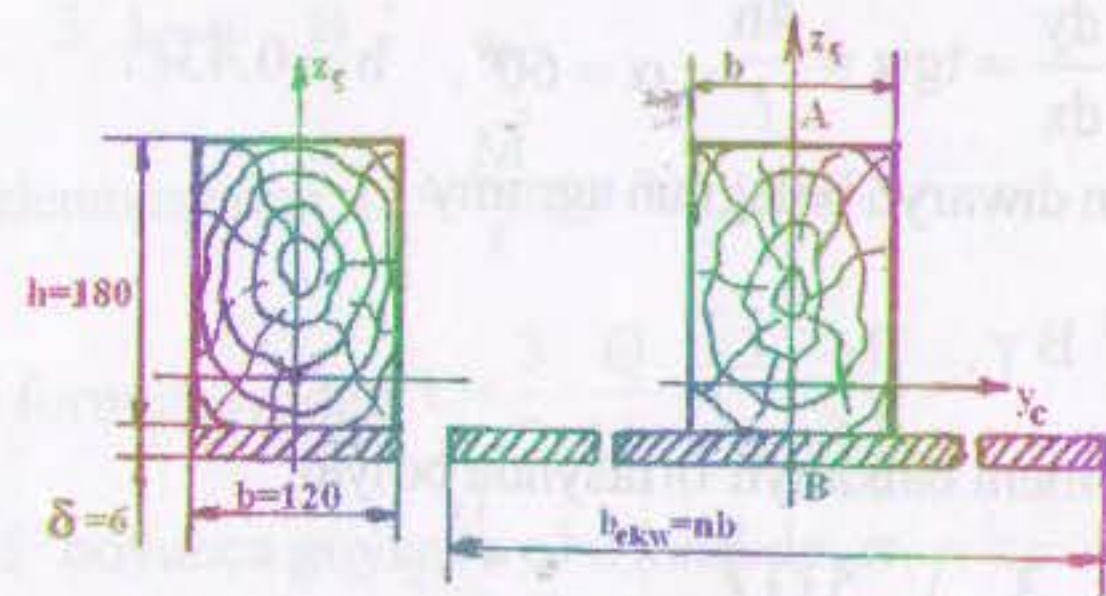
$$Z_C = \frac{A^\ell Z^\ell + A^a Z^a}{A^\ell + A^a} = \frac{b_{ekw} \cdot \delta \cdot \frac{\delta}{2} + b \cdot h + \left(\delta + \frac{h}{2} \right)}{b_{ekw} \cdot \delta + b h} = 5,88 \text{ sm},$$

$$I_{Z_C} = \frac{b_{ekw} \cdot \delta^3}{12} + b_{ekw} \cdot \delta \cdot 5,58^2 + \frac{b h^3}{12} + b \cdot h \cdot 3,72^2 = 13310 \text{ sm}^4.$$

A we B nokatdakylary dartgynlylyklar.

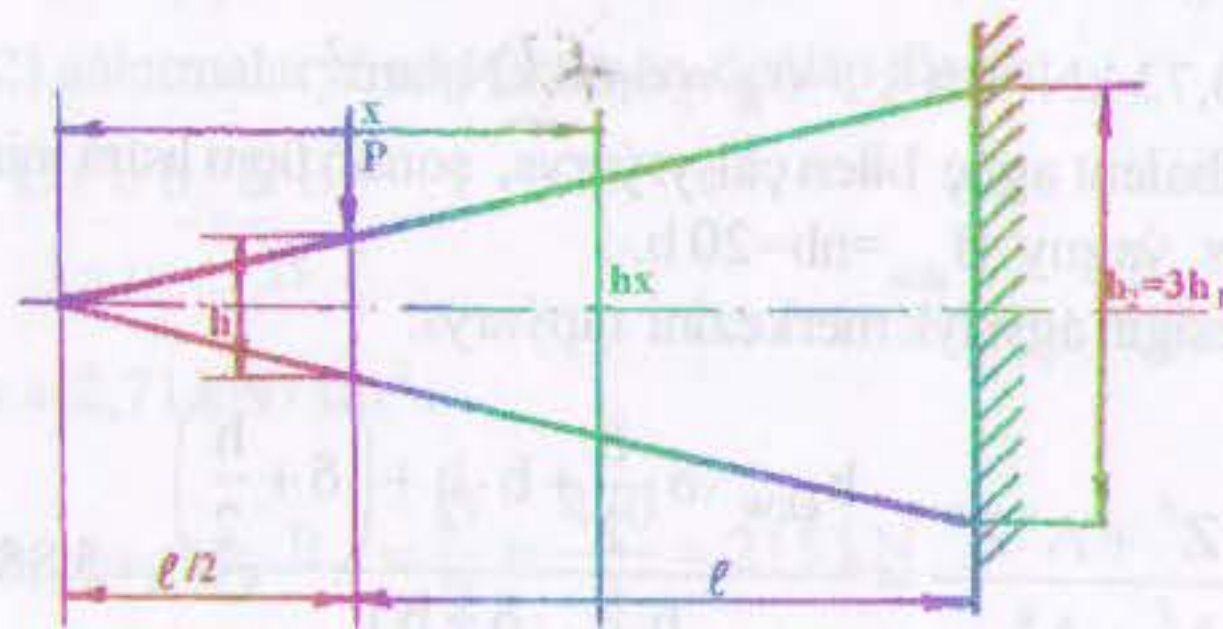
$$\sigma_B = \frac{M_{\max}}{I_{Z_C}} \cdot Z_B = \frac{q \ell^2}{8 I_{Z_C}} Z_B = 0,334 \text{ kN/sm}^2,$$

$$\sigma_A = \frac{q \ell^2}{8 I_{Z_C}} \cdot Z_A = 0,734 \text{ kN/sm}^2 \text{ onda } \sigma_B^{\text{list}} = \sigma_B \cdot n = 6,68 \frac{\text{kN}}{\text{sm}^2}.$$



5.37-nji surat

5.38. $\sigma_{\max} = \frac{3}{4} \cdot \frac{P \ell}{b h_1^2}$ - balkanyň oratasyndaky kesikde.



5.38-nji surat

Çyzgydan $h_x = \frac{2 h_1}{\ell} \cdot x,$

$$W_z = \frac{b}{6} \cdot h_x^2 = \frac{b}{6} \cdot \frac{4 h_1^2}{\ell^2} x^2, \quad M_x = -P \left(x - \frac{\ell}{2} \right).$$

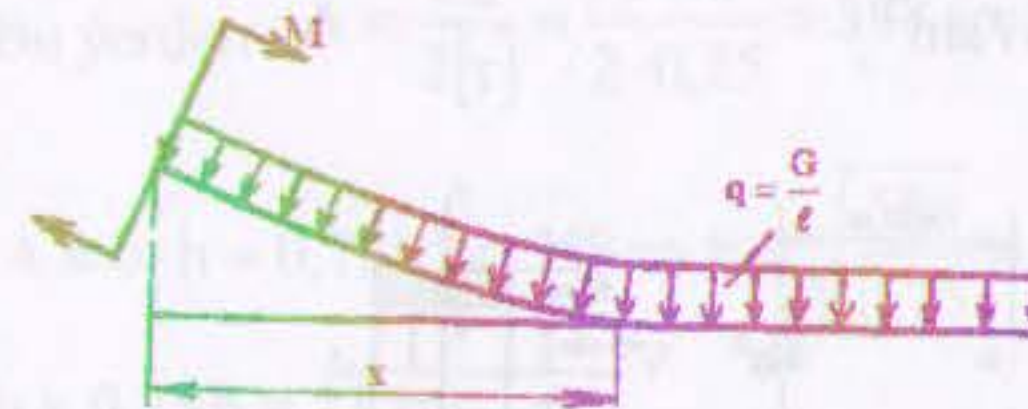
$$\sigma_x = \frac{M_x}{W_z} = - \frac{P \left(x - \frac{\ell}{2} \right)}{\frac{b}{6} \cdot \frac{4 h_1^2}{\ell^2} x^2} = - \frac{3 P \ell^2}{2 b h_1^2} \left[x^{-2} \cdot \left(x - \frac{\ell}{2} \right) \right].$$

Bu aňlatmanyň maksimumyny barlaýarys:

$$\frac{d\sigma_x}{dx} = - \frac{3 P \ell^2}{2 b h_1^2} \left[x^{-2} \cdot \left(x - \frac{\ell}{2} \right) \right]' = 0$$

Bu ýerden $x_{\max} = \frac{\ell}{2}.$

$$\text{Onda } \sigma_{\max} = \frac{3 P \ell^2}{2 b h_1^2} \cdot \frac{1}{\ell^2} \cdot \frac{\ell}{2} = \frac{3}{4} \cdot \frac{P \ell}{b h_1^2}.$$



5.39-nji surat

5.39. $x = 0,5 \ell.$

$$M_B^{\text{zer}} = M - q \frac{x^2}{2} = 0,$$

Bu ýerden $\frac{q x^2}{2} = \frac{q \ell^2}{8},$

onda $x = 0,5 \ell.$

5.40. $P_{r,e} = \sigma_{\text{wagt}} b^3 / (3 n \ell).$

Berklik şerti: $\sigma_{\max} = \frac{M_{\max}}{I_z} \cdot y_{\max} \leq [\sigma].$

Hasaby balkanyň süýnýän gatlagy üçin geçirýäris, $y = \frac{h}{3}.$

$$[\sigma] = \sigma_{\text{wagt}} / n \quad \text{we} \quad M = \frac{P\ell}{4},$$

$$I_z = \frac{bh^3}{36} \quad \text{hasaba alyp,}$$

$$\frac{P_{r.e} \ell}{4} \frac{36}{bh^3} \cdot \frac{h}{3} = \frac{\sigma_{\text{wagt}}}{n}$$

$$\text{Bu ýerden } P_{r.e} = \frac{\sigma_{\text{wagt}} \cdot b^3}{3n\ell}.$$

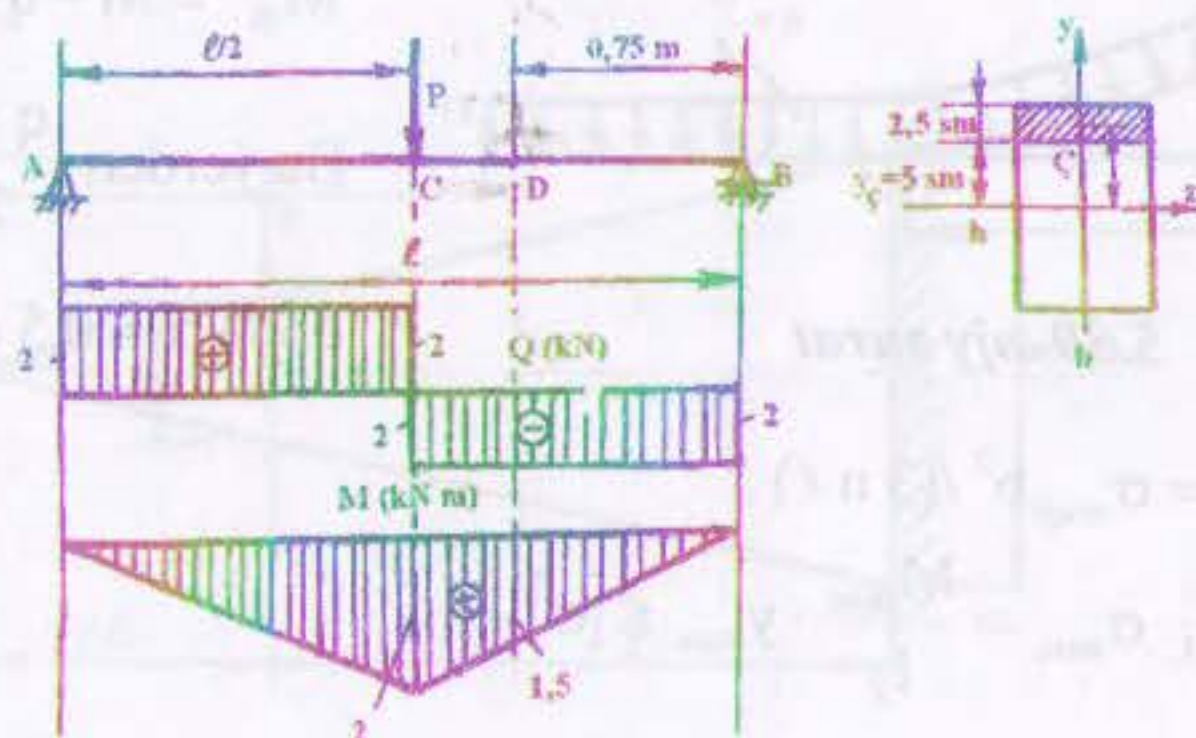
$$5.41. \quad \sigma_c = 0,355 \text{ kN/sm}^2, \quad \tau_c = 0,015 \text{ kN/sm}^2.$$

$$\sigma_c = \frac{M_D}{I_z} \cdot y_c = \frac{12M_D}{bh^3} \cdot y_c = \frac{12 \cdot 1,5 \cdot 10^2}{7,5 \cdot 15^3} \cdot 5 = 0,355 \frac{\text{kN}}{\text{sm}^2}.$$

$$\tau_c = \frac{Q \cdot S_z^{\text{kes}}}{I_z \cdot b},$$

$$S_z^{\text{kes}} = A^{\text{kes}} \cdot y = 7,5 \cdot 2,5 \cdot 6,25 = 117 \text{ sm}^3,$$

$$\tau_c = \frac{2 \cdot 117}{7,5 \cdot 15^3 \cdot 7,5} = 0,015 \text{ kN/sm}^2.$$



5.41-nji surat

$$5.42. \quad b \times h = 21 \times 28 \text{ sm}^2.$$

$$Q_{\text{max}} = P = 98 \text{ kN},$$

$$M_{\text{max}} = P \cdot C = 98 \cdot 0,2 = 19,6 \text{ kN} \cdot \text{m}.$$

Normal dartgynlyk boýunça berklik şertinden

$$\sigma_{\text{max}} = \frac{M_{\text{max}}}{W_z} \leq [\sigma], \quad W_z = \frac{0,75 h^3}{6} = 0,125 h^3.$$

$$\text{Onda } h = \sqrt[3]{\frac{M_{\text{max}}}{0,125 \cdot [\sigma]}} = \sqrt[3]{\frac{19,6 \cdot 10^2}{0,125 \cdot 1}} = 25 \text{ sm},$$

$$b = 0,75 \cdot 25 = 18,75 \text{ sm}.$$

Galtaşma dartgynlyk boýunça barlaýarys:

$$\tau = \frac{3}{2} \cdot \frac{Q}{A} = \frac{3}{2} \cdot \frac{98}{25 \cdot 18,75} = 0,31 \text{ kN/sm}^2 > [\tau] = 0,25 \frac{\text{kN}}{\text{sm}^2}$$

$\tau > [\tau]$, şonuň üçin kesigi galtaşma dartgynlygyň berklik şertinden saýlaýarys.

$$\tau = \frac{3}{2} \cdot \frac{Q}{A} \leq [\tau],$$

$$\text{Bu ýerden } A = \frac{3Q}{2[\tau]} = \frac{3 \cdot 98}{2 \cdot 0,25} = 588 \text{ sm}^2,$$

$$A = b \cdot h = 0,75 h^2 = 588 \Rightarrow h = \sqrt{\frac{588}{0,75}} = 28 \text{ sm},$$

$$b = 0,75 h = 21 \text{ sm}.$$

$$5.43. \quad q = 10 \text{ kN/m}, \quad \tau_{\text{max}} = 2,48 \text{ kN/sm}^2.$$

$$\text{Berklik şertinden } M_{\text{max}} = \frac{q\ell^2}{8}, \quad W_z = 143 \text{ sm}^3,$$

$$\sigma = \frac{M_{\text{max}}}{W_z} \leq [\sigma] \Rightarrow \frac{q\ell^2}{8 \cdot W_z} \leq q = \frac{8W_z[\sigma]}{\ell^2} = 10 \text{ kN/m},$$

$$\text{Galtaşma dartgynlyk } d = 0,51 \text{ sm}, \quad I_z = 1290 \text{ sm}^4,$$

$$S_z = 81,4 \text{ sm}^3, \quad Q = \frac{q \ell}{2} = 20 \text{ kN},$$

$$\tau_{\max} = \frac{Q \cdot S_z}{d \cdot I_z} = \frac{20 \cdot 81,4}{0,51 \cdot 1290} = 2,48 \text{ kN/sm}^2.$$

5.44. $\tau_{\max} = 2 \text{ kN/sm}^2$.

Žurawskiniñ formulasyny ulanyrys.

$$\tau_{\max} = \frac{Q \cdot S_z^{\max}}{b I_z}; \quad S_z^{\max} = S_{z_1}^{\max} = A_1 \cdot Z_{C_1} - A_2 \cdot Z_{C_2} = \frac{1}{6}(D^3 - d^3),$$

$$I_z = 0,1 D^4 (1 - \alpha^4), \quad \alpha = 0,9, \quad b = 2(D - d),$$

$$\tau_{\max} = \frac{Q(D^3 - d^3)}{6 \cdot 2(D - d) \cdot 0,1 D^4 (1 - \alpha^4)} = \frac{60 \cdot (20^3 - 18^3)}{1,2(20 - 18) \cdot 20^4 (1 - 0,9^4)} = 2 \frac{\text{kN}}{\text{sm}^2}.$$

5.45. $\sigma_{\max} = 0,86 \text{ kN/sm}^2, \quad \tau_{\max} = 0,18 \text{ kN/sm}^2$.

Çyzgydan $\varphi = 60^\circ = 1,0466 \text{ rad}, \quad M_{\max} = P \cdot 3 = 12 \text{ kN m}.$

$$I_z = \frac{d^4}{32} (\varphi - 0,25 \sin 4 \varphi) = \frac{25^4}{32} (1,0466 - 0,25 \cdot (-0,866)) = 15454 \text{ sm}^4,$$

$$\sigma_{\max} = \frac{M_{\max}}{I_z} \cdot y, \quad y = \sqrt{\frac{d^2}{4} - \frac{d^2}{16}} = \frac{\sqrt{3}}{4} d = 10,83 \text{ sm},$$

Onda $\sigma_{\max} = \frac{12 \cdot 10^2}{15454} \cdot 10,83 = 0,86 \text{ kN/sm}^2 < [\sigma].$

$$S_z = \frac{d^3}{12} (1 - \cos 3 \varphi) = \frac{25^3}{12} (1 - 0,5^3) = 1139,3 \text{ sm}^3,$$

$$\tau_{\max} = \frac{P \cdot S_z}{I_z \cdot d} = \frac{60 \cdot 1139,3}{15454 \cdot 25} = 0,18 \text{ kN/sm}^2 < [\tau].$$

5.46. $\tau_{\max} = 9,8 \text{ kN/sm}^2, \quad \tau_{\min} = 6,98 \text{ kN/sm}^2,$

$$Q = 288 \text{ kN}, \quad \frac{Q_{\text{diw}}}{Q} = 0,96$$

$$I_{Z_C} = \sum (I_{Z_i} + A_i \cdot y_i^2) = 9590 \text{ sm}^4,$$

$$S_{Z_C} = \sum A_i y_C = 376,5 \text{ sm}^3 - \text{ýarym kesigiñ statiki momenti},$$

$$S_{Z_C}^I = A \cdot y = 267,2 \text{ sm}^2 - \text{polkanyñ merkezi oka görä statiki momenti}.$$

$$\text{Onda } \tau_{\max} = \frac{Q \cdot S_{Z_C}}{I_{Z_C} \cdot d} = 9,8 \text{ kN/sm}^2, \quad \tau_{\min} = \frac{Q \cdot S_{Z_C}'}{I_{Z_C} \cdot d} = 6,98 \text{ kN/sm}^2$$

$$Q_{\text{diw}} = \tau_{\min} \cdot A_{\text{diw}} + \frac{2}{3} (\tau_{\max} - \tau_{\min}) A_{\text{diw}} = 288 \text{ kN};$$

$$\frac{Q_{\text{diw}}}{Q} = \frac{288}{300} = 0,96.$$

5.47. $\sigma_{\max} = 2,54 \text{ kN/sm}^2, \quad \tau_{\max} = 0,8 \text{ kN/sm}^2$.

$$Q = P = 60 \text{ kN}, \quad M_{\max} = Pa = 60 \cdot 70 = 4200 \text{ kN sm},$$

$$I_z = \frac{b^4}{12} - \frac{\pi d^4}{64} = \frac{24^4}{12} - \frac{3,14 \cdot 20^4}{64} = 19798 \text{ sm}^4,$$

$$\sigma_{\max} = \frac{M_{\max}}{I_z} \cdot y_{\max} = \frac{4200}{19798} \cdot 12 = 2,54 \text{ kN/sm}^2, \quad y_{\max} = \frac{b}{2} = 12 \text{ sm}.$$

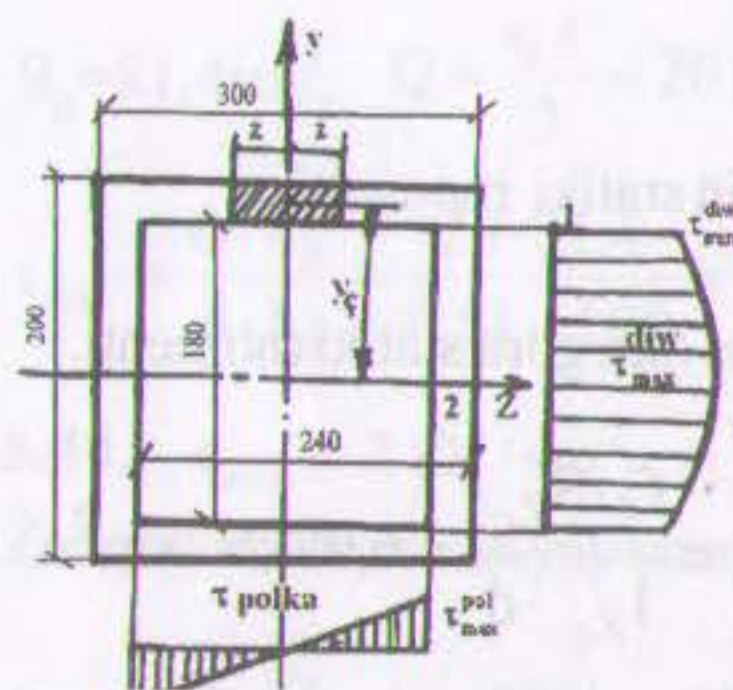
Ýarym kesigiñ statiki momenti

$$S_z = b \cdot \frac{b}{2} \cdot \frac{b}{4} - \frac{\pi d^2}{8} \cdot \frac{2d}{3\pi} = \frac{24^3}{8} - \frac{20^3}{12} = 1061,33 \text{ sm}^3,$$

$$\tau_{\max} = \frac{Q \cdot S_z}{I_z (b - d)} = \frac{60 \cdot 1061,33}{19798 \cdot 4} = 0,8 \text{ kN/sm}^2.$$

5.48. $\tau_{\max} = 3,3 \text{ kN/sm}^2$ bu bolsa diwardaky dartgynlylykdan 30% ýokary.

$$I_z = \frac{30 \cdot 20^3}{12} - \frac{24 \cdot 18^3}{12} = 8336 \text{ sm}^4,$$



5.48-nji surat

$$S_{Z_1}^{diw} = 30 \cdot 1 \cdot 9,5 = 285 \text{ sm}^3,$$

$$S_{Z_1}^{diw} = S_{Z_1}^{diw} + 2 \cdot 9 \cdot 3 \cdot 4,5 = 528 \text{ sm}^3,$$

$$\tau_{Z_1}^{diw} = \frac{Q S_{Z_1}^{diw}}{I_Z \cdot 2 \cdot 3} = \frac{240 \cdot 285}{8336 \cdot 6} = 1,36 \text{ kN/sm}^2,$$

$$\tau_{Z_1}^{diw} = \frac{Q S_{Z_1}^{diw}}{I_Z \cdot 6} = \frac{240 \cdot 528}{8336 \cdot 6} = 2,53 \text{ kN/sm}^2,$$

$$S_Z^{pol} = t \cdot z \cdot y_C = 9,5 z,$$

$$z = 0, \quad \tau = 0, \quad z = 12 \text{ sm},$$

$$\tau_{\max}^{pol} = \frac{Q \cdot S_Z^{pol}}{I_Z \cdot t} = \frac{240 \cdot 9,57}{8336 \cdot 1} = \frac{240 \cdot 9,5 \cdot 12}{8336} = 3,3 \frac{\text{kN}}{\text{sm}^2}.$$

5.49. $P = 605 \text{ kN}, \quad \tau_{\max} = 6,95 \text{ kN/sm}^2.$

$$I_Z = \left(\frac{36 \cdot 2^3}{12} + 36 \cdot 2 \cdot 19^2 \right) \cdot 2 + \frac{1,2 \cdot 36^3}{12} = 56697,6 \text{ sm}^4,$$

$$S_Z = 36 \cdot 2 \cdot 19 + 1,2 \cdot 18 \cdot 9 = 1562,4 \text{ sm}^3.$$

1) Normal dartgynlyk boýunça berklik şertinden

$$\frac{P \ell}{4W_Z} \leq [\sigma] \Rightarrow P = \frac{4W_Z [\sigma]}{\ell} = \frac{4 \cdot 2834,88 \cdot 16}{300} = 605 \text{ kN}.$$

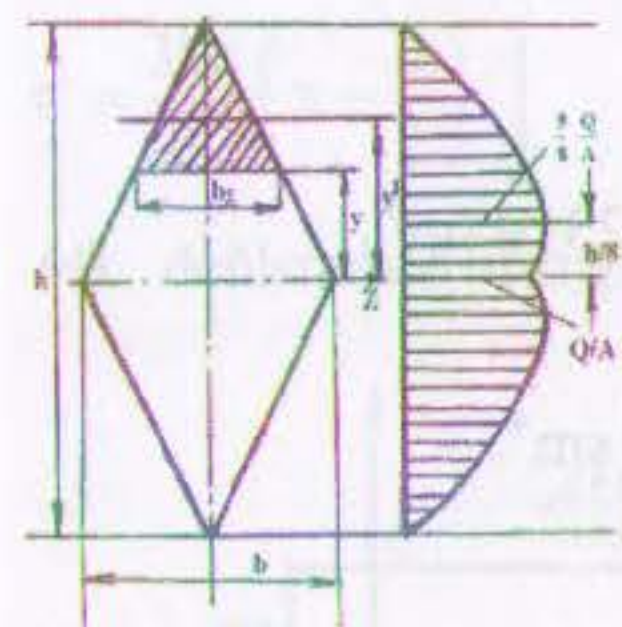
2) Galtaşma dartgynlyk boýunça berklik şertinden

$$\tau_{\max} = \frac{Q \cdot S_Z}{I_Z \cdot D} \leq [\tau], \quad Q = \frac{P}{2}$$

$$\frac{Q \cdot S_Z}{2I_Z \cdot d} \leq [\tau] \Rightarrow P = \frac{2I_Z d [\tau]}{S_Z} = \frac{2 \cdot 56697,6 \cdot 1,2 \cdot 10}{1562,4} = 871 \frac{\text{kN}}{\text{sm}^2}.$$

Kabul edýäris: $P = 605 \text{ kN}.$

$$\text{Onda } \tau_{\max} = \frac{Q \cdot S_Z}{I_Z \cdot d} = \frac{605 \cdot 1562,4}{2 \cdot 56697,6 \cdot 1,2} = 6,95 \text{ kN/sm}^2.$$



5.50-nji surat

5.50. $\tau_{\max} = \frac{9}{8} \cdot \frac{Q}{A},$

$$\tau = \frac{2Q}{bh^3} (h-2y) \cdot (h+4y).$$

Žurawskiniň formulasyndan

$$\tau = \frac{Q \cdot S_Z^{kes}}{I_Z \cdot b_z}$$

Çyzgydan alarys:

$$S_Z^{kes} = \frac{1}{2} \cdot b_z \left(\frac{h}{2} - y \right) \cdot \frac{h+4y}{6} = \frac{1}{4} \cdot \frac{b}{h} (h-2y)^2 \cdot \frac{h+4y}{6}.$$

$$I_Z = 2 \cdot \frac{b \left(\frac{h}{2} \right)^3}{12} = \frac{bh^3}{48}$$

Onda:

$$\frac{Q \cdot 48}{bh^3} \cdot \frac{b (h-2y)^2 (h+4y)}{24h} \cdot \frac{h}{b(h-2y)} = \frac{2Q}{bh^3} (h-2y)(h+4y),$$

$$\text{Eger: } y = \pm \frac{h}{2} \Rightarrow \tau = 0,$$

$$\text{Eger: } y = 0 \Rightarrow \tau = \frac{Q}{A}.$$

Galtaşma dartgynlygyň iň uly bahasyny tapýarys:

$$\frac{d\tau}{dy} = \left[\frac{2Q}{bh^3} \cdot (h-2y)(h+4y) \right]' = 0 \Rightarrow y = \frac{h}{8},$$

$$\tau_{\max} = \frac{2Q}{bh^3} \left(h - 2 \cdot \frac{h}{8} \right) \left(h + 4 \cdot \frac{h}{8} \right) = \frac{9}{8} \cdot \frac{Q}{A}.$$

5.51. $h=0,3$ sm.

Polka bilen diwaryň sepgidindäki dartgynlyk

$$\tau = \frac{Q \cdot S_z}{I_z \cdot \delta}; \quad S_z^{\text{pol}} = 3 \cdot 20 \cdot 38,5 = 2310 \text{ sm}^3,$$

$$I_z = 2 \left(3 \cdot 20 \cdot 38,5^2 + \frac{203^3}{12} \right) + \frac{1 \cdot 74^3}{12} = 211729 \text{ sm}^4$$

$$\tau = \frac{300 \cdot 2310}{211729 \cdot 1} = 3,27 \text{ kN/sm}^2; \quad T = \tau \cdot \delta \cdot 1 = 3,27 \text{ kN}.$$

$$\text{Tikiniň meýdany } A = \frac{T}{[\tau]} = \frac{3,27}{5} = 0,654 \text{ sm}^2,$$

$$A = 2 \cdot 1 \cdot 0,7 h_t = 0,654, \quad h_t = 0,47 \text{ sm}.$$

$$5.52. \quad \sigma^I = \frac{3Px}{2h^3} (3h - 4x), \quad \tau^I = \frac{3Px}{h^3} \left(x - \frac{h}{2} \right).$$

Diregden x uzaklykdaky balkanyň çep böleginiň kese kesigindäki σ we τ aňlatmalary aşakdaky ýaly ýazylyr ($b=1$):

$$\sigma = -\frac{6Pxy}{h^3}, \quad \tau = \frac{3P \left(\frac{h^2}{4} - y^2 \right)}{h^3}.$$

a-b kesik boýunça dartgynlyk aşakdaky formula bilen tapylýar:

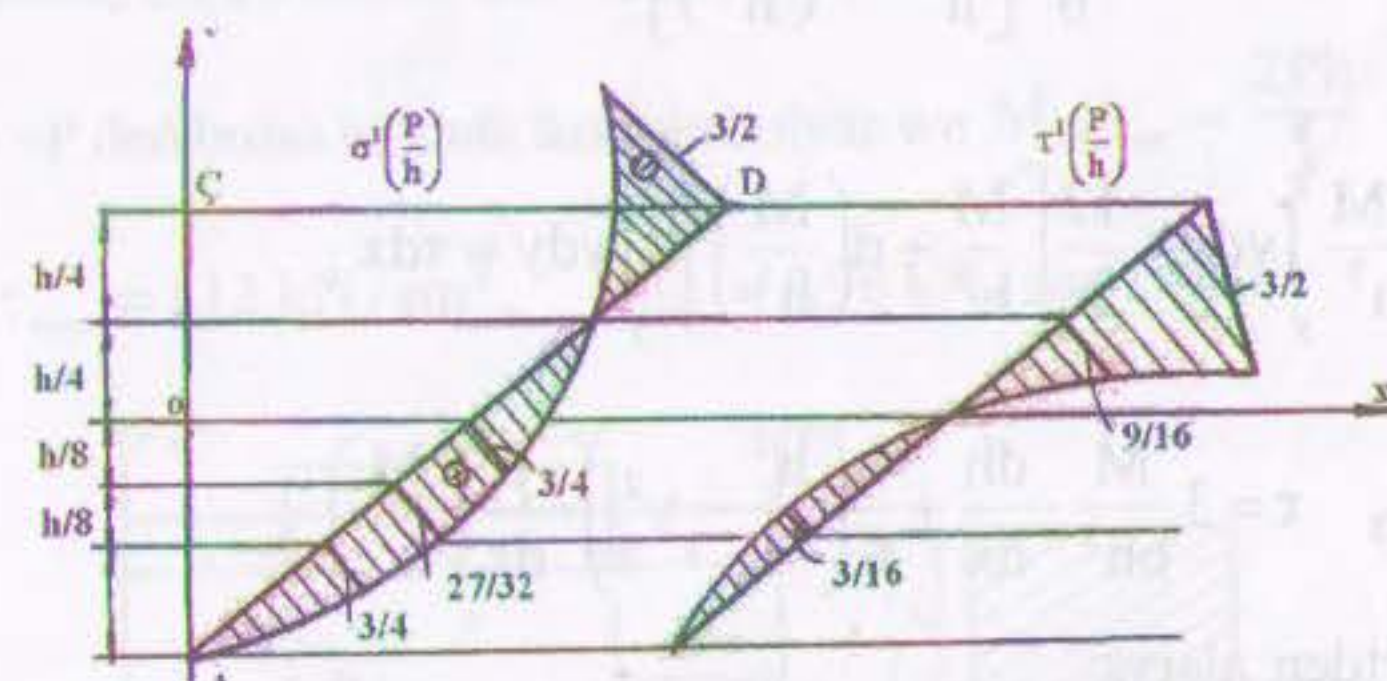
$$(2) \quad \begin{cases} \sigma^I = \frac{\sigma}{2} (1 - \cos 2\alpha) - \tau \sin 2\alpha, & 1 - \cos 2\alpha = 2 \cos^2 \alpha \\ \tau^I = \frac{\sigma}{2} \sin 2\alpha - \tau \cos 2\alpha, & \text{bu yerde } \alpha = 135^\circ \end{cases}$$

$$\sigma^I \text{ we } \tau^I \text{ meýdançasý a-b gönüde ýatyr, onuň deňlemesi } y = x - \frac{h}{2} \quad (3)$$

(1), (2) we (3) aňlatmalary bilelikde çözüp alarys:

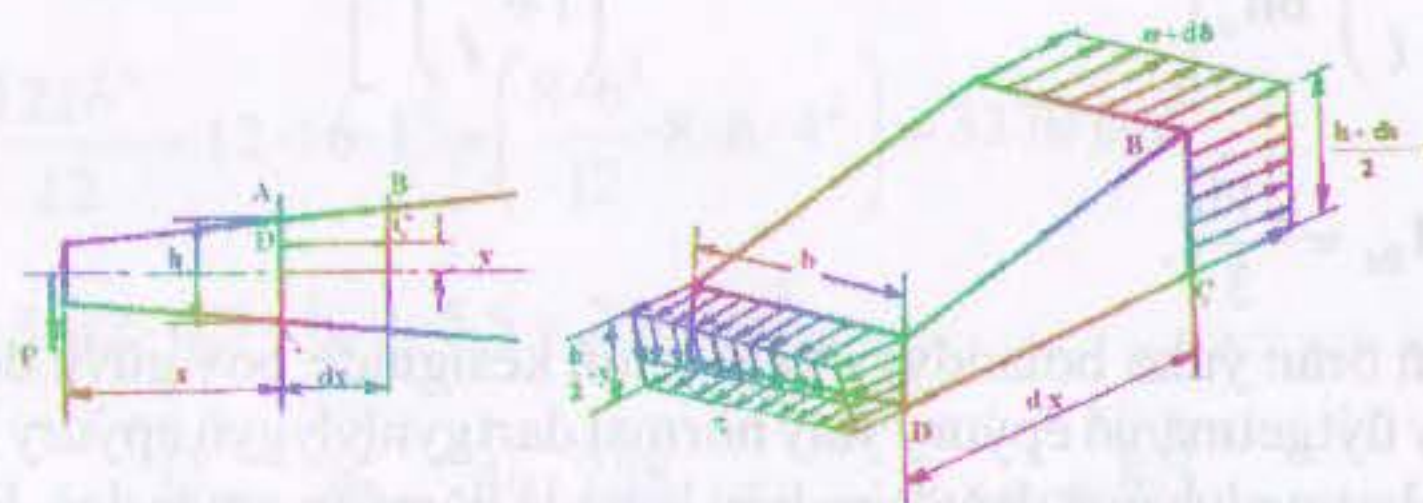
$$\left. \begin{aligned} \sigma^I &= \frac{3Px}{2h^3} (3h - 4x) \\ \tau^I &= \frac{3Px}{h^3} \left(x - \frac{h}{2} \right) \end{aligned} \right\} \quad (4)$$

(4) deňlemeleri ulanyp, aşakdaky epýurlary alarys.



5.52-nji surat

$$5.53. \quad \tau = 6P \left[\left(1 + \frac{x}{\ell} \right)^2 bh_0 \right]^{-1} \cdot \left[\frac{x}{2\ell} + \frac{1}{h_0^2} \left(\frac{h^2}{4} - y^2 \right) \right] \cdot \frac{1 - \frac{2x}{\ell}}{\left(1 + \frac{x}{\ell} \right)^2}$$



5.53-nji surat

Uzynlygy dx bolan elementar bölegi bölüp alýarys we onuň deňagramlylygyna seredýäris.

$$\sum X = - \int_y^{\frac{h}{2}} \sigma b dy + \int_y^{\frac{h+dh}{2}} (\sigma + d\sigma) dy = \tau b dx, \quad \sigma = \frac{12M}{bh^3} \cdot y.$$

Bu ýerde $\sigma + d\sigma = \frac{12y}{b} \left[\frac{M}{h^3} + d\left(\frac{M}{h^3}\right) \right],$

Onda $\frac{12M}{bh^3} \int_y^{\frac{h}{2}} y dy + \frac{12}{b} \left[\frac{M}{h^3} + d\left(\frac{M}{h^3}\right) \right] \int_y^{\frac{h+dh}{2}} y dy = \tau dx,$

Bu ýerden $\tau = 3 \frac{M}{bh^2} \cdot \frac{dh}{dx} + \frac{6}{b} \left(\frac{h^2}{4} - y^2 \right) \cdot \frac{d}{dx} \left(\frac{M}{h^3} \right),$

$h_1 = 2h_0$ şertden alarys:

$$h = h_0 \left(1 + \frac{x}{\ell} \right), \quad M = Px.$$

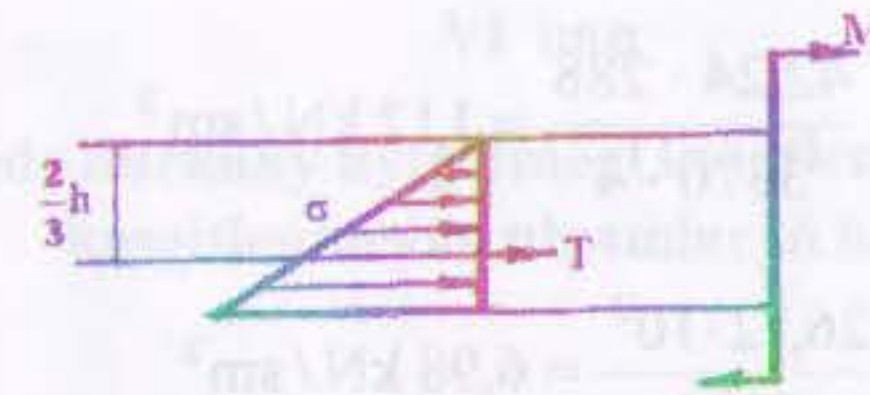
Onda ýerine goýup aşakdaky aňlatmany alarys:

$$\tau = \frac{6P}{\left(1 + \frac{x}{\ell} \right)^2 bh_0} \left[\frac{1}{2} \cdot \frac{x}{\ell} + \frac{1}{h_0^2} \left(\frac{h^2}{4} - y^2 \right) \cdot \frac{1 - \frac{2x}{\ell}}{\left(1 + \frac{x}{\ell} \right)^2} \right].$$

5.54. $M_{üz} = \frac{2Ph}{3}.$

Lentanyň örän ýuka bolandygy üçin onuň kesiginde boý güýji döreýär. Durkuny üýtgetmäniň epýury ýaly normal dartgynlylygyň epýury bolýar. Normal dartgynlylygyň deňtäsi redijisi lentada döreýän güýje deň. Hemme

güýçler bir jübüt güýje $\left(T \cdot \frac{2h}{3} \right)$ getirilýär.

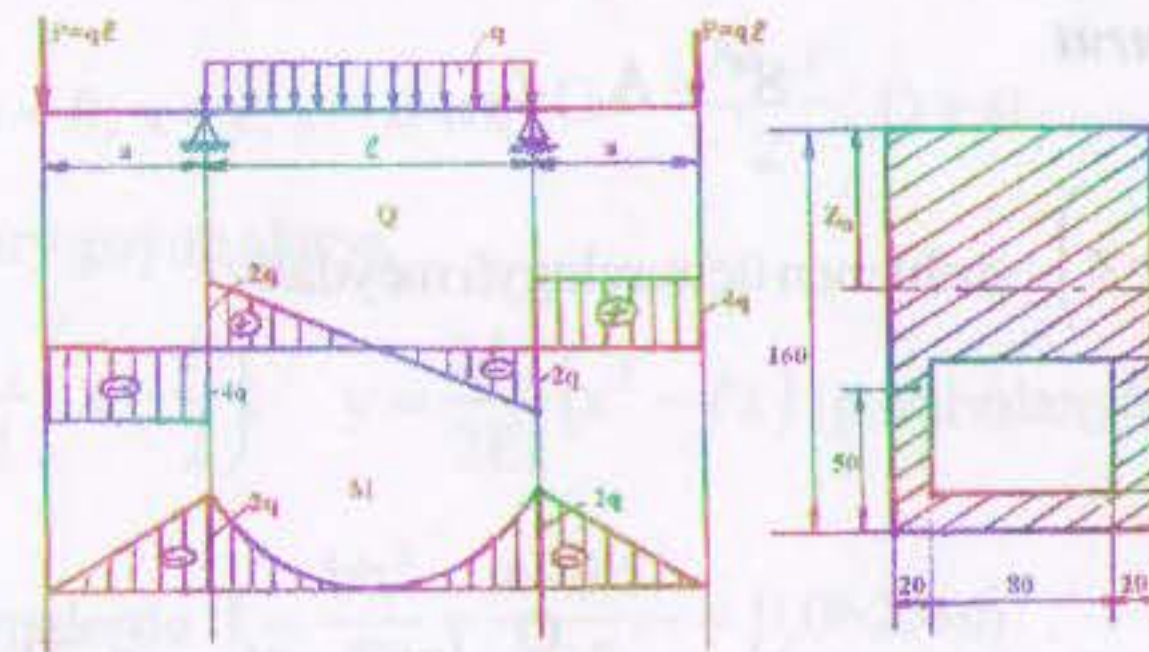


5.54-nji surat

Deňagramlylyk şertinden $M = T2h/3,$

Eger $T=P$ deň bolsa lentada üzülme bolýar we $M_{üzülme} = \frac{2Ph}{3}$

5.55. $\tau_{\max} = 1,12 \text{ kN/sm}^2, \quad \sigma_{\max} = 6,98 \text{ kN/sm}^2.$



5.55-nji surat

$$Z_0 = \frac{16 \cdot 12 \cdot 8 - 8 \cdot 6 \cdot 11}{16 \cdot 12 - 8 \cdot 6} = 7 \text{ sm},$$

$$I_y = \frac{1216^3}{12} + 12 \cdot 16 \cdot 1^2 - \left(\frac{8 \cdot 6^3}{12} - 8 \cdot 6 \cdot 4^2 \right) = 3370 \text{ sm}^4,$$

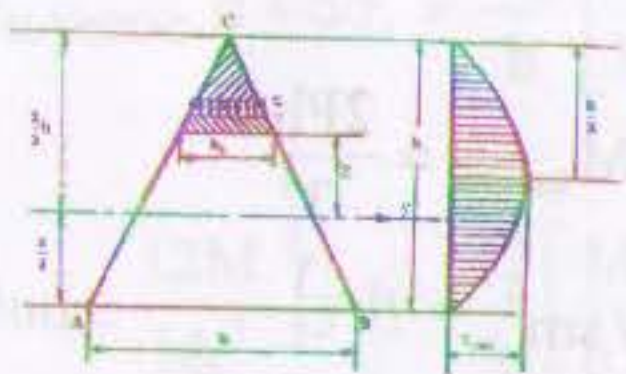
$$S_y^c = 5 \cdot 12 \cdot 6,5 - 8 \cdot 3 \cdot 5,5 = 258 \text{ sm}^3.$$

Onda $\tau_{\varphi} = \frac{Q_{\max} \cdot S_y^c}{I_y \cdot \delta_3} = \frac{4q \cdot 258}{3370 \cdot 4} = 1 \Rightarrow q = 13,06 \frac{\text{kN}}{\text{sm}}$

$$S_y^{\max} = 12 \cdot 8 \cdot 5 - 6 \cdot 8 \cdot 4 = 288 \text{ sm}^3$$

$$\tau_{\max} = \frac{Q_{\max} \cdot S_y^{\max}}{I_y \cdot \delta} = \frac{42,24 \cdot 288}{3370 \cdot 4} = 1,12 \text{ kN/sm}^2$$

$$\sigma_{\max} = \frac{M_{\max}}{I_y} \cdot y_{\max} = \frac{26,12 \cdot 10^2}{3370} = 6,98 \text{ kN/sm}^2$$



5.56-njy surat

$$5.56. \tau_{\max} = \frac{3}{2} \cdot \frac{Q}{A}$$

Žurawskiniň formulasy boýunça

$$\tau = \frac{Q \cdot S_y^0}{I_y \cdot b_z}$$

$$S_y^0 = A_0 \cdot Z_0,$$

$$A_0 = \frac{1}{2} b_z \left(\frac{2}{3} h - z \right) - \text{ştrihlenen üçburçlugyň meýdany}$$

$$Z_0 = \frac{2}{3} (h + z)$$

$$\text{Onda } S_y^0 = \frac{b_z}{27} (2h^2 + 3hz - 9z^2), \quad \tau = \frac{Q}{27I_y} (2h^2 + 3hz - 9z^2)$$

$$\frac{d\tau}{dz} = 3h - 18z = 0 \Rightarrow z = \frac{h}{6}$$

Diýmek $\tau = \tau_{\max}$, eger $z = \frac{h}{6}$ ýa-da üçburçlugyň orta çyzygynda iň uly

galtaşma dartgynlylyk bolýar, ýagny $\tau_{\max} = \frac{3Q}{bh} = \frac{3}{2} \cdot \frac{Q}{A}$.

$$\text{Eger } z=0 \Rightarrow \tau = \frac{4}{3} \cdot \frac{Q}{A}, \quad z = \frac{2}{3}h \rightarrow \tau = 0 \text{ we } z = \frac{h}{3} \rightarrow \tau = 0; \tau$$

epýury suratda görkezilen.

VI bap

Egilmede durkuny üýtgetmegi kesgitlemek we statiki kesgitlenmeýän ulgamlaryň hasaby

$$6.1. \theta_{\max} = 0,04 \text{ rad}; y_{\max} = f = 1 \text{ sm.}$$

$EJy'' = M_x = M_0$ egreden okuň differensial deňlemesini integrirläp, burç we çyzyk ornuny üýtgetmeleriniň bahalaryny alarys.

Iki gezek integrirläp alarys:

$$EJy' = M_0 x + C; \quad EJy = M_0 \frac{x^2}{2} + Cx + D.$$

Balkany berkitmek şertinden C we D hemişelikleri tapýarys.

$$x=0; y=0; x=\ell; y=0 \text{ we } C = -\frac{M_0 \ell}{2}, D=0.$$

Bu bahalary goýup alarys.

$$y' = \frac{M_0}{EI} \left(x - \frac{\ell}{2} \right); \quad y = \frac{M_0}{2EI} (x^2 - \ell x) \text{ (parabolanyň deňlemesi).}$$

$$\text{Bu deňlemelerde } I = \frac{bh^3}{12} = \frac{6 \cdot 0,5^3}{12} = 0,0625 \text{ sm}^4.$$

Iň uly öwrülme burçy ($x=0$ ýa-da $x=1$ m)

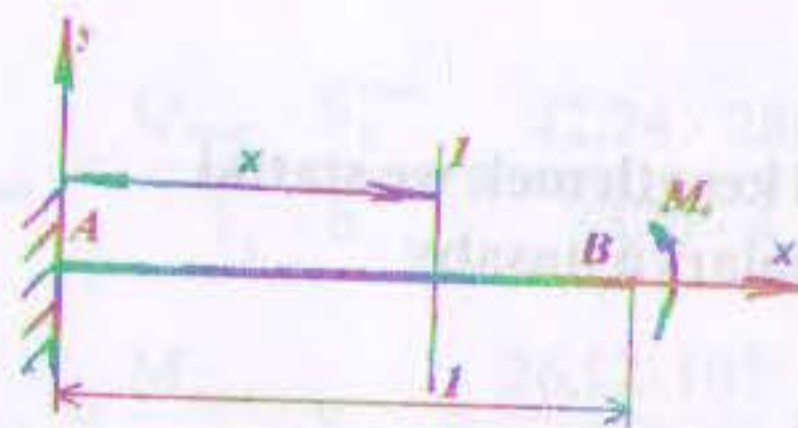
$$x=0 \Rightarrow \theta_A = \frac{-M_0 \ell}{2EI} = -0,04 \text{ rad (minus alamaty A diregde kesik sagat}$$

diliniň ugruna öwrülýär).

Iň uly progib prolyotyň ortasynda bolýar.

$$x = \frac{\ell}{2} \Rightarrow f = -\frac{M_0 \ell^2}{EI} = -1 \text{ sm (progibiň ugry y okuň ugruna gapma-garşy).}$$

$$6.2. E = 2 \cdot 10^4 \text{ kN/sm}^2, \rho = 26,75 \text{ m.}$$



6.2-nji surat

$$EIy'' = M_{x_1} = M_0,$$

$$EIy' = M_0x + C;$$

$$EIy = M_0 \frac{x^2}{2} + Cx + D,$$

$$x = 0; C = 0; D = 0; x = l;$$

$$EI\theta_{\max} = M_0 l;$$

$$E = \frac{M_0 l}{\theta_{\max}} = \frac{10 \cdot 100 \cdot 12}{2^4 \cdot 0,075} = 2 \cdot 10^4 \text{ kN/sm}^2.$$

$$\text{Egrelmäniň radiusy } \rho = \frac{EI}{M_0} = \frac{2 \cdot 10^4 \cdot 2^4}{12 \cdot 10} = 2675 \text{ sm} = 26,75 \text{ m}.$$

6.3. $\rho = 100 \text{ m}, M = 23 \text{ kN} \cdot \text{sm},$

$$\text{Egrelmäniň deňlemesi } y = \frac{M_0}{2EI} x^2 + Cx + D.$$

$$\text{Bu ýerde } D = 0, C = -\frac{M_0 l}{2EI}.$$

$$\text{Onda } y = \frac{Mx^2}{2EI} - \frac{Ml}{2EI} x.$$

$$\text{Eger } x = \frac{l}{2} \Rightarrow y_{\max} = -\frac{Ml^2}{8EI} \Rightarrow M = \frac{8EI \cdot y_{\max}}{l^2} = 23 \text{ kN} \cdot \text{sm}.$$

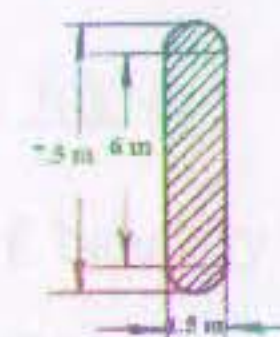
Egilmäniň esasy deňlemesinden:

$$\rho = \frac{EI}{M_0} = \frac{10^3 \cdot 230}{23} = 10^4 \text{ sm} = 100 \text{ m}.$$

6.4. $E = 8,08 \cdot 10^2 \text{ kN/sm}^2.$

Konsol balkanyň T güýçden iň uly egrelmesi

$$y_{\max} = \frac{Tl^3}{3EI} \Rightarrow E = \frac{Tl^3}{3Iy_{\max}} = \frac{240 \cdot 12^3 \cdot 10^6}{3 \cdot 0,875 \cdot 19553 \cdot 10^4} = 8,08 \cdot 10^2 \text{ kN/sm}^2.$$



6.4-nji surat

Bu ýerde

$$I = \frac{600 \cdot 150^3}{12} + \frac{3,14 \cdot 150^4}{64} = 19553 \cdot 10^4 \text{ sm}^4$$

$$6.5. a) \theta = \frac{2M_0 a}{EI}, f = \frac{4M_0 a^2}{EI};$$

$$b) \theta = \frac{13Pa^2}{2EI}, f = -\frac{41Pa^3}{3EI};$$

$$c) \theta = \frac{qa^3}{6EI}, f = -\frac{7qa^4}{24EI};$$

$$d) \theta = \frac{49qa^3}{3EI}, f = -\frac{59qa^4}{EI}$$

ç) Balkanyň birinji bölegi üçin:

$$EIy_1'' = 0, EIy_1' = C_1,$$

$$EIy_1 = C_1 x_1 + D_1.$$

Balkanyň ikinji bölegi üçin:

$$EIy_2'' = -q \frac{(x_2 - a)^2}{2}$$

$$EIy_2' = -q \frac{(x_2 - a)^3}{6} + C_2, EIy_2 = -q \frac{(x_2 - a)^4}{24} + C_2 x_2 + D_2.$$

$$\text{Eger } x_1 = x_2 = a,$$

$$\theta_c = y_1' = y_2' \text{ we } y_c = y_1 = y_2.$$

Onda ýokardaky deňlemelerden alarys:

$$C_1 = C_2 = C, D_1 = D_2 = D.$$

C we D hemişelikleri balkany berkitmek şertinden alarys:

$$x_2 = 2a \text{ bolanda } y_2^I = 0, y_2 = 0, C = \frac{qa^3}{6}, D = -\frac{7}{24}qa^4,$$

Eger $x_1 = 0$,

$$\theta_A = \frac{qa^3}{6EI} \text{ we } y_A = -\frac{7}{24EI}qa^4.$$

6.6. IN22, $\sigma_{\max} = 8,62 \text{ kN/sm}^2$.

$$y_{\max} = \frac{q\ell^4}{8EI} = \frac{\ell}{450} \Rightarrow I = \frac{459q\ell^3}{8E} = 2250 \text{ sm}^4.$$

8239-56 DÖST boýunça $I_z = 2250 \text{ sm}^4$, $W_z = 232 \text{ sm}^3$.

22-nji belgili iki tawra gabat gelyär.

Iň uly normal dartgynlyk:

$$\sigma_{\max} = \frac{M_{\max}}{W_z} = \frac{q\ell^2}{2W_z} = 8,62 \text{ kN/sm}^2 < 14 \text{ kN/sm}^2.$$

6.7. $f = -1,39 \text{ sm}$; $\theta_A = -0,0097 \text{ rad}$; $\theta_B = 0,0125 \text{ rad}$.

$$q = \frac{2Q}{\ell} = 10 \text{ kN/m}; R_A = \frac{q\ell}{8}; R_B = \frac{3}{8}q\ell.$$

Differensial deňlemeleri düzýäris we olary integrirleýäris:

$$EIy_1'' = R_A x_1, \quad EIy_2'' = R_B x_2 - q \frac{x_2^2}{2}$$

$$EIy_1' = R_A \frac{x_1^2}{2} + C_1; \quad EIy_2' = R_B \frac{x_2^2}{2} - q \frac{x_2^3}{6} + C_2;$$

$$EIy_1 = R_A \frac{x_1^3}{6} + C_1 x_1 + D_1. \quad EIy_2 = R_B \frac{x_2^3}{6} - q \frac{x_2^4}{24} + C_2 x_2 + D_2.$$

Deňlemelere girýän dört hemişelikleri kesgitlemek üçin aşakdaky şertleri ulanýarys:

a) $x_1 = 0$; $y_1 = 0$; b) $x_2 = 0$; $y_2 = 0$;

$$\zeta) x_1 = \frac{\ell}{2} \text{ we } x_2 = \frac{\ell}{2}; \theta_{\zeta} = -y_1' = y_2';$$

d) we; $f_{\zeta} = y_1 = y_2$.

Bu şertleri differensial deňlemelere goýup, C_1, C_2, D_1, D_2 bahalaryny

$$\text{tapýarys we } x = \frac{\ell}{2} \text{ bolanda } f = -\frac{5Q\ell^3}{384EI} = -1,39 \text{ sm, bu ýerde}$$

$$Q = \frac{q\ell}{2} = 20 \text{ kN}.$$

$x = 0, x = \ell$ bahalary berip θ_A we θ_B tapýarys:

$$\theta_A = -\frac{7Q\ell^2}{192EI} = -0,0097 \text{ rad}, \quad \theta_B = -\frac{9Q\ell^2}{192EI} = 0,0125 \text{ rad}.$$

$$6.8. y_{\max} = 0,0641 \frac{M\ell^2}{EI}, \quad y_{\frac{\ell}{2}} = 0,0625 \frac{M\ell^2}{EI}.$$

θ we y deňlemeler aşakdaky ýaly aňladylýar:

$$y_x = \frac{M\ell^2}{6EI} \left(\frac{x}{\ell} - \frac{x^3}{\ell^3} \right), \quad \theta_x = \frac{M\ell}{6EI} \left(1 - \frac{3x^2}{\ell^2} \right),$$

$\theta_x = 0$ deň bolanda egrelmäniň iň uly bahasy bolýar:

$$1 - \frac{3x^2}{\ell^2} = 0 \Rightarrow x = \frac{\ell}{\sqrt{3}}.$$

$$\text{Onda } y_{\max} = \frac{\ell}{9\sqrt{3}} \frac{M\ell^2}{EI} = 0,0641 \frac{M\ell^2}{EI}.$$

Balkanyň ortasyndaky egrelme:

$$y_{\frac{\ell}{2}} = \frac{M\ell^2}{15EI} = 0,0625 \frac{M\ell^2}{EI}.$$

$$6.9. P = \frac{3}{5}q\ell.$$

BÇ bölek üçin differensial deňleme düzýäris we ony integrirleýäris:

$$EIy'' = -Px - q\frac{x^2}{2}, \quad EIy' = -P\frac{x^2}{2} - q\frac{x^3}{6} + C,$$

$$EIy = \frac{Px^3}{6} - q\frac{x^4}{24} + Cx + D.$$

C we D hemişelikleri aşakdaky şertlerden tapýarys:

$$x = 0,5\ell, y = 0, \quad EIy = -\frac{P(2,5\ell)}{6} - q\frac{(0,5\ell)^4}{24} + 0,5C\ell + D = 0,$$

$$x = 2,5\ell, y = 0, \quad EIy = -\frac{P(2,5\ell)}{6} - q\frac{(2,5\ell)^4}{24} + 0,5C\ell + D = 0.$$

Bilelikde işläp alarys:

$$C = \frac{31}{24}P\ell^2 + \frac{13}{16}q\ell^3, \quad D = -\frac{5}{8}P\ell^3 + \frac{3}{8}q\ell^4.$$

Hemişelik D, koordinatlar okunyň başlangyjyndaky egrelme, şerte görä $D = 0$

$$\text{Onda } \frac{5}{8}P\ell^3 = \frac{3}{8}q\ell^4 \Rightarrow P = \frac{3}{5}q\ell.$$

$$6.10. f_{\varphi} = \frac{Pa^2(\ell + a)}{3EI}.$$

$$R_A = -\frac{Pa}{\ell}, \quad M_{x_1} = -\frac{Pa}{\ell}x_1, \quad M_{x_2} = -Px_2.$$

$$\text{Onda } U = \int_0^{\ell} \frac{M_{x_1}^2 dx}{2EI} + \int_0^a \frac{M_{x_2}^2 dx}{2EI} = \frac{P^2 a^2 (\ell + a)}{6EI}.$$

$$\text{Daşky güýjüň işi } A = A_{R_A} + A_P = A_P = \frac{1}{2}Pf_{\varphi}, \quad (A_{R_A} = 0).$$

Daşky güýjüň işi balkanyň durkuny üýtgetmesiniň doly potensial energiýasyna geçýär we $A = U$, onda

$$\frac{1}{2}Pf_{\varphi} = \frac{P^2 a^2 (1 + a)}{6EI},$$

$$\text{Bu ýerden } f_{\varphi} = \frac{Pa^2(\ell + a)}{3EI}.$$

$$6.11. U = 2,7 \text{ kN} \cdot \text{sm}.$$

$$I_z = \frac{\pi d^4}{64} = \frac{3,14 \cdot 12^4}{64} = 1017 \text{ sm}^4, \quad I_p = 2I_z = 2034 \text{ sm}^4.$$

Onda

$$U = \frac{M_k^2 \ell^2}{2GI_p} + \frac{M_{\ell}^2 \ell^2}{2EI_z} = \frac{800^2 \cdot 10^2}{2 \cdot 8,5 \cdot 2034} + \frac{600^2 \cdot 10^2}{2 \cdot 2,1 \cdot 10^4 \cdot 1017} = 2,7 \text{ kN} \cdot \text{sm}.$$

$$6.12. U = \frac{\sigma^2 A \ell}{6E}.$$

Balkada toplanan potensial energiýa

$$U = \frac{M^2 \ell}{2EI_z}, \quad \text{bu ýerde } M = \sigma W_z; \quad W_z = \frac{bh^2}{6}; \quad I_z = \frac{bh^3}{12}.$$

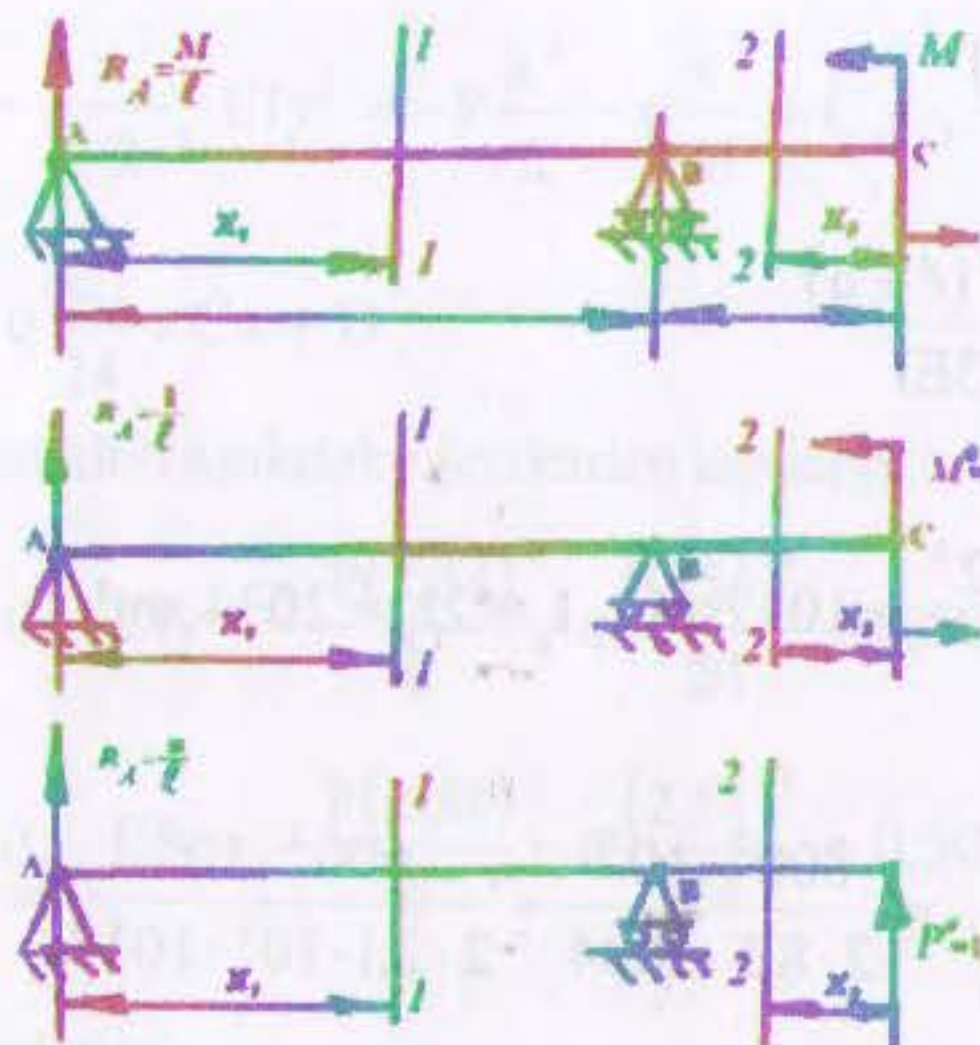
$$\text{Onda } U = \frac{\sigma^2 W_z^2 \ell}{2EI_z} = \frac{\sigma^2 A \ell}{6E}; \quad A = bh.$$

$$6.13. \theta_{\varphi} = \frac{M}{3E\ell}(\ell + 3a), \quad f_{\varphi} = \frac{Ma}{6EI}(2\ell + 3a).$$

Makswell – Mor boýunça balkanyň islendik kesigindäki ornuny üýtgetme aşakdaky formulalar bilen kesgitlenilýär:

$$\theta = \frac{1}{EI} \int_0^{\ell} M_x M_x^{\circ} dx, \quad y = \frac{1}{EI} \int_0^{\ell} M_x M_x^{\circ} dx$$

M_x° – birlik ýagdaýdaky egme moment (birlik güýçden ýa-da birlik momentden ýüklenme).



6.13-nji surat

Balkanyň hakyky ýüklenmesinden $M_{x_1} = \frac{M}{\ell} x_1$, $M_{x_2} = M$.

Birlik momentiň ýüklenmesinden $M_1^0 = \frac{1}{\ell} x_1$, $M_2^0 = 1$.

Onda gözlenýän öwrülme burç:

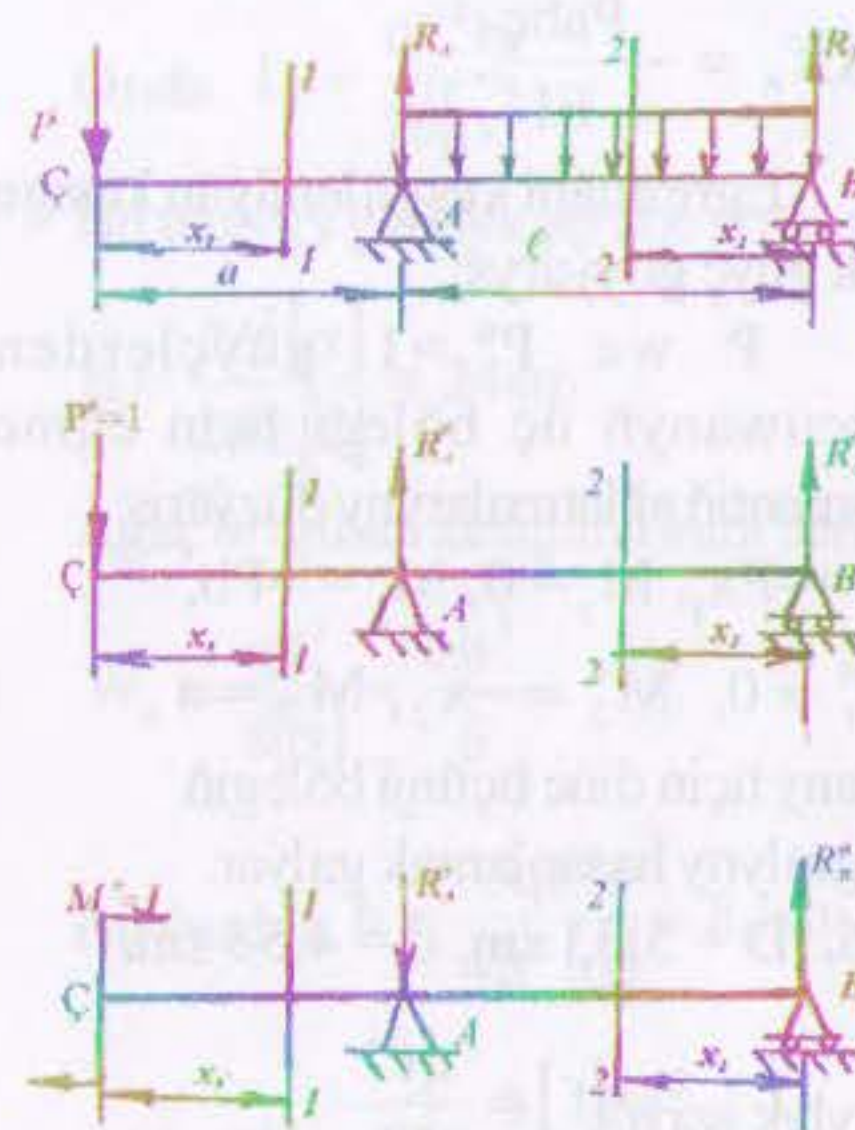
$$\theta_{\varphi} = \frac{1}{EI} \left(\int_0^{\ell} \frac{M}{\ell} x_1 \cdot \frac{1}{\ell} x_1 dx_1 + \int_0^a M \cdot 1 dx_2 \right) = \frac{M}{3EI} (\ell + 3a).$$

Balkanyň egrelmesini tapmak üçin birlik güýç bilen balkany Ç kesikde ýükleýäris we egme momentiň aňlatmasyny ýazýarys:

$$M_1^0 = \frac{1 \cdot a}{\ell} x_1, \quad M_2^0 = 1 \cdot x_2.$$

Onda idelýän egrelme:

$$f_{\varphi} = \frac{1}{EI} \left(\int_0^{\ell} \frac{M}{\ell} x_1 \cdot \frac{1 \cdot a}{\ell} x_1 dx_1 + \int_0^a M \cdot 1 \cdot x_2 dx_2 \right) = \frac{Ma}{6EI} \ell (2\ell + 3a).$$



6.14-nji surat

Birlik momentden $R_B^0 = \frac{1}{\ell}$, $M_1^0 = 1$, $M_2^0 = -\frac{x_2}{\ell}$.

$$y = \frac{1}{EI} \left[\int_0^a M_{x_1} \cdot M_1^0 dx_1 + \int_0^{\ell} M_{x_2} \cdot M_2^0 dx_2 \right] =$$

$$\begin{aligned} \text{Onda } \frac{1}{EI} \left[\int_0^a (-Px) \cdot (-x) dx + \int_0^{\ell} \left(\frac{q\ell x}{2} - \frac{Pax}{\ell} - \frac{qx^2}{2} \right) \left(-\frac{ax}{2} \right) dx \right] = \\ = \frac{Pa^2(a + \ell)}{3EI} - \frac{qa\ell^3}{24EI} = -0,667 \text{ sm}, \end{aligned}$$

$$\begin{aligned} \theta = \frac{1}{EI} \int_0^a (-Px) \cdot 1 \cdot dx + \int_0^{\ell} \left(\frac{q\ell x}{2} - \frac{Pax}{\ell} - \frac{qx^2}{2} \right) \frac{x}{\ell} dx = \\ = \frac{1}{EI} \left[-P \frac{a}{6} (3a + 2\ell) + \frac{q\ell^3}{24} \right] = 0,0062 \text{ rad} \end{aligned}$$

$$\begin{aligned} 6.14. \quad y &= -0,667 \text{ sm}, \\ \theta &= 0,0062 \text{ rad}. \end{aligned}$$

$$R_B = \frac{q\ell}{2} - P \frac{a}{\ell}$$

Berlen güýçden

$$M_{x_1} = -Px_1,$$

$$M_{x_2} = \left(\frac{q\ell}{2} - P \frac{a}{\ell} \right) x_2 - q \frac{x_2^2}{2}.$$

Birlik güýçden $R_B^0 = \frac{a}{\ell}$,

$$M_1^0 = -1 \cdot x_1, \quad M_2^0 = -\frac{a}{1} x_2.$$



6.15-nji surat

$$6.15. f_A = -\frac{Pab\zeta}{EI}$$

Egrelmäni kesgitlenilýän kesige birlik güýç goýýarys:

P we $P^0=1$ güýçlerden çarçuwanyň üç bölegi üçin egme momentiniň aňlatmalaryny düzýäris:

$$M_1 = -Px_1, M_2 = 0, M_3 = -Pb,$$

$$M_1^0 = 0, M_2^0 = -x_2, M_3^0 = a$$

bolany üçin diňe üçünji bölegiň integralyny hasaplamak galýar.

$$6.16. D = 5,33 \text{ sm}, d = 4,53 \text{ sm}.$$

$$\text{Gatylyk şerti } [f] = \frac{q\ell^4}{8EI_z}$$

$$I_z = \frac{\pi D^4}{64} (1 - \alpha^4). \text{ Turbanyň ýüküniň depgini}$$

$$q = \frac{\pi D^2}{4} (1 - \alpha^4) \gamma_{\text{pol}} + \frac{\pi (\alpha D)^2}{4} \gamma_s.$$

$$\text{Onda } D = \sqrt{\frac{[(1 - \alpha^2) \gamma_p + \alpha^2 \gamma_s] 2\ell}{0,003E(1 - \alpha^4)}} = 5,33 \text{ sm},$$

$$\text{we } D = d\alpha = 5,33 \cdot 0,85 = 4,53 \text{ sm}.$$

$$6.17. b = 8,1 \text{ sm}, h = 24 \text{ sm}.$$

$$\text{Gatylyk şerti } [f] = \frac{5q\ell^4}{384EI}$$

$$\text{Berklik şerti } [\sigma] = \frac{M_{\max}}{W_z} = \frac{q\ell^2}{8W_z}, \quad W_z = \frac{I_z \cdot 2}{h}.$$

$$\text{Onda } I_z = \frac{q\ell^2 h}{16[\sigma]}.$$

Bu ululygy gatylyk şertine goýup alarys:

$$h = \frac{5\ell^2 [\sigma]}{24E[f]} \approx 24 \text{ sm}.$$

Agaç örtgüniň kesiginiň inini berklik şertinden tapýarys:

$$W_z = \frac{q\ell^2}{8[\sigma]} = \frac{bh^2}{6}.$$

$$\text{Bu ýerden } b = \frac{3q\ell^2}{4h^2 [\sigma]} = 8,1 \text{ sm}.$$

$$6.18. \theta_{\max} = -\frac{3}{2} \cdot \frac{P\ell^2}{Eh^3 b} \quad \text{we} \quad f_{\max} = -\frac{3}{8} \cdot \frac{P\ell^3}{Eh^3 b}.$$

$$M_x = \frac{P}{2} x; \quad I_x = \frac{b_x h^2}{12}; \quad W_x = \frac{b_x h^2}{6} = \frac{Px}{2[\sigma]} \Rightarrow b_x = \frac{3Px}{h^2 [\sigma]},$$

$$x=0 \Rightarrow b_x=0; \quad x=\frac{\ell}{2} \Rightarrow b = \frac{3}{2} \cdot \frac{P\ell}{h^2 [\sigma]} \Rightarrow [\sigma] = \frac{3}{2} \cdot \frac{P\ell}{h^2 [\sigma]}.$$

$$\text{Onda } I_x = \frac{b_x h^2}{12} = \frac{Phx}{4[\sigma]}.$$

$$Ey'' = \frac{M_x}{I_x} = \frac{2[\sigma]}{h} \Rightarrow \frac{Eh}{2[\sigma]} y'' = 1,$$

$$\frac{Eh}{2[\sigma]} y' = x + C \quad \text{we} \quad \frac{Eh}{2[\sigma]} y = \frac{x^2}{2} + Cx + D,$$

$$x=0, y=0 \Rightarrow D=0; \quad x=\frac{\ell}{2}, y'=0 \Rightarrow C = -\frac{\ell}{2}.$$

Şonuň üçin hem

$$\theta_{\max} = \theta_A = -\theta_B = (y')_{x=0} = \frac{2C[\sigma]}{Eh} = -\frac{\ell[\sigma]}{Eh}$$

$$f_{\max} = (y)_{x=\frac{\ell}{2}} = -\frac{\ell^2[\sigma]}{4Eh},$$

$[\sigma]$ -yn ýokarda tapylan bahasyny goýup alarys:

$$\theta_{\max} = -\frac{3}{2} \cdot \frac{P\ell^2}{Eh^3b} \quad \text{we} \quad f_{\max} = -\frac{3}{8} \cdot \frac{P\ell^3}{Eh^3b}.$$

$$\mathbf{6.19.} \quad EIy = -\frac{q\ell^3}{2}(x \ln x - x - x \ln \ell + \ell), \quad f_{\max} = -\frac{q\ell^4}{2EI_0}.$$

Deň garşylykly balkanyň islendik kesiginde

$$\sigma_{\max} = \frac{6M_x}{bh_x^2} = \text{const},$$

$$h_x = h \cdot \frac{x}{\ell}.$$

Onda balkanyň erkin tarapyndan x we ℓ uzaklykdaky kesiklerde $\sigma_x = \sigma_\ell$

$$\text{we} \quad \frac{qx^2 \cdot 6}{2bh_x^2} = \frac{q\ell^2 \cdot 6}{2bh^2}.$$

$$\text{Onda} \quad EI_0 y'' = -\frac{q\ell^3}{2} \cdot \frac{1}{x},$$

$$EI_0 y' = -\frac{q\ell^3}{2} \ln x + C.$$

$$\text{Eger } x = \ell \rightarrow y' = 0 \Rightarrow C = \frac{q\ell^3}{2} \ln \ell.$$

$$\text{Onda} \quad EI_0 y' = -\frac{q\ell^3}{2} \ln x + \frac{q\ell^3}{2} \ln \ell.$$

Ikinji gezek integrirläp alarys:

$$EIy = -\frac{q\ell^3}{2} x \ln x + \frac{q\ell^3}{2} x \ln \ell + D,$$

$$x = \ell, \quad y = 0 \Rightarrow D = \frac{q\ell^4}{2}.$$

$$\text{Onda} \quad EIy = -\frac{q\ell^3}{2}(x \ln x - x - x \ln \ell + \ell),$$

$$x = 0, \quad f_{\max} = -\frac{q\ell^4}{2EI_0}.$$

$$\mathbf{6.20.} \quad f_{\max} = -1,2 \text{ sm.}$$

Islendik kesikde $M_x = -x^2$, $h_x = 9 + 0,05x$,
 $I_x = 0,5(9 + 0,05x)^3$

$$\text{Onda} \quad y'' = -\frac{2x^2}{E(9 + 0,05x)^3}.$$

$$\text{Belleýäris: } a = \frac{2}{E}; \quad b = 9, \quad \zeta = 0,05 \text{ onda } y'' = -\frac{ax^2}{(b + \zeta x)^3}.$$

Bir gezek integrirläp alarys:

$$y' = -\frac{a}{\zeta^3} \left[\ln(b + \zeta x) + \frac{2b}{b + \zeta x} - \frac{b^2}{2(b + \zeta x)^2} \right] + C,$$

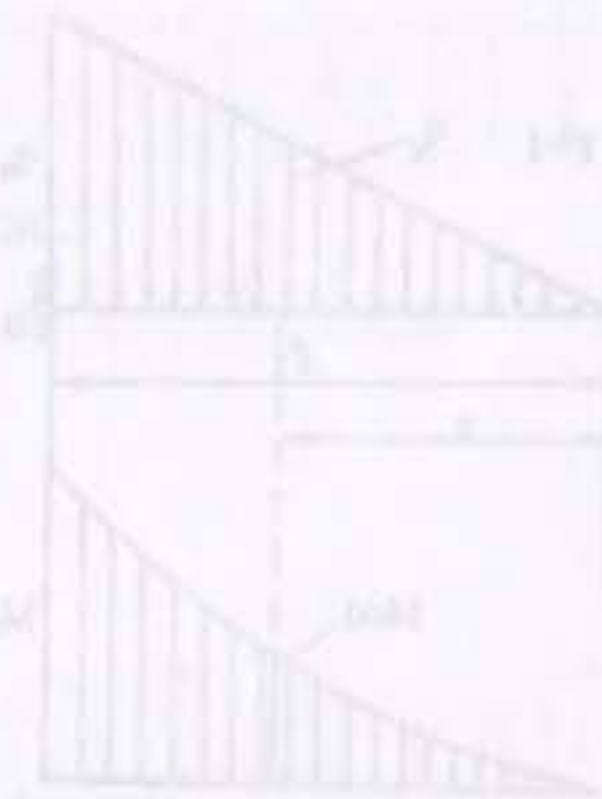
$$x = \ell, \quad y' = 0.$$

$$\text{Onda} \quad C = -\frac{a}{\zeta^3} \left[\ln(b + \zeta \ell) + \frac{2\ell}{b + \zeta \ell} - \frac{b^2}{2(b + \zeta \ell)^2} \right].$$

Ikinji gezek integrirläp alarys:

$$y = -\frac{a}{\zeta^3} \left[\left(x + \frac{3b}{\zeta} \right) \ln(b + \zeta x) - x + \frac{b^2}{2\zeta(b + \zeta x)} \right] + Cx + D,$$

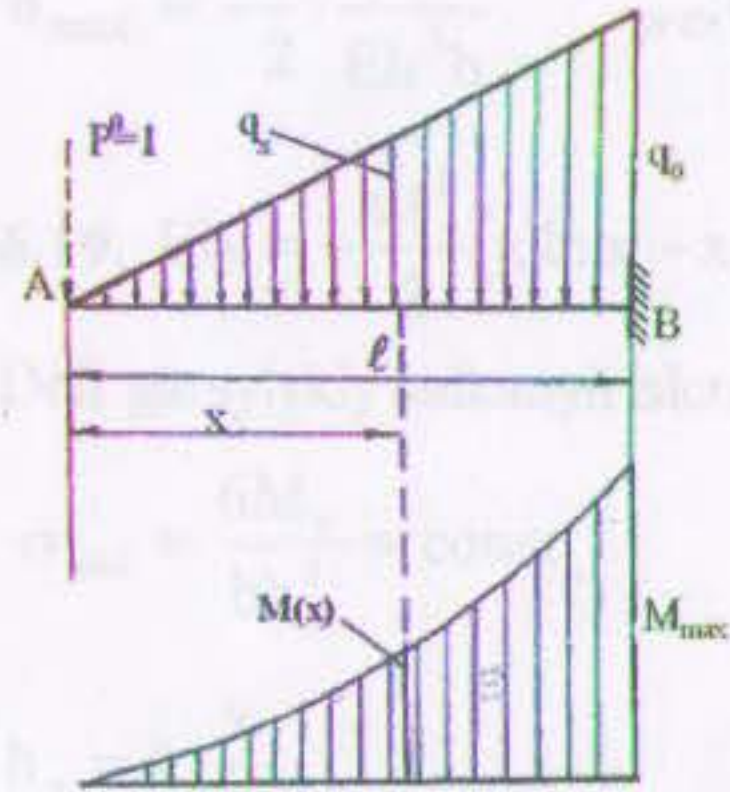
$$x = \ell, \quad y = 0,$$



$$D = -\frac{a}{\zeta^3} \left[\left(\ell + \frac{3b}{\zeta} \right) \ln(b + \zeta \ell) - \ell + \frac{b^2}{2\zeta(b + 2\zeta)} \right] - \zeta \ell.$$

a, b, c, C we D bahalaryny goýup we $x = 0$ baha berip alarys:

$$f_{\max} = -\frac{a}{\zeta^3} \left(\frac{3b}{\zeta} \ln b + \frac{b}{2\zeta} \right) + D = 1,2 \text{ sm.}$$



6.21-nji surat

$$6.21. f_A = \frac{q_0 \ell^4}{30EI}, \theta_A = \frac{q_0 \ell^3}{24EI}.$$

$$M_x = -q_0 \frac{x^3}{6\ell},$$

$$M_1^0 = -x, M_2^0 = -1,$$

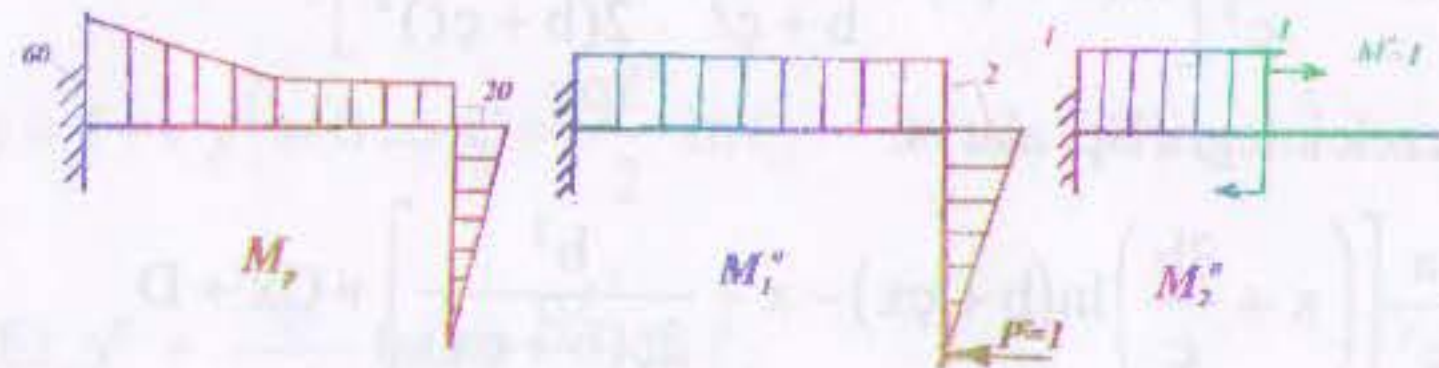
$$f_A = \frac{1}{EI} \int_0^\ell -\frac{q_0 x^3}{6\ell} (-x) dx = \frac{q_0 \ell^4}{30EI},$$

$$\theta_A = \frac{1}{EI} \int_0^\ell -\frac{q_0 x^3}{6\ell} (-1) dx = \frac{q_0 \ell^3}{24EI}.$$

$$6.22. U = 53,40 \text{ kN} \cdot \text{sm.}$$

$$U = A = \frac{1}{2} P \left(f + \frac{1}{2} \lambda \right) = \frac{P^2 \ell^2}{96EI} + \frac{P^2 R^3 n}{2Gr^4} = 53,40 \text{ kN} \cdot \text{sm.}$$

$$6.23. f_A = 4,45 \text{ sm}, \theta_A = 0,0133 \text{ rad.}$$



6.23-nji surat

Wereşaginiň usulyny peýdalanyp alarys:

$$\Delta_{ip} = \sum \frac{\omega_p \cdot M_\zeta^0}{EI}.$$

$$\text{Onda } f_A = \frac{\left[\frac{1}{2} \cdot 20 \cdot 2 \cdot \frac{2}{3} \cdot 2 + 20 \cdot 2 \cdot 2 \cdot 2 + \frac{1}{2} \cdot 40 \cdot 2 \cdot 2 \right] 10^6}{2 \cdot 10^4 \cdot 3000} = 4,45 \text{ sm},$$

$$\theta_A = \frac{\left[20 \cdot 2 \cdot 1 + \frac{1}{2} \cdot 40 \cdot 2 \cdot 1 \right] 10^4}{2 \cdot 10^4 \cdot 3000} = 0,0133 \text{ rad.}$$

$$6.24. M_2 = 2M_1.$$

$$6.25. \text{a) } y = \frac{\alpha t}{h} \cdot \frac{\ell^2}{2}, \text{ b) } y = \frac{\alpha t}{h} \cdot \frac{\ell^2}{8}.$$

$$\text{Moruň integralyny ulanýarys: } y = \int_\ell \frac{M_x M^0}{EI_x} dx.$$

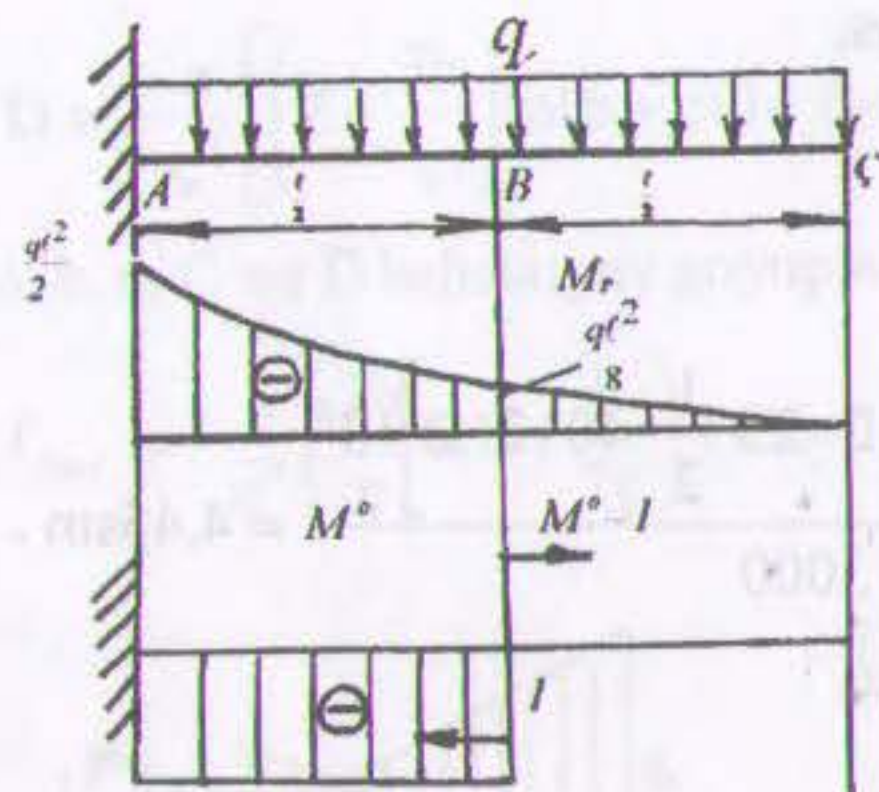
$$\text{Egilme nazaryýetinden } \frac{M_x}{EI_x} = \frac{1}{\rho}, \text{ ýöne } \frac{1}{\rho} = \frac{\varepsilon_t}{y}, \varepsilon_t = \alpha t, y = \frac{h}{2}.$$

$$\text{Onda } y = \int_\ell \frac{\alpha t}{h} M^0 dx.$$

$$\text{Birinji balka üçin } M_1^0 = x,$$

$$y_1 = \frac{\alpha t}{h} \int_0^\ell x dx = \frac{\alpha t}{h} \cdot \frac{\ell^2}{2}.$$

$$\text{Ikinji balka üçin } M_2^0 = \frac{x}{2}, \text{ onda } y_2 = \frac{\alpha t}{h} \cdot 2 \int_0^\ell \frac{x}{2} dx = \frac{\alpha t}{h} \cdot \frac{\ell^2}{8}.$$



6.26-njy surat

$$6.26. \theta_B = \frac{1}{8} \cdot \frac{q l^2}{EI}$$

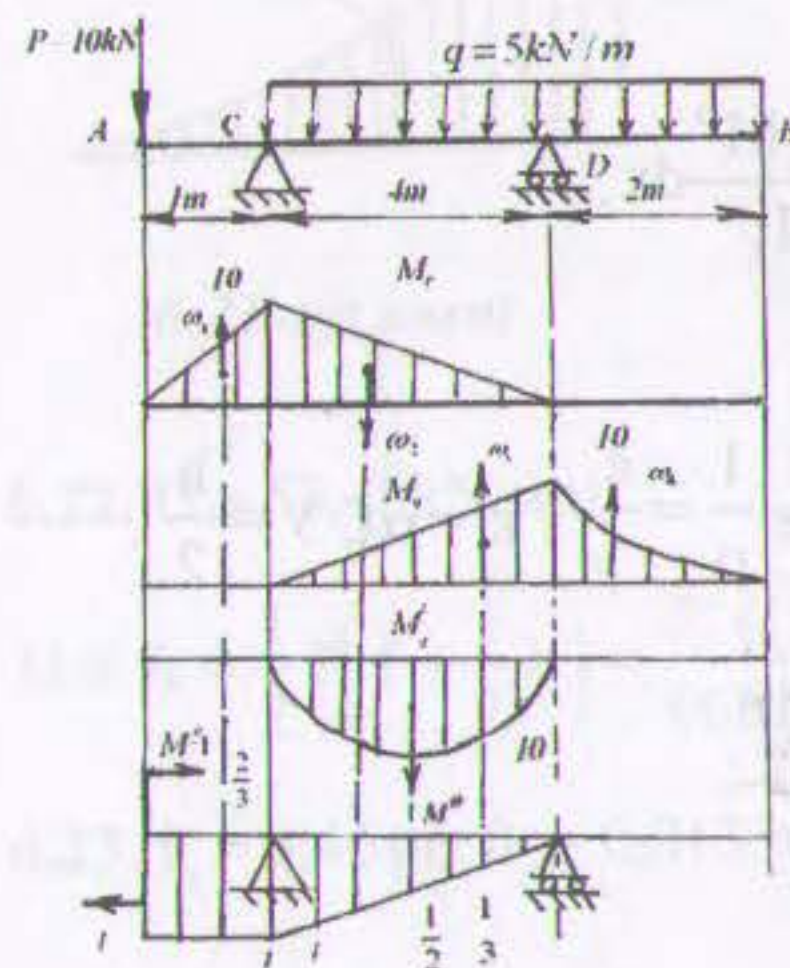
Wereşaginiň formulasy:

$$\theta = \sum \frac{\omega_p \cdot M_c^0}{EI}$$

$$\omega_p = -\frac{q l^2}{8} \cdot \frac{l}{2} - \frac{1}{3} \cdot \frac{3 q l^2}{8} \cdot \frac{l}{2} = -\frac{q l^3}{8}$$

$$M_c^0 = -1$$

$$\text{Onda } \theta_B = \frac{q l^2}{8 EI}$$



6.27-nji surat

$$6.27. \theta_A = -\frac{7}{2400} \text{ rad.}$$

Güýçleriň täsirini goşmak ýörelgesini ulanyp, balka täsir edýän güýçleriň egme momentiniň epýurlaryny aýratynlykda gurýarys.

Berlen güýçlerden gurlan epýurlaryň meýdanlary:

$$\omega_1 = \frac{1}{2} \cdot 10 \cdot 1 = 5 \text{ kN} \cdot \text{m}^2,$$

$$\omega_2 = \frac{1}{2} \cdot 10 \cdot 4 = 20 \text{ kN} \cdot \text{m}^2,$$

$$\omega_3 = \frac{1}{2} \cdot 10 \cdot 4 = 20 \text{ kN} \cdot \text{m}^2,$$

$$\omega_4 = \frac{1}{3} \cdot 10 \cdot 2 = \frac{20}{3} \text{ kN} \cdot \text{m}^2,$$

$$\omega_5 = \frac{2}{3} \cdot 10 \cdot 4 = \frac{80}{3} \text{ kN} \cdot \text{m}^2.$$

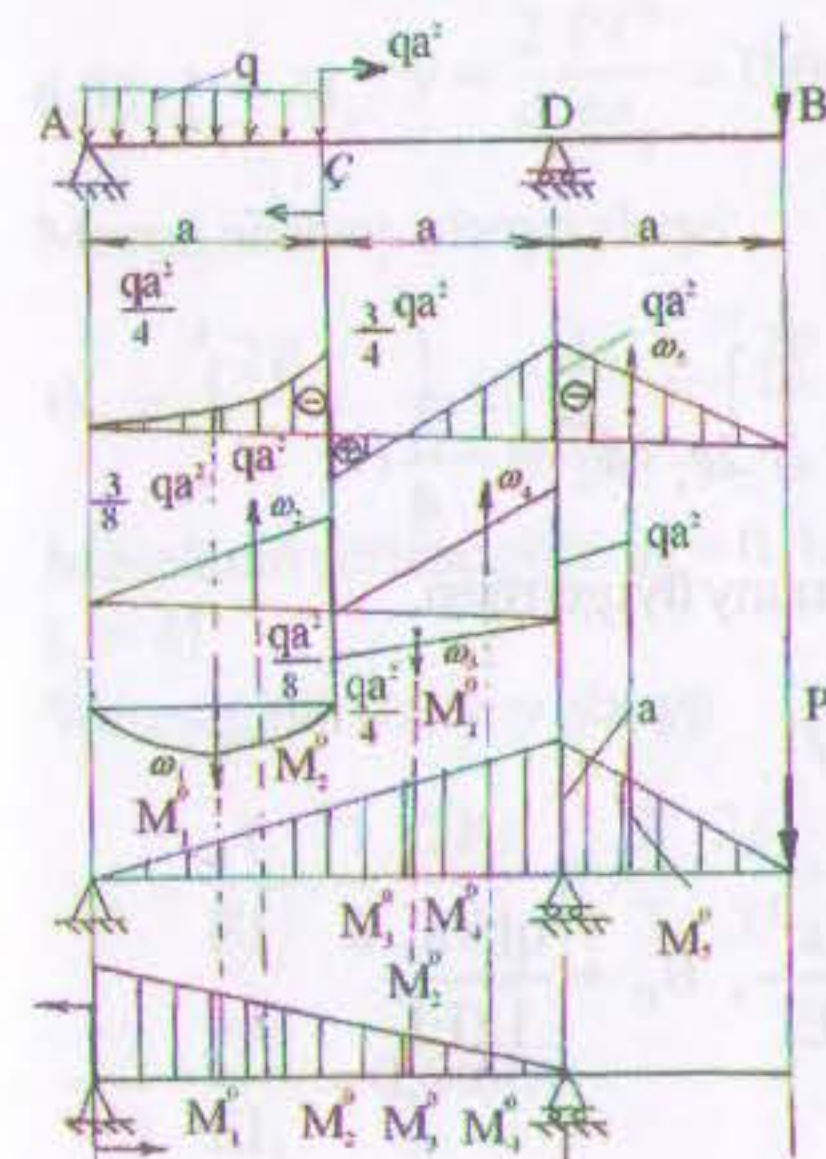
Birlik momentden epýur gurup, M_c^0 ordinatalaryny belleýäris.

Hasaplama geçirýäris:

$$EI \theta_A = -5 \cdot 1 - 20 \cdot \frac{2}{3} - 20 \cdot \frac{1}{3} + \frac{80}{3} \cdot \frac{1}{2} = -\frac{35}{3} \text{ kN} \cdot \text{m}^2,$$

$$\theta_A = -\frac{35}{3 EI} = -\frac{35 \cdot 10^4}{32 \cdot 10^4 \cdot 2 \cdot 10^3} = -\frac{35}{12000} = -\frac{7}{2400} \text{ rad.}$$

$$6.28. y_B = \frac{37}{48} \cdot \frac{q a^4}{EI}, \theta_B = \frac{11}{48} \cdot \frac{q a^3}{EI}.$$



6.28-nji surat

AB we ÇD böleklerde egme momentiň epýuryny ýönekeý epýurlara dargadýarys we olaryň meýdanlaryny kesgitleýäris:

$$\omega_1 = \frac{q a^3}{12}, \omega_2 = -\frac{3}{8} q a^3,$$

$$\omega_3 = -\frac{1}{8} q a^3, \omega_4 = -\frac{1}{2} q a^3,$$

$$\omega_5 = \frac{1}{2} q a^3.$$

Ýokarky meýdanlaryň agyrlık merkezine degişli birlik güýçden gurlan egme momentleriň ordinatalary:

$$M_1^0 = -\frac{1}{3} a, M_2^0 = -\frac{1}{4} a,$$

$$M_3^0 = -\frac{2}{3}a, \quad M_4^0 = -\frac{5}{6}a, \quad M_5^0 = -\frac{2a}{3}.$$

B nokatdaky gözlenýän egrelme:

$$y_B = \sum \frac{\omega_p M_c^0}{EI} = \frac{1}{EI} (\omega_1 M_1^0 + \omega_2 M_2^0 + \dots + \omega_5 M_5^0) = \frac{37}{48} \cdot \frac{qa^4}{EI}.$$

M_2^0 epýuryndan alarys:

$$M_1^0 = -\frac{2}{3}, \quad M_2^0 = -\frac{3}{4},$$

$$M_3^0 = -\frac{1}{3}, \quad M_4^0 = -\frac{1}{6}.$$

Onda gözlenýän öwrülme burçy:

$$\theta_A = \frac{1}{EI} (\omega_1 M_1^0 + \omega_2 M_2^0 + \omega_3 M_3^0 + \omega_4 M_4^0) = \frac{11}{48} \cdot \frac{qa^3}{EI}.$$

$$6.29. \quad y_C = \frac{q\ell^3}{8EI} (4h + \ell).$$

Epýurlardan alarys:

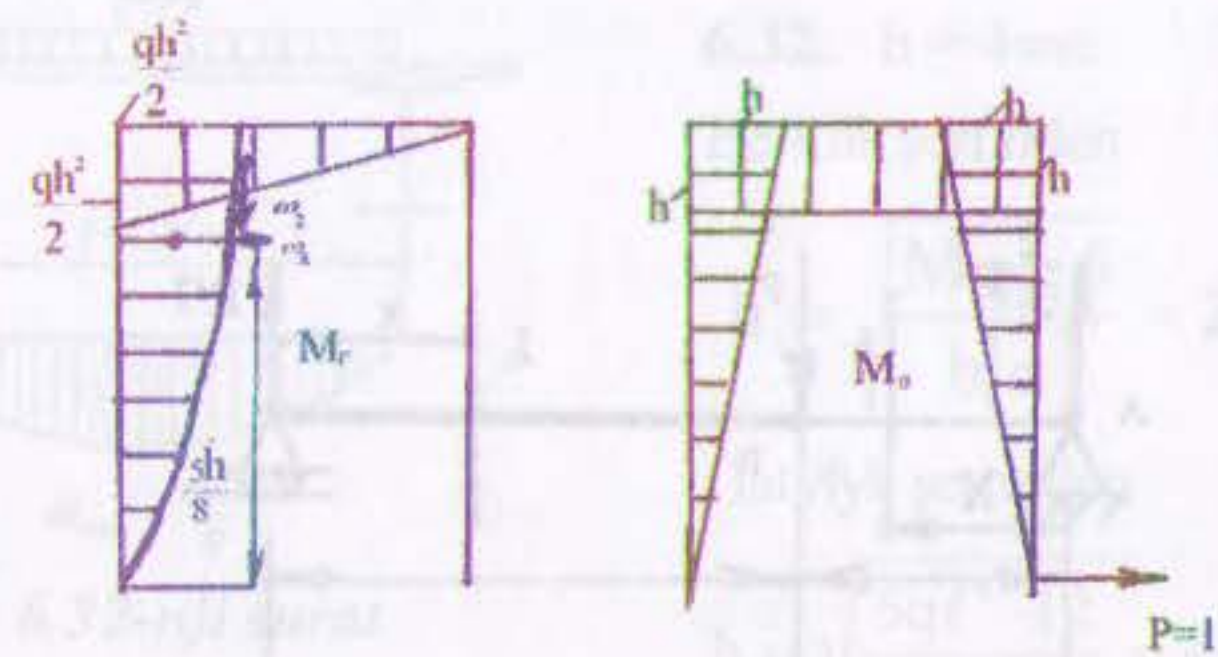
$$\omega_1 = -\frac{q\ell^2 h}{2}, \quad \omega_2 = -\frac{q\ell^3}{6}, \quad M_1^0 = -\ell, \quad M_2^0 = -\frac{3}{4}\ell.$$

Onda çarçuwanyň Ç kesiginiň wertikal ornuny üýtgetmesi.

$$y_C = \frac{1}{EI} (\omega_1 M_1^0 + \omega_2 M_2^0) = \frac{q\ell^2}{8EI} (4h + \ell).$$

$$6.30. \quad \Delta_B = \frac{qh^3}{24EI} (5h + 6a); \quad y_C = \frac{qh^2 a^2}{32EI}, \quad \theta_D = \frac{qh^2 a}{12EI}.$$

$$\text{Epýurlardan } \omega_1 = \frac{qh^3}{3}, \quad \omega_2 = \frac{qh^2 a}{4},$$



6.30-njy surat

$$\text{Onda } \Delta_B = \frac{1}{EI} \left(\frac{qh^3}{3} \cdot \frac{5}{8}h + \frac{qh^2 a}{4} \right) = \frac{qh^3}{24EI} (5h + 6a).$$

Kesgitlemek talap edilyän beýleki ornuny üýtgetmeler ýokardaky zygiderlilikde hasaplanylýar.

$$6.31. \quad I_2 = 4I_1, \quad y = \frac{2P\ell^3}{9EI_1} = 0,6\text{mm}.$$

Moruň usulyny ulanyp alarys:

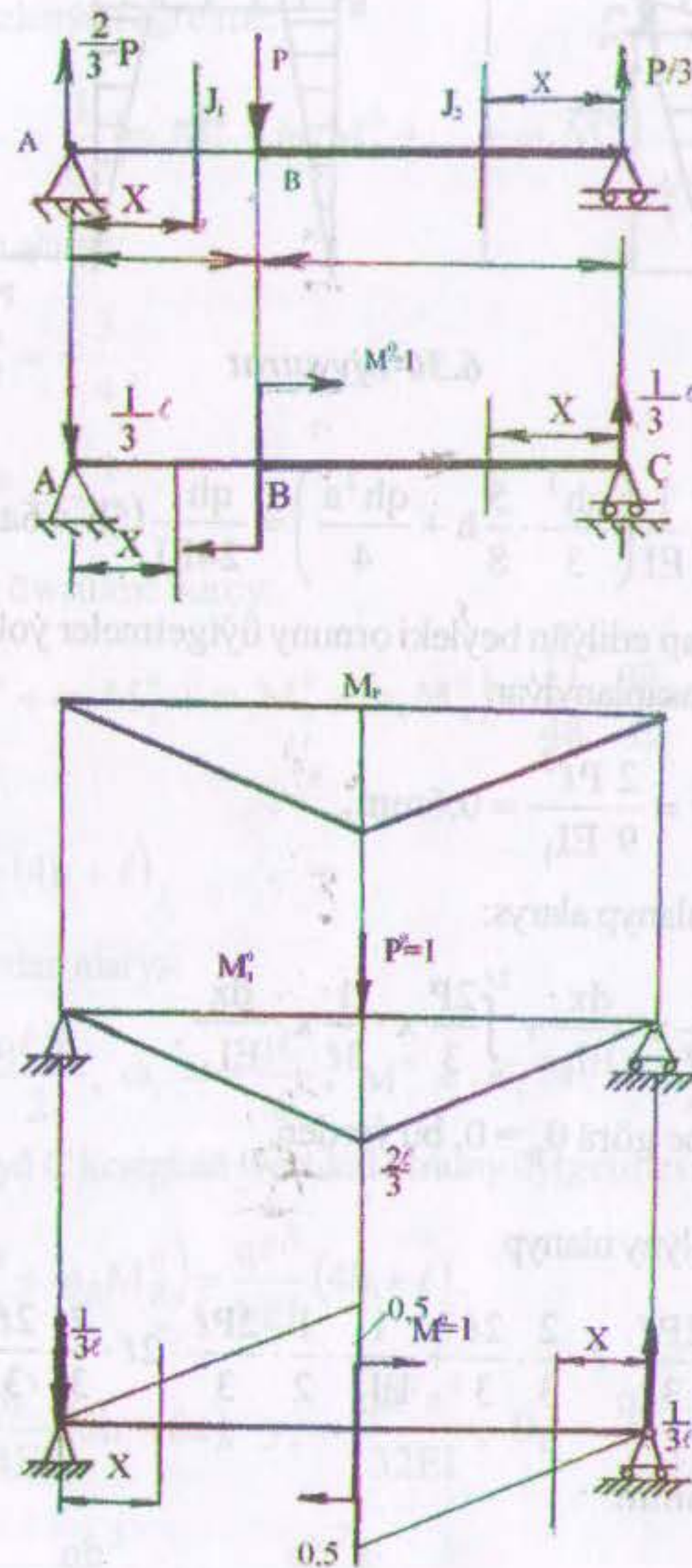
$$\theta_B = \int_0^\ell \frac{2P}{3} x \cdot \frac{1}{3\ell} x \cdot \frac{dx}{EI_1} + \int_0^{2\ell} \frac{2P}{3} x \cdot \frac{1}{3\ell} x \cdot \frac{dx}{EI_2}.$$

Meseläniň şertine görä $\theta_B = 0$, bu ýerden,

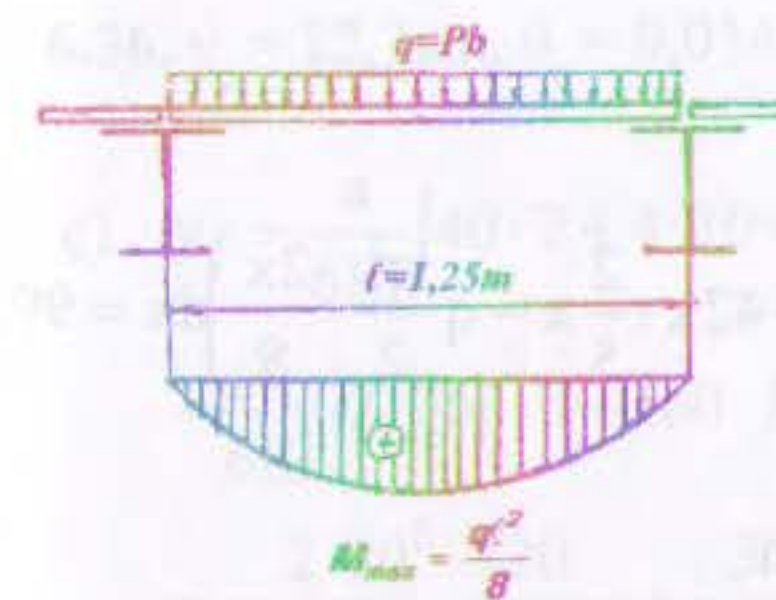
$$I_2 = 4I_1.$$

Weraşaginiň usulyny ulanyp

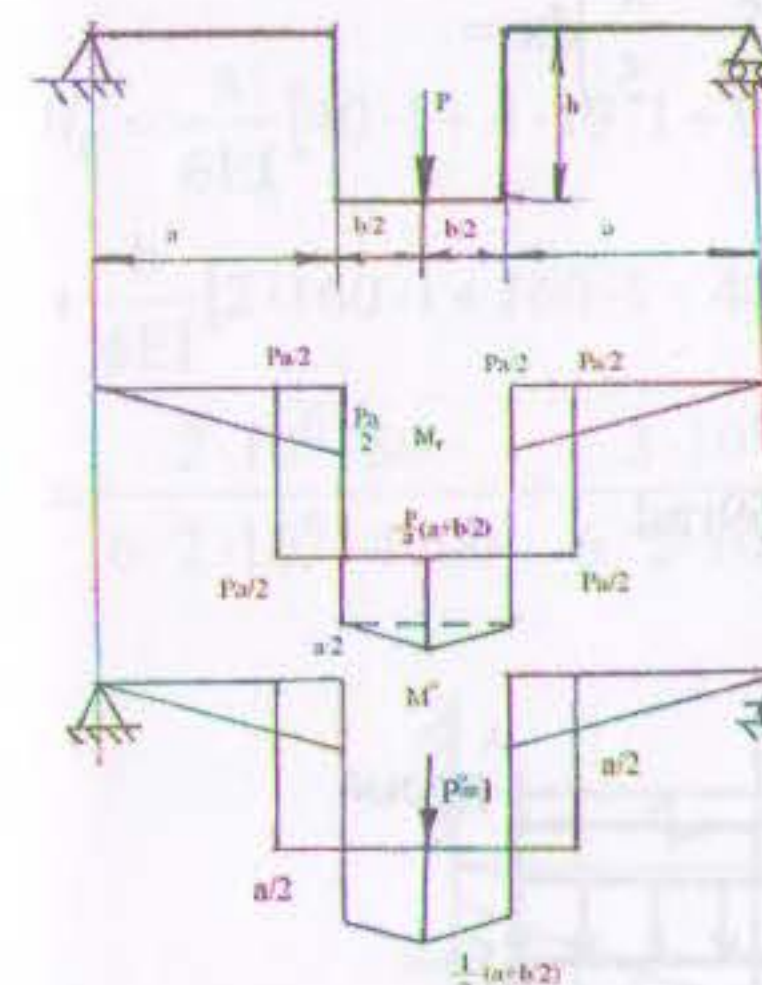
$$y_B = \frac{1}{EI_1} \cdot \frac{1}{2} \cdot \frac{2P\ell}{3} \cdot \ell \cdot \frac{2}{3} \cdot \frac{2\ell}{3} + \frac{1}{EI_2} \cdot \frac{1}{2} \cdot \frac{2P\ell}{3} \cdot 2\ell \cdot \frac{2}{3} \cdot \frac{2\ell}{3} = \frac{2}{9} \cdot \frac{P\ell^3}{EI_1} = 0,6\text{mm}.$$



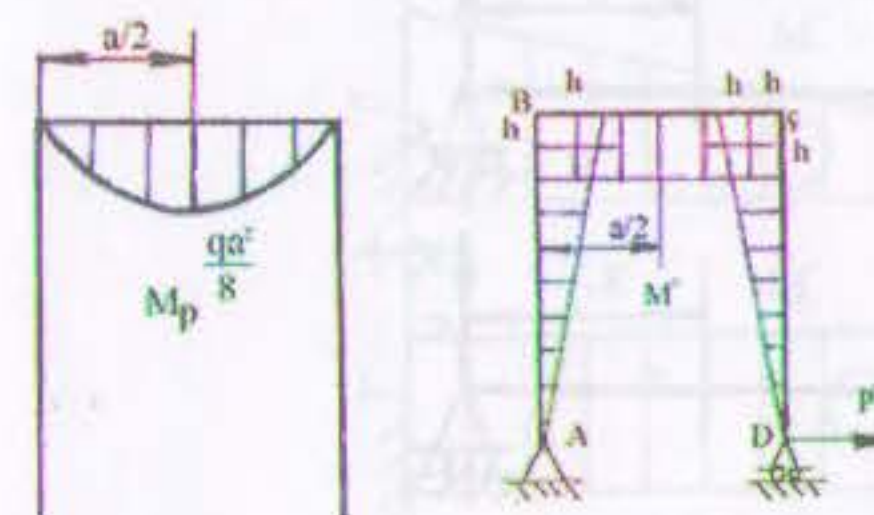
6.31-nji surat



6.32-nji surat



6.33-nji surat



6.34-nji surat

6.32. $h = 4 \text{ sm}$.

Berklik şertinden

$$h = \sqrt{\frac{M_{\max} 6}{b[\sigma]}} = 2,9 \text{ sm}.$$

Gatylyk şertinden

$$h = \sqrt[3]{\frac{5q\ell^4 \cdot 12}{384E[f]b}} = 4 \text{ sm},$$

$h = 4 \text{ sm}$ kabul edýäris.

$$6.33. f = \frac{P(2a+b)^3}{48EI} + \frac{Pa^2h}{2EI}.$$

$$f = 2 \frac{1}{EI} \left(\frac{Pa}{2} \cdot a \cdot \frac{2}{3} \cdot \frac{a}{2} + 2 \frac{Pa}{2} \cdot h \cdot \frac{a}{2} \right) + \frac{1}{EI} \cdot \frac{Pa}{2} \cdot b \cdot \frac{1}{2} \left(a + \frac{b}{2} \right) + 2 \frac{Pb}{4} \cdot \frac{b}{2} \cdot \frac{b}{4} \cdot \frac{2}{3} = \frac{P(2a+b)^3}{48EI} + \frac{Pa^2h}{2EI}.$$

$$6.34. \Delta_B = \frac{qa^3h}{12EI}.$$

$$\Delta_B = \frac{\omega_p M_c^0}{EI} = \frac{2}{3} \cdot \frac{qa^2}{8} \cdot a \cdot \frac{h}{EI} = \frac{qa^3h}{12EI}$$

6.35. $y_A = 1,2375 \text{ sm}$, $\theta_B = 0,00769 \text{ rad}$.

Moruň usulyny ulanyrys:

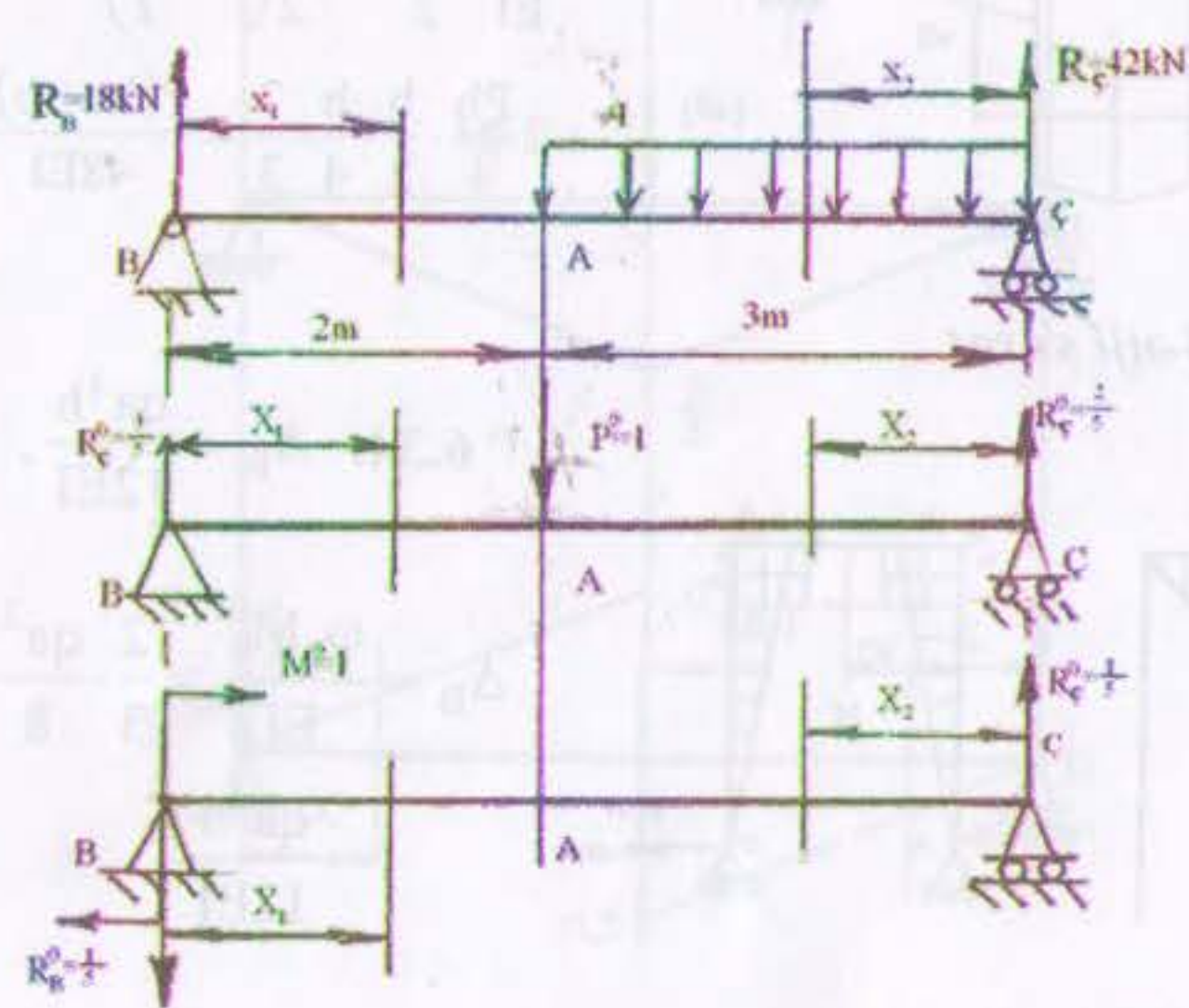
$$EI y_A = \int_0^{\ell} M_p \cdot M^{\circ} dx = \int_0^2 18x \cdot \frac{2}{5}x \cdot dx + \int_0^3 \left(42x \cdot \frac{2}{5}x - q \frac{x^2}{2} \cdot \frac{2x}{5} \right) dx = 99;$$

$$y_A = \frac{99}{EI} = \frac{99 \cdot 10^6}{2 \cdot 10^4 \cdot 4000} = \frac{99}{80} = 1,2375 \text{ sm},$$

$$EI \theta_A = \int_0^2 18x \cdot \left(1 - \frac{x}{5} \right) dx + \int_0^3 \left(42x \cdot \frac{x}{5} - q \frac{x^2}{2} \cdot \frac{x}{5} \right) dx =$$

$$= \left[9x^2 - \frac{6}{5}x^3 \right]_0^2 + \left[\frac{14}{5}x^3 - \frac{x^4}{2} \right]_0^3 = 615;$$

$$\theta_B = \frac{615}{EI} = \frac{615 \cdot 10^4}{2 \cdot 10^4 \cdot 400} = \frac{61,5}{8000} = 0,00769 \text{ rad}.$$



6.35-nji surat

6.36. $y_{\zeta} = 12,3 \text{ sm}$, $\theta_{\zeta} = 0,034 \text{ rad}$.

$$\zeta) y_{\zeta} = \frac{a}{6EI} [40 \cdot 2 + 4 \cdot 10 \cdot 1 + 0 \cdot 0] +$$

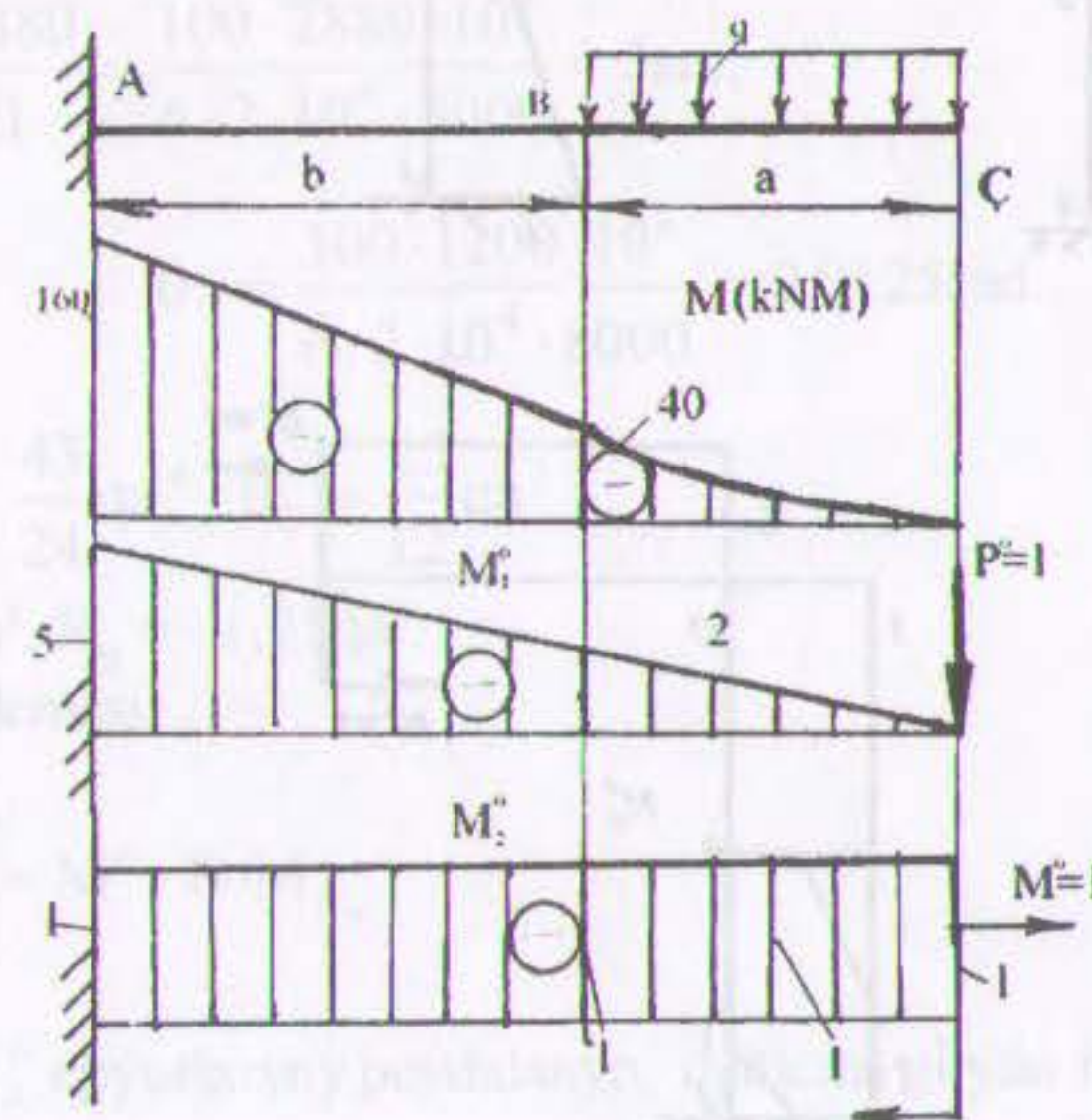
$$+ \frac{b}{6EI} [2 \cdot 160 \cdot 5 + 160 \cdot 2 + 40 \cdot 5 + 2 \cdot 40 \cdot 2] =$$

$$= \frac{2 \cdot 10^6 \cdot 120}{6 \cdot 2 \cdot 10^4 \cdot 4800} + \frac{3 \cdot 10^6 \cdot 2280}{6 \cdot 2 \cdot 10^4 \cdot 4800} = 12,3 \text{ sm},$$

$$\theta_{\zeta} = \frac{a}{6EI} [40 \cdot 1 + 4 \cdot 10 \cdot 1 + 0 \cdot 1] +$$

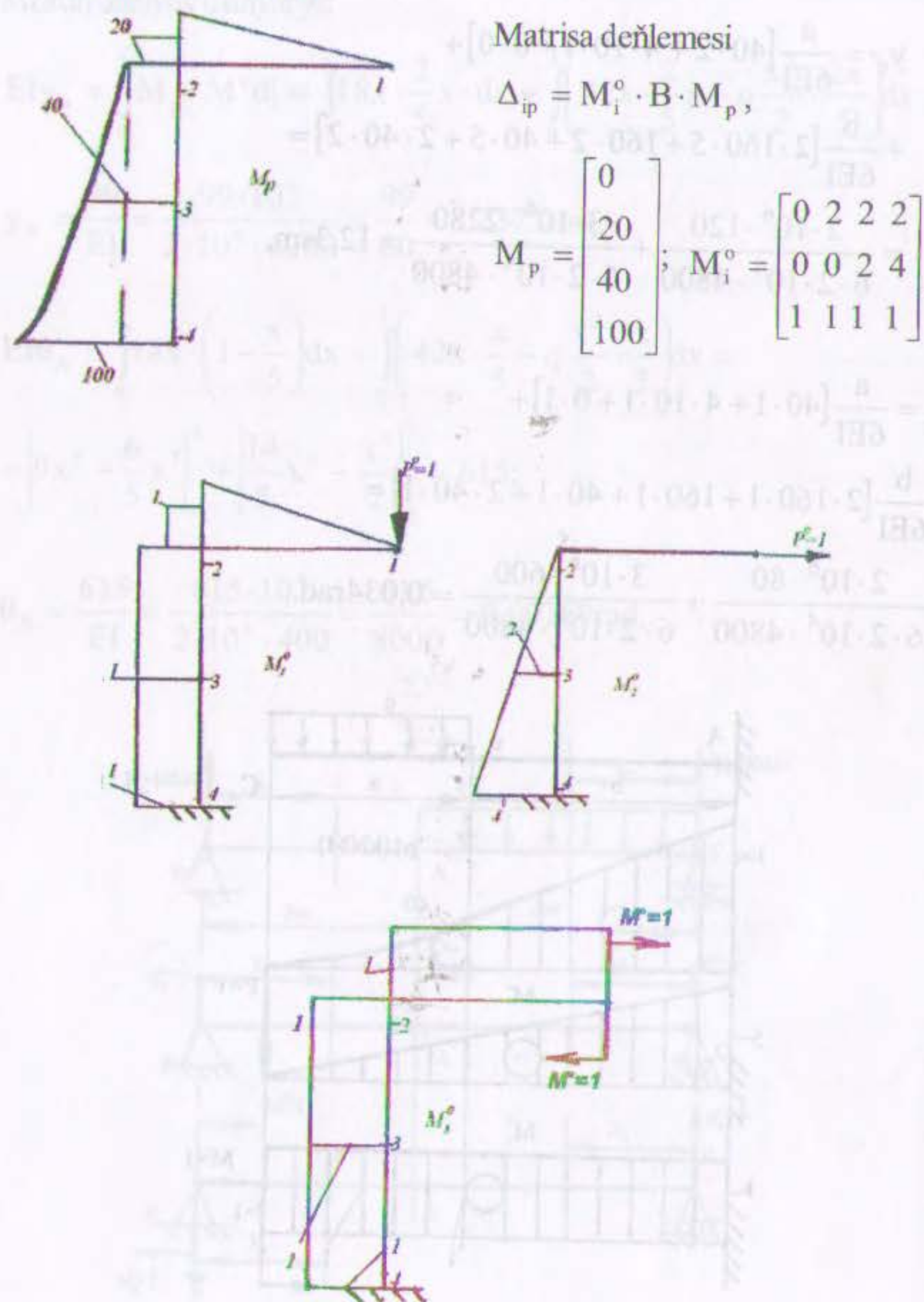
$$+ \frac{b}{6EI} [2 \cdot 160 \cdot 1 + 160 \cdot 1 + 40 \cdot 1 + 2 \cdot 40 \cdot 1] =$$

$$= \frac{2 \cdot 10^6 \cdot 80}{6 \cdot 2 \cdot 10^4 \cdot 4800} + \frac{3 \cdot 10^6 \cdot 600}{6 \cdot 2 \cdot 10^4 \cdot 4800} = 0,034 \text{ rad}.$$



6.36-nji surat

6.37. $y_{\text{wert}} = 1,21\text{sm}$, $y_{\text{gor}} = 3\text{sm}$, $\theta = 0,0125\text{rad}$.



6.37-nji surat

Ýumşaklyk matrisasy

$$B = \begin{bmatrix} b_I & 0 \\ 0 & b_{II} \end{bmatrix} = \frac{a}{6EI} \begin{bmatrix} 2 & 1 & 0 & 0 & 0 \\ 1 & 2 & 0 & 0 & 0 \\ 0 & 0 & 4 & 0 & 0 \\ 0 & 0 & 0 & 16 & 0 \\ 0 & 0 & 0 & 0 & 4 \end{bmatrix} = \frac{a}{6EI} \begin{bmatrix} 2 & 1 & 0 & 0 \\ 1 & 6 & 0 & 0 \\ 0 & 0 & 16 & 0 \\ 0 & 0 & 0 & 4 \end{bmatrix}$$

$$\Delta_{ip} = \begin{bmatrix} y_{\text{wert}} \\ y_{\text{gor}} \\ \theta \end{bmatrix} = \begin{bmatrix} 0 & 2 & 2 & 2 \\ 0 & 0 & 2 & 4 \\ 1 & 1 & 1 & 1 \end{bmatrix} \frac{a}{6EI} \begin{bmatrix} 2 & 1 & 0 & 0 \\ 1 & 6 & 0 & 0 \\ 0 & 0 & 16 & 0 \\ 0 & 0 & 0 & 4 \end{bmatrix} \begin{bmatrix} 0 \\ 20 \\ 40 \\ 100 \end{bmatrix} = \frac{a}{6EI} \begin{bmatrix} 1160 \\ 2880 \\ 1200 \end{bmatrix},$$

Bu ýerden $y_{\text{wert}} = \frac{a \cdot 1160}{6EI} = \frac{100 \cdot 1160 \cdot 10^4}{6 \cdot 2 \cdot 10^4 \cdot 8000} = 1,21\text{sm},$

$$y_{\text{gor}} = \frac{a \cdot 2880}{6EI} = \frac{100 \cdot 2880 \cdot 10^4}{6 \cdot 2 \cdot 10^4 \cdot 8000} = 3\text{sm},$$

$$\theta = \frac{100 \cdot 1200 \cdot 10^2}{6 \cdot 2 \cdot 10^4 \cdot 8000} = 0,0125\text{rad}.$$

6.38. $y_c = \frac{43}{24} qa^4$, $\theta_c = \frac{25}{12} qa^3$.

$R_A = 2,25qa^2$, $R_B = -1,25qa^2$.

Matrisa deňlemesi

$$\Delta_{ip} = \begin{bmatrix} y_c \\ \theta_c \end{bmatrix} = M^0 \cdot B \cdot M_p,$$

M_p, M_1^0, M_2^0 epýurlaryny peýdalanyň, deňlemä girýän matrisalary we balkanyň bölekleriniň ýumşaklyk matrisasyny düzýäris:

M_1^0, M_2^0 matrisalary transponirläp ýazýarys.

$$M^o = \begin{bmatrix} 0 & 0,25a & 0,5a & 0,5a & 0,75a & 0,5a & 0 \\ 0 & 0,25 & 0,5 & 0,5 & 0,75 & 0,5 & 0 \end{bmatrix};$$

$$b_1 = b_{II} = b_{III} = \frac{a}{6EI} \begin{bmatrix} 1 & 0 & 0 \\ 0 & 4 & 0 \\ 0 & 0 & 1 \end{bmatrix};$$

$$M_p = \begin{bmatrix} 1 \\ 1 \\ 1,75 \\ 0,75 \\ 1,25 \\ 1,5 \\ 0,875 \\ 0 \end{bmatrix} qa^2; \quad B = \frac{a}{6EI} \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 4 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 4 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 4 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix};$$

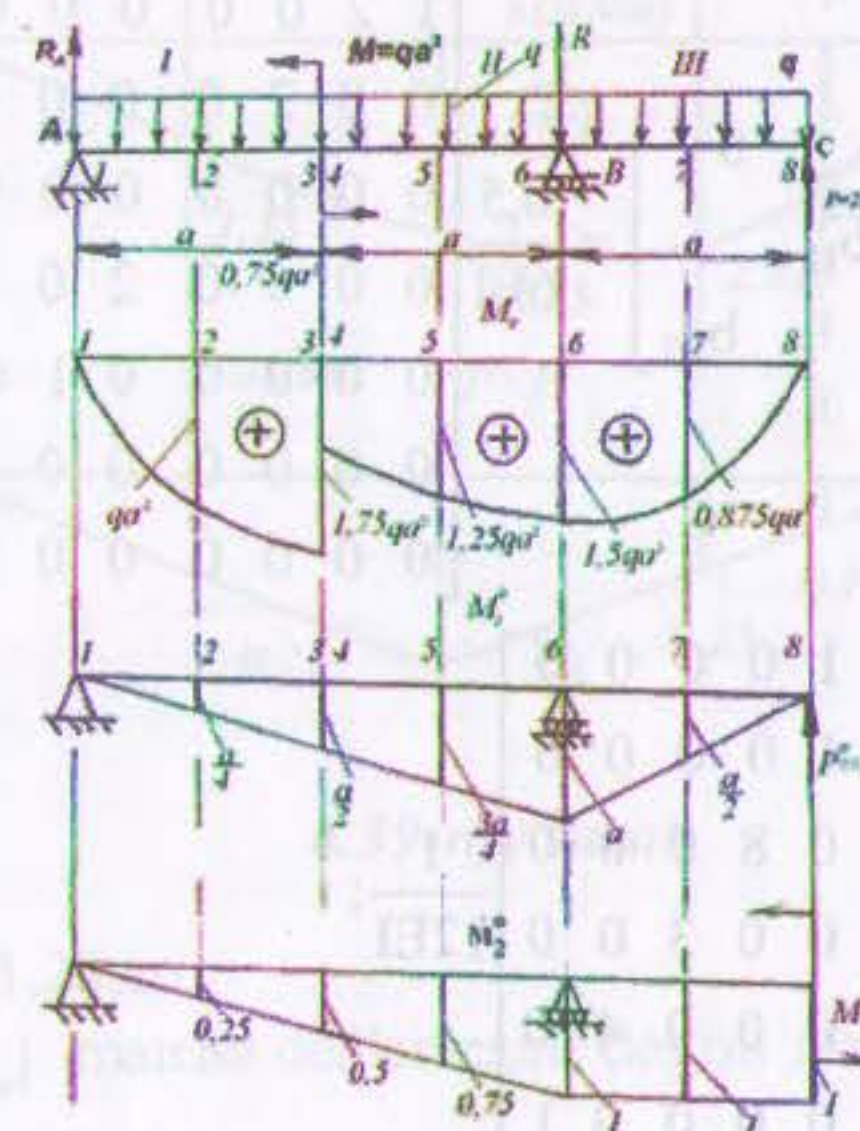
$$B = \frac{a}{6EI} \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 4 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 4 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 2 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 4 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 4 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}.$$

Matrisa deñlemesine goýup alarys:

$$\Delta_{ip} = \begin{bmatrix} y_c \\ \theta_c \end{bmatrix} = \frac{qa^3}{6EI} \begin{bmatrix} 0 & 0 & 25a & 0,5a & 0,5a & 0,75a & 0,5a & 0 \\ 0 & 0 & 25 & 0,5 & 0,5 & 0,75 & 0,5 & 0 \end{bmatrix}.$$

$$\begin{bmatrix} 1 \\ 1 \\ 1,75 \\ 0,75 \\ 1,25 \\ 1,5 \\ 0,875 \\ 0 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 4 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 4 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 2 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 4 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix} = \frac{qa^3}{6EI} \begin{bmatrix} 43a \\ 4 \\ 25 \\ 2 \end{bmatrix},$$

onda $y_c = \frac{43}{24} qa^4$, $\theta_c = \frac{25}{12} qa^3$.



6.38-nji surat

6.39. $y_{\text{ort}} = 1,28\text{sm}$, $I \geq 66,5 \cdot 2 = 133\text{sm}^4$.

Berlen:

$P = 4\text{kN}$, $q = 3\text{kN/m}$, $\ell = 2\text{m}$, $I = 51,98\text{sm}^4$.

$E = 7,5 \cdot 10^3\text{kN/sm}^2$, $[y] = \frac{\ell}{200}$.

$R_A = 2,7\text{kN}$, $R_B = 5,8\text{kN}$.

$M^0 = [0 \ 0,25 \ 0,5 \ 0,25 \ 0,125 \ 0]$;

$$M_p = \begin{bmatrix} 0 \\ 1,35 \\ 2,325 \\ 2,525 \\ 1,36 \\ 0 \end{bmatrix}; \ell_1 = \ell_3 = \frac{\ell}{2} = 0,5\text{m}, \ell_2 = 1\text{m}.$$

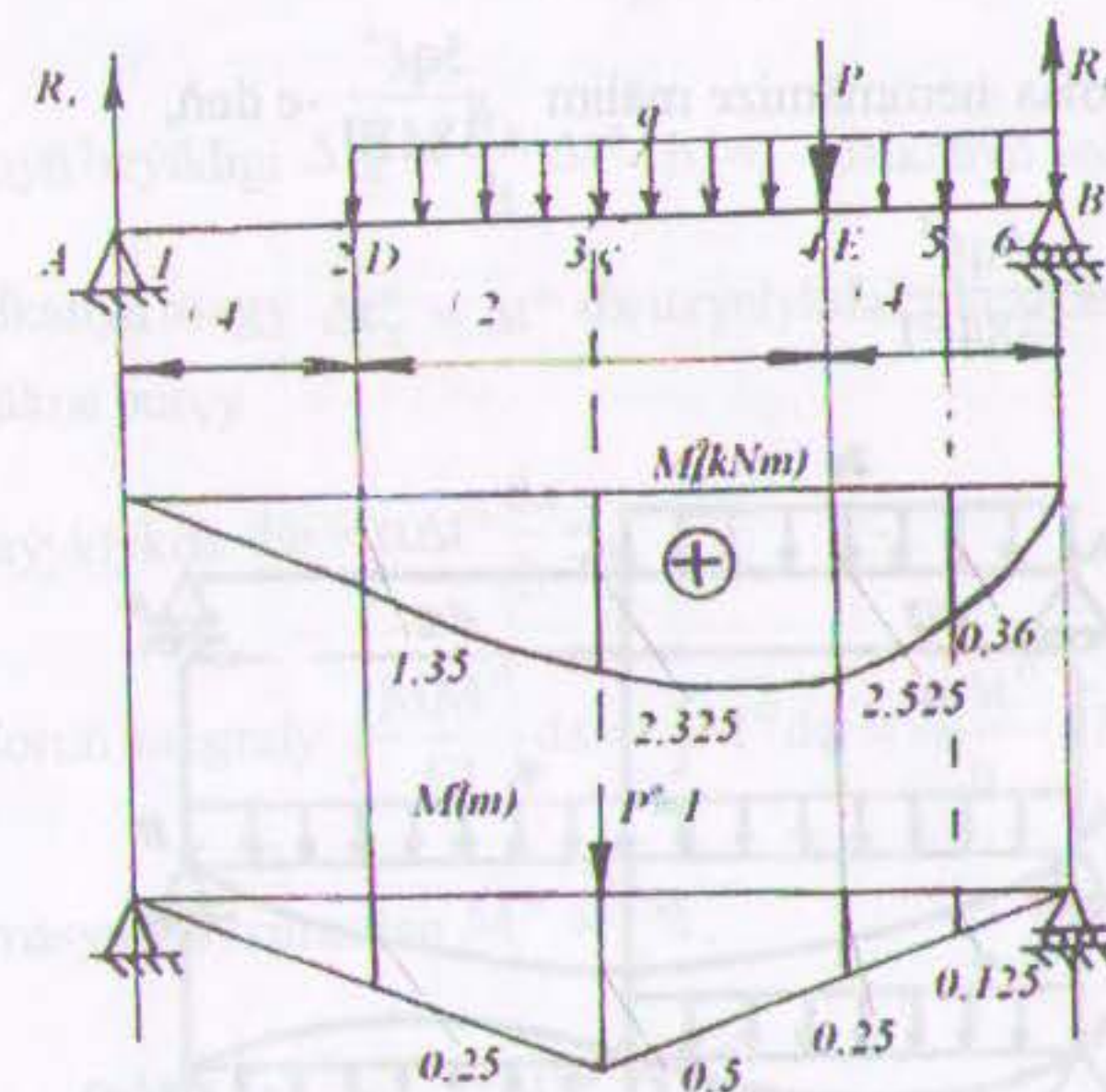
$$B = \begin{bmatrix} b_I & 0 \\ & b_{II} \\ 0 & b_{III} \end{bmatrix} = \frac{0,5}{6EI} \begin{bmatrix} 2 & 1 & 0 & 0 & 0 & 0 & 0 \\ 1 & 2 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 2 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 8 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 2 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 4 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

$$= \frac{1}{12EI} \begin{bmatrix} 2 & 1 & 0 & 0 & 0 & 0 \\ 1 & 4 & 0 & 0 & 0 & 0 \\ 0 & 0 & 8 & 0 & 0 & 0 \\ 0 & 0 & 0 & 3 & 0 & 0 \\ 0 & 0 & 0 & 0 & 4 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

$$y_{\text{ort}} = \frac{10^6}{2 \cdot 3,75 \cdot 10^3 \cdot 2 \cdot 51,98} [0 \ 0,25 \ 0,5 \ 0,25 \ 0,125 \ 0] x$$

Onda

$$x \begin{bmatrix} 2 & 1 & 0 & 0 & 0 & 0 \\ 1 & 4 & 0 & 0 & 0 & 0 \\ 0 & 0 & 8 & 0 & 0 & 0 \\ 0 & 0 & 0 & 3 & 0 & 0 \\ 0 & 0 & 0 & 0 & 4 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ 1,35 \\ 2,325 \\ 2,525 \\ 1,36 \\ 0 \end{bmatrix}$$



6.39-njy surat

Bu ýerden $y_{\text{ort}} = 1,28\text{sm}$.

$y_{\text{ort}} = [M^0][B][M_p]$ matrisa deňlemesine degişli matrisalaryň bahalaryny

goýup we $y_{\text{ort}} = \frac{\ell}{200} = 1\text{sm}$ kabul edip, matrisa deňlemesinden balkanyň

kesiginiň gerek bolan inersiýa momentini tapýarys: $I = 66,5 \text{ sm}^4$ - bir şwelleriň inersiýa momenti.

$$6.40. y_{\varphi} = \frac{5q\ell^4}{384EI}$$

Bu de berlen ýüki özgerdip hasaplamak çözüwi has ýeňilleşdirýär. Şol maksat bilen berlen ýüki b) we ç) suratlarda görkezilişi ýaly, simmetriýa we simmetriýa ters bolan ýüklere dargadýarys.

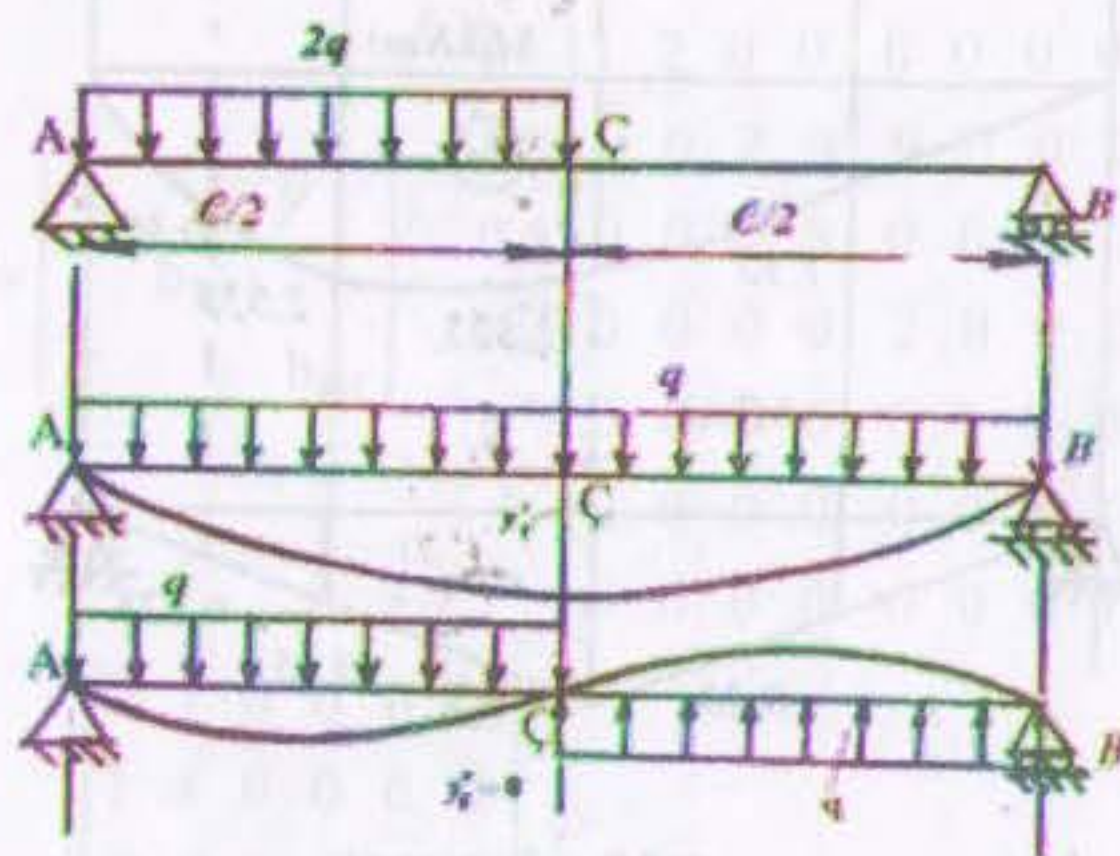
Umumy egrelme

$$y_{\varphi} = y_{\varphi}^I + y_{\varphi}^{II};$$

$$\text{ýöne } y_{\varphi}^{II} = 0.$$

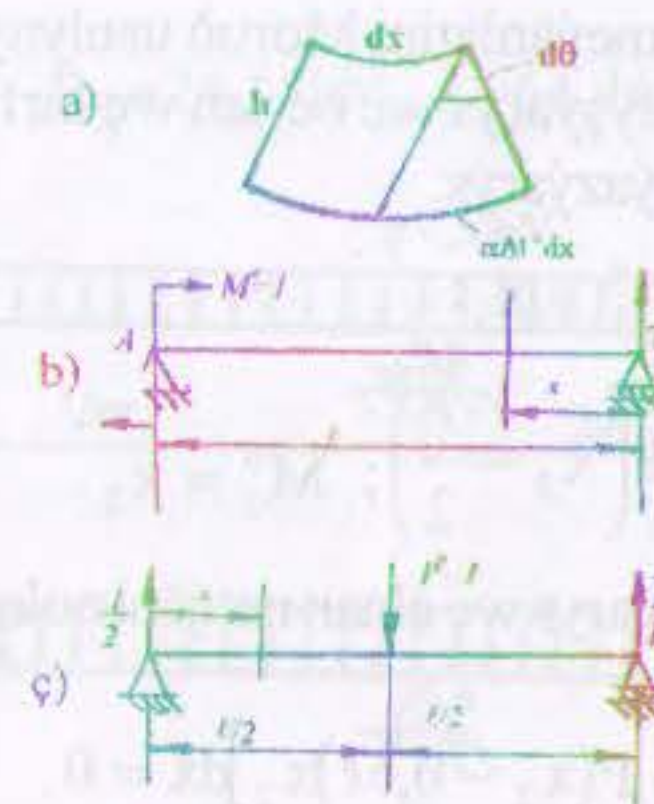
y_{φ}^I bahasy bolsa hemmämize mälim $\frac{5q\ell^4}{384EI}$ -e deň,

$$\text{onda } y_{\varphi} = y_{\varphi}^I = \frac{5q\ell^4}{384EI}.$$



6.40-njy surat

$$6.41. \theta_A = \frac{\alpha \Delta t^{\circ} \ell}{2h}, f = \frac{\alpha \Delta t^{\circ} \ell^2}{8h}.$$



6.41-nji surat

h – halkanyň beýikligi $\Delta t_x^{\circ} = \frac{h_x}{h} \Delta t^{\circ}$, $h_x = 0$ – balkanyň ýokarsy $\Delta t_x^{\circ} = 0$.

$h_x = h$ – balkanyň aşagy $\Delta t_x^{\circ} = \Delta t^{\circ}$ dx uzynlykdaky kesikleriň biri-birine görä öwrülme burçy.

a) çyzga laýyklykda $d\varphi = \alpha \Delta t^{\circ} \frac{dx}{h}$.

Onda Moruň integraly $\int \frac{MM^{\circ}}{EI} dx = \int M^{\circ} d\varphi = \frac{\alpha \Delta t^{\circ}}{h} \int M^{\circ} dx$

M° aňlatmasyny: b) suratdan $M^{\circ} = \frac{1}{\ell} x$.

$$\text{Onda } \theta_A = \frac{\alpha \Delta t^{\circ} \ell}{h} \int_0^{\ell} \frac{x}{\ell} dx = \frac{\alpha \Delta t^{\circ} \ell}{2h}.$$

Balkanyň ortasyny $P^{\circ} = 1$ birlik güýç bilen ýükleýäris.

$$\text{Onda } M^{\circ} = \frac{x}{2} \text{ we } f = \frac{\alpha \Delta t^{\circ}}{h} \cdot 2 \int_0^{\ell} \frac{x}{2} dx = \frac{\alpha \Delta t^{\circ} \ell^2}{8h}.$$

$$6.42. Q_{\max} = 30 \text{ kN}, M_{\max} = 2,75 \text{ kN/m}.$$

Meselaniň statiki kesgitlenmeýänligini Moruň usulyny ulanyp açýarys. A diregi R_A gaýtargy bilen çalyşýarys we berlen we birlik güýçlerden egme momentleriň aňlatmalaryny ýazýarys:

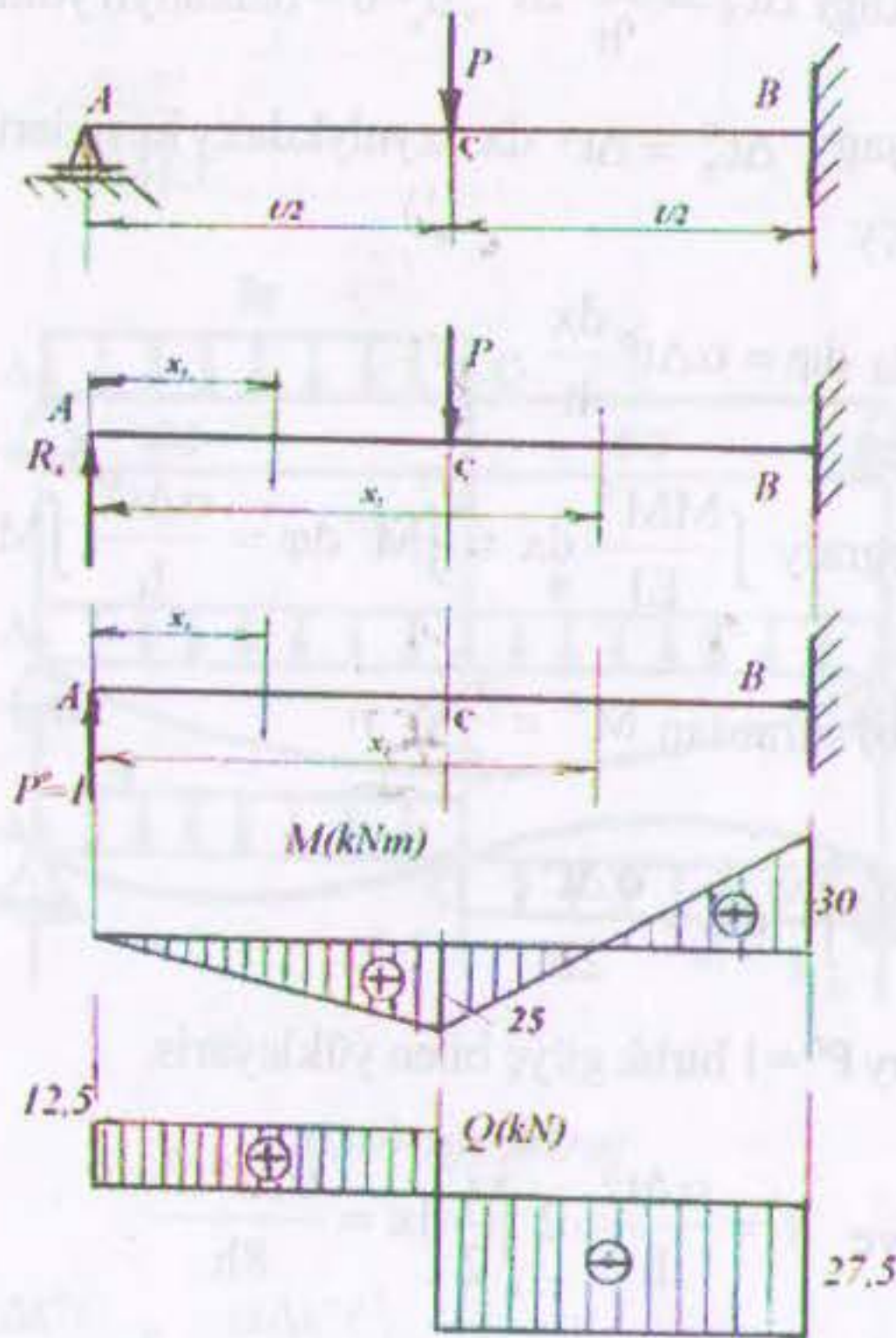
I bölek $M_{x_1} = R_A \cdot x_1$; $M_1^0 = x_1$;

II bölek $M_{x_2} = R_A \cdot x_2 - P\left(x_2 - \frac{\ell}{2}\right)$; $M_2^0 = x_2$.

Moruň integralyny hasaplaýarys we alnan netijäni nola deňleýäris:

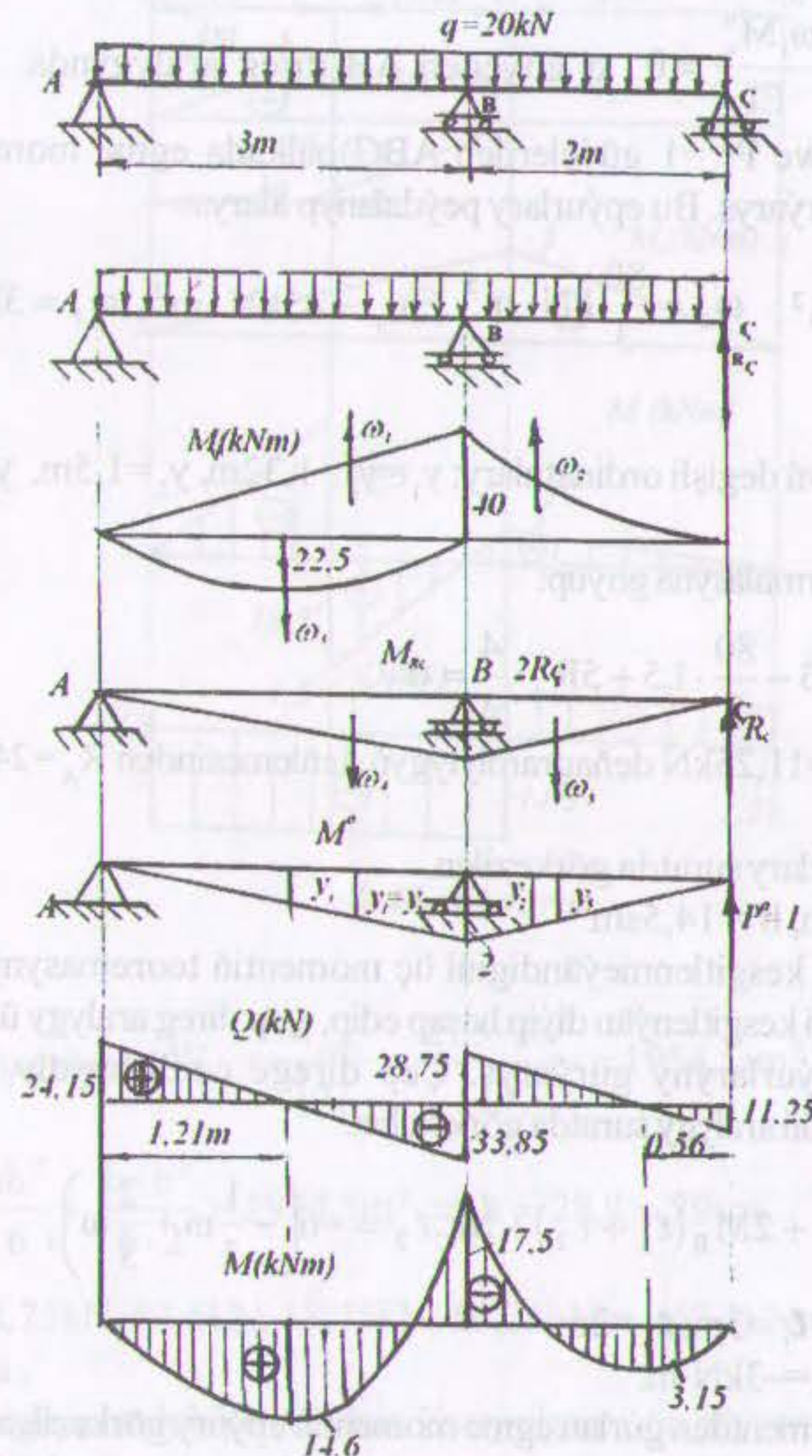
$$\int_0^{0,5\ell} R_A \cdot x_1^2 dx + \int_{0,5\ell}^{\ell} [R_A x_2^2 - P(x_2 - 0,5\ell)x_2] dx = 0.$$

Bu ýerden $R_A = \frac{5\ell}{16}$ alarys: Q we M epýurlaryny adaty usul bilen gurýarys.



6.42-nji surat

6.43. $R_{\varphi} = 11,25 \text{ kN}$, $R_A = 24,15 \text{ kN}$, $\ell = 64,46 \text{ kNm}$.



6.43-nji surat

Balkanyň statiki kesgitlenmeýändigini Wereşaginiň usuly boýunça açýarys. Artykmaç berkitme hökmünde sag diregi alýarys:

onda $f_{\varphi} = \sum \frac{\omega_i M_{\varphi}^0}{EI} = 0$, q güýçden AB direg aralygynda we BÇ konsolda, R_{φ} we $P^0 = 1$ güýçlerden ABC balkada egme momentleriň epýurlaryny gurýarys. Bu epýurlary peýdalanyp alarys:

$$\omega_1 = 60 \text{ kN} \cdot \text{m}^2, \quad \omega_2 = \frac{80}{3} \text{ kN} \cdot \text{m}^2, \quad \omega_3 = 45 \text{ kN} \cdot \text{m}^2, \quad \omega_4 = 3R_{\varphi},$$

$$\omega_5 = 2R_{\varphi}.$$

Bu meýdanlaryň deňişli ordinatalary: $y_1 = y_4 = 1,32 \text{ m}$, $y_2 = 1,5 \text{ m}$, $y_3 = 1 \text{ m}$, $y_5 = 1,33 \text{ m}$.

Wereşaginiň formulasyna goýup:

$$45 \cdot 1 - 60 \cdot 1,33 - \frac{80}{3} \cdot 1,5 + 5R_{\varphi} \cdot \frac{4}{3} = 0.$$

Bu ýerden $R_{\varphi} = 11,25 \text{ kN}$ deňagramlylygyň deňlemesinden $R_A = 24,15 \text{ kN}$, $R_B = 64,6 \text{ kN}$.

Q we M epýurlary suratda görkezilen.

6.44. $h = 29 \text{ sm}$, $b = 14,5 \text{ sm}$.

Statiki kesgitlenmeýändigini üç momentiň teoremasyny ulanyp açýarys. Statiki kesgitlenýän diýip hasap edip, çep direg aralygy üçin egme momentiň epýurlaryny gurýarys. Çep direge çenli hyýaly ýükleriň deňtäsi redijisiniň aralygy suratda görkezilen.

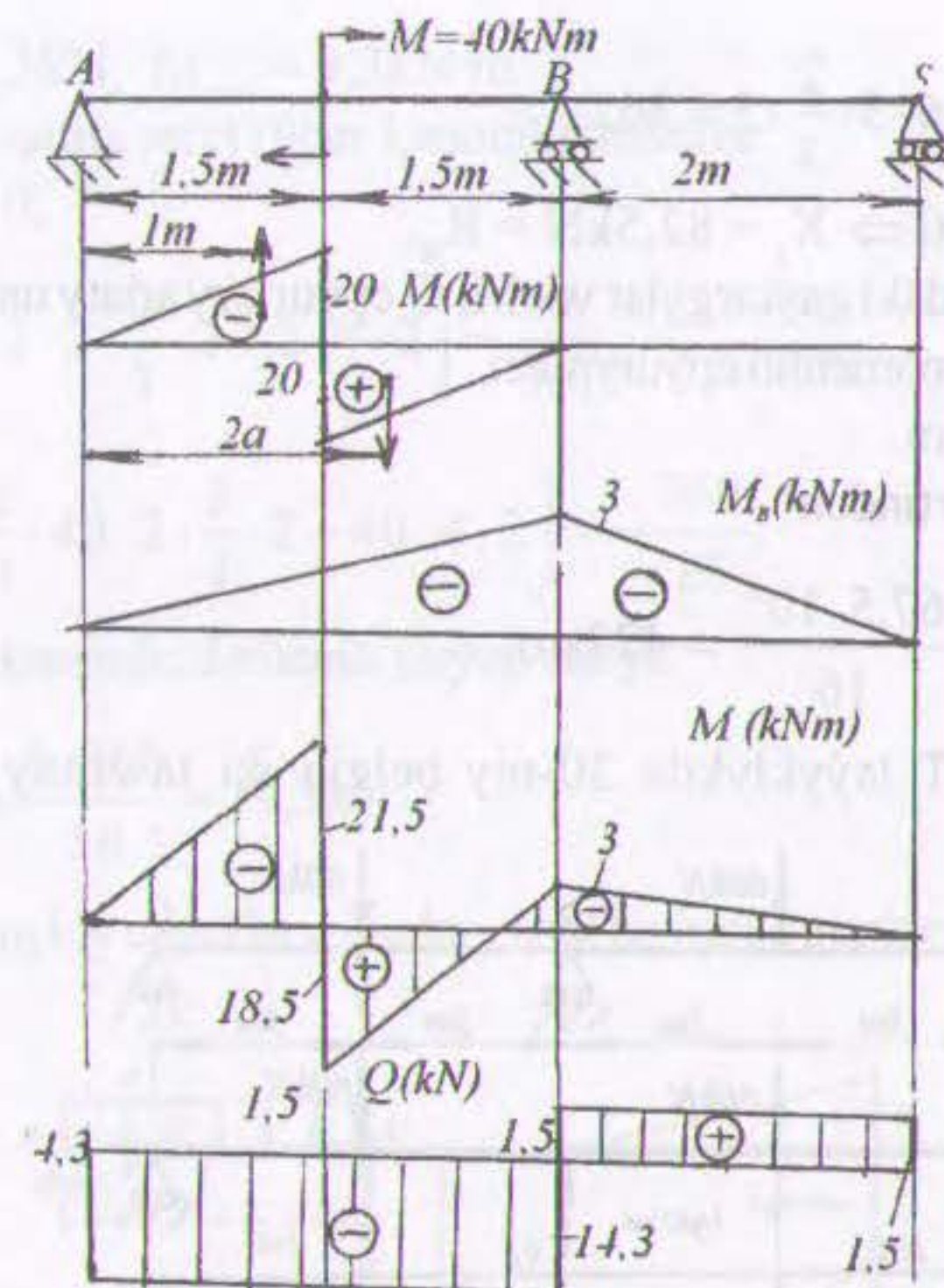
$$M_A \ell_1 + 2M_B (\ell_1 + \ell_2) + M_C \ell_2 = -6 \left(-\frac{1}{3} \omega + \frac{2}{3} \omega \right),$$

$$M_A = M_C = 0, \quad \ell_1 = 3 \text{ m}, \quad \ell_2 = 2 \text{ m}.$$

Bu ýerden $M_B = -3 \text{ kN} \cdot \text{m}$.

Suratda bu momentden gurlan egme momentiň epýury görkezilen. Bu epýury çep ýönekeý balka üçin gurlan epýur bilen goşup, berlen balka üçin egme momentiň epýuryny alarys.

Direglerdäki gaýtargylary kesgitläp, kese güýjüň epýuryny gurarys (surata seret):



6.44-nji surat

$$\text{Berklik şertinden } W_z = \frac{M_{\max}}{[\sigma]} = \frac{21,5 \cdot 10^2}{1,1} = 1954,5 \text{ sm}^3;$$

$$W_z = \frac{bh^2}{6} = \frac{h \cdot h^2}{6 \cdot 2} = 1954,5 \text{ sm}^2 \Rightarrow h = 28,8 \approx 29 \text{ sm}.$$

6.45. 18,75kN, 82,5kN, 18,75kN, 56,25kNm – 67,5kNm, 30-njy belgili iki tawra.

Meseläni güýç usuly bilen çözüäris. Esasy ulgam üçin güýç usulynyň kanoniki deňlemesi:

$$X_1 \delta_{11} + \Delta_{1p} = 0,$$

$$EI \Delta_{1p} = -2 \cdot \frac{1}{2} \cdot 180 \cdot 3 \cdot \frac{2}{3} \cdot 1,5 - 2 \cdot 180 \cdot 3 \cdot 2,25 = -2970;$$

$$EI\delta_{11} = -2 \cdot \frac{1}{2} \cdot 6 \cdot 3 \cdot \frac{2}{3} \cdot 3 = 36;$$

$$36X_1 - 2970 = 0 \Rightarrow X_1 = 82,5 \text{ kN} = R_B.$$

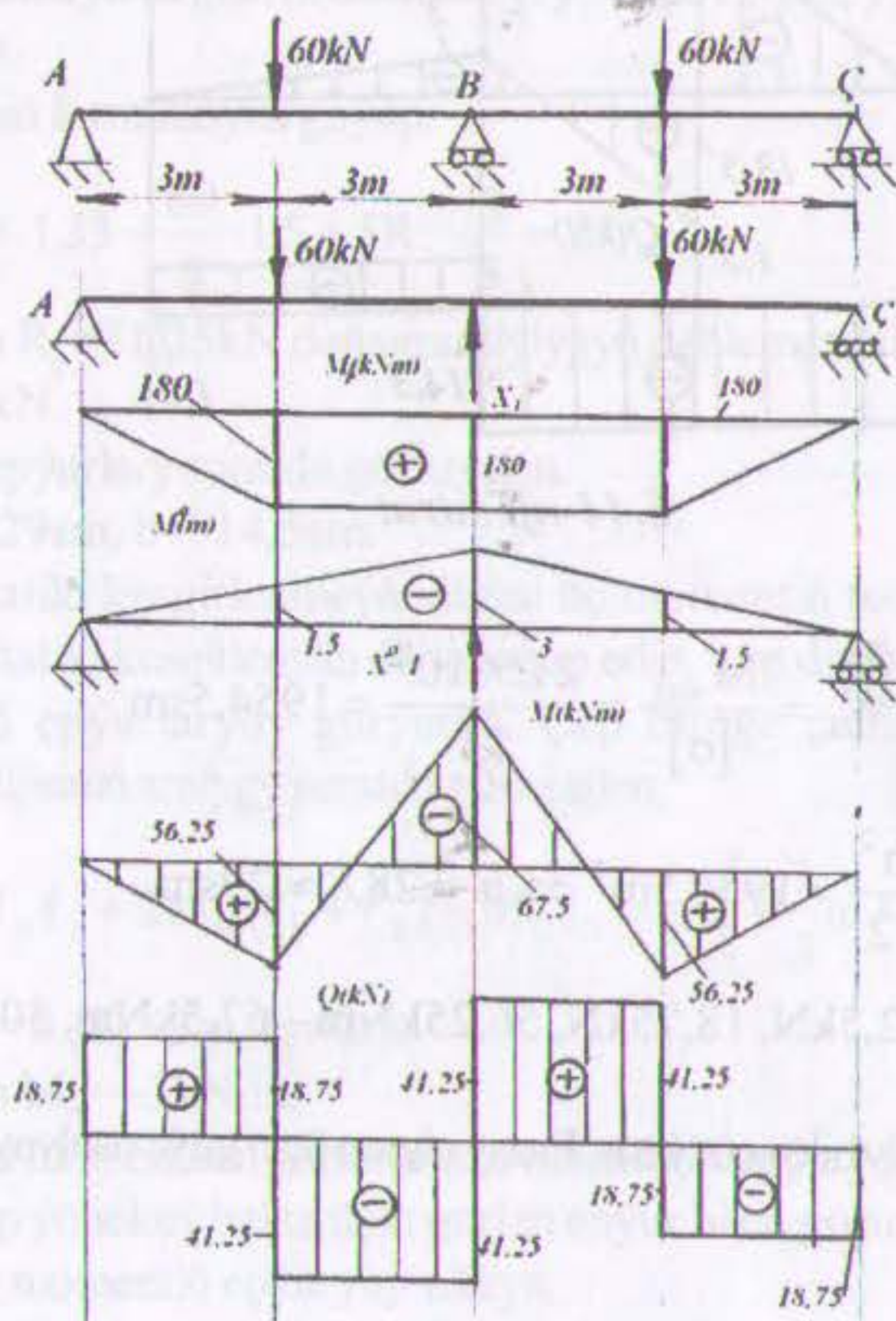
A we Ç direglerdäki gaytargylar we M, Q epýurlary adaty usul bilen ýerine ýetirilen. Egme momentin epýuryndan

$$M_{\max} = 67,5 \text{ kN} \cdot \text{m}.$$

Onda berklik şertinden

$$W_z \geq \frac{M_{\max}}{[\sigma]} = \frac{67,5 \cdot 10^2}{16} = 422 \text{ sm}.$$

8239-56 DÖST laýyklykda 30-njy belgili iki tawrany saýlaýarys.



6.45-nji surat

$$6.46. R_A = 19,3 \text{ kN}, M_{\max} = 9,3 \text{ kN} \cdot \text{m}.$$

Esasy ulgam (surata seret) üçin kanoniki deňleme:

$$X_1 \delta_{11} + \Delta_{ip} = 0,$$

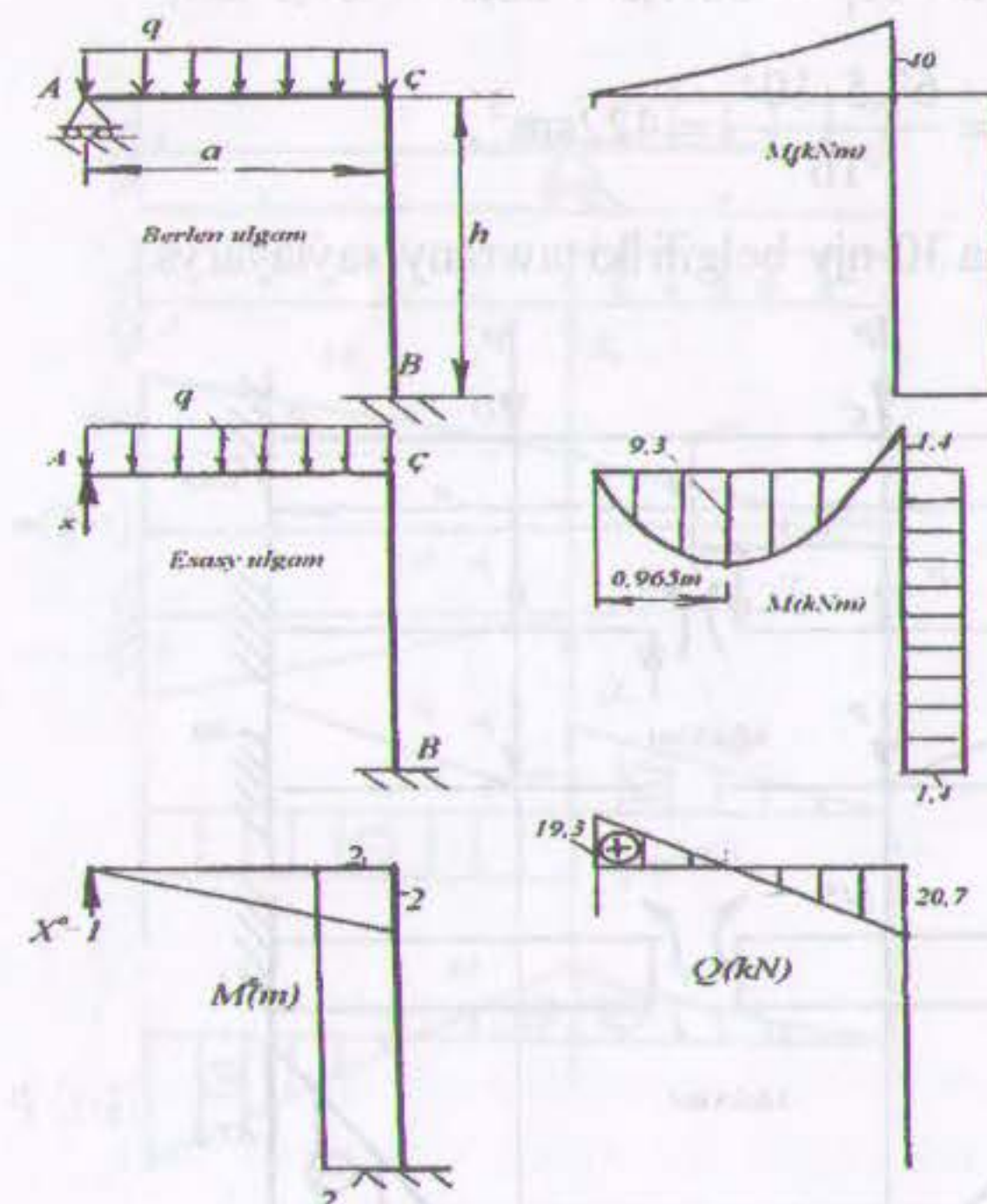
$$\delta_{11} = \frac{1}{EI} \left(\frac{1}{2} \cdot 2 \cdot 2 \cdot \frac{2}{3} \cdot 2 + 2 \cdot 4 \cdot 2 \right) = \frac{56}{3EI},$$

$$\Delta_{ip} = \frac{1}{EI} \left(-\frac{1}{3} \cdot 40 \cdot 2 \cdot \frac{3}{4} \cdot 2 - 40 \cdot 4 \cdot 2 \right) = -\frac{360}{EI}.$$

Bu ululyklary kanoniki deňlemä goýup alarys:

$$X_1 = -\frac{\Delta_{ip}}{\delta_{11}} = \frac{3 \cdot 360}{56} = 19,3 \text{ kN}.$$

Q we M gutarnykly epýurlaryny adaty usul boýunça gurýarys (surata seret).



6.46-nji surat

6.47. $M_A = -67,5 \text{ kN} \cdot \text{m}$, $M_C = 22,5 \text{ kN} \cdot \text{m}$, 30-njy belgili iki tawra. Statiki kesgitlenmeyändigini açmak üçin, balkanyň we ýükleriň simmetriýalygyny, peýdalanyrys. Balkanyň we daşky güýçleriň simmetriýaly X_2 güýjüň tersleyin. Simmetriýaly bolany üçin, δ_{22} , δ_{21} , δ_{12} , Δ_{2p} nola deň we kanoniki deňleme aşakdaky ýaly ýazylyar:

$$X_1 \delta_{11} + \Delta_{ip} = 0,$$

$$\Delta_{ip} = \left(-\frac{1}{2} \cdot 90 \cdot 1,5 \cdot \frac{2}{3} \cdot 90 \right) \cdot 2 = -135.$$

$$\delta_{11} = 2 \cdot 6 \cdot 1 = 12,$$

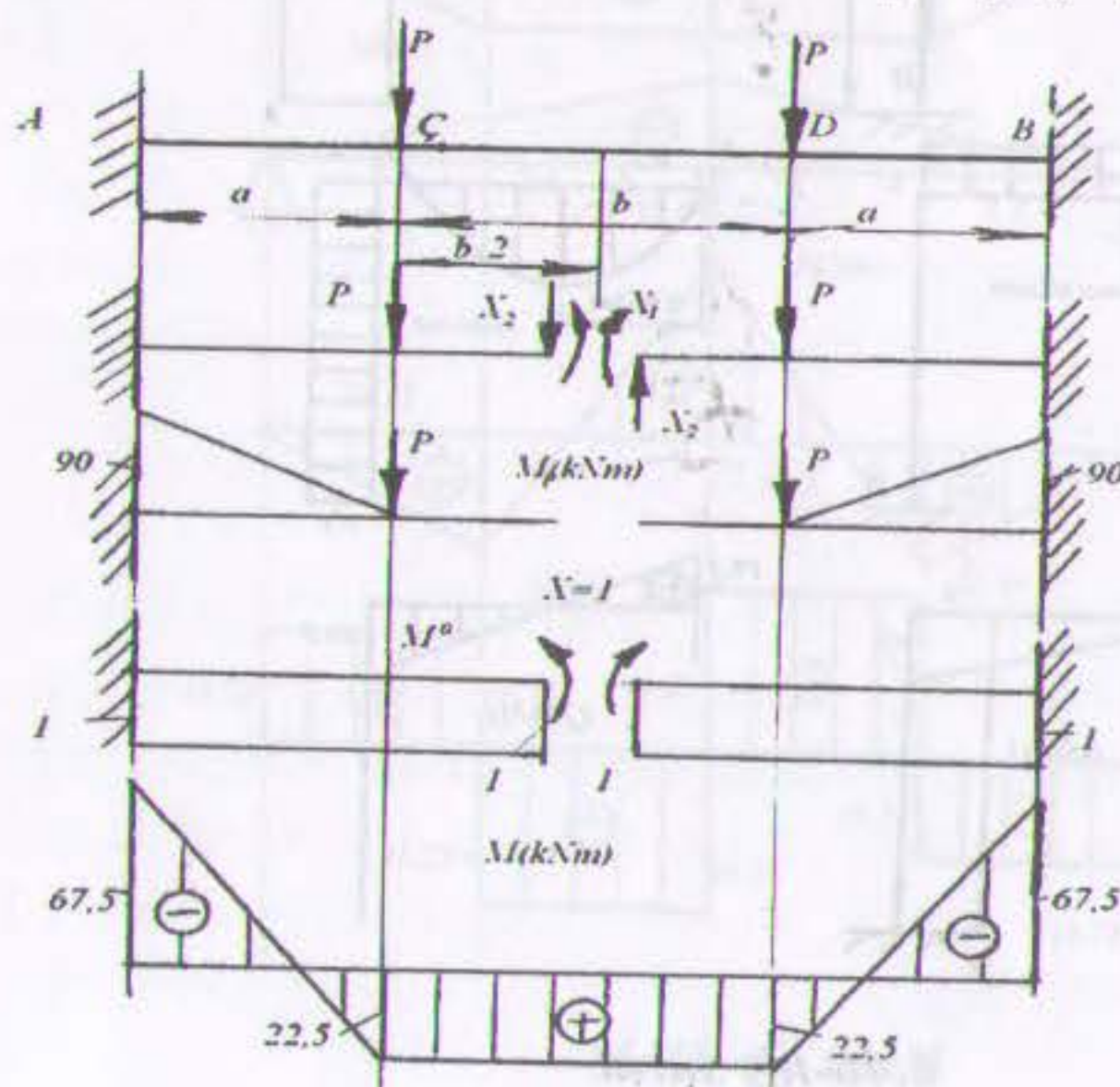
$$X_1 = -\frac{\Delta_{ip}}{\delta_{11}} = \frac{135}{12} = 22,5 \text{ kN} \cdot \text{m}.$$

Onda

$$M_B = M_A = -P \cdot a + X_1 = -60 \cdot 1,5 + 22,5 = -67,5 \text{ kN},$$

$$W_z \geq \frac{M_{\max}}{[\sigma]} = \frac{67,5 \cdot 10^2}{16} = 422 \text{ sm}^3.$$

DÖST boýunça 30-njy belgili iki tawrany saýlaýarys.



6.47-nji surat

6.48. Bu ýerde güýç usulyny ulanmak amatly bolýar.

$$X_1 \delta_{11} + \Delta_{ip} = 0,$$

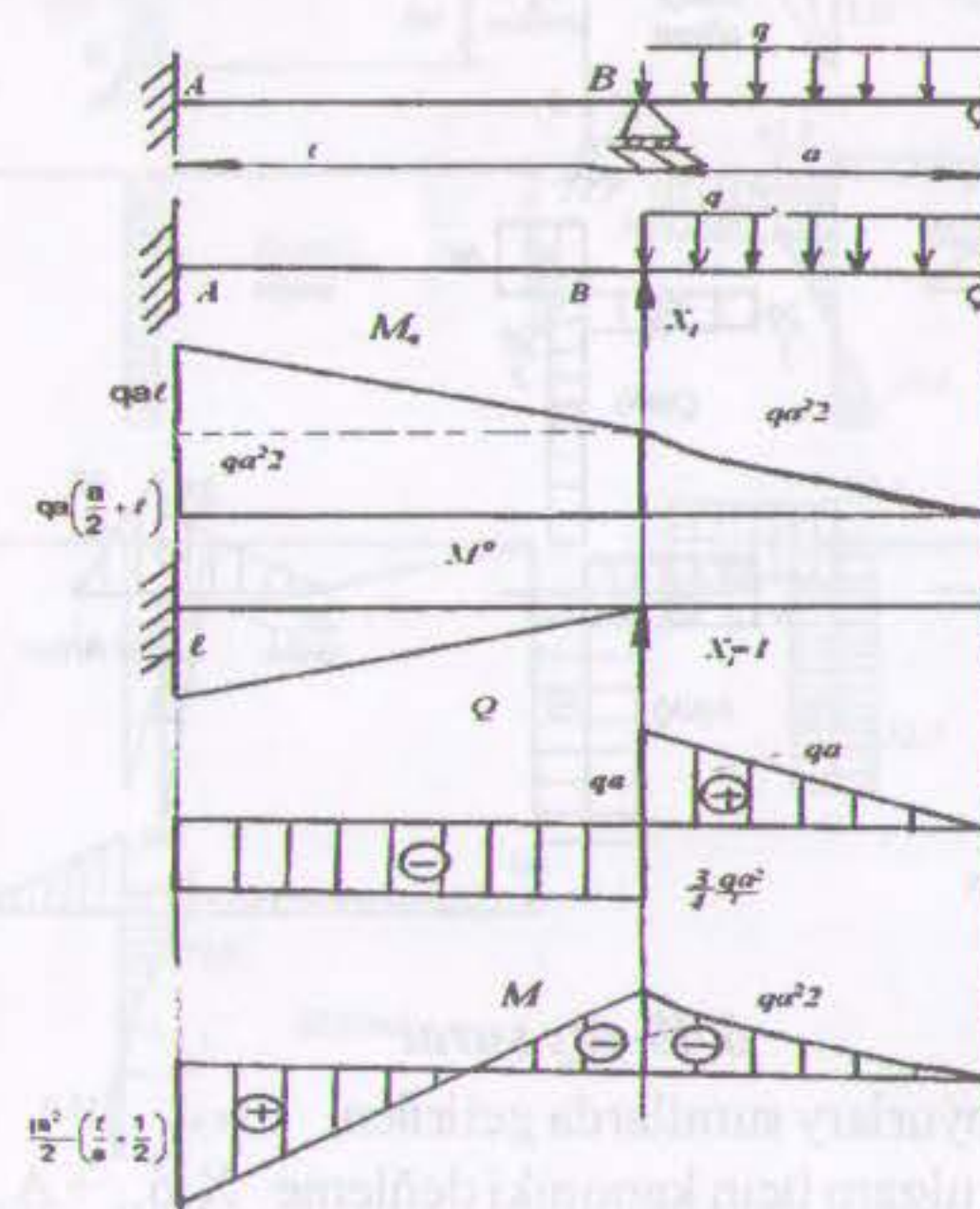
$$\delta_{11} = \frac{1}{2} \cdot \ell \cdot \ell \cdot \frac{2\ell}{3} = \frac{\ell^3}{3},$$

$$\Delta_{ip} = -\frac{qa^2}{2} \cdot \ell \cdot \frac{1}{2} \cdot \ell - qa\ell \cdot \frac{1}{2} \cdot \ell \cdot \frac{2}{3} \cdot \ell = -qa\ell^2 \left(\frac{a}{4} + \frac{\ell}{3} \right),$$

$$X_1 = -\frac{\Delta_{ip}}{\delta_{11}} = \frac{qa\ell^2 \cdot 3 \left(\frac{a}{4} + \frac{\ell}{3} \right)}{\ell^3} = qa \left(1 + \frac{3}{4} \cdot \frac{a}{\ell} \right),$$

$$M_A = M_q^A - X_1 \cdot M_A^0 = qa \left(\frac{a}{2} + \ell \right) - qa \left(1 + \frac{3}{4} \cdot \frac{a}{\ell} \right) \cdot \ell = -\frac{qa^2}{2} \left(\frac{1}{2} + \frac{\ell}{a} \right)$$

M we Q epýurlary suratda görkezilen.



6.48-nji surat

6.49. Esasy ulgamyň kanoniki deňlemesi.

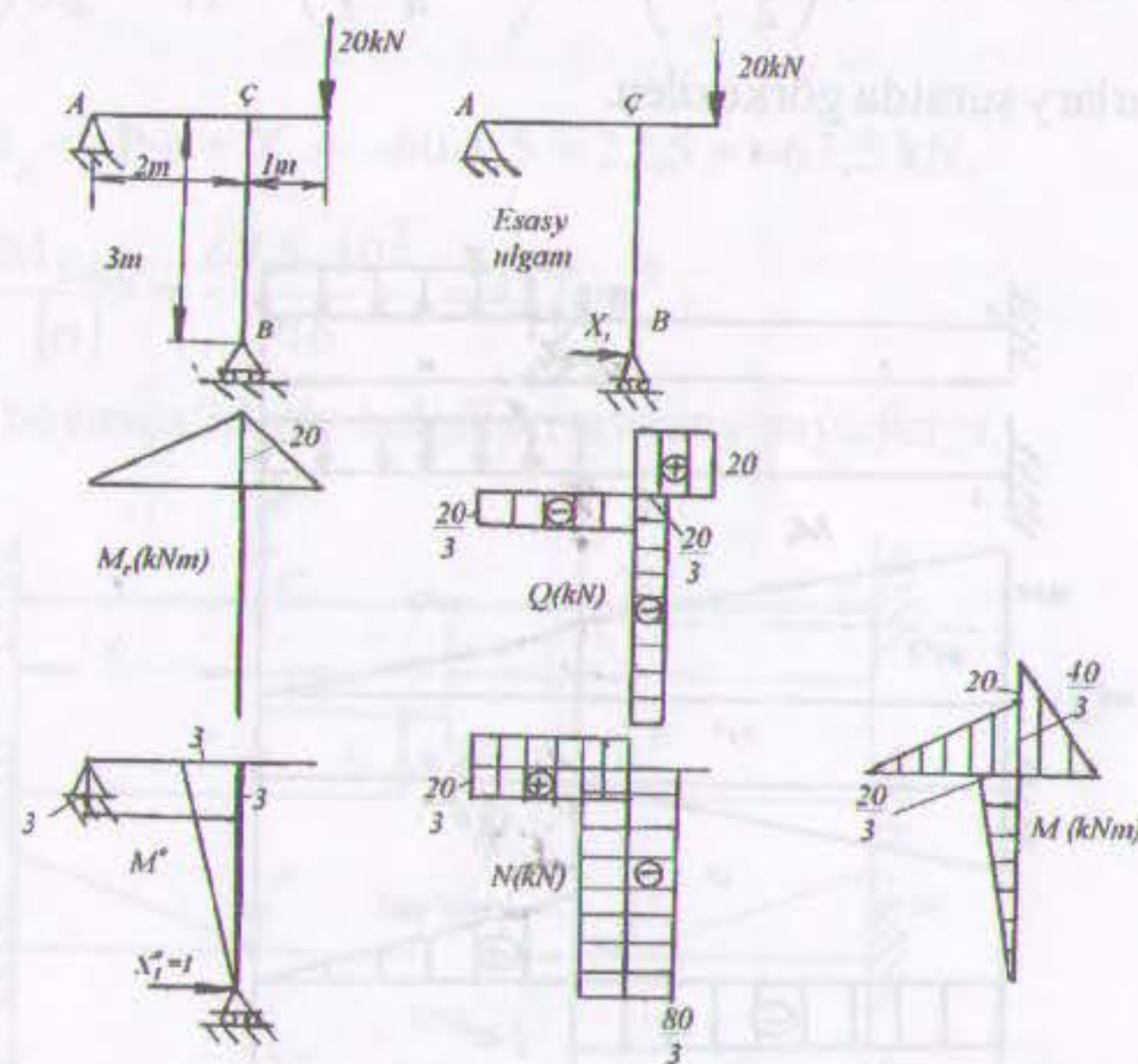
$$X_1 \delta_{11} + \Delta_{1P} = 0,$$

$$\delta_{11} = \frac{1}{2} \cdot 3 \cdot 3 \cdot \frac{2}{3} \cdot 3 + 3 \cdot 3 \cdot 2 = 27,$$

$$\Delta_{1P} = -\frac{1}{2} \cdot 20 \cdot 2 \cdot 3 = -60, \quad X_B = X_1 = \frac{60}{27} = \frac{20}{9} \text{ kN},$$

$$X_A = X_B = \frac{20}{9} \text{ kN}, \quad R_A = \frac{20}{3} \text{ kN}, \quad R_B = \frac{80}{3} \text{ kN}.$$

M, Q we N epýurlary suratda görkezilen.



6.49-njy surat

6.50. Q, M we N epýurlary suratlarda getirilen.

Kabul edilen esasy ulgam üçin kanoniki deňleme $X_1 \delta_{11} + \Delta_{1P} = 0$,

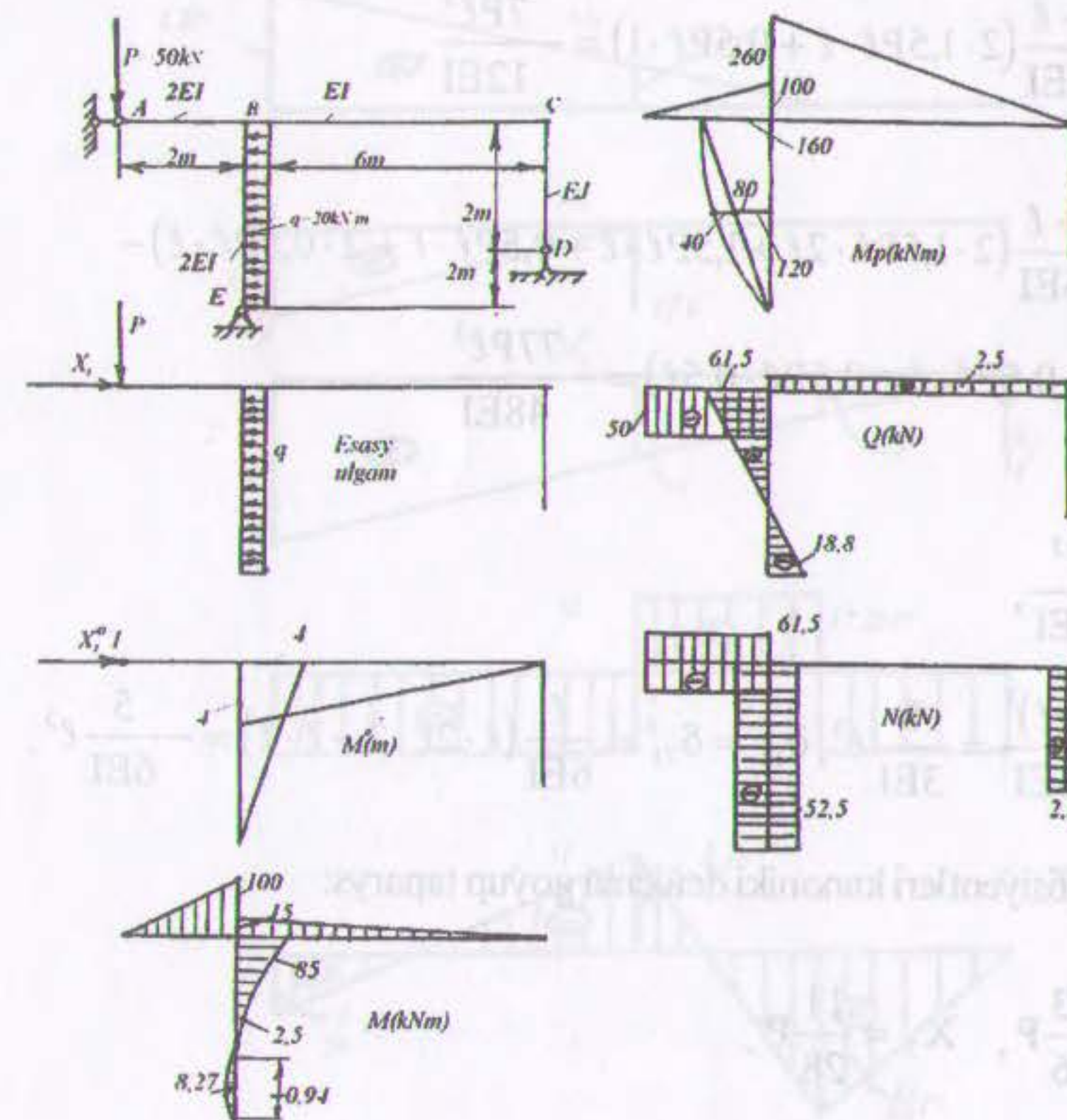
$$\delta_{11} = \frac{1}{EI} \cdot \frac{1}{2} \cdot 4 \cdot 6 \cdot \frac{2}{3} \cdot 4 + \frac{1}{2EI} \cdot \frac{1}{2} \cdot 4 \cdot 4 \cdot \frac{2}{3} \cdot 4 = \frac{128}{3EI},$$

$$\Delta_{1P} = \frac{1}{EI} \cdot \frac{1}{2} \cdot 260 \cdot 6 \cdot \frac{2}{3} \cdot 4 - \frac{2}{3} \cdot 40 \cdot 4 \cdot 2 \cdot \frac{1}{2EI} - \frac{1}{2} \cdot 160 \cdot 4 \cdot \frac{2}{3} \cdot 4 \cdot \frac{1}{2EI} = -\frac{7840}{3EI}$$

$$\text{Kanoniki deňlemeden } X_1 = -\frac{\Delta_{1P}}{\delta_{11}} = \frac{7840}{128} = 61,25 \text{ kN}.$$

Berlen statiki kesgitlenmeyän çarçuwanyň häsiýetli kesiklerindäki egme momentini gutarnykly epýurlarynyň ordinatalaryny aşakdaky formula bilen kesgitleýäris: $M = M_p + M^0 X_1$

Kese we boý güýçleriň epýurlary adaty usul bilen gurlan.



6.50-nji surat

6.51. Esasy ulgam üçin balkanyň kanoniki deňlemesi:

$$\begin{cases} X_1 \delta_{11} + X_2 \delta_{12} + \Delta_{1p} = 0 \\ X_1 \delta_{21} + X_2 \delta_{22} + \Delta_{2p} = 0 \end{cases}$$

X_1, X_2 – näbelli gaýtargylar. Kanoniki deňlemäniň koeffisiýentlerini Simpson–Karnouhowyň usuly bilen tapýarys:

$$\Delta_{1p} = \frac{-\ell}{6EI} (2 \cdot 1,5Pl \cdot \ell + 0,5Pl \cdot \ell) = -\frac{7Pl^3}{12EI},$$

$$\Delta_{2p} = \frac{-\ell}{6EI} (2 \cdot 1,5Pl \cdot 2\ell + 1,5Pl \cdot \ell + 0,5Pl \cdot \ell + 2 \cdot 0,5Pl \cdot \ell) -$$

$$\frac{0,51}{6EI} (2 \cdot 0,5Pl \cdot \ell + 0,5Pl \cdot 0,5\ell) = -\frac{77Pl^3}{48EI}$$

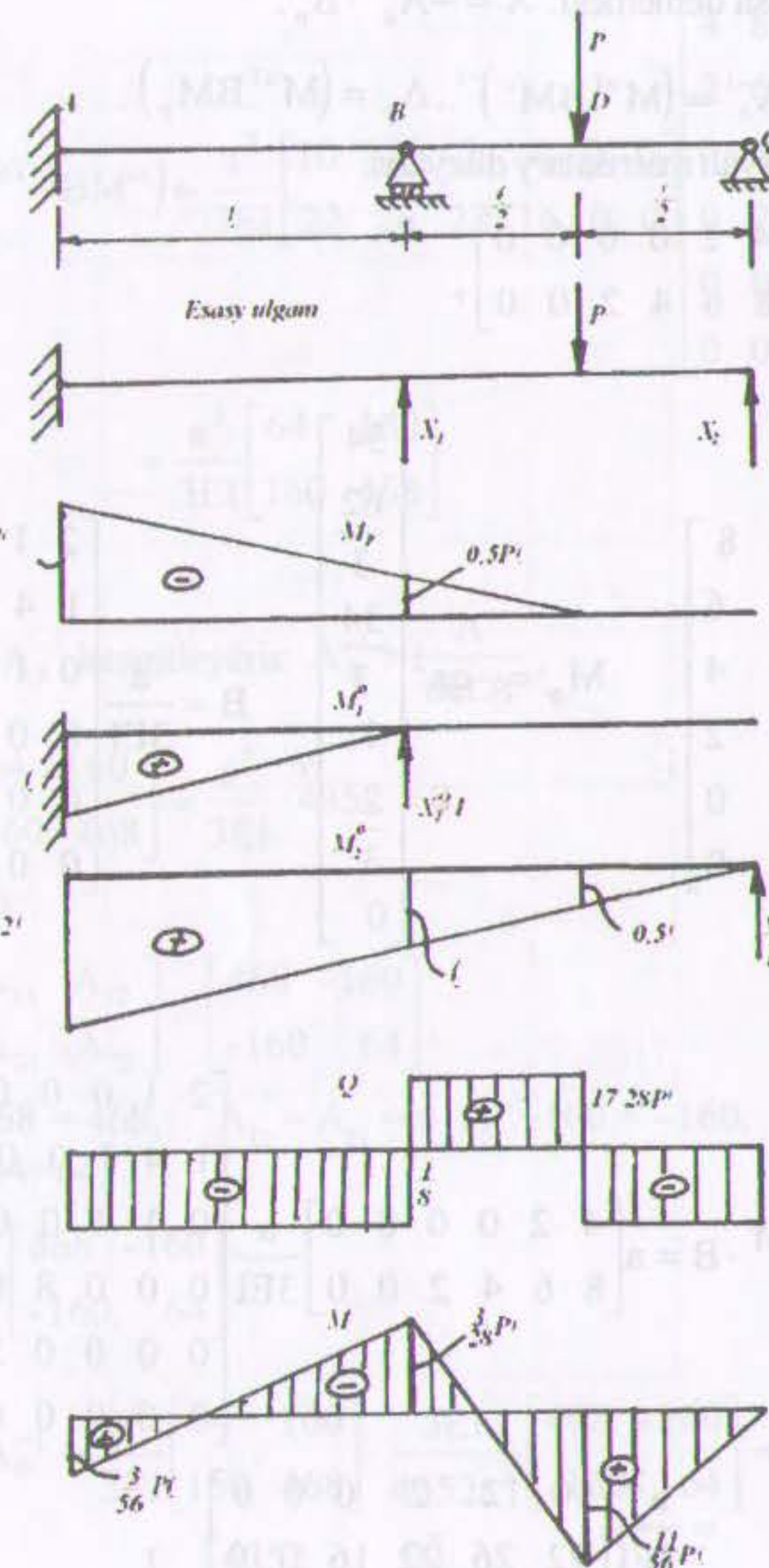
$$\delta_{11} = \frac{\ell^3}{3EI},$$

$$\delta_{22} = \frac{(2\ell)^3}{3EI} = \frac{8}{3EI} \ell^3, \delta_{12} = \delta_{21} = \frac{\ell}{6EI} (\ell \cdot 2\ell \cdot 2 + \ell \cdot \ell) = -\frac{5}{6EI} \ell^3.$$

Bu koeffisiýentleri kanoniki deňlemä goýup taparys:

$$X_1 = \frac{43}{56}P, \quad X_2 = \frac{11}{28}P.$$

Q we M epýurlary adaty usul bilen gurlan.



6.51-nji surat

6.52. Matrisa deňlemesi: $X = -A_{\delta}^{-1} \cdot \Delta_p$.

Bu ýerde $A_{\delta}^{-1} = (M^{oT} B M^o)^{-1}$, $\Delta_p = (M^{oT} B M_p)$.

Deňlemä girýän matrisalary düzyäris:

$$M^{oT} = a \begin{bmatrix} 4 & 2 & 0 & 0 & 0 & 0 \\ 8 & 6 & 4 & 2 & 0 & 0 \end{bmatrix},$$

$$M^o = a \begin{bmatrix} 4 & 8 \\ 2 & 6 \\ 0 & 4 \\ 0 & 2 \\ 0 & 0 \\ 0 & 0 \end{bmatrix}; \quad M_p = -qa^2 \begin{bmatrix} 34 \\ 62 \\ 3 \\ 34 \\ 3 \\ 4 \\ 2 \\ 3 \\ 0 \end{bmatrix}, \quad B = \frac{a}{3EI} \begin{bmatrix} 2 & 1 & 0 & 0 & 0 & 0 \\ 1 & 4 & 1 & 0 & 0 & 0 \\ 0 & 1 & 4 & 0 & 0 & 0 \\ 0 & 0 & 0 & 8 & 0 & 0 \\ 0 & 0 & 0 & 0 & 3 & 1 \\ 0 & 0 & 0 & 0 & 0 & 2 \end{bmatrix}.$$

$$M^{oT} \cdot B = a \begin{bmatrix} 4 & 2 & 0 & 0 & 0 & 0 \\ 8 & 6 & 4 & 2 & 0 & 0 \end{bmatrix} \frac{a}{3EI} \begin{bmatrix} 2 & 1 & 0 & 0 & 0 & 0 \\ 1 & 4 & 1 & 0 & 0 & 0 \\ 0 & 1 & 4 & 0 & 0 & 0 \\ 0 & 0 & 0 & 8 & 0 & 0 \\ 0 & 0 & 0 & 0 & 3 & 1 \\ 0 & 0 & 0 & 0 & 0 & 2 \end{bmatrix} =$$

$$= \frac{a^2}{3EI} \begin{bmatrix} 10 & 12 & 2 & 0 & 0 & 0 \\ 22 & 26 & 22 & 16 & 0 & 0 \end{bmatrix}$$

Birlik güýçlerden ornuny üýtgetmäniň matrisasy

$$A_{\delta} = (M^{oT} \cdot B M^o) = \frac{a^2}{3EI} \begin{bmatrix} 10 & 12 & 2 & 0 & 0 & 0 \\ 22 & 26 & 22 & 16 & 0 & 0 \end{bmatrix} a =$$

$$= \frac{a^3}{3EI} \begin{bmatrix} 64 & 160 \\ 160 & 468 \end{bmatrix}$$

Ters matrisany A_{δ}^{-1} kesgitleýäris: $A_{\delta}^{-1} = \frac{\tilde{A}}{\det A}$,

$$\det A = \frac{a^3}{3EI} \begin{bmatrix} 64 & 160 \\ 160 & 468 \end{bmatrix} = \frac{a^3}{3EI} \cdot 4352 \neq 0$$

Baglaýjy matrisa:

$$\tilde{A} = \begin{bmatrix} A_{11} & A_{12} \\ A_{21} & A_{22} \end{bmatrix} = \begin{bmatrix} 468 & -160 \\ -160 & 64 \end{bmatrix},$$

$$A_{11} = (-1)^{1+1} \cdot 468 = 468, \quad A_{12} = A_{21} = (-1)^{1+2} \cdot 160 = -160,$$

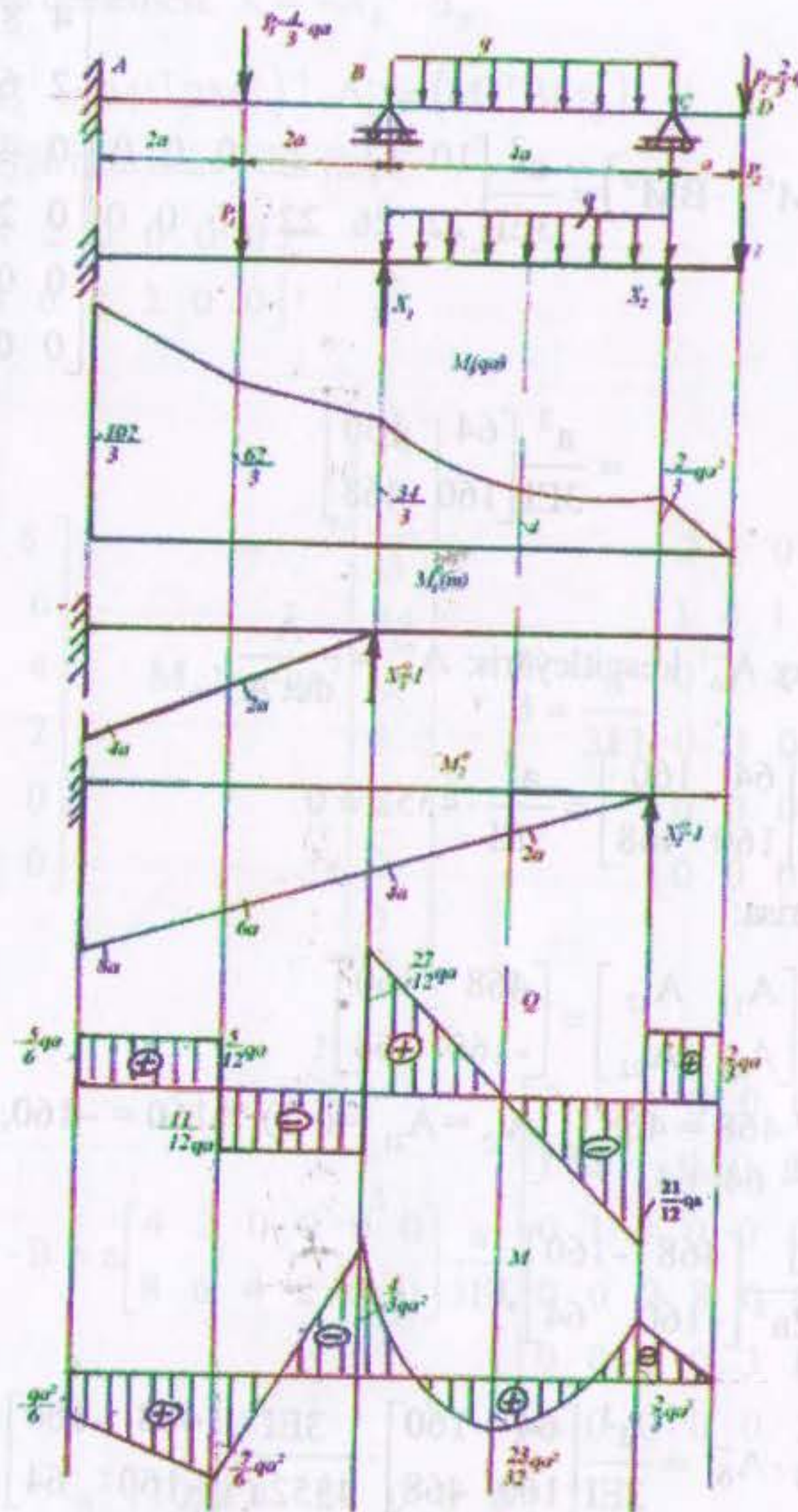
$$A_{22} = (-1)^{2+2} \cdot 64 = 64,$$

$$A_{\delta}^{-1} = \frac{3EI}{4352a^3} \begin{bmatrix} 468 & -160 \\ -160 & 64 \end{bmatrix},$$

$$A_{\delta} \cdot A_{\delta}^{-1} = \frac{a^3}{3EI} \begin{bmatrix} 64 & 160 \\ 160 & 468 \end{bmatrix} \cdot \frac{3EI}{4352a^3} \begin{bmatrix} 468 & -160 \\ -160 & 64 \end{bmatrix} =$$

$$\text{Barlagy} = \frac{1}{4352} \begin{bmatrix} 4352 & 0 \\ 0 & 4352 \end{bmatrix} = E$$

Ters matrisa dogry hasaplanan.



6.53-nji surat

$$\Delta_p = -\frac{a^2}{3EI} \begin{bmatrix} 10 & 12 & 2 & 0 & 0 & 0 \\ 22 & 36 & 22 & 16 & 0 & 0 \end{bmatrix} \begin{bmatrix} 34 \\ 62 \\ 3 \\ 34 \\ 3 \\ 4 \\ 2 \\ 3 \\ 0 \end{bmatrix} qa^2 = -\frac{qa^4}{9EI} \begin{bmatrix} 1764 \\ 6416 \end{bmatrix}$$

$$\text{Onda } X = \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} = \frac{3EI}{4352a^3} \begin{bmatrix} 468 & -160 \\ -160 & 64 \end{bmatrix} \cdot \frac{qa^4}{9EI} \begin{bmatrix} 1764 \\ 5416 \end{bmatrix} = \begin{bmatrix} 3,14 \\ -4,93 \end{bmatrix} qa$$

$$X_1 = 3,14qa, \quad X_2 = -4,93qa.$$

6.53. $N = 1,06 \text{ kN}$.

$$ql = q_1 l + P_2 \quad (1), \quad f_1 = f_2,$$

$$f_1 = \frac{5q_1 l^4}{384EI_1}, \quad f_2 = \frac{P_2 l^3}{48EI_2};$$

$$\frac{5q_1 l}{384I_1} = \frac{P_2}{48I_2} \Rightarrow \frac{5q_1 l}{8I_1} = \frac{P_2}{I_2};$$

$$q_1 = \frac{8}{5l} \cdot \frac{I_1}{I_2} P_2, \quad (2).$$

(2) aňlatmany (1) goýup alarys:

$$ql = P_2 \left(1 + \frac{8}{5} \cdot \frac{I_1}{I_2} \right),$$

$$P_2 = \frac{ql}{1 + \frac{8}{5} \cdot \frac{I_1}{I_2}} = \frac{5 \cdot 1}{1 + \frac{8}{5} \cdot \frac{12,56 \cdot 10^3}{5,44 \cdot 10^3}} = \frac{5}{4,7} = 1,06 \text{ kN}.$$

$$6.54. P_1 = \frac{\ell_2^3 I_1}{(\ell_2^3 I_1 + \ell_1^3 I_2)} \cdot P, \quad P_2 = \frac{\ell_1^3 I_2}{(\ell_2^3 I_1 + \ell_1^3 I_2)} \cdot P.$$

Goý, ýokarky we aşaky balkalar, degişlilikde, P_1 we P_2 güýçleri kabul edýän bolsunlar, onda

$$P = P_1 + P_2, \quad (1).$$

Balkalaryň ortasyndaky egrelmeleriň deňligi üçin

$$\frac{P_1 \ell_1^3}{48EI_1} = \frac{P_2 \ell_2^3}{48EI_2} \quad (2).$$

(1) we (2) aňlatmalardan

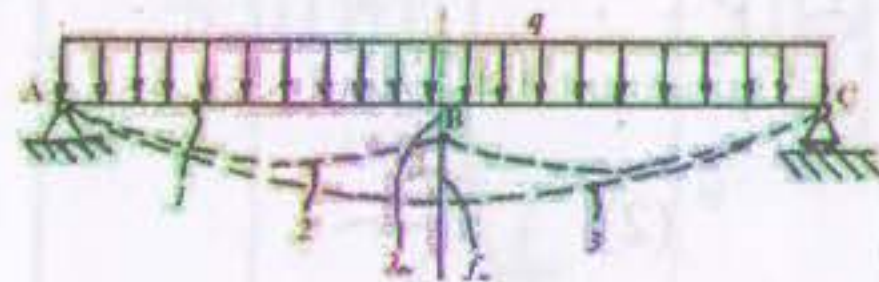
$$P_1 = \frac{\ell_2^3 I_1}{(\ell_2^3 I_1 + \ell_1^3 I_2)} \cdot P, \quad P_2 = \frac{\ell_1^3 I_2}{(\ell_2^3 I_1 + \ell_1^3 I_2)} \cdot P.$$

$$6.55. P_1 = 0,19P, \quad P_2 = 0,81P.$$

$$P_1 + P_2 = P, \quad \frac{P_1 \ell_1^3}{3EI_1} = \frac{P_2 \ell_2^3}{3EI_2}$$

Bu ýerden $P_1 = 0,19P$, $P_2 = 0,81P$.

$$6.56. R_{pr} = 30,32 \text{ kN}.$$



6.56-njy surat

Durkuny üýtgetmäniň bilelikdäki deňlemesi:

$$f_q = f_B + \lambda_{pr} \quad \text{ýa-da} \quad \frac{5q(2\ell)^4}{384EI} = \frac{R_B}{c} + \frac{R_B(2\ell)^3}{48EI};$$

$$\text{Bu ýerden} \quad R_B = R_{pr} = \frac{5cq\ell^4}{4(6EI + c\ell^3)} = 30,32 \text{ kN}.$$

$$6.57. P = 0,55 \text{ kN}.$$

$$X_1 \delta_{11} + \Delta_{1p} = 0, \quad \delta_{11} = \frac{\ell^3}{3},$$

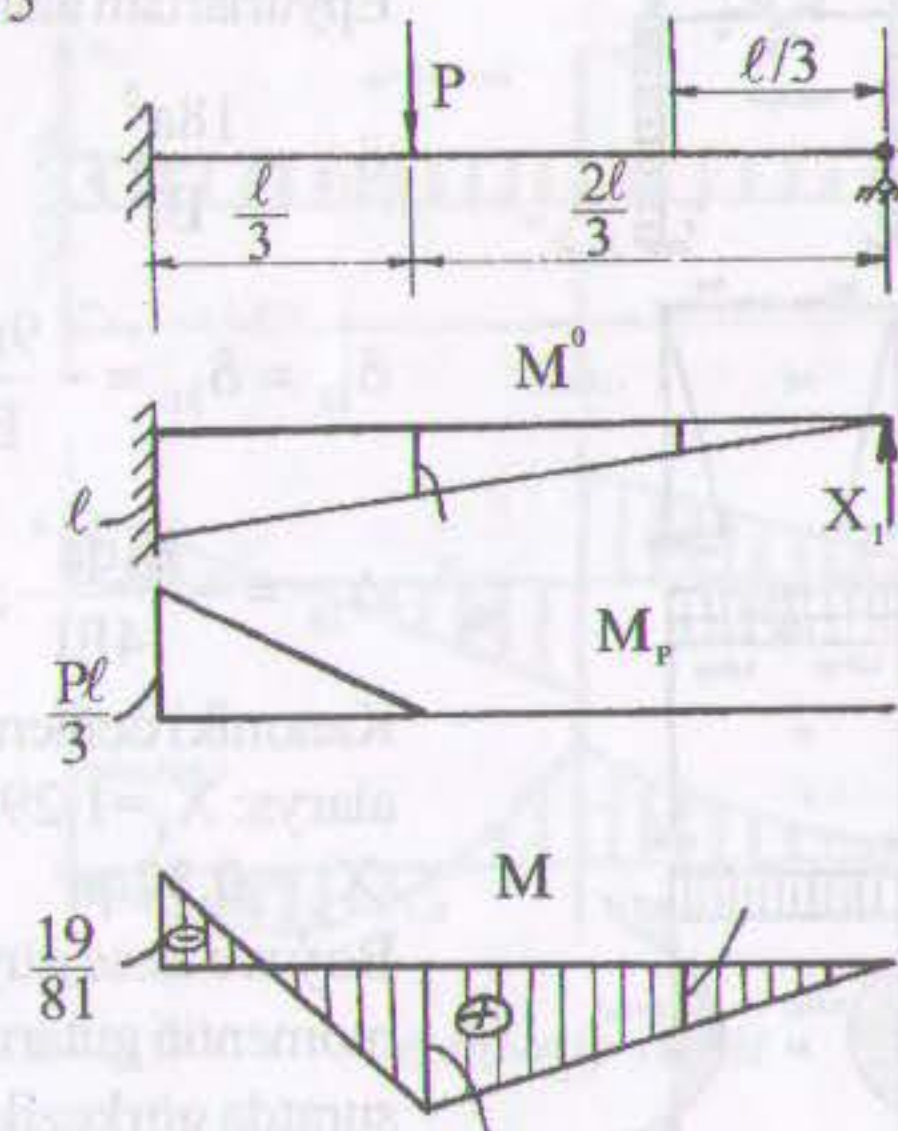
$$\Delta_{1p} = \frac{-\ell}{18EI} \left(2 \frac{P\ell}{3} \cdot \ell + \frac{P\ell}{3} \cdot \frac{2\ell}{3} \right) = \frac{-4P\ell^3}{81},$$

$$X_1 = \frac{4P\ell^3 \cdot 3}{81 \cdot \ell^3} = \frac{4}{27} P,$$

$$\sigma = E\varepsilon = 2 \cdot 10^4 \cdot 10^{-4} = 2 \text{ kN/sm}^2,$$

$$\sigma = \frac{M \cdot y}{I} = \frac{4 \cdot 150 \cdot 12 \cdot 3}{81 \cdot 4 \cdot 12^3} P = 2.$$

$$\text{Bu ýerden} \quad P = \frac{41}{75} \text{ kN} = 0,55 \text{ kN}.$$



6.57-njy surat

6.58. Berlen çarçuwa üç gezek statiki kesgitlenmeyän. Çarçuwany ok simmetriýasy boýunça kesýäris.

Kanoniki deňlemeler:

Kanoniki deňlemeler:

$$\begin{cases} X_1\delta_{11} + X_2\delta_{12} + X_3\delta_{13} + \Delta_{1p} = 0 \\ X_1\delta_{21} + X_2\delta_{22} + X_3\delta_{23} + \Delta_{2p} = 0 \\ X_1\delta_{31} + X_2\delta_{32} + X_3\delta_{33} + \Delta_{3p} = 0 \end{cases}$$

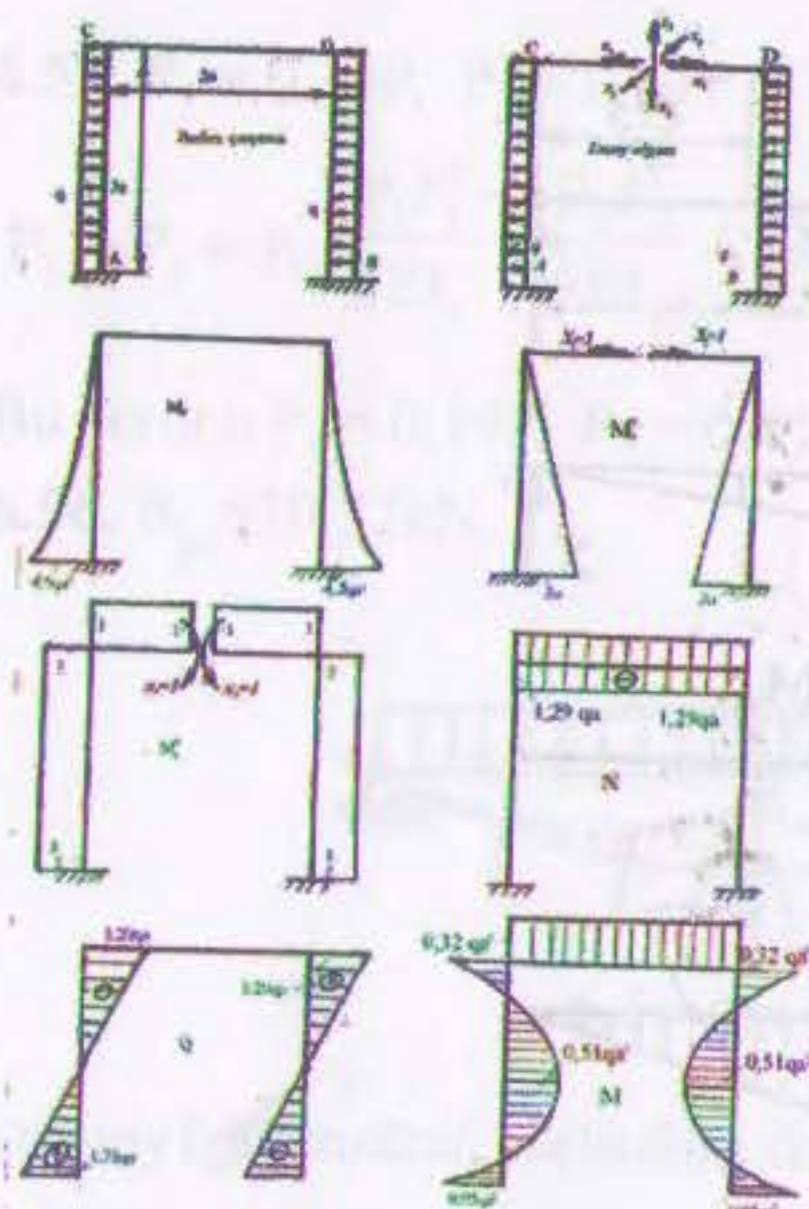
M_1^0, M_3^0 – simmetriýaly epýurlar, M_2^0 – ters simmetriýaly epýur.

Şonuň üçin hem $\delta_{12} = \delta_{21} = 0$; $\delta_{23} = \delta_{32} = 0$.

M_p epýur simmetriýaly, onda $\Delta_{2p} = 0$.

Kanoniki deňlemeler aşakdaky ýaly görnüşe geçýär:

$$\begin{cases} X_1\delta_{11} + X_3\delta_{13} + \Delta_{1p} = 0 \\ X_1\delta_{31} + X_3\delta_{33} + \Delta_{3p} = 0 \end{cases}$$



6.58-nji surat

6.59. $f_B = \frac{q\ell^4}{24EI}$

Ortaký diregi aýryp, B nokatdaky egrelmäni tapýarys:

Epýurlardan alarys:

$$\delta_{11} = \frac{18a^3}{EI};$$

$$\delta_{13} = \delta_{31} = -\frac{9a^2}{EI}; \delta_{33} = \frac{8a}{EI};$$

$$\Delta_{1p} = -\frac{81qa^4}{4EI}; \Delta_{3p} = \frac{9qa^3}{EI}.$$

Kanoniki deňlemeleri işläp

alarys: $X_1 = 1,29qa$,

$X_3 = 0,32qa^2$.

Boý we kese güýçleriň we egme momentiniň gutarnykly epýurlary suratda görkezilen.

$$f_{B_q} = \frac{5q\ell^4}{24EI},$$

B nokatdaky R_B güýçden egrelme

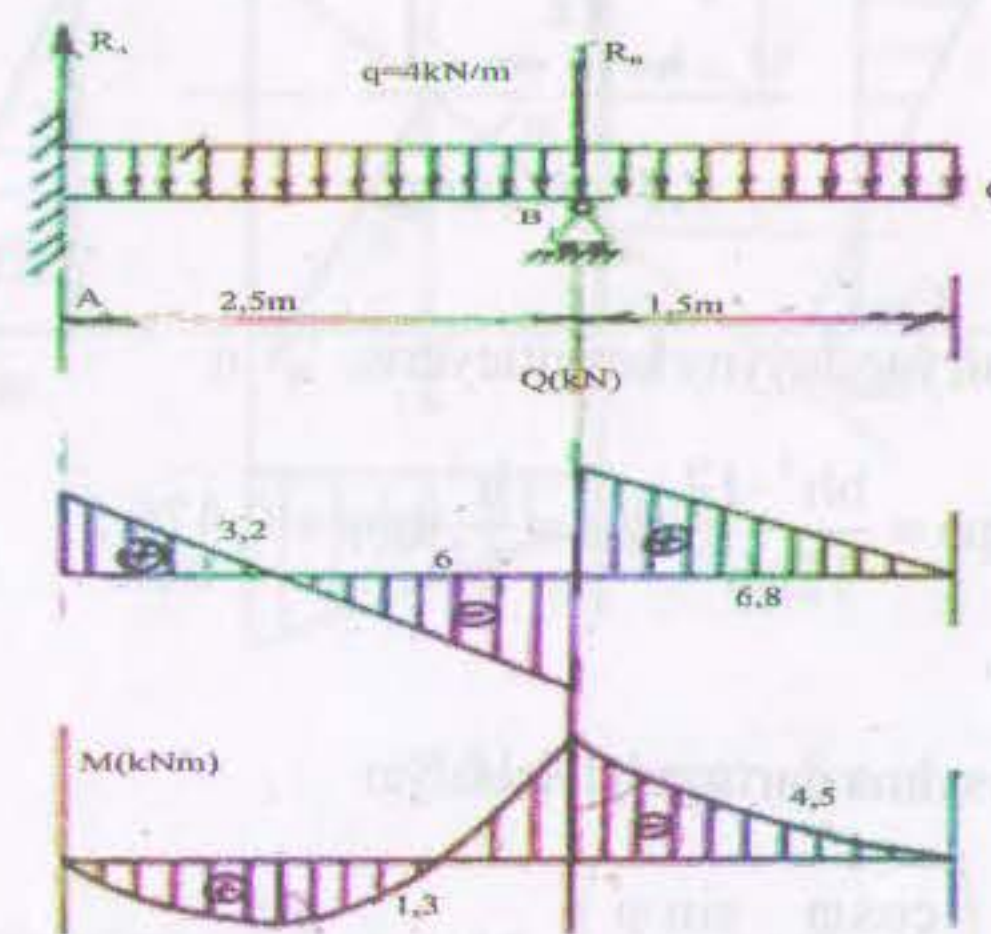
$$f_{BR_B} = \frac{q\ell^4}{6EI},$$

Onda B kesigiň mümkin bolan egrelmesi:

$$f_B = f_{B_q} - f_{BR_B} = \frac{q\ell^4}{24EI}.$$

Bu ýerden çetki direglere garanyňda ortaky direg $\frac{q\ell^4}{24EI}$ deň ululykda aşakda ýerleşen.

6.60. $R_B = 12,8\text{kN}$.



6.60-njy surat

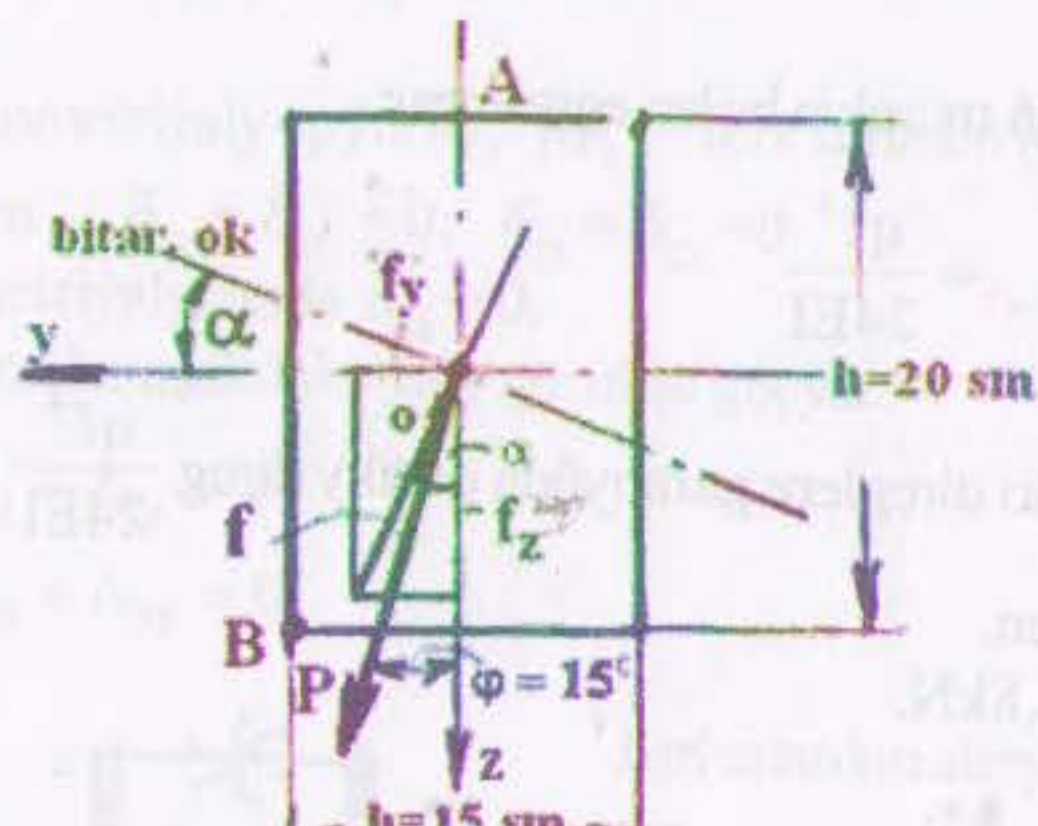
$$\sum M_A = q \frac{4^2}{2} - R_B \cdot 2,5 = 0, \quad R_B = 12,8\text{kN}.$$

$$R_A = q \cdot 4 - R_B = 16 - 12,8 = 3,2\text{kN}.$$

Q we M epýurlary adaty usul bilen gurlan we suratda görkezilen.

VII bap Çylşyrymly garşylyk

7.1. $\alpha = 25^\circ 28'$; $f = 0,605 \text{ sm}$; $\sigma_A = -0,98 \text{ kN/sm}^2$.



7.1-nji surat

Bitarap okuň ýagdaýyny kesgitleýäris.

$$\operatorname{tg} \alpha = \frac{I_y}{I_z} \operatorname{tg} \varphi = \frac{bh^3 \cdot 12}{12hb^3} \operatorname{tg} \varphi = \frac{h^2}{b^2} \operatorname{tg} \varphi = 0,476;$$

$$\alpha = 25^\circ 28'$$

Anokatda iň uly gysylma dartgynlyk bolýar.

$$\sigma_A = -M_{\max} \left(\frac{\cos \varphi}{w_z} + \frac{\sin \varphi}{w_y} \right); \quad M_{\max} = \frac{P\ell}{4}$$

$$\sigma_A = -\frac{P\ell}{4} \left(\frac{6 \cos \varphi}{bh^2} + \frac{6 \sin \varphi}{b^2h} \right) = -0,98 \text{ kN/sm}^2,$$

z we y oklaryň ugry boýunça iň uly progib

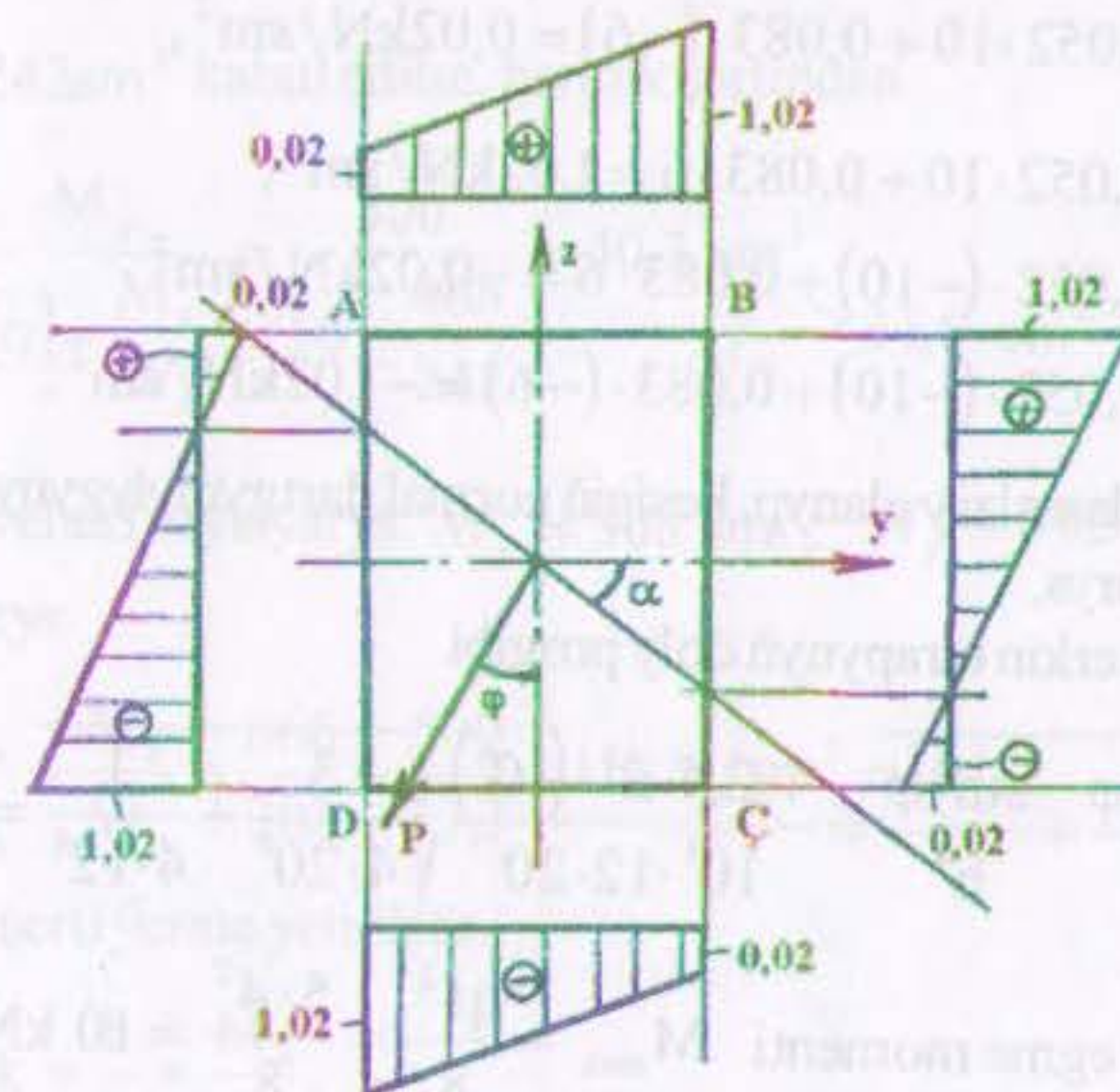
$$f_z = \frac{P_z \ell^3}{48EI_y}; \quad f_y = \frac{P_y \ell^3}{48EI_z}; \quad I_y = \frac{bh^3}{12}; \quad I_z = \frac{b^3h}{12},$$

$$\text{onda } f = \sqrt{f_z^2 + f_y^2} = \sqrt{\left(\frac{P\ell^3 \sin \varphi}{48EI_z} \right)^2 + \left(\frac{P\ell^3 \cos \varphi}{48EI_y} \right)^2} = 0,605 \text{ sm.}$$

Progibiň ugry z ok bilen $\alpha = 25^\circ 28'$ burç boýunça ugrukdyrylan.

7.2. $\sigma_A = 0,02 \text{ kN/sm}^2$, $\sigma_B = 1,02 \text{ kN/sm}^2$,

$$\sigma_C = 0,02 \text{ kN/sm}^2, \quad \sigma_D = -1,02 \text{ kN/sm}^2, \quad f = 1,31 \text{ sm.}$$



7.2-nji surat

Bitarap okuň ýagdaýy

$$\operatorname{tg} \alpha = \frac{I_z}{I_y} \operatorname{tg} \varphi = \frac{h^2}{b^2} \operatorname{tg} 30^\circ = 1,58,$$

$$\alpha = 57^\circ 42'$$

Iň uly egme moment $M = P\ell$.

Kesigiň islendik nokadyndaky doly dartgynlyk

$$\begin{aligned}\sigma &= M \left(\frac{\cos \varphi}{I_z} \cdot y + \frac{\sin \varphi}{I_y} \cdot z \right) = \\ &= 2,4 \cdot 200 \left(\frac{\cos 30^\circ \cdot 12}{12 \cdot 20^3} \cdot y + \frac{\sin 30^\circ \cdot 12}{20 \cdot 12^3} \cdot z \right) = \\ &= 0,052y + 0,083z.\end{aligned}$$

onda

$$\begin{aligned}\sigma_A &= 0,052 \cdot 10 + 0,083 \cdot (-6) = 0,02 \text{ kN/sm}^2, \\ \sigma_B &= 0,052 \cdot 10 + 0,083 \cdot 6 = 1,02 \text{ kN/sm}^2, \\ \sigma_C &= 0,052 \cdot (-10) + 0,083 \cdot 6 = -0,02 \text{ kN/sm}^2, \\ \sigma_D &= 0,052 \cdot (-10) + 0,083 \cdot (-6) = -1,02 \text{ kN/sm}^2.\end{aligned}$$

Ýokardaky hasaplamalary ulanyp, kesigiň normal dartgynlygynyň epýurlaryny gurýarys.

Balkanyň erkin tarapynyň doly progibi

$$f = \frac{4P\ell^3}{Eb^3} \sqrt{\frac{\cos^2 \varphi}{h^4} + \frac{\sin^2 \varphi}{b^4}} = \frac{4 \cdot 2,4 \cdot 2^3 \cdot (10^6)}{10^3 \cdot 12 \cdot 20} \sqrt{\frac{3}{4 \cdot 20^4} + \frac{1}{4 \cdot 12^4}} = 1,31 \text{ sm}$$

7.3. İn uly doly egme momenti $M_{\max} = \frac{q\ell^2}{8} = \frac{5 \cdot 4^2}{8} = 10 \text{ kNm}.$

Baş oklar boýunça egme momentler

$$M_x = M_{\max} \cdot \cos 30^\circ = 8,66 \text{ kNm}, \quad M_y = M_{\max} \cdot \sin 30^\circ = 5 \text{ kNm}.$$

Berklik şerti $\sigma = \frac{M_x}{W_x} + \frac{M_y}{W_y} \leq [\sigma].$

Diňe M_x täsirinden talap edilyän garşylyk moment

$$W_x = \frac{M_x}{[\sigma]} = \frac{8,66 \cdot 10^2}{16} = 54 \text{ sm}^3,$$

DÖST 8240-56 boýunça N12 şweller gabat gelyär.

M_y täsirinden

$$W_y = \frac{5 \cdot 10^2}{16} = 31,2 \text{ sm}^3 \Rightarrow \text{N24 şweller degişli.}$$

Diýmek, şweller N24 kiçi bolmaly däl.

Meseläni yzygiderli ýakynlaşdyrma usuly bilen işleýäris.

Birinji ýakynlaşmada 24-nji belgili şwelleri saýlaýarys. DÖST 8240-56

boýunça $W_x = 242 \text{ sm}^3$, $W_y = 31,6 \text{ sm}^3$.

$W_x = 242 \text{ sm}^3$ kabul edilse, berklik şertinden

$$W_y = \frac{M_y}{[\sigma] - \frac{M_x}{W_x}} = \frac{500}{16 - \frac{866}{242}} = 40,3 \text{ sm}^3 > 31,6 \text{ sm}^3$$

№27 şwelleri saýlaýarys: $W_x = 308 \text{ sm}^3$; $W_y = 37,3 \text{ sm}^3$.

Barlaýarys:

$$\sigma = \frac{M_x}{W_x} + \frac{M_y}{W_y} = \frac{866}{308} + \frac{500}{37,3} = 16 \text{ kN/sm}^2 = [\sigma].$$

Berklik şerti ýerine ýetirilyär.

7.4. $k = \frac{h}{b} = \frac{M_x}{M_y}.$

Berklik şertinden

$$\frac{M_x}{W_x} + \frac{M_y}{W_y} \leq [\sigma], \quad W_x = \frac{k^2 b^3}{6}; \quad W_y = \frac{kb^3}{6}.$$

$$b = \sqrt[3]{\frac{6M_x + 6M_y k}{[\sigma]^2 k}}; \quad A = h \cdot b = \sqrt[3]{\frac{36(M_x + kM_y)^2}{[\sigma]^2 k}}.$$

İn kiçi meýdan $\frac{dA}{dk} = 0.$

onda $k = \frac{h}{b} = \frac{M_x}{M_y}$.

7.5. $k = \frac{1}{\sqrt{\operatorname{tg} \varphi}}$.

Konsolyn erkin tarapyndaky progibiň deňlemesinden,

$$[f] = \sqrt{\left(\frac{P\ell^3 \cos \varphi}{3EI_x} \right)^2 + \left(\frac{P\ell^3 \sin \varphi}{3EI_x} \right)^2}$$

Balkanyň kesiginiň meýdanyny tapýarys.

$$A = \sqrt[4]{\frac{144P^2\ell^6(k^4 \cos^2 \varphi + \sin^2 \varphi)}{9k^2 E[f^2]}}; \quad \frac{dA}{dk} = 0 \text{ şertden,}$$

$$k = \frac{1}{\sqrt{\operatorname{tg} \varphi}}.$$

7.6. №22 iki tawra.

Gyýa egilmäniň berklik şertinden alarys:

$$W_z = \frac{P\ell}{4[\sigma]} \left(\cos \varphi + \frac{W_z}{W_y} \sin \varphi \right) = 58,75 + 21,38 \frac{W_z}{W_y};$$

Yzygiderli çemeleşme ýoly arkaly kesigi saýlaýarys. W_z/W_y

gatnaşyk iki tawra balka üçin 6-15 aralygynda $\frac{W_z}{W_y} = 6$ kabul edýäris.

$$\text{Onda } W_z \geq 58,75 + 21,38 \cdot 6 = 185 \text{ sm}^3,$$

$$\text{Eger } \frac{W_z}{W_y} = 15 \text{ bolsa, onda } W_z \geq 58,75 + 21,38 \cdot 15 = 380 \text{ sm}^3.$$

$$W_z = 184 \text{ sm}^3 \text{ N20 iki tawra, } W_z = 371 \text{ sm}^3 \text{ N27 iki tawra degişli.}$$

$$\text{N22 saýlaýarys, } W_z = 232 \text{ sm}^3; \quad W_y = 28,6 \text{ sm}^3$$

$$\frac{W_z}{W_y} = \frac{232}{28,6} = 8,11$$

Bu belgidäki iki tawranyň iň uly normal dartgynlygy

$$\sigma_{\max} = \frac{P\ell}{4W_z} \left(\cos \varphi + \frac{W_z}{W_y} \sin \varphi \right) = 16,01 \text{ kN/sm}^2 \approx [\sigma].$$

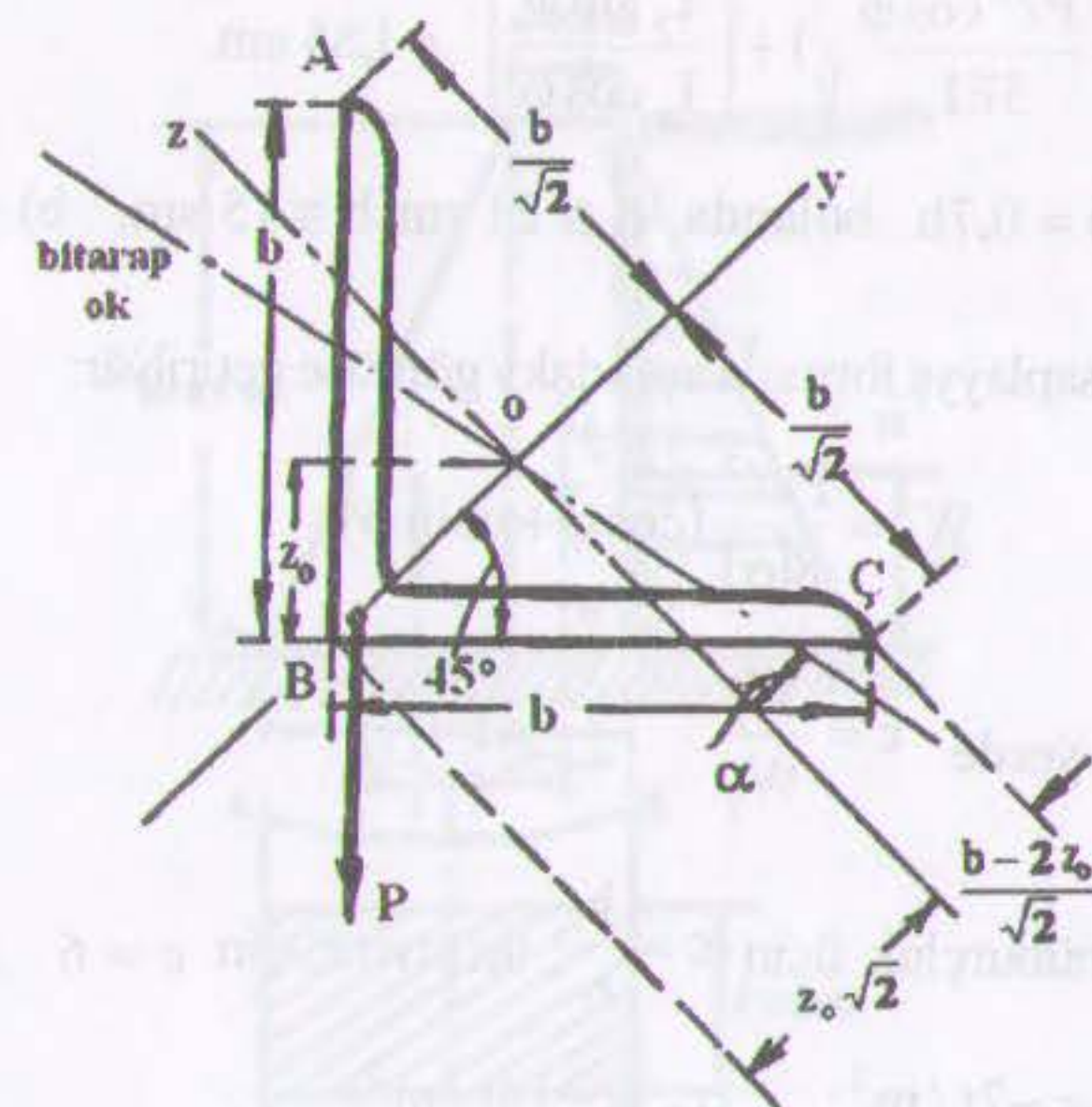
№22 iki tawrany saýlaýarys.

$$7.7. \sigma_A = 16,64 \text{ kN/sm}^2; \quad \sigma_B = -13,32 \text{ kN/sm}^2; \quad \sigma_C = 4,33 \text{ kN/sm}^2;$$

$$f = 1,85 \text{ sm.}$$

Burçlugyň howply kesiginiň islendik nokadyndaky normal dartgynlyk

$$\sigma = M_{\max} \left(\frac{\sin \varphi}{I_z} \cdot y + \frac{\cos \varphi}{I_y} \cdot z \right) = 419y + 108,8z \quad (1), \quad \varphi = 45^\circ.$$



7.7-nji surat

Bu deňlemeden bitarap okuň ugruny kesgitleýäris:

$$\operatorname{tg} \alpha = \frac{y}{z} = \frac{108,8}{419} \approx -0,26 = \operatorname{tg}(-14^{\circ}33'),$$

A, B we Ç nokatlaryň koordinatlary

$$y_A = y_C = \frac{b - 2z_0}{\sqrt{2}} = 2,5 \text{ sm};$$

$$z_A = -z_C = \frac{b}{\sqrt{2}} = 5,66 \text{ sm}.$$

$$y_B = -z_0 \sqrt{2} = -3,15 \text{ sm}; \quad z_B = 0.$$

(1) deňlemä goýup alarys:

$$\sigma_A = 16,64 \text{ kN/sm}^2; \quad \sigma_B = -13,32 \text{ kN/sm}^2; \quad \sigma_C = 4,33 \text{ kN/sm}^2.$$

Burçlugyň iň uly progibi

$$f = \frac{P\ell^3 \cos \varphi}{3EI_y} \sqrt{1 + \left(\frac{I_y \sin \varphi}{I_z \cos \varphi} \right)^2} = 1,85 \text{ sm}.$$

7.8. a) $b = 0,7h$ bolanda, $h \approx 21 \text{ sm}$, $b \approx 15 \text{ sm}$. b) N20a ikitawra.

Hasaplaýyş formula aşakdaky görnüşe getirilýär:

$$W_z = \frac{Pa\ell^3}{8[\sigma]} (\cos \varphi + c \sin \varphi);$$

Bu ýerde $c = \frac{W_z}{W_y}$

gönüburçluk üçin $c = \frac{h}{b}$; iki tawra üçin $c = 6 \dots 8$.

7.9. $\sigma_A = -2 \text{ t/m}^2; \quad \sigma_B = -14 \text{ t/m}^2.$

$$\sigma = \frac{Q}{A} \pm \frac{M_{\max}}{W} - \text{sütüniň esasyndaky dartgynlylyk}$$

A nokatdaky dartgynlylyk, $Q = \gamma \cdot \ell A$; $A = 1 \text{ m}^2$;

$$W = \frac{1}{6} \text{ m}^3.$$

$$\sigma_A = -\gamma \ell + \frac{q\ell^2}{2W} = -1,6 \cdot 5 + \frac{0,08 \cdot 5^2 \cdot 6}{2 \cdot 1} = -8 + 6 = -2 \text{ t/m}^2;$$

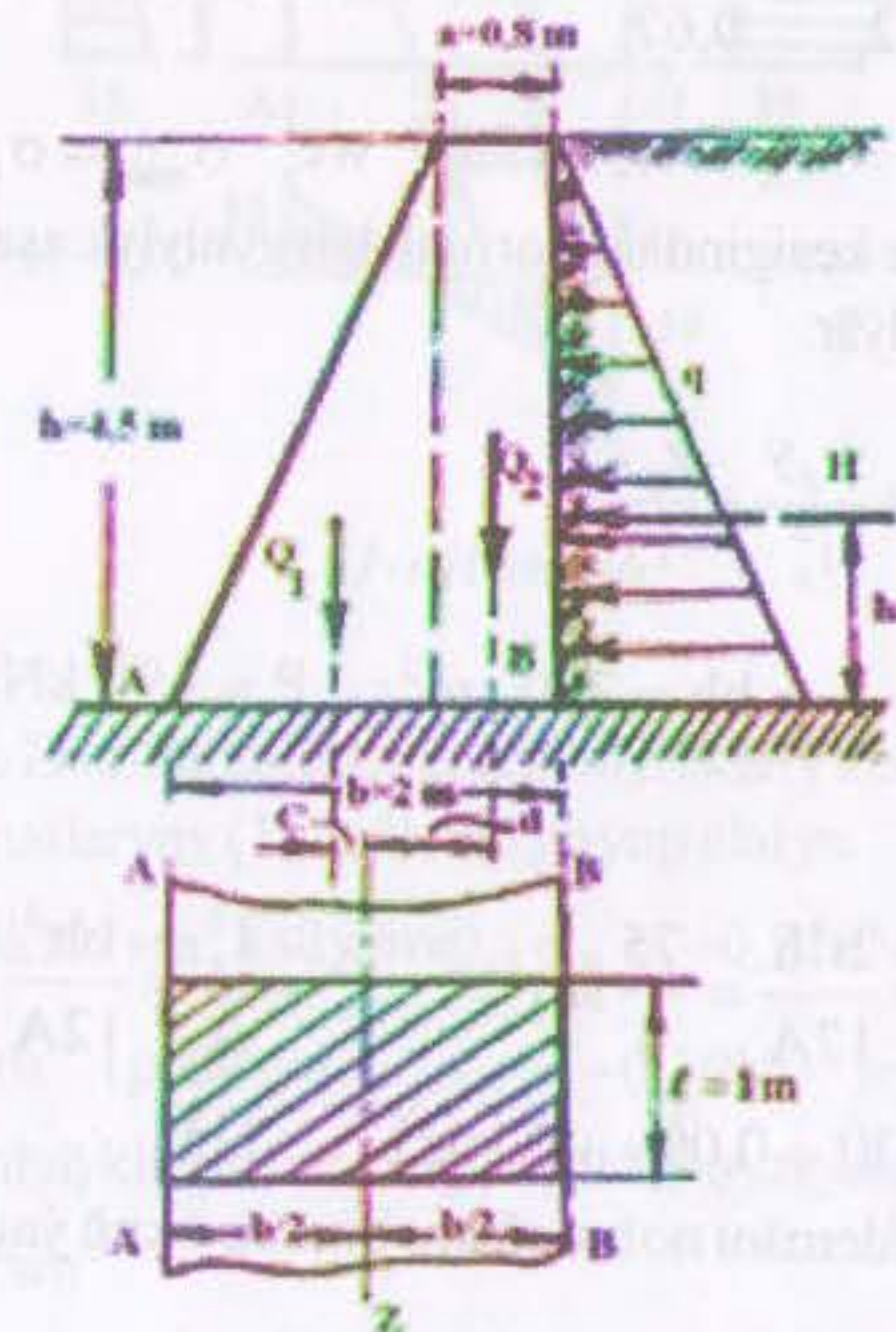
B nokatdaky dartgynlylyk

$$\sigma_B = -\gamma A - \frac{q\ell^2}{2W} = -8 - 6 = -14 \text{ t/m}^2.$$

7.10. $\sigma_A = 8,89 \text{ t/m}^2; \quad \sigma_B = 2,45 \text{ t/m}^2.$

Diwaryň 1 m uzynlygyna seredýäris.

Diwaryň esasyndaky kesikde iň uly we iň kiçi dartgynlylyk aşakdaky formula boýunça kesgitlenýär:



7.10-njy surat

$$\sigma_{\max/\min} = \frac{N}{A} \pm \frac{M}{W};$$

$N = Q_1 + Q_2$. $Q_1 = \frac{1}{2}h(b-a)\gamma\ell = 4,86\text{ t}$ – diwaryň 1m uzynlygynyň üçburçluk böleginiň agramy,

$Q_2 = ha \cdot \gamma\ell = 6,48\text{ t}$ – diwaryň 1m uzynlygynyň prizma böleginiň agramy.

Diwaryň esasynyň merkezi okuna görä egme momenti

$$M_z = Q_1\left(a + \frac{b-a}{3} - \frac{b}{2}\right) + Q_2\left(\frac{b}{2} - \frac{a}{2}\right) + \frac{q_{\max}h}{2} \cdot \frac{h}{3} = 2,15\text{ tm}.$$

$$A = b\ell = 2\text{ m}^2; \quad W_z = \frac{\ell b^2}{6} = 0,67\text{ m}^2;$$

$$\text{Onda } \sigma_{\max/\min} = \frac{11,34}{2} \pm \frac{2,5}{0,67} = 5,67 \pm 3,22\text{ t/m}^2.$$

Bu ýerden, $\sigma_{\max} = \sigma_A = 8,89\text{ t/m}^2$ we $\sigma_{\min} = \sigma_B = 2,45\text{ t/m}^2$.

7.11. Diregiň kese kesigindäki normal dartgynlylyk aşakdaky formula boýunça kesgitlenilýär.

$$\sigma = \frac{P}{A} \left(1 + \frac{y_p y}{i_z^2} + \frac{z_p z}{i_y^2} \right);$$

bu ýerde $A = bh = 300\text{ sm}^2$; $P = -90\text{ kN}$;

$y_p = z_p = 3\text{ sm}$.

$$i_y^2 = \frac{I_y}{A} = \frac{b^3 h}{12A} = \frac{75}{4}\text{ sm}^2; \quad i_z^2 = \frac{I_z}{A} = \frac{bh^3}{12A} = \frac{100}{3}.$$

$$\text{Onda } \sigma = -0,3(1 + 0,09y + 0,16z) \quad (1)$$

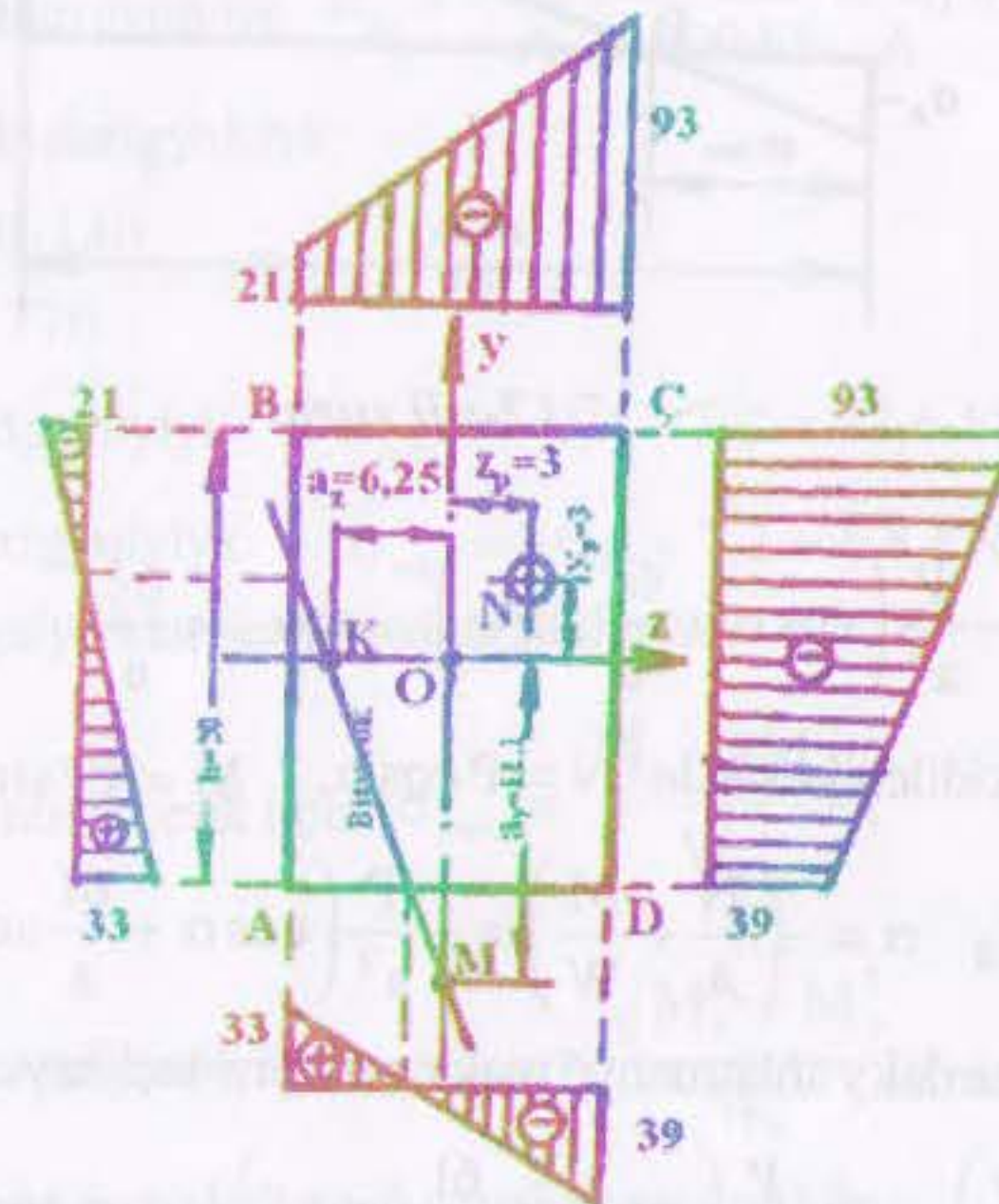
Soňky deňlemäni nola deňläp, bitarap okuň ýagdaýyny kesgitleýäris.

$$1 + 0,09y_o + 0,16z_o = 0;$$

Eger $z_o = 0$; $a_y = -11,1\text{ sm}$. (M nokat)

$$y_o = 0; \quad a_z = -\frac{1}{0,16} = -6,25\text{ sm}. \quad (\text{K nokat})$$

Bitarap ok M we K nokatlaryň üstünden geçýär.



7.11-nji surat

A, B, Ç we D nokatlardaky dartgynlylyklary kesgitleýäris. Bu nokatlaryň koordinatlaryny (1) deňlemä goýup alarys.

$$\sigma_A = 0,33\text{ kN/sm}^2 \text{ (süýnme)}, \quad \sigma_B = -0,21\text{ kN/sm}^2 \text{ (gysylma)},$$

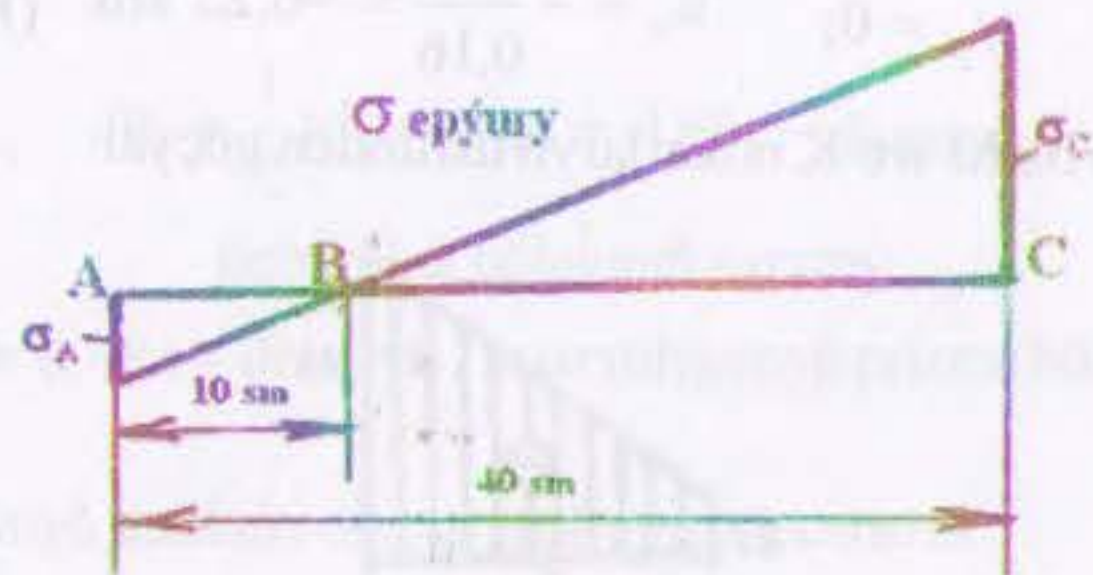
$$\sigma_C = -0,93\text{ kN/sm}^2 \text{ (gysylma)}, \quad \sigma_D = -0,39\text{ kN/sm}^2 \text{ (gysylma)}.$$

Bu dartgynlylyklaryň bahalary boýunça çyzgyda epýurlar gurlan.

7.12. $\sigma = 0,6\text{ kN/sm}^2$.

Üçburçluklaryň meňzeşliklerinden

$$\frac{\sigma_A}{10} = \frac{\sigma_C}{30} \Rightarrow \sigma_C = 3\sigma_A = 3 \cdot 0,2 = 0,6 \text{ kN/sm}^2$$



7.12-nji surat

7.13. $\sigma = -\frac{P}{a^2} \left(\cos \alpha + \frac{6\ell}{a} \sin \alpha \right); \quad \text{tg} \alpha_0 = \frac{6\ell}{a}.$

Berkidilen kesikde $N = P \cos \alpha$, $M = P\ell \sin \alpha$

Onda $\sigma = -\left(\frac{N}{A} + \frac{M}{W} \right) = -\frac{P}{a^2} \left(\cos \alpha + \frac{6\ell}{a} \sin \alpha \right).$

Ýokardaky aňlatmanyň maksimumyny tapýarys.

$$\left(\frac{d\sigma}{d\alpha} \right)_{\alpha=\alpha_0} = \frac{P}{a^2} \left(\sin \alpha_0 + \frac{6\ell}{a} \cos \alpha_0 \right) = 0 \Rightarrow \text{tg} \alpha_0 = \frac{6\ell}{a}$$

onda $\sigma = -\frac{P}{a^2} \cdot \frac{\cos(\alpha - \alpha_0)}{\cos \alpha_0}.$

7.14. 26-njy belgili şweller.

Zynjyryň dartuwy $P = Q$, onda bu güýçleriň deňtäsi redijisi bloguň okundan geçýär we dargadylandan soň $N = T = Q = 40 \text{ kN}$ balka gysylma we egilmä sezewar bolýar.

Ilki bilen gysylmany hasaba alman, şwelleriň belgisini kesgitleýäris.

$$W = \frac{M}{[\sigma]} = \frac{40 \cdot 140}{8} = 700 \text{ sm}^3$$

Goşmaça gysylmany hasaba alyp, garşylyk momentiň bahasyny artdyryp alarys.

N26 iki şweller degişli.

$$W_x = 2 \cdot 388 = 776 \text{ sm}^3; \quad A = 2 \cdot 49,95 = 99,85 \text{ sm}^2$$

Gysylma dartgynlylyk $\sigma_g = -\frac{N}{A} = -\frac{40}{99,85} = -0,4 \text{ kN/sm}^2.$

Egilmedäki dartgynlylyk

$$\sigma_e = \pm \frac{M}{W} = \pm \frac{40 \cdot 140}{776} = \pm 7,2 \text{ kN/sm}^2.$$

Iň uly dartgynlylyk $\sigma_{\max} = -0,4 - 7,2 = -7,6 \text{ kN/sm}^2.$

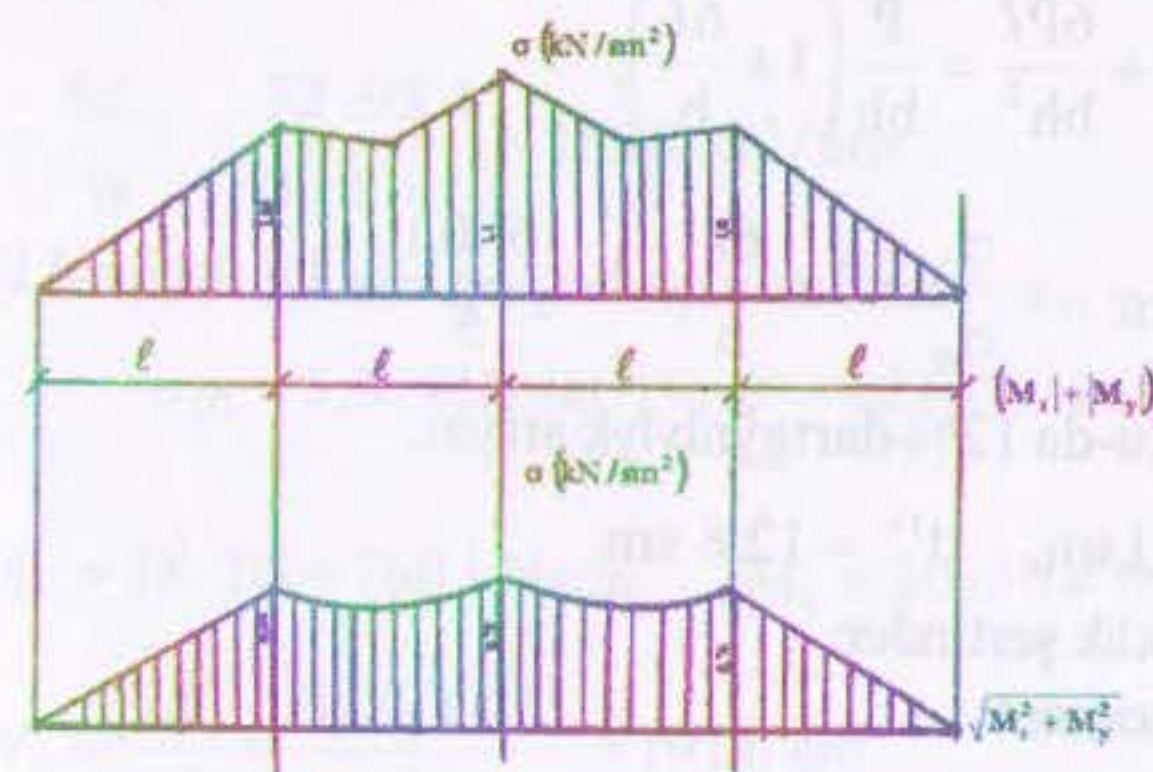
Iň kiçi dartgynlylyk $\sigma_{\min} = -0,4 + 7,2 = 6,8 \text{ kN/sm}^2.$

Bu dartgynlylyklar şerti kanagatlandyryýar.

7.15. Birinji görnüşli kesik üçin $\sigma_{\max} = \frac{|M_x| + |M_y|}{W_x};$

Ikinji görnüşli kesik üçin $\sigma_{\max} = \frac{\sqrt{M_x^2 + M_y^2}}{W_x}.$

Dartgynlylyklaryň balkanyň uzynlygyna ýaýraýşy:



7.15-nji surat

7.16. $xy = \frac{h\ell}{12}$ – giperbolanyň deňlemesi.

Direglerdäki gaýtargylar

$$R_A = R_B = H \cdot \frac{h}{\ell};$$

Takmynan alnan nokatdaky dartgynlylyk

$$\sigma = \frac{H}{A} + \frac{H \cdot \frac{h}{2} \cdot y}{I} + \frac{R_B \left(\frac{1}{2} - x \right) \cdot y}{I};$$

bu aňlatma $\sigma = 0$, $I = \frac{bh^3}{12}$ goýup alarys $xy = \frac{1}{12} h\ell$.

Bu asimptotlar ox we oy deň bolan deňgapdally giperbolanyň deňlemesi

Bu egri çyzgyda punktir bilen görkezilen.

7.17. 12%

Ýük takyk goýlandaky dartgynlylyk

$$\sigma_0 = \frac{P}{bh};$$

Çyzgyda görkezilen ýüklenme boýunça

$$\sigma_1 = \frac{P}{bh} + \frac{6P\ell}{bh^2} = \frac{P}{bh} \left(1 + \frac{6\ell}{h} \right);$$

bu ýerden $\frac{\sigma_1}{\sigma_0} = 1 + \frac{6\ell}{h} = 1 + \frac{6 \cdot 0,1}{5} = 1 + 0,12 = 1,12$ esse,

ýa-da 12% dartgynlylyk artýar.

7.18. $d^{III} = 13,1 \text{ sm}$, $d^{IV} = 12,8 \text{ sm}$.

III – berklik şertinden

Hasap moment

$$M_{III} = \sqrt{M_e^2 + M_t^2} = \sqrt{12,5^2 + 12,5^2} = 17,625 \text{ kNm}.$$

$$\text{onda } d_{III} = \sqrt[3]{\frac{32M_{III}}{\pi[\sigma]}} = \sqrt[3]{\frac{32 \cdot 17,625 \cdot 10^2}{3,14 \cdot 8}} = 13,1 \text{ sm}.$$

IV – berklik şertinden

$$M_{IV} = \sqrt{12,5^2 + 0,75 \cdot 12,5^2} = 16,53 \text{ kNm}.$$

$$d_{IV} = \sqrt[3]{\frac{32 \cdot 16,53 \cdot 10^2}{3,14 \cdot 8}} = 12,8 \text{ sm}.$$

7.19. $\sigma_1 = 12,73 \text{ kN/sm}^2$; $\sigma_2 = 15,18 \text{ kN/sm}^2$.

1) Sterženiň berkidilen kesiginde egme moment

$$M_e = 2P \cdot 40 = 2 \cdot 1 \cdot 40 = 80 \text{ kNsm}.$$

Towlanma moment $M_t = 0$,

$$\text{onda } \sigma_1 = \frac{M_e}{W_z} = \frac{32M_e}{\pi d^3} = \frac{32 \cdot 80}{3,14 \cdot 4^3} = 12,73 \text{ kN/sm}^2;$$

2) Haýsy hem bolsa bir güýç aýrylan ýagdaýynda

$$M_e = P \cdot 40 = 40 \text{ kNsm},$$

$$M_t = P \cdot 100 = 100 \text{ kNsm},$$

$$\text{onda } M_{IV} = \sqrt{M_e^2 + 0,75 \cdot M_t^2} = \sqrt{40^2 + 0,75 \cdot 100^2} = 95,4 \text{ kNsm},$$

$$\text{we } \sigma_2 = \frac{M_{IV}}{W_z} = \frac{32 \cdot 95,4}{3,14 \cdot 4^3} = 15,18 \text{ kN/sm}^2.$$

7.20. $\sigma_1 = 4,51 \text{ kN/sm}^2$; $\sigma_3 = -0,56 \text{ kN/sm}^2$; $\sigma_{II} = 4,67 \text{ kN/sm}^2$;

$$\sigma_{III} = 5,06 \text{ kN/sm}^2; \sigma_{IV} = 4,81 \text{ kN/sm}^2.$$

$$M_e = 38 \cdot 20 = 760 \text{ kNsm}; \quad M_t = 20 \cdot 30 = 600 \text{ kNsm}.$$

$$W_z = \frac{\pi d^3}{32} = \frac{3,14 \cdot 12,5^3}{32} = 191,6 \text{ sm}^3$$

$$\sigma = \frac{M_e}{W_z} = \frac{760}{191,3} = 3,97 \text{ kN/sm}^2;$$

$$\tau = \frac{M_t}{2W_z} = \frac{600}{2 \cdot 191,3} = 1,57 \text{ kN/sm}^2$$

Baş dartgynlyklary belli formula boýunça kesgitleýäris.

$$\sigma_{1,3} = \frac{\sigma}{2} \pm \frac{1}{2} \sqrt{\sigma^2 + 4\tau^2} = \frac{3,97}{2} \pm \frac{1}{2} \sqrt{3,97^2 + 4 \cdot 1,57^2} = 1,985 \pm 2,53$$

$$\text{onda } \sigma_1 = 4,51 \text{ kN/sm}^2; \quad \sigma_3 = -0,56 \text{ kN/sm}^2.$$

II – berklik nazaryýeti boýunça

$$\sigma_{II} = \sigma_1 - \mu \sigma_3 = 4,51 + 0,3 \cdot 0,56 = 4,67 \text{ kN/sm}^2.$$

III – berklik nazaryýeti boýunça

$$\sigma_{III} = \sqrt{\sigma^2 + 4\tau^2} = \sqrt{3,97^2 + 4 \cdot 1,57^2} = 5,06 \text{ kN/sm}^2.$$

IV – berklik nazaryýeti boýunça

$$\sigma_{IV} = \sqrt{\sigma^2 + 3\tau^2} = \sqrt{3,97^2 + 3 \cdot 1,57^2} = 4,81 \text{ kN/sm}^2.$$

7.21. $d = 6,3 \text{ sm}$.

Deňagramlylyk şertinden

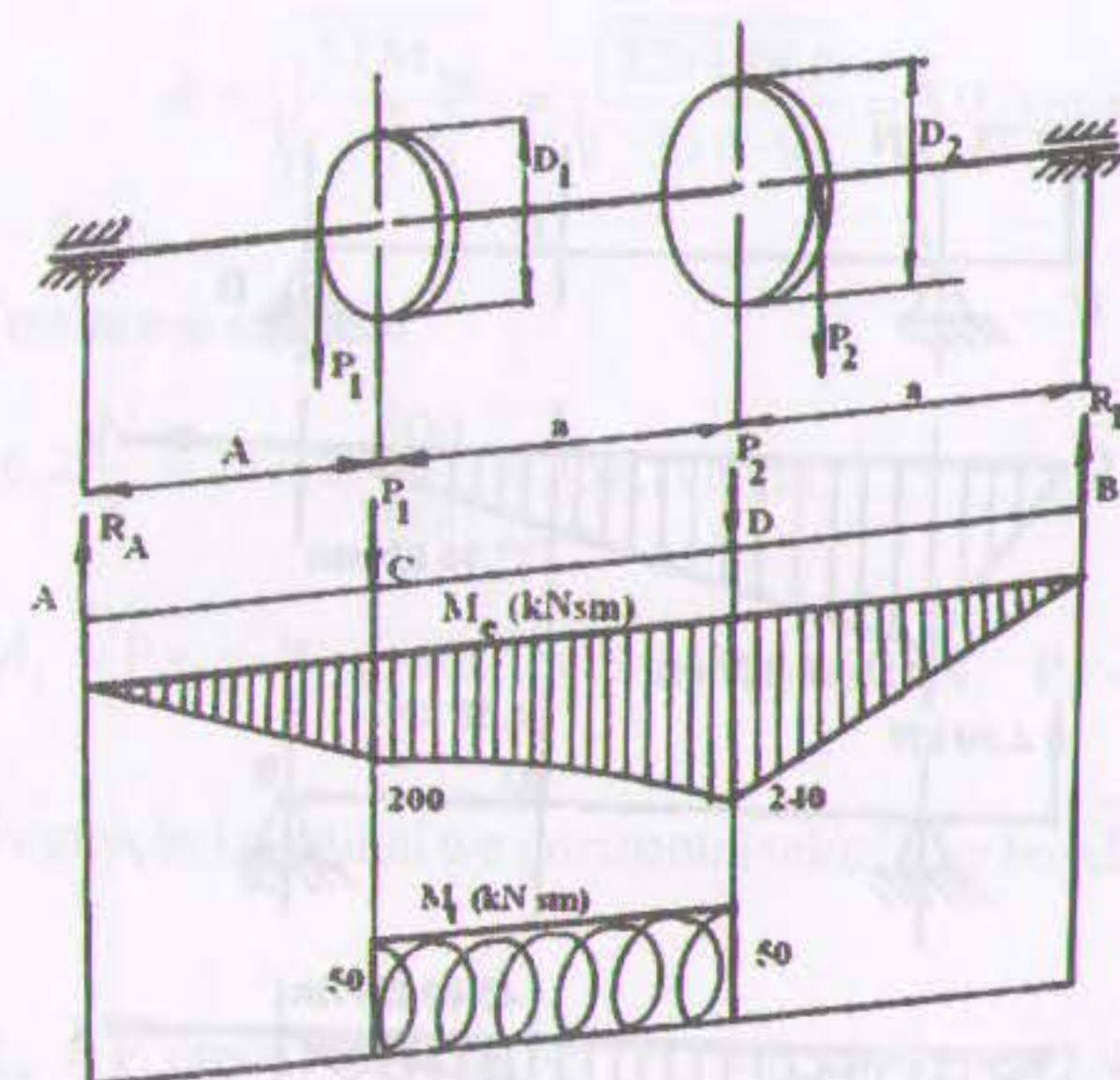
$$P_2 = \frac{R_1}{R_2} P_1 = \frac{10}{25} \cdot 5 = 2 \text{ kN} \quad \text{onda } M_t = P_1 R_1 = 5 \cdot 10 = 50 \text{ kNsm}.$$

Howply kesik D kesik bolýar. $M_e = 240 \text{ kNsm}; \quad M_t = 50 \text{ kNsm}.$

III- berklik nazaryýeti boýunça

$$M_{III} = \sqrt{M_e^2 + M_t^2} = \sqrt{240^2 + 50^2} = 245 \text{ kNsm},$$

$$\text{Walyň talap edýän diametri } d = \sqrt[3]{\frac{32 \cdot M_{III}}{\tau \cdot [\sigma]}} = \sqrt[3]{\frac{32 \cdot 245}{3,14 \cdot 10}} = 6,3 \text{ sm}.$$



7.21-nji surat

7.22. $d = 6 \text{ sm}$.

Wala täsir edýän güýçleriň düzüjilerini gorizonta we wertikal tekizlikler boýunça dargadyrys.

$$\text{Gorizonta tekizlikde } H_C = (6 + 3) \cos 30^\circ = 7,79 \text{ kN};$$

$$H_D = 3 + 1,5 = 4,5 \text{ kN}.$$

$$\text{Wertikal tekizlikde } R_C = (6 + 3) \sin 30^\circ = 4,5 \text{ kN}.$$

Gorizonta tekizlikde in uly egme moment A kesikde

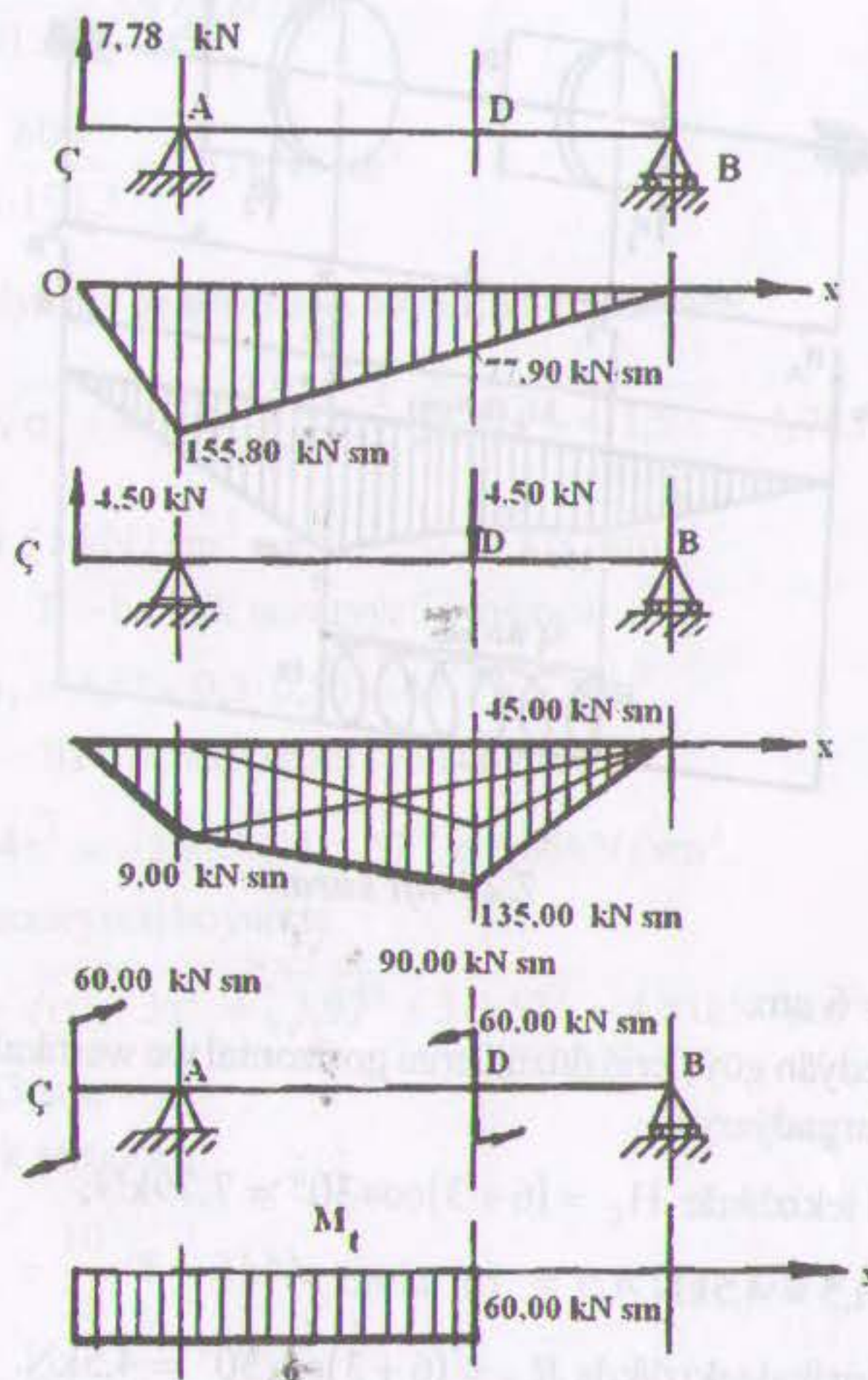
$$M_A^{\text{gor}} = 7,79 \cdot 20 = 155,8 \text{ kNsm} \quad (\text{surata seret}).$$

Wertikal tekizlikde

$$M_A^{\text{wert}} = R_C \cdot 20 = 4,5 \cdot 20 = 90 \text{ kNsm},$$

$$M_D^{\text{wert}} = \frac{R_D \cdot 80}{4} + \frac{R_C \cdot 20}{2} = 135 \text{ kNsm}.$$

$$\text{Towlanma moment } M_t = (3 - 1,5) \cdot 40 = 60 \text{ kNsm}$$



7.22-nji surat

D kesikdäki jemleýji egme moment

$$M_{\text{jeml}} = \sqrt{155,8^2 + 90^2} = 179,9 \text{ kN} \cdot \text{sm}$$

III – berklik nazaryýeti boýunça D kesikdäki hasaplaýjy moment

$$M_{\text{has}} = \sqrt{(179,9)^2 + 60^2} = 189,6 \text{ kN} \cdot \text{sm},$$

Walýň diametri

$$d = \sqrt[3]{\frac{32M_{\text{has}}}{\pi[\sigma]}} = \sqrt[3]{\frac{32 \cdot 189,6}{3,14 \cdot 9}} = 5,97 \text{ sm} \approx 6 \text{ sm}.$$

7.23. $d = 8 \text{ sm}.$

Towlanma moment

$$M_t = 716,2 \frac{\text{N}}{\text{m}} = 716,2 \frac{500}{1000} = 358,1 \text{ kNsm}.$$

$$M_t = P_1 r_1 = P_2 r_2 \text{ aňlatmadan } P_1 = 60 \text{ kN}; P_2 = 30 \text{ kN}.$$

Bu güýçleri wertikal we gorizontalkler boýunça dargadyp alarys:

$$P_{1w} = P_1 \cos \alpha_1 = 42,4 \text{ kN}; P_{1g} = P_1 \sin \alpha_1 = 42,4 \text{ kN}.$$

$$P_{2w} = P_2 \cos \alpha_2 = 25,9 \text{ kN}; P_{2g} = P_2 \sin \alpha_2 = 15 \text{ kN}.$$

Bu güýçlerden aýratynlykda wertikal we gorizontalklerde egme momentleriň epýurlaryny gurýarys (surata seret).

Häsiýetli kesiklerdäki jemleýji egme momentler

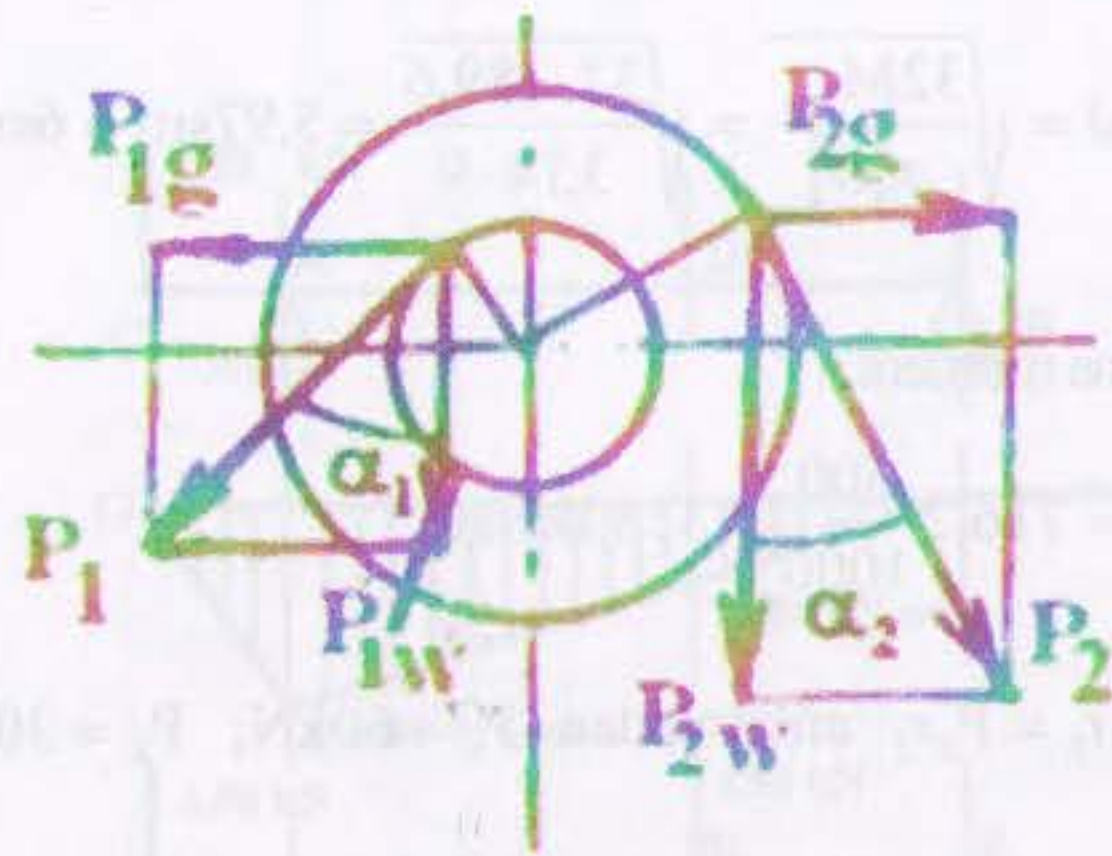
$$M_1 = \sqrt{(M_1^w)^2 + (M_1^g)^2} = \sqrt{418^2 + 295^2} = 510 \text{ kNsm};$$

$$M_2 = \sqrt{(M_2^w)^2 + (M_2^g)^2} = \sqrt{398^2 + 31,5^2} = 400 \text{ kNsm}.$$

$$\text{Howply kesik 1-nji kesik we } M_{IV} = \sqrt{M_1^2 + 0,75 \cdot M_t^2} = 600 \text{ kNsm}.$$

Walýň diametri

$$d = \sqrt[3]{\frac{32M_{IV}}{\pi[\sigma]}} = \sqrt[3]{\frac{32 \cdot 600}{3,14 \cdot 12}} = 8 \text{ sm}.$$



7.23-nji surat

7.24. Kwadrat kesik 6% tegelek kesikden ýeňil.

Tegelek kesikli pürs üçin

$$(\sigma_{\text{teg}}^{\text{III}})^2 = \left(\frac{32M_e}{\pi d^3} \right)^2 + 4 \left(\frac{16M_t}{\pi d^3} \right)^2 = 55,8 \frac{M_e^2}{A_{\text{teg}}^3};$$

Kwadrat kesik üçin

$$(\sigma_{\text{kw}}^{\text{III}})^2 = \left(\frac{6M_e}{a^3} \right)^2 + 4 \left(\frac{M_t}{0,208a^3} \right)^2 = 46 \frac{M_e^2}{A_{\text{kw}}^3};$$

$A_{\text{teg}}, A_{\text{kw}}$ - tegelek we kwadrat kesikleriniň meýdanlary.

Ýokardaky dartgynlyklary deňeşdirip alarys:

$A_{\text{kw}} = 0,94A_{\text{teg}}$, diýmek, kwadrat kesik tegelekden 6% ýeňil.

7.25. $d = 7 \text{ sm}$.

Walyň geçirýän tovlanma momentini kesgitläýäris.

$$M_t = 973,8 \frac{\text{N}}{\text{n}} = 973,8 \cdot \frac{12}{80} = 146 \text{ kNsm}.$$

$$\text{Töwerekleýin täsir edýän güýç } P = \frac{2M_t}{D} = \frac{2 \cdot 146}{46} = 6,35 \text{ kN}.$$

Wala radial we ok boýunça täsir edýän güýçler

$$P_r = 0,36P = 2,28 \text{ kN}; \quad P_{ok} = 0,28P = 1,78 \text{ kN}.$$

Suratda wertikal we gorizontalk tekizliklerde gurlan egme momentleriň epýurlary görkezilen.

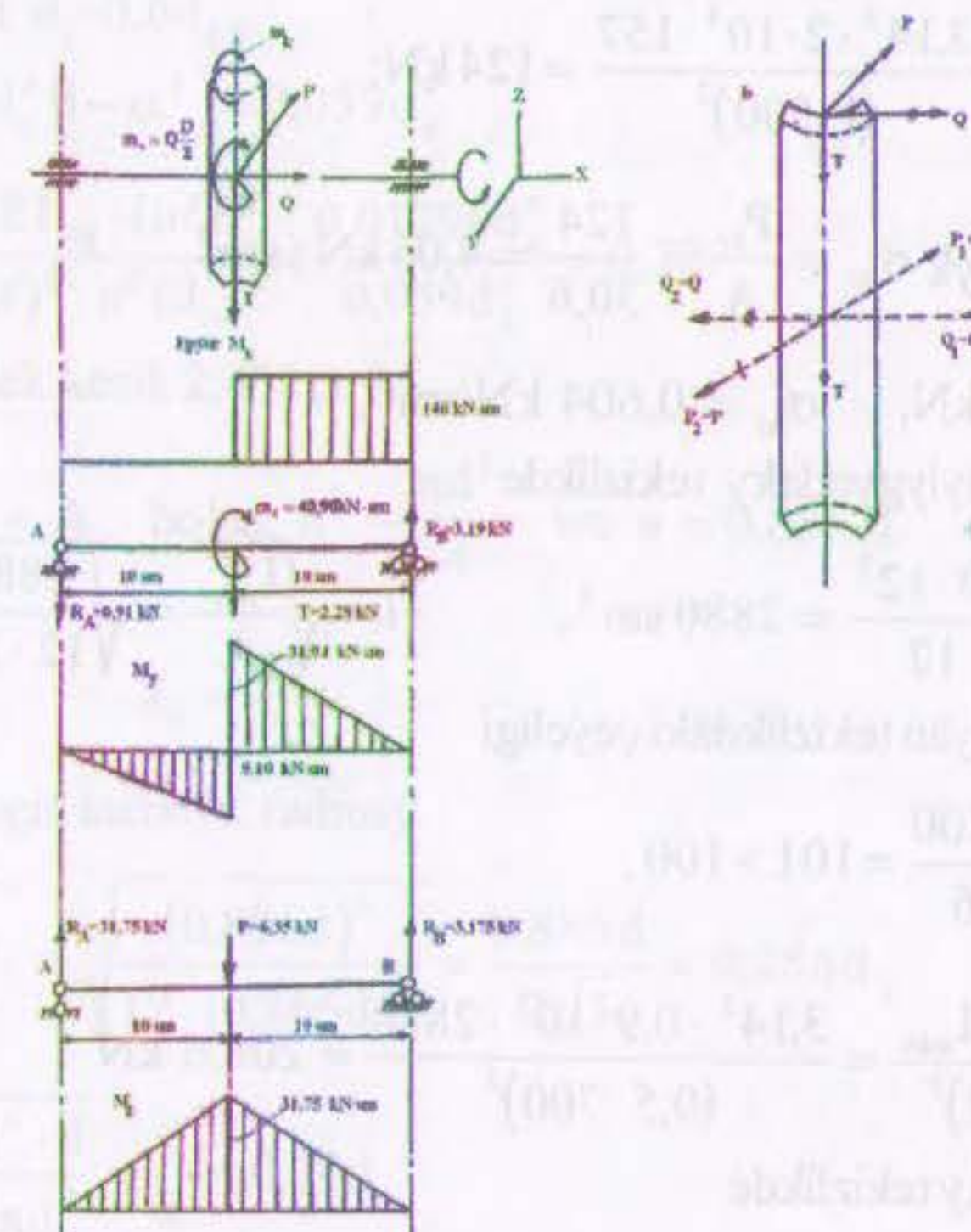
Jemleýji egme moment howply kesik üçin

$$M_{\text{jeml}} = \sqrt{M_w^2 + M_g^2} = \sqrt{31,94^2 + 31,75^2} = 37 \text{ kNsm}.$$

IV – berklik nazaryýeti boýunça

$$M_{\text{IV}} = \sqrt{M_{\text{jeml}}^2 + 0,75M_t^2} = \sqrt{37^2 + 0,75 \cdot 146^2} = 133 \text{ kNsm},$$

$$\text{onda } d = \sqrt[3]{\frac{32M_{\text{IV}}}{\pi[\sigma]}} = \sqrt[3]{\frac{32 \cdot 133}{3,14 \cdot 4}} = 6,99 \text{ sm} \approx 7 \text{ sm}.$$



7.25-nji surat

VIII bap

Gysylan sterženleriň durnuklylygy

8.1. $P_{kr} = 124 \text{ kN}$, $\sigma_{kr} = 4,05 \text{ kN/sm}^2$.

22-nji belgili iki tawra üçin

$$I_{min} = 157 \text{ sm}^4, \quad A = 30,6 \text{ sm}^2, \quad i_{min} = 2,27 \text{ sm}$$

sterženiň getirilen çeyeligi $\lambda = \frac{\mu \ell}{i_{min}} = \frac{1 \cdot 500}{2,27} = 220 > \lambda_{\varphi} = 100$.

Şonuň üçin hem Eýleriň formulasyny ulanyp bolýar.

$$P_{kr} = \frac{\pi^2 EI_{min}}{(\mu \ell)^2} = \frac{3,14^2 \cdot 2 \cdot 10^4 \cdot 157}{(1 \cdot 500)^2} = 124 \text{ kN};$$

Kritiki dartgynlylyk $\sigma_{kr} = \frac{P_{kr}}{A} = \frac{124}{30,6} = 4,05 \text{ kN/sm}^2$.

8.2. $P_{kr} = 145 \text{ kN}$, $\sigma_{kr} = 0,604 \text{ kN/sm}^2$.

Iň kiçi gatylygyndaky tekizlikde

$$I_{min} = \frac{20 \cdot 12^3}{12} = 2880 \text{ sm}^4, \quad i = \sqrt{\frac{I_{min}}{A}} = \sqrt{\frac{2880}{12 \cdot 20}} = 3,46 \text{ sm}$$

Sterženiň seredilýän tekizlikdäki çeyeligi

$$\lambda = \frac{\mu \ell}{i_{min}} = \frac{0,5 \cdot 700}{3,46} = 101 > 100.$$

Onda $P_{kr} = \frac{\pi^2 EI_{min}}{(\mu \ell)^2} = \frac{3,14^2 \cdot 0,9 \cdot 10^3 \cdot 2880}{(0,5 \cdot 700)^2} = 208,6 \text{ kN}$

Iň uly gatylykdaky tekizlikde

$$I = \frac{20^3 \cdot 12}{12} = 8000 \text{ sm}^4, \quad i = \sqrt{\frac{8000}{240}} = 5,7 \text{ sm},$$

$$P_{kr} = \frac{3,14^2 \cdot 0,9 \cdot 10^3 \cdot 8000}{(1 \cdot 700)^2} = 145 \text{ kN}$$

Kabul edýäris $P_{kr} = 145 \text{ kN}$;

Kritiki dartgynlylyk

$$\sigma_{kr} = \frac{P_{kr}}{A} = \frac{145}{240} = 0,604 \text{ kN/sm}^2.$$

8.3. $P_{teg} : P_{tur} = 0,22$

$$n_{\sigma} = \frac{\sigma_{ak}}{\sigma_m + \sigma_a} = \frac{30}{5} = 6, \text{ bu ýerde } \alpha = \frac{d_i}{d_d} = 0,8$$

bu ýerden $d_i = 0,6d_d$,

$$I_{tur} = 0,1d_d^4(1 - \alpha^4) = 0,059d_d^4$$

$$\frac{P_{teg}}{P_{tur}} = \frac{\pi^2 EI_{teg} \cdot (\mu \ell)^2}{(\mu \ell)^2 \cdot \pi^2 EI_{tur}} = \frac{0,01296d_d^4}{0,059d_d^4} = 0,22.$$

8.4. Tegelek kesik 2,4% çeye.

Eger $A_{\diamond} = A_o$ bolsa, $a^2 = \frac{\pi d^2}{4}$ we $a = 0,886 d$,

$$I_{\diamond} = \frac{a^4}{12}, \quad I_o = \frac{\pi d^4}{32}$$

Onda kesigiň inersiýa radiusy

$$i_{\diamond} = \sqrt{\frac{I_{\diamond}}{A_{\diamond}}} = \sqrt{\frac{(0,886d)^4}{12 \cdot (0,866d)^2}} = \frac{0,886d}{2\sqrt{3}} = 0,256d,$$

$$i_o = \sqrt{\frac{\pi d^4 \cdot 4}{64\pi d^2}} = \frac{d}{4} = 0,25d$$

Çeyeligiň gatnaşygyny tapýarys

$$\frac{\lambda_o}{\lambda_o} = \frac{i_o}{i_o} = \frac{0,256d}{0,25d} = 1,024$$

$$8.5. [P_d] = 178,5 \text{ kN}.$$

İki tawranyň berlen belgisi boýunça tablisadan alarys:

$$I_{\min} = 260 \text{ sm}^4, \quad i_{\min} = 2,63 \text{ sm}, \quad A = 37,5 \text{ sm}^2.$$

$$\text{Sütüniň çeyeligi } \lambda_1 = \frac{\mu \ell}{i_{\min}} = \frac{1 \cdot 320}{2,63} = 122.$$

Polat 3 üçin Eýleriň formulasyny ulanmagyň aşaky çäginini tapýarys.

$$\lambda_2 = \sqrt{\frac{\pi^2 E}{\sigma_{p-s}}} = \sqrt{\frac{3,14^2 \cdot 2 \cdot 10^4}{20}} = 99,3$$

$\lambda_1 > \lambda_2$, şonuň üçin hem Eýleriň formulasy boýunça kritiki güýji hasaplamaga rugsat edilyär.

$$P_{kr} = \frac{\pi^2 E I_{\min}}{(\mu \ell)^2} = \frac{3,14^2 \cdot 2 \cdot 10^4 \cdot 260}{(1 \cdot 320)^2} = 500 \text{ kN}.$$

$$\text{Rugsat edilyän ýük } [P_d] = \frac{P_{kr}}{n_d} = \frac{500}{2,8} = 178,5 \text{ kN}.$$

$$8.6. d_2 = 20 \text{ sm}, \quad d_1 = 17 \text{ sm}.$$

İlki Eýleriň formulasyny ulanyp, soň barlap görýäris.

$$P_{kr} = [P_d] n_d = \frac{\pi^2 E \pi d_2^4 (1 - \alpha^4)}{(\mu \ell)^2 \cdot 64};$$

$$\text{bu ýerden } d_2 = \sqrt[4]{\frac{64 [P_d] n_d \cdot \mu^2 \ell^2}{\pi^3 E (1 - \alpha^4)}} = 19,3 \text{ sm kabul edýäris.}$$

$$d_2 = 20 \text{ sm}, \quad d_1 = 0,85 \cdot d_2 = 17 \text{ sm}.$$

$$\text{Barlagy: } \lambda = \frac{\mu \ell}{i}, \quad i = \frac{d_2}{4} \sqrt{1 + \alpha^2} = 7,57 \text{ sm, onda}$$

$$\lambda = \frac{2 \cdot 320}{7,57} = 97,5.$$

Sütüniň materialyna Eýleriň formulasyny peýdalanmagyň aşaky çägi

$$\lambda = \sqrt{\frac{\pi^2 E}{\sigma_{p-s}}} = \sqrt{\frac{3,14 \cdot 2 \cdot 10^4}{17,2}} = 81,2.$$

Saýlanan sütüniň çeyeligi bu çäkden ýokary, şonuň üçin hem Eýleriň formulasy dogry ulanylan.

$$8.7. [P_d] = 144 \text{ kN}.$$

Tegelegiň inersiýa radiusy

$$i = \frac{d}{4} = \frac{20}{4} = 5 \text{ sm, onda } \lambda = \frac{\mu \ell}{i} = \frac{1 \cdot 270}{5} = 54.$$

Eýleriň formulasyny ulanmagyň aşaky çägi

$$\lambda = \sqrt{\frac{\pi^2 E}{\sigma_{p-s}}} = \sqrt{\frac{3,14^2 \cdot 1,1 \cdot 10^3}{2,1}} = 71,8.$$

Eýleriň formulasyny ulanyp bolmaýar.

Boý egilmäniň koeffisiýentiniň kömegi bilen hasaplaýarys. Tablisadan

$\lambda = 54$ çeyelikdäki diregiň koeffisiýentiniň interpolýasiýany ulanyp tapýarys.

$$\lambda = 50 \Rightarrow \varphi = 0,8,$$

$$\lambda = 60 \Rightarrow \varphi = 0,71,$$

$$\Delta \lambda = 10 \quad \Delta \varphi = 0,09,$$

$$\lambda = 54 \Rightarrow \varphi = 0,8 - \frac{0,8 - 0,71}{10} (54 - 50) = 0,764.$$

Durnuklylyga rugsat edilyän dartgynlyk

$$[\sigma_d] = \varphi [\sigma] = 0,764 \cdot 0,6 = 0,458 \text{ kN/sm}^2.$$

Direge rugsat edilyän güýç $[P_d] = A[\sigma_d] = \frac{3,14 \cdot 20^2}{4} \cdot 0,458 = 144 \text{ kN}$.

8.8. $d_1 = 5,2 \text{ sm}$.

Eýleriň formulasyny ulanyp, nurbatyň içki diametrini kesgitleýäris.

$$d_1 = \sqrt[4]{\frac{64 \cdot P[n_d](\mu\ell)^2}{\pi^3 E}} = \sqrt[4]{\frac{64 \cdot 50 \cdot 4 \cdot (2 \cdot 90)^2}{3,14^3 \cdot 2,1 \cdot 10^4}} = 5,04 \text{ sm},$$

Bu ýerde $\mu = 2$ -nurbat bir tarapy gaty berkidilen direg görnüşinde seredilen.

Kabul edýäris: $d_1 = 5,2 \text{ sm}$, bu bolsa daşky diametri $d = 6 \text{ sm}$ we ädimi $t = 0,8 \text{ mm}$ (9484-60 DÖST boýunça) trapeseidal hyra gabat gelýär. Ýokarky hasaby barlaýarys.

$$i = \frac{d_1}{4} = 1,3 \text{ sm}, \quad \text{onda} \quad \lambda = \frac{\mu\ell}{i} = \frac{2 \cdot 90}{1,3} = 138 > \lambda_{\varphi} = 90 \text{ (polat 30)}.$$

Şonuň üçin hem hasap Eýleriň formulasynyň ulanylyan çäginde geçirilen.

8.9. $P = 81 \text{ kN}$, $[\sigma]_d = 0,25 \text{ kN/sm}^2$, $\varphi = 0,25$.

$$\text{Kwadrat kesik üçin } i = \frac{a}{2\sqrt{3}} = \frac{18}{2\sqrt{3}} = 5,2 \text{ sm}, \text{ onda}$$

$$\lambda = \frac{\mu\ell}{i} = \frac{1 \cdot 600}{5,2} = 115 > 100 \text{ we kritiki güýji Eýleriň formulasy}$$

boýunça kesgitleýäris:

$$P_{kr} = \frac{\pi^2 EI}{(\mu\ell)^2} = \frac{3,14^2 \cdot 10^3 \cdot 18^4}{12 \cdot 600^2} = 243 \text{ kN}.$$

$$\text{Kritiki dartgynlylyk } \sigma_{kr} = \frac{P_{kr}}{A} = \frac{243}{18 \cdot 18} = 0,75 \text{ kN/sm}^2.$$

$$\text{Onda } [\sigma]_d = \frac{\sigma_{kr}}{n_d} = \frac{0,75}{3} = 0,25 \text{ kN/sm}^2,$$

$$[P]_d = \frac{P_{kr}}{n_d} = \frac{243}{3} = 81 \text{ kN}.$$

Rugsat edilyän dartgynlylygy azaldýan koeffisiýent

$$\varphi = \frac{[\sigma]_d}{[\sigma]} = \frac{0,25}{1} = 0,25.$$

8.10. $d = 19,75 \text{ sm}$.

Ulgamyň deňagramlylyk şertinden $N = 238 \text{ kN}$ – söýegdäki boý güýji.

$$\text{Inersiýa radiusy } i = \frac{d}{4}.$$

Meseläni çemeleşme ýoly bilen işleýäris.

1-nji çemeleşme $\varphi_1 = 0,5$,

$$[\sigma]_d = 0,5 \cdot 1,1 = 0,55 \text{ kN/sm}^2.$$

$$\text{Kesigiň meýdany } A = \frac{N}{[\sigma]_d} = \frac{238}{0,55} = 432,7 \text{ sm}^2.$$

$$\text{Bu ýerden } d = \sqrt{\frac{4A}{\pi}} = 23,5 \text{ sm} \rightarrow i = \frac{d}{4} = 5,87 \text{ sm},$$

$$\lambda = \frac{\mu\ell}{i} = \frac{1 \cdot 291,5}{5,87} \approx 50 \Rightarrow \text{tablisadan } \varphi_1' = 0,8,$$

$$[\sigma]_d = 0,8 \cdot 1,1 = 0,88 > 0,55 \text{ kN/sm}^2 - \text{kesigi kiçeltmeli.}$$

$$\text{2-nji çemeleşme } \varphi_2 = \frac{\varphi_1 + \varphi_1'}{2} = \frac{0,5 + 0,8}{2} = 0,65;$$

$$[\sigma]_d = 0,65 \cdot 1,1 = 0,715 \text{ kN/sm}^2.$$

Hasaplardan alarys: $A = 332,86 \text{ sm}^2$; $d = 20,6 \text{ sm}$;

$$i = 5,15 \text{ sm}; \quad \lambda = 56,6$$

Interpolýasiýany ulanyp alarys.

$$\lambda = 50 \rightarrow \varphi = 0,8; \quad \lambda = 60 \rightarrow 0,71,$$

$$\text{onda } \varphi_2' = 0,8 - \frac{0,09}{10} \cdot 6,6 = 0,7406,$$

$$[\sigma]_d = 1,1 \cdot 0,7406 = 0,815 > 0,715 \text{ kN/sm}^2.$$

Kesigiň ölçegi ýene-de uly

$$\text{3-nji çemeleşme } \varphi_3 = \frac{\varphi_2 + \varphi_2'}{2} = \frac{0,65 + 0,7406}{2} = 0,6953,$$

$$[\sigma]_d = 0,6953 \cdot 1,1 = 0,765$$

$$A = 311,11 \text{ sm}^2; \quad d = 19,93 \text{ sm}; \quad i = 4,98 \text{ sm}; \quad \lambda = 58,5$$

$$\text{onda } \varphi_3' = 0,8 - \frac{0,09}{10} \cdot 8,5 = 0,7235$$

$$[\sigma]_d = 1,1 \cdot 0,7235 = 0,796 > 0,765 \text{ kN/sm}^2.$$

$$\text{4-nji çemeleşme } \varphi_4 = \frac{\varphi_3 + \varphi_3'}{2} = 0,71,$$

$$[\sigma]_d = 0,71 \cdot 1,1 = 0,78 \text{ kN/sm}^2,$$

$$A = 305 \text{ sm}^2; \quad d = 19,74 \text{ sm}; \quad i = 4,93 \text{ sm}; \quad \lambda = 59.$$

$$\varphi_4' = 0,8 - \frac{0,09}{10} \cdot 9 = 0,719,$$

$$[\sigma]_d = 1,1 \cdot 0,719 = 0,79 \approx 0,78 \text{ kN/sm}^2$$

Diýmek, $d = 19,75 \text{ sm}$ kabul edýäris.

$$\text{8.11. } [P]_d = 689 \text{ kN}; \quad a = 12,4 \text{ sm.}$$

$$\text{Tablisadan alarys: } I_y = 2330 \text{ sm}^4; \quad I_z = 187 \text{ sm}^4;$$

$$A = 28,8 \text{ sm}^2; \quad y_o = 2,46 \text{ sm.}$$

Iň kiçi inersiýa radiusy

$$i_{\min} = i_{y_c} = \sqrt{\frac{I_{y_c}}{A}} = \sqrt{\frac{2330}{2 \cdot 28,8}} = 8,99 \text{ sm.}$$

$$\text{Sütüniň çeyeligi } \lambda_{\max} = \frac{\mu \ell}{i_{\min}} = \frac{1 \cdot 500}{8,99} = 55,7$$

Interpolýasiýany ulanyp, tablisadan tapýarys $\varphi = 0,749$

$$\text{Rugsat edilyän yük } [P]_d = A \varphi [\sigma] = 28,8 \cdot 0,749 \cdot 16 = 689 \text{ kN}$$

Şwelleriň aralygyny $I_{y_c} = I_{z_c}$ şertden tapýarys.

$$2 \cdot 2330 = 2(187 + b^2 \cdot 28,8); \quad b = 8,64 \text{ sm.}$$

$$\text{onda } a = 2b - 2y_c = 2 \cdot 8,46 - 2 \cdot 2,46 = 12,36 \approx 12,4 \text{ sm.}$$

8.12. a) 23,1m; b) 23,7m; c) 20,2m.

Sterženiň kritiki uzynlygyny kesgitlemek üçin Ýasinskiň formulasyny peýdalanýarys:

$$(q\ell)_{kr} = \frac{\pi^2 EI_{\min}}{(\mu \ell)^2}; \quad \text{bu ýerde } \mu = 1,12; \quad q = \gamma A$$

1)

$$\ell_{kr}^3 = \frac{\pi^2 EI_{\min}}{\gamma A \mu^2} = \frac{\pi^2 E \pi d^4 \cdot 4}{64 \cdot \gamma \pi d^2 \cdot \mu^2} = \frac{3,14^2 \cdot 2 \cdot 10^4 \cdot 10^2}{16 \cdot 80 \cdot 10^{-6} \cdot 1,12^2} = 0,0123 \cdot 10^{12}$$

$$\ell_{kr} = 10^2 \sqrt[3]{12300} = 23,1 \cdot 10^2 \text{ sm} = 23,1 \text{ m};$$

$$2) \quad \ell_{kr}^3 = \frac{3,14^2 \cdot 0,7 \cdot 10^4 \cdot 10^2}{16 \cdot 26 \cdot 10^{-6} \cdot 1,12^2} = 0,0132 \cdot 10^{12} \Rightarrow \ell_{kr} = 23,7 \text{ m};$$

$$3) \quad \ell_{kr}^3 = \frac{3,14^2 \cdot 10^3 \cdot 10^2}{16 \cdot 6 \cdot 10^{-6} \cdot 1,12^2} = 0,00822 \cdot 10^{12} \Rightarrow \ell_{kr} = 20,2 \text{ m.}$$

8.13. $140 \times 140 \times 9$ burçluk, $A = 24,7 \text{ sm}^2; \quad i_x = 4,34 \text{ sm};$

$$n_d = 1,95$$

Fermanyň gaýtargylary $R_A = 231 \text{ kN}$; $R_B = 269 \text{ kN}$;

$$N_{AC} = \frac{R_A}{\sin \beta} = 352 \text{ kN}.$$

$$\sin \beta = 0,657; \text{ sterženiň uzynlygy } \ell = \frac{4}{\cos \beta} = 5,31 \text{ m}; \quad A = \frac{N}{\varphi[\sigma]};$$

$$\cos \beta = 0,753.$$

Boý egilmäniň koeffisiýenti boýunça hasap geçirýäris.

$$1\text{-nji çemeleşme } \varphi_1 = 0,6; \text{ onda } A = 36,7 \text{ sm}^2; \quad A_1 = \frac{A}{2} \cong 18,4 \text{ sm}^2.$$

DÖST boýunça $100 \times 100 \times 10$ burçluk $A_1 = 19,2 \text{ sm}^2$;

$$i_{\min} = 3,05 \text{ sm}; \quad \lambda = 174.$$

$$\varphi_1' = 0,26 - \frac{0,26 - 0,23}{10} \cdot 4 = 0,248; \quad \varphi_1 = 0,6 - \text{dan köp}$$

tapawutlanýar.

$$2\text{-nji çemeleşme } \varphi_2 = \frac{\varphi_1 + \varphi_1'}{2} = 0,424$$

$$A = 51,9 \text{ sm}^2; \quad A_1 \cong 26 \text{ sm}^2$$

DÖST boýunça $125 \times 125 \times 12$, $A_1 = 28,9 \text{ sm}^2$; $i_{\min} = 3,82 \text{ sm}$;

$$\lambda = \frac{531}{3,82} = 139; \quad \varphi_2' = 0,36.$$

$$3\text{-nji çemeleşme } \varphi_3 = \frac{\varphi_2 + \varphi_2'}{2} = 0,392; \quad A = 56,2 \text{ sm}^2;$$

$$A_1 = 28,1 \text{ sm}^2.$$

$140 \times 140 \times 9$ burçluga kabul edýäris.

$$A_1 = 24,7 \text{ sm}^2; \quad i_x = 4,34 \text{ sm}.$$

$$\text{onda } \sigma = \frac{N}{A} = \frac{352}{2 \cdot 24,7} = 7,12 \text{ kN/sm}^2; \quad \lambda = \frac{531}{4,34} = 122;$$

$$\varphi_{\text{tabl}} = 0,44,$$

$$[\sigma]_d = \varphi_{\text{tabl}} \cdot [\sigma] = 0,44 \cdot 16 = 7,04 \text{ kN/sm}^2.$$

Aşa ýüklenme 1%-den hem köp däl.

Kabul edilen kesigiň ölçegleri boýunça durnuklylyga ätiýaçlyk koeffisiýentini kesgitleýäris.

$$n_d = \frac{\sigma_{kr}}{\sigma} \quad \lambda > \lambda_c; \text{ Eýleriň formulasyny ulanýarys}$$

$$\sigma_k = \frac{\pi^2 E}{\lambda^2} = \frac{3,14^2 \cdot 2,1 \cdot 10^4}{122^2} = 13,9 \text{ kN/sm}^2;$$

$$n_d = \frac{13,9}{7,12} = 1,95.$$

IX bap

Dinamiki we dowamly ýüklenmeler.

9.1. 3,58 sm; 3,74sm.

Ýüki galdyrmagyň tizlenmesi $a = \frac{2h}{t^2} = \frac{2 \cdot 9}{3^2} = 2 \text{ m/s}^2$.

Urganyň hususy agramyny hasaba almazdan berklik şerti

$$A[\sigma] = P \left(1 + \frac{a}{g} \right).$$

Bu ýerden $A = \frac{P}{[\sigma]} \left(1 + \frac{a}{g} \right) = \frac{50}{6} \left(1 + \frac{2}{9,81} \right) = 10,03 \text{ sm}^2$,

onda $d = \sqrt{\frac{4A}{\pi}} = \sqrt{\frac{4 \cdot 10,03}{3,14}} = 3,58 \text{ sm}$

Urganyň hususy agramyny hasaba alarys:

$$[\sigma] = \frac{P}{A} \left(1 + \frac{a}{g} \right) + \gamma \ell \left(1 + \frac{a}{g} \right).$$

Bu ýerden

$$A = \frac{P \left(1 + \frac{a}{g} \right)}{[\sigma] - \gamma \ell \left(1 + \frac{a}{g} \right)} = \frac{50 \left(1 + \frac{2}{9,81} \right)}{6 - 70 \cdot 10^{-6} \cdot 60 \cdot 10^2 \left(1 + \frac{2}{9,81} \right)} = 11 \text{ sm}^2.$$

Onda $d = \sqrt{\frac{4 \cdot 11}{3,14}} = 3,74 \text{ sm}$.

9.2. $[n] = 1090 \text{ aýl/min}$, $\Delta \ell = 0,251 \text{ mm}$.

0-0 okdan x uzaklykda uzynlygy dx elementi bölüp alyp, onuň inersiýa güýjüni kesgitleýäris:

$$dP_d = \frac{\gamma A dx}{g} \omega^2 x$$

mn kesigiň süýnme dartgynlylygy

$$\sigma = \frac{P_d}{A} = \frac{1}{A} \int_x^{\ell/2} dP_d = \int_x^{\ell/2} \frac{\gamma \omega^2 x dx}{g} = \frac{\gamma \omega^2}{2g} \left(\frac{\ell^2}{4} - x^2 \right).$$

Iň uly süýnme dartgynlylyk $x = 0$ deň bolanda bolýar:

$$\sigma_{\max} = \frac{\gamma \omega^2 \ell^2}{8g} \leq [\sigma] \Rightarrow [\omega] = \sqrt{\frac{8g[\sigma]}{\gamma \ell^2}} = \frac{\pi[n]}{30} \Rightarrow [n] = 1090 \text{ aýl/min}.$$

Uzynlygy dx bolan sterženiň uzalmasy

$$d\Delta \ell = \frac{\sigma dx}{E} = \frac{\gamma \omega^2}{2gE} \left(\frac{\ell^2}{4} - x^2 \right) dx.$$

Sterženiň uzalmasy

$$\begin{aligned} \Delta \ell &= 2 \int_0^{\ell/2} \frac{\sigma dx}{E} = 2 \int_0^{\ell/2} \frac{\gamma \omega^2}{2gE} \left(\frac{\ell^2}{4} - x^2 \right) dx = \\ &= \frac{\gamma \omega^2 \ell^2}{12gE} = \frac{\gamma \pi^2 n^2 \ell^2}{12 \cdot 30^2 \cdot gE} = 0,0251 \text{ sm} = 0,251 \text{ mm}. \end{aligned}$$

9.3. $d_A = 3,1 \text{ sm}$, $d_B = 3,93 \text{ sm}$.

Inersiýa güýji goşulanda garşylyk agramyň boltlara täsiri

$$P_d = P \left(1 + \frac{a}{g} \right) = 42 \left(1 + \frac{1,5}{9,81} \right) = 48,42 \text{ kN}$$

A boltlaryň kese kesiginiň meýdany $A_a = \frac{P_d}{2[\sigma]} = \frac{48,42}{2 \cdot 3,2} = 7,56 \text{ sm}^2$ (iki bolt).

Onda onuň diametri $d_A = \sqrt{\frac{4A_a}{\pi}} = \sqrt{\frac{4 \cdot 7,56}{3,14}} = 3,1 \text{ sm}$.

B boltuň kese kesiginiň meýdany

$$A_B = \frac{P_d}{[\tau]} = \frac{48,42}{2 \cdot 2} = 12,10 \text{ sm}^2 \text{ (iki kesme).}$$

$$d_B = \sqrt{\frac{4 \cdot 12,10}{3,14}} = 3,93 \text{ sm}.$$

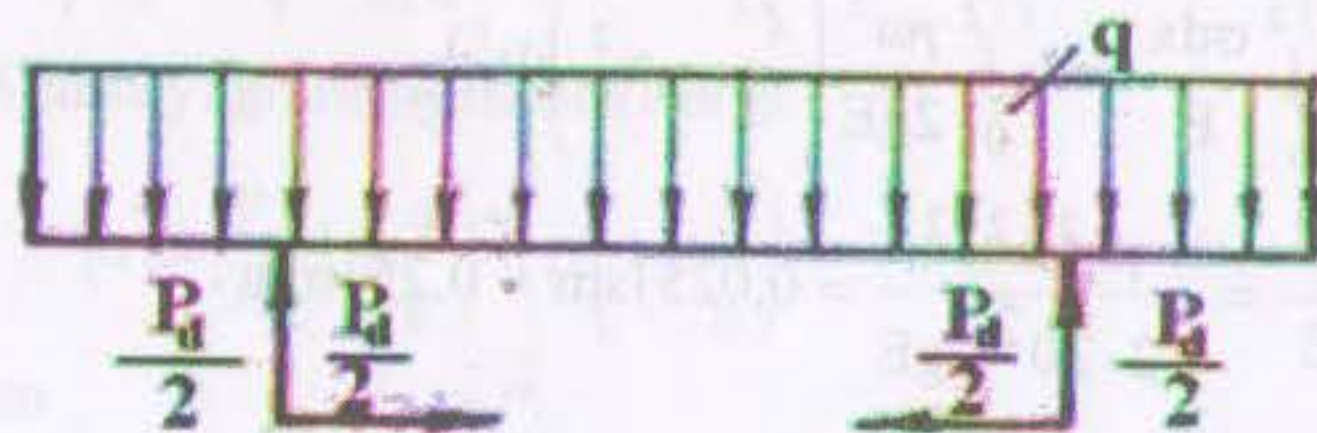
9.4. $\sigma_{\max} = 0,149 \text{ kN/sm}^2$, $\sigma_{\text{urg}} = 2,56 \text{ kN/sm}^2$.

Balkanyň agramy $G = \gamma A \ell = 24 \cdot 10^{-6} \cdot 20^2 \cdot 600 = 5,76 \text{ kN}$,

Inersiýa güýjünden balkanyň dinamiki ýüklenmesi

$$P_d = \left(1 + \frac{a}{g}\right) G = 1,6 \cdot 5,76 = 9,2 \text{ kN}$$

Balkanyň 1 metrine düşýän ýüklenme $q = \frac{P_d}{\ell} = \frac{9,2}{6} = 1,53 \text{ kN/m}$



9.4-nji surat

Balkanyň egme momentlerini kesgitleýäris.

Urganyň berkidilen kesiginde $M_1 = 0,77 \text{ kN} \cdot \text{m}$

Balkanyň ortasyndaky kesikde $M_2 = -1,83 \text{ kN} \cdot \text{m}$

Balkanyň maksimal dartgynlylygy

$$|\sigma_{\max}| = \sigma_{\ell} + \sigma_g = \frac{M_2}{W} + \frac{P_d}{2A} = \frac{1,83 \cdot 10^2}{1333} + \frac{9,2}{2 \cdot 400} = 0,149 \text{ kN/sm}^2.$$

Bu ýerde $W = \frac{b^3}{6} = 1333 \text{ sm}^3$, $A = b^2 = 400 \text{ sm}^2$.

$$\text{Urgandaky dartgynlylyk } \sigma_{\text{urg}} = \frac{\sqrt{2} P_d}{4A} = \frac{\sqrt{2} \cdot 9,2}{4 \cdot 1,27} = 2,56 \text{ kN/sm}^2.$$

9.5. $\tau = 10,9 \text{ kN/sm}^2$.

Deň haýallanyan hereketde mahowigiň burç tizlenmesi

$$\varepsilon = \omega^2 / 2\varphi = 75,4^2 / 2 \cdot 2 \cdot 20 \cdot 3,14 = 22,6 \text{ rad/s}^2.$$

Towlandyryjy momenti

$$M_t = m i \varepsilon = 200 \cdot 0,6 \cdot 22,6 = 2716 \text{ Nm} = 2,716 \text{ kNm}.$$

$$\text{Galtaşma dartgynlylyk } \tau = \frac{M_k}{W_p} = \frac{2,716 \cdot 10^2}{25} = 10,9 \text{ kN/sm}^2,$$

bu ýerde $W_p = 0,2 \cdot 5^3 = 25 \text{ sm}^3$.

9.6. $\sigma_{\max} = 21,78 \text{ kN/sm}^2$.

$$\text{Kriwoşipiň burç tizligi } \omega = \frac{\pi n}{30} = \frac{3,14 \cdot 2800}{30} = 293 \text{ rad/s},$$

$$\text{Normal tizlenme } a_n = \omega^2 r = 293^2 \cdot 0,075 = 6441 \text{ m/s}^2.$$

$$\text{Şatunyň kese kesiginiň meýdany } A = 2 \cdot 30 \cdot 4 + 32 \cdot 4 = 368 \text{ mm}^2,$$

Inersion ýüküň depgini

$$q_{\text{in max}} = \gamma A a_n \cdot \frac{1}{g} = 78 \cdot 10^{-6} \cdot 3,68 \cdot 6441 \cdot 10^2 \cdot \frac{1}{981} = 0,188 \text{ kN/sm} = 1,91 \cdot 10^{-2} \text{ kN/m}$$

Şatunyň iň uly egme momenti

$$M_{\max} = \frac{q_{\max} \ell^2}{15,6} = \frac{1,91 \cdot 10^{-2} \cdot 0,25^2}{15,6} = 0,75 \text{ kN} \cdot \text{m}.$$

Kesigiň inersiýa momenti

$$I_x = \frac{30 \cdot 40^3}{12} - \frac{26 \cdot 32^3}{12} = 8,9 \text{ sm}^4,$$

Kesigiň garşylyk momenti

$$W_x = \frac{I_x}{b} \cdot 2 = \frac{8,9}{4,0} \cdot 2 = 4,45 \text{ sm}^3.$$

İň uly dartgynlyk

$$\sigma_{\max} = \frac{M_{\max}}{W_x} + \frac{P_{90^\circ}}{A} = \frac{75}{4,45} + \frac{0,65 \cdot 30}{3,68} = 21,78 \text{ kN/sm}^2.$$

9.7. $n = 106 \text{ ayl/min}$, $f_d = 2,4 \text{ sm}$.

Steržen BÇ aýlananda, merkezden daşlaşýan inersiýa güýjüň P_d täsirinden egilýär.

$$P_d = \frac{P}{g} \omega^2 r, \text{ bu ýerde } r = a + f_d, f_d = \frac{P_d \ell^3}{3EI} - \text{B Ç sterženiň } P_d$$

güýçden iň uly progibi,

$$\text{bu ýerde } I = \frac{bh^3}{12}.$$

$$\text{Onda } P_d = \frac{P}{g} \omega^2 r = \frac{P}{g} \left(\frac{\pi n}{30} \right)^2 (a + f_d) = \frac{\pi^2 n^2}{30^2 g} P \left(a + \frac{P_d \ell^3}{3EI} \right).$$

$$\text{Bu ýerden } P_d = \frac{Pa}{30^2 g - \frac{P \ell^3}{\pi^2 n^2}} \quad (a)$$

$$\text{BC sterženiň berklik şerti } \sigma_{\max} = \frac{M_{\max}}{W} = \frac{P_d \ell}{W} \leq [\sigma], W = \frac{bh^2}{6}.$$

$$\text{Onda } P_d \text{ güýjüň aňryçäk bahasy } P_d = \frac{[\sigma]W}{\ell} \quad (b)$$

(a) we (b) aňlatmalary deňeşdirip alarys:

$$n = \frac{30}{\pi} \sqrt{\frac{gbh^2}{6P\ell \left(\frac{a}{[\sigma]} + \frac{2\ell^2}{3Eh} \right)}} = 106 \text{ ayl/min}$$

BÇ sterženiň iň uly progibi

$$f_d = \frac{P_d \ell^3}{3EI} = \frac{[\sigma]W\ell^2}{3EI} = \frac{2[\sigma]\ell^2}{3Eh} = \frac{2 \cdot 18 \cdot 40^2}{3 \cdot 2 \cdot 10^4 \cdot 0,4} = 2,4 \text{ sm}.$$

9.8. $[\omega] = 32,4 \text{ rad/s}$.

Deňölçeqli aýlawda merkezden daşlaşýan inersiýa güýjüň depgini aşakdaky ýaly bolýar.

$$\text{DE bölekde } q_{in} = m\omega^2 \ell = \frac{\gamma A}{g} \cdot \omega^2 \ell$$

ÇD bölekde noldan (Ç nokatda), q_{in} (D nokatda) çenli çyzyk kanuny esasynda ýaýraýar.

$$\text{Direglerdäki gaýtargylar } R_A = \frac{q_{in} \ell}{2}, R_B = q_{in} \cdot \ell.$$

Statiki kesgitlenýän tekiz çarçuwanýň egme momentiniň epýury suratda görkezilen.

$$\text{Epýurdan } M_{\max} = q_{in} \cdot \ell^2$$

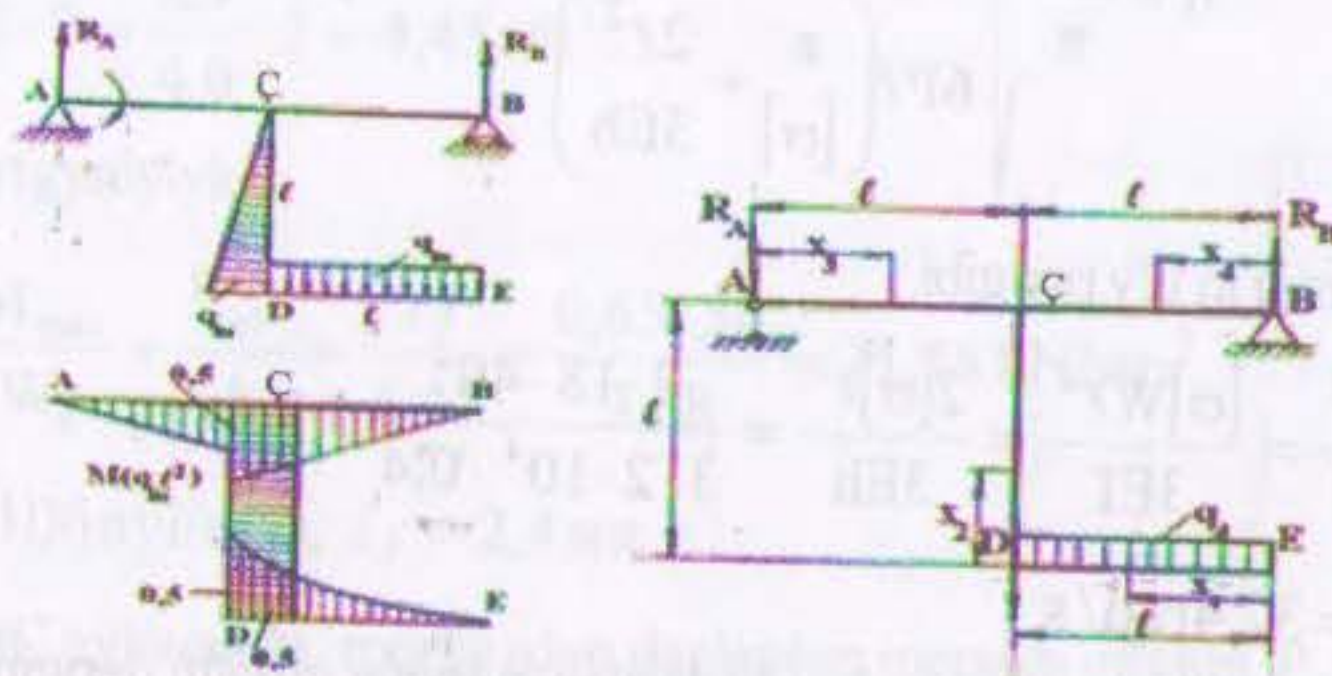
AB bölegiň berklik şertinden iň uly rugsat edilýän burç tizligini kesgitleýäris,

$$\sigma = \frac{M_{\max}}{W} \leq [\sigma] \Rightarrow [M_{\max}] = [\sigma]W = [\sigma] \cdot \frac{\pi d^3}{32} = 10 \cdot \frac{3,14 \cdot 1,8^3}{32} = 5,72 \text{ kN} \cdot \text{sm}$$

Başga tarapdan

$$M_{\max} = \frac{\gamma A}{g} \omega^2 \ell^3 = \frac{78 \cdot 10^{-6} \cdot 3,14 \cdot 1,8^2}{981 \cdot 4} \cdot 30^3 \cdot \omega^2 = 0,545 \cdot 10^{-2} \omega^2.$$

Onda $0,545 \cdot 10^{-2} [\omega]^2 = 5,72$, Bu ýerden $[\omega] = 32,4 \text{ rad/s}$.



9.8-nji surat

9.9. $\sigma_{\max} = 10 \text{ kN/sm}^2$.

Oka täsir edýän güýç

$$P_1 = P + \frac{mv^2}{r} = P + \frac{P}{rg} \cdot 2gH = P \left(1 + \frac{2H}{r} \right) = P \left(1 + \frac{2 \cdot 2r}{r} \right) = 0,25(1 + 4) = 1,25 \text{ kN}$$

Maýatnigiň okunyň iň uly egme momenti

$$M_{\max} = \frac{P\ell}{4} = \frac{1,25 \cdot 25}{4} = 7,8 \text{ kN} \cdot \text{sm},$$

onda $\sigma_{\max} = \frac{32 \cdot M_{\max}}{\pi d^3} = \frac{32 \cdot 7,8}{3,14 \cdot 2^3} = 10 \text{ kN/sm}^2$.

9.10. $\sigma_{\max} = 10,2 \text{ kN/sm}^2$, $\Delta \ell_d = 0,765 \text{ mm}$.

Birdenkä goýlan güýç steržende $k_d = 2$ deň bolan dinamiki güýji döredýär, ýagny $P_d = 2P$.

Iň uly dartgynlyk $\sigma_{\max} = \frac{P_d}{A} = \frac{8P}{\pi d^2} = \frac{8 \cdot 25}{3,14 \cdot 2,5^2} = 10,2 \text{ kN/sm}^2$,

Dinamiki durkuny üýtgetme $\Delta \ell_d = k_d \cdot \Delta \ell_{st} = 2 \cdot \frac{P\ell}{EA} = 0,0765 \text{ sm}$.

9.11. $\Delta_d = 4,83 \text{ mm}$.

Urguda dinamiki koeffisiýent $k_d = 1 + \sqrt{1 + \frac{2h}{\Delta_{st}}}$.

Bu ýerde $h = 1 \text{ mm}$, $\Delta_{st} = 2 \text{ mm}$ we $k_d = 1 + \sqrt{1 + \frac{2 \cdot 1}{2}} = 2,414$,

$\Delta_d = k_d \cdot \Delta_{st} = 2,41 \cdot 2 = 4,83 \text{ mm}$.

9.12. $d = 2,53 \text{ sm}$, $d' = 2,26 \text{ sm}$.

1) Takyk çözüw $\sigma_d = \sigma_{st} \left(1 + \sqrt{1 + \frac{2h}{\Delta_{st}}} \right) \leq [\sigma]$

$$\left(\frac{[\sigma]}{\sigma_{st}} - 1 \right)^2 = \left(\sqrt{1 + \frac{2h}{\Delta_{st}}} \right)^2 \Rightarrow \left(\frac{[\sigma]}{\sigma_{st}} \right)^2 - 2 \cdot \frac{[\sigma]}{\sigma_{st}} + 1 = 1 + \frac{2h}{\Delta_{st}}$$

$$\left(\frac{[\sigma]A}{P} \right)^2 - 2 \frac{[\sigma]A}{P} = \frac{2h \cdot EA}{P\ell} \Rightarrow A = 5 \text{ sm}^2 \Rightarrow d = 2,53 \text{ sm};$$

2) Ýakynlaşdyrylan çözüw $\sigma_d = \sigma_{st} \sqrt{\frac{2h}{\Delta_{st}}} \leq [\sigma]$

$$\left(\frac{[\sigma]}{\sigma_{st}} \right)^2 = \frac{2h}{\Delta_{st}} \Rightarrow \left(\frac{[\sigma]A}{P} \right)^2 = \frac{2hEA}{P\ell} \Rightarrow A = 4 \text{ sm}^2 \Rightarrow d' = 2,26 \text{ sm}.$$

9.13. $\sigma_d = 15,43 \text{ kN/sm}^2$, $\sigma_d^i = 16,7 \text{ kN/sm}^2$.

1) Urganyň agramyny hasaba almazdan, lebýodka birden togtadylan

ýagdaýynda $k_d = 1 + \sqrt{\frac{v^2 EA}{gP\ell}}$, onda

$$\sigma_d = \sigma_{st} \cdot k_d = \frac{P}{A} \left(1 + \sqrt{\frac{v^2 EA}{gP\ell}} \right) = \frac{50}{10} \left(1 + \sqrt{\frac{160^2 \cdot 2 \cdot 10^4 \cdot 10}{981 \cdot 50 \cdot 24000}} \right)$$

bu ýerden $\sigma_d = 15,43 \text{ kN/sm}^2$.

2) Urganyň agramy hasaba alnan ýagdaýynda

$$k_d^i = 1 + \sqrt{\frac{v^2 EA}{gP\ell(1+\beta)}}, \quad \beta - \text{urganyň göterilen massasynyň} \quad \frac{Q_{urg}}{3g} = \frac{\gamma A \ell}{3g}$$

urýan jisimiň massasyna P/g bolan gatnaşygy $\beta = \frac{\gamma A \ell}{3P} = 0,125$.

Urganyň hususy agramyndan döreýän dartgynlyk $\sigma_{st}^i = \gamma \ell$,

Lebýodka togtadylandaky dartgynlyk $\sigma_d'' = \sigma_{st} \cdot k_d^i$,

$$\begin{aligned} \sigma_d' &= \sigma_{st}' + \sigma_d'' = \gamma \ell + \frac{P}{A} \left(1 + \sqrt{\frac{v^2 EA}{gP\ell(1+\beta)}} \right) = \\ \text{Onda} \quad &= 1,87 + 14,83 = 16,7 \text{ kN/sm}^2. \end{aligned}$$

$$\mathbf{9.14.} \quad f_d = 0,355 \text{ sm}, \quad \sigma_{\max} = 5,87 \text{ kN/sm}^2.$$

Güýç duýdansyz goýlanda dinamiki koeffisiýent $k_d = 2$, 14-nji belgili balka üçin $I_x = 572 \text{ sm}^4$, $W_x = 81,7 \text{ sm}^3$.

Statiki goýlan güýçden balkanyň in uly progibi

$$f_{st} = \frac{P\ell^3}{3EI} = \frac{1,5 \cdot 160^3}{3 \cdot 2 \cdot 10^4 \cdot 572} = 0,1755 \text{ sm}.$$

Dinamiki progib $f_d = f_{st} \cdot k_d = 0,1775 \cdot 2 = 0,355 \text{ sm}$.

Dinamiki dartgynlyk $M_{\max} = P\ell = 1,5 \cdot 1,6 = 2,4 \text{ kN} \cdot \text{m}$.

$$\sigma_d = \sigma_{st} \cdot k_d = \frac{M_{\max}}{W} \cdot k_d = \frac{2,4 \cdot 10^2}{81,7} \cdot 2 = 5,87 \text{ kN/sm}^2.$$

$$\mathbf{9.15.} \quad \tau_{\max} = 9 \text{ kN/sm}^2.$$

Walyň kesigindäki towlanma momenti energiýanyň balansyndan tapýarys. Birden togtadylanda $T = U$

$$T = \frac{I_0 \omega^2}{2} - \text{hereketiň kinetiki energiýasy}$$

$$U = \frac{M_k^2 \ell}{2GI_p} - \text{durkuny üýtgetmäniň potensial energiýasy}$$

$$\frac{I_0 \omega^2}{2} = \frac{M_k^2 \ell}{2GI_p} \Rightarrow M_k = \omega \sqrt{\frac{I \cdot GI_p}{\ell}};$$

$$I_0 = \frac{QD^2}{8g} - \text{diskiň massasynyň inersiýa momenti}$$

Q – diskiň agramy.

$$\text{Onda } \tau_{\max} = \frac{M_k}{W_p} = \omega_0 \sqrt{\frac{I_0 GI_p}{\ell W_p^2}} = \omega \sqrt{\frac{2I_0 G}{\ell A}}.$$

$$\text{Bu ýerde } \frac{I_p}{W_p^2} = \frac{\pi d^4}{32} \cdot \frac{16^2}{(\pi d^3)^2} = \frac{2 \cdot 4}{\pi d^2} = \frac{2}{A}; \quad Q = \gamma \frac{\pi D^2}{4} \cdot t = 0,88 \text{ kN};$$

$$I_0 = \frac{QD^2}{8g} = \frac{0,88 \cdot 60^2}{8 \cdot 981} = 0,403 \text{ kN} \cdot \text{sm} \cdot \text{s}^2;$$

$$\omega = \frac{\pi n}{30} = \frac{3,14 \cdot 150}{30} = 15,7 \text{ s}^{-1};$$

$$A = \frac{\pi d^2}{4} = \frac{3,14 \cdot 10^2}{4} = 78,5 \text{ sm}^2,$$

$$\tau_{\max} = \omega \cdot \sqrt{\frac{2I_0 G}{\ell A}} = \omega \cdot \sqrt{\frac{2 \cdot 0,403 \cdot 8 \cdot 10^3}{250 \cdot 78,5}} = 9 \text{ kN/sm}^2.$$

$$\mathbf{9.16.} \quad v = 117 \text{ sm/s}.$$

Balkanyň statiki progibi, 5 kN güýçden

$$f_{st} = \frac{P_2}{P_1} \cdot f_d = \frac{5}{45} \cdot 2 = 0,222 \text{ sm},$$

$$\text{Onda } k_d = \frac{f_d}{f_{st}} = \frac{2}{0,222} = 9; \text{ ýöne } k_d = 1 + \sqrt{1 + \frac{v^2}{gf_{st}}} = 9.$$

$$\text{Bu ýerden } v = \sqrt{[(9-1)^2 - 1] \cdot 981 \cdot 0,222} = 117 \text{ sm/s}.$$

9.17. $h = 4 \text{ sm}$.

16-njy belgili iki tawra balka üçin

$$I_x = 873 \text{ sm}^4, W_x = 109 \text{ sm}^3.$$

$$\text{Balkanyň statiki progibi } f_{st} = \frac{P\ell^3}{48EI} = \frac{2 \cdot 300^3}{48 \cdot 2 \cdot 10^4 \cdot 873} = 0,0644 \text{ sm}.$$

Balka ýüküň gaçýan ýerinde pružiniň çökmesi

$$\lambda_{st} = \frac{\lambda_{pr}}{2} = \frac{4PR^3 \cdot n}{2 \cdot Gr^4 \cdot 2} = \frac{4 \cdot 2 \cdot 5^3 \cdot 10}{2 \cdot 8 \cdot 10^3 \cdot 1^4 \cdot 2} = 0,3125 \text{ sm}.$$

Balkanyň berklik şertinden

$$\sigma_d = \sigma_{st} \cdot k_d \leq [\sigma] \Rightarrow \frac{P\ell}{4W_x} \cdot k_d = [\sigma],$$

$$k_d = \frac{4W_x[\sigma]}{P\ell} \Rightarrow 1 + \sqrt{1 + \frac{2h}{f_{st}}} = \frac{4 \cdot 109 \cdot 16}{2 \cdot 300} \Rightarrow 10,6 = \sqrt{1 + \frac{2h}{0,0644}},$$

Bu ýerden $h = 3,586 \text{ sm}$.

Pružiniň berklik şertinden $\tau_d = \tau_{st} \cdot k_d \leq [\tau]$,

$$k_d \cdot \frac{2PR}{2 \cdot \pi r^3} = [\tau] \Rightarrow k_d \cdot \frac{2 \cdot 2 \cdot 5}{2 \cdot 3,14 \cdot 1^3} = 20 \Rightarrow k_d = 6,28,$$

$$1 + \sqrt{1 + \frac{2h}{0,3125}} = 6,28 \Rightarrow h = 4 \text{ sm}.$$

$$9.18. f_{\max} = 9,25 \text{ sm}, \sigma_d = 37 \text{ kN/sm}^2.$$

$$\text{Balkanyň egrenen okunyň deňlemesi } y'' = \frac{P\ell}{EI_0}.$$

Iki gezek integrirläp we hemişelikleri kesgitläp alarys:

$$y = \frac{P\ell}{EI_0} \left(\frac{x^2}{2} - \ell x + \frac{\ell^2}{2} \right), f_{st} = \frac{P\ell^3}{2EI_0} = \frac{0,2 \cdot 100^3 \cdot 12}{2 \cdot 2 \cdot 10^4 \cdot 5 \cdot 2^3} = 1,5 \text{ sm},$$

$$y = \frac{f_{st}}{\ell^2} (\ell - x)^2.$$

Balkanyň kinetiki energiýasy

$$T = \int_0^\ell \frac{P}{2g} V_0^2 \frac{(\ell - x)^4}{\ell^4} dx = \frac{P\ell}{2g} V_0^2 \int_0^\ell \frac{(\ell - x)^4}{\ell^5} dx = \frac{P\ell}{2g} V_0^2 \frac{1}{5},$$

Massanyň getirilen koeffisiýenti $k = 0,2$.

$$\text{Balkanyň agramy } Q = \frac{1}{2} 5 \cdot 2 \times 100 \cdot 78,5 \cdot 10^{-6} = 0,0393 \text{ kN}.$$

Dinamiki progib

$$f_d = f_{st} \left[1 + \sqrt{\frac{2h}{f_{st} \left(1 + \frac{kQ}{P} \right)}} \right] =$$

$$1,5 \left[1 + \sqrt{\frac{2 \cdot 20}{1,5 \left(1 + \frac{0,2 \cdot 0,0393}{0,2} \right)}} \right] = 9,25 \text{ sm}.$$

$$\sigma_d = \frac{2y_{\max} E f_d}{\ell^2} = \frac{2 \cdot 1 \cdot 2 \cdot 10^4 \cdot 9,25}{100^2} = 37 \text{ kN/sm}^2.$$

9.19. 41% dartgynlyk köpelyär.

$$1) \lambda_d = \lambda_{st} \cdot k_d = \sqrt{2h\lambda_{st}}, k_d = \frac{\sqrt{2h\lambda_{st}}}{\lambda_{st}},$$

$$\sigma_d = \sigma_{st} \cdot k_d = \frac{P}{A} \cdot \frac{\sqrt{2h\lambda_{st}}}{\lambda_{st}} = \frac{P \cdot \sqrt{2h}}{A \cdot \lambda_{st}} = \frac{P\sqrt{2h}}{A\sqrt{\lambda_{st}}}.$$

2) Eger meýdany iki gezek azaltsaň

$$\sigma'_d = \frac{2P\sqrt{2h}}{A\sqrt{\lambda'_{st}}}$$

$$\text{Onda } \frac{\sigma'_d}{\sigma_d} = 2 \cdot \sqrt{\frac{\lambda_{st}}{\lambda'_{st}}} = 2 \cdot \sqrt{\frac{Pl \cdot EA}{EA \cdot 2Pl}} = \frac{2}{\sqrt{2}} = 1,41.$$

9.20. 1) $\omega_o = 219,4s^{-1}$, $t_o = 0,02863s$; 2) $\omega_o = 219,3s^{-1}$,

$t_o = 0,02864s$.

1) Diregiň agramyny hasaba almazdan, yrgyldynyň ýygylgy

$$\Delta \ell_{st} = \frac{Pl}{EA} = \frac{100 \cdot 80 \cdot 4}{2 \cdot 10^4 \cdot 3,14 \cdot 5^2} = 0,0204 \text{ sm}$$

$$\omega_o = \sqrt{\frac{g}{\Delta \ell_{st}}} = \sqrt{\frac{gEA}{Pl}} = \sqrt{\frac{gE\pi d^2}{4Pl}} = \sqrt{\frac{981 \cdot 2 \cdot 10^4 \cdot 3,14 \cdot 5^2}{4 \cdot 100 \cdot 80}} = 219,4s^{-1};$$

$$\text{onda period } t_o = \frac{2\pi}{\omega_o} = \frac{3,14 \cdot 2}{219,4} = 0,02863s.$$

2) Diregiň agramyny hasaba alýarys:

$$\Delta \ell'_{st} = \Delta \ell_{st} + \frac{\gamma \ell^2}{2E} = 0,0204 + \frac{78 \cdot 10^{-6} \cdot 80^2}{2 \cdot 10^4} = 0,02;$$

$$\text{onda } \omega_o = \sqrt{\frac{g}{\Delta \ell'_{st}}} = \sqrt{\frac{981}{0,02}} = 219,3s^{-1},$$

$$t_o = \frac{2\pi}{\omega_o} = \frac{2 \cdot 3,14}{219,3} = 0,02864s.$$

9.21. $t_o = 0,048s$, $\omega_o = 131s^{-1}$.

9.22. 9.21 meseleden $\omega_o = 131s^{-1}$

Mejbury yrgyldynyň ýygylgy

$$\omega = \frac{\pi n}{30} = \frac{3,14 \cdot 1300}{30} = 136,2s^{-1}$$

Yrgyldynyň ösme koeffisiýenti

$$\beta = \frac{1}{\left(\frac{\omega}{\omega_o}\right)^2 - 1} = \frac{1}{\left(\frac{136,2}{131}\right)^2 - 1} = 12,35.$$

$$\text{Dinamiki koeffisiýent } k_d = 1 + \frac{\delta_H}{\delta_Q} \cdot \beta = 1 + \frac{H}{Q} \beta = \frac{80}{500} \cdot 12,35 = 2,98.$$

$\frac{\delta_H}{\delta_Q} = \frac{H}{Q}$, δ_Q - dwigateliň ýarym agramyndan kronşteýniň statiki deformasiýasy.

δ_H - mejbury güýjüň ýarysyndan kronşteýniň statiki deformasiýasy.

Iň uly dartgynlyk AB pürsde döreyär.

$$\sigma_{\max} = \frac{P_{AB}}{A} \cdot k_d = \frac{10 \cdot 2,98}{10 \cdot 10} = 0,298kN/sm^2.$$

9.23. $\Delta\omega = 35,7\%$, $\tau_d = 4,72 \text{ kN/sm}^2$, $\lambda_d = 10,8 \text{ mm}$.

9.24. $\omega = 23,4 \text{ s}^{-1}$.

Maşynlaryň agramy bilen balkany ýükleýäris. $P_1 = m_1 g = 5 \text{ kN}$,

$P_2 = m_2 g = 15 \text{ kN}$. Direglerdäki gaýtargylary $R_A = 8,3 \text{ kN}$,

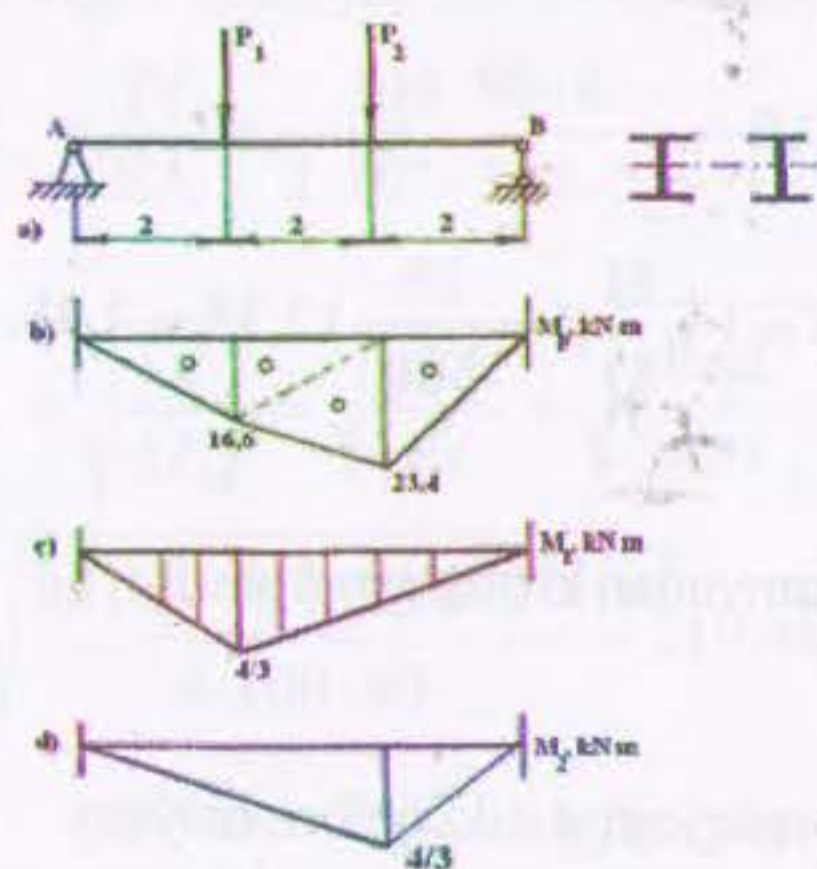
$R_B = 11,7 \text{ kN}$ kesgitläp, berlen güýçlerden egme momentiň M_p epýuryny gurýarys (surata seret).

Güýçleriň goýlan nokatlaryna birlik güýçleri goýup, birlik güýçlerden \bar{M}_1 we \bar{M}_2 momentleriň epýurlaryny gurýarys (surata seret).

Epýurlary köpeltmek usulyny ulanyp a_1 we a_2 ornuny üýtgetmeleri kesgitleýäris:

$$a_1 = \frac{1}{EI} \left[\frac{1}{2} \cdot 2 \cdot 16,6 \cdot \frac{8}{9} + \frac{1}{2} \cdot 2 \cdot 16,6 \cdot \frac{10}{9} + \frac{1}{2} \cdot 2 \cdot 23,4 \cdot \frac{8}{9} + \frac{1}{2} \cdot 2 \cdot 23,4 \cdot \frac{4}{9} \right];$$

onda $a_1 = \frac{64,4}{EI} = 17,03 \cdot 10^{-3} \text{ m}$.



9.25-nji surat

Şonuň ýaly-da

$$a_2 = \frac{69}{EI} = 18,2 \cdot 10^{-3} \text{ m}.$$

a_1 we a_2 bahalaryny Releýiň formulasyna goýup alarys:

$$\omega = \sqrt{\frac{\sum m_i a_i}{\sum m_i a_i^2} \cdot g} = 23,4 \text{ s}^{-1}.$$

9.25. $\omega_0 = 16,4$, $\omega = 99,5 \text{ s}^{-1}$, diýmek, rezonans hadysasy bolmaýar.

Birlik momentden walyň towlanma burçy

$$\delta = \frac{1 \cdot \ell}{GI_p} = \frac{1 \cdot \ell \cdot 32}{G \cdot \pi d^4} = 3,05 \cdot 10^{-6}.$$

Walyň erkin yrgyldysynyň periody

$$t = 2\pi \sqrt{I_m \cdot \delta} = 2 \cdot 3,14 \sqrt{31 \cdot 3,05 \cdot 10^{-6}} = 0,061 \text{ s}.$$

Walyň erkin yrgyldysynyň ýygylgy

$$\omega_0 = \frac{1}{t} = \frac{1}{0,061} = 16,4 \text{ s}^{-1};$$

Walyň mejbury yrgyldysynyň ýygylgy

$$\omega = \frac{\pi n}{30} = \frac{3,14 \cdot 950}{30} = 99,5 \text{ s}^{-1},$$

$\omega > \omega_0$; rezonans hadysasy bolmaýar.

9.26. $v_{kr} = 117 \text{ km/sag}$.

Pružiniň çökmesi $\lambda = \frac{4PR^3 n}{Gr^4} = 1,53 \text{ sm}$.

Bu ýerde $P = \frac{Q + S}{8} = \frac{50 + 35}{8} = 10,62 \text{ kN}$.

Wagonyň erkin yrgyldysynyň periody

$$t_0 = 2\pi \sqrt{\frac{\lambda}{g}} = 6,28 \sqrt{\frac{1,53}{981}} = 0,247 \text{ s}.$$

Onda yrgyldynyň ýygylgy

$$\omega_0 = \frac{1}{t_0} = \frac{1}{0,247} = 4,05 \text{ s}^{-1} = 243 \frac{1}{\text{min}}.$$

Wagonyň hereketiniň kritiki tizligi $\omega = \omega_0$ ýagdaýynda bolýar we

$$V_{kr} = \frac{\omega \cdot 60 \ell}{1000} = \frac{243 \cdot 60 \cdot 8}{10^3} = 117 \text{ km/sag.}$$

9.27. $c = 0,255 \text{ sm}, \sigma_{\max} = 1265 \text{ kg/sm}^2.$

Dwigateliň massasy $m = \frac{Q}{g} = \frac{2500}{981} = 2,55 \text{ kg} \cdot \text{s}^{-2} / \text{sm},$

Birlik güýçden ýüküň aşagyndaky balkanyň progibi

$$\delta = \frac{1 \cdot \ell^3}{48EI} = \frac{1 \cdot 350^3}{48 \cdot 2 \cdot 10^6 \cdot 5010} = 8,91 \cdot 10^{-5} \text{ sm/kg},$$

Erkin yrgyldynyň ýygyllygy

$$\omega_o = \frac{1}{\sqrt{m\delta}} = \frac{1}{\sqrt{2,55 \cdot 8,91 \cdot 10^{-5}}} = 66,5 \text{ s}^{-1}.$$

Mejbury yrgyldynyň ýygyllygy

$$\omega = \frac{\pi n}{30} = \frac{3,14 \cdot 540}{30} = 56,5 \text{ s}^{-1},$$

Mejbury yrgyldynyň amplitudasy

$$c = \frac{P}{m} \cdot \frac{1}{\omega_o^2 - \omega^2} = \frac{800}{2,55} \cdot \frac{1}{66,5^2 - 56,5^2} = 0,255 \text{ sm}.$$

Bu amplituda ekwiwalent statiki güýç degişli

$$P_{st} = \frac{c}{\delta} = \frac{0,255}{8,91 \cdot 10^{-5}} = 2860 \text{ kg} = 28,6 \text{ kN}.$$

Bu güýjüň egilmeden döredýän dartgynlylygy

$$\sigma = \frac{M}{W} = \frac{P_{st} \ell}{4W} = \frac{2860 \cdot 350}{4 \cdot 371} = 675 \text{ kg/sm}^2.$$

Dwigateliň agramyndan döreýän dartgynlylyk

$$\sigma = \frac{M}{W} = \frac{Q \ell}{4W} = \frac{2500 \cdot 350}{4 \cdot 371} = 590 \text{ kg/sm}^2.$$

Normal dartgynlylyk aşakdaky çäkde üýtgeýär,

$$\sigma_{\min} = 590 - 675 = -85 \text{ kg/sm}^2,$$

$$\sigma_{\max} = 590 + 675 = 1265 \text{ kg/sm}^2.$$

9.28. $\omega = 302 \text{ s}^{-1}.$

Konstruksiýanyň statiki progibi

$$\Delta_{st} = \frac{P \ell^3}{3EI} = \frac{0,01 \cdot 20^3 \cdot 12}{3 \cdot 2,2 \cdot 10^4 \cdot 0,3^3 \cdot 5} = 1,08 \cdot 10^{-2} \text{ sm}.$$

Konstruksiýanyň ýygyllygy

$$\omega = \sqrt{\frac{g}{\Delta_{st}}} = \sqrt{\frac{981}{1,08 \cdot 10^{-2}}} = 302 \text{ s}^{-1}.$$

9.29. $\omega = 1070 \text{ s}^{-1}, T = 0,00587 \text{ s}, n_{kr} = 10223 \text{ aýl/min}.$

Şatunyň yrgyldysynyň ýygyllygyny aşakdaky takyk formula boýunça kesgitleýäris,

$$\omega = \frac{\pi^2}{\ell^2} \sqrt{\frac{EI \cdot g}{P}};$$

Şatunyň kesiginiň inersiýa momenti

$$I_x = 2 \left[\frac{bt^3}{12} + bt \left(\frac{h}{2} - \frac{t}{2} \right)^2 \right] + \frac{t_1 \cdot (h - 2t)^3}{12} =$$

$$= 2 \left[\frac{3 \cdot 0,5^3}{12} + 3 \cdot 0,5 \cdot 2,25^2 \right] + \frac{0,4 \cdot 4^3}{12} = 17,37 \text{ sm}.$$

$$\text{Onda } \omega = \frac{3,14^2}{30^2} \sqrt{\frac{2 \cdot 10^4 \cdot 17,37 \cdot 981}{0,035}} = 1070 \text{ s}^{-1}.$$

Şatunyň hususy yrgyldysynyň periody,

$$T = 0,00587 \text{ s}^{-1};$$

Dwigateliň kritiki aýlaw sany,

$$\omega_{kr} = \frac{\pi n_{kr}}{30} = 1070,$$

$$n_{kr} = \frac{1070 \cdot 30}{3,14} = 10223 \text{ aýl/min.}$$

9.30. $M_{\max} = 300 \text{ kN} \cdot \text{sm}.$

Şaýyň çydamlylyk çägi $\sigma_{-1s}^e = \frac{\sigma_{-1}^e}{\alpha_{kh} \alpha_m}$

$\alpha_{kh} = 1 + q(\alpha_{kt} - 1)$ - konsentrasıyanyň hakyky koeffisiýenti,

α_{kt} - konsentrasıyanyň nazary koeffisiýenti,

q - materialyň ýerli dartgynlylyga duýgurlyk koeffisiýenti,

$\alpha_{kt} = 1,5$ bahasyny $r/d = 0,125$ baglylykda tablisadan alýarys,

$q = 0,36$ bahasy $\sigma_B = 45 \text{ kN/sm}^2$ baglylykda grafikden alynýar.

Onda $\alpha_{kh} = 1 + 0,36(1,5 - 1) = 1,18.$

$\alpha_m = 1,56$ - masştab koeffisiýenti, walyň diametrine baglylykda grafikden alynýar.

Onda $\sigma_{-1s}^e = \frac{22}{1,18 \cdot 1,56} = 11,95 \text{ kN/sm}^2$

Rugsat edilýän dartgynlylyk $[\sigma_{-1s}^e] = \frac{\sigma_{-1s}^e}{k} = \frac{11,95}{2} = 5,97 \text{ kN/sm}^2.$

Berklik şertinden $M_{\max} = \frac{[\sigma_{-1s}^e] \cdot \pi d^3}{32} = \frac{5,97 \cdot 3,14 \cdot 8^3}{32} = 300 \text{ kN} \cdot \text{sm}.$

9.31. $n_a = 4,1$; $n_d = 1,5.$

Hasapda kabul edilen: $\psi_\sigma = 0,06$, $\alpha_\sigma = 2$, $\beta = 0,92$,

şaýyň konsentrasıyasynyň effekt koeffisiýenti $k_{os} = \frac{k_\sigma}{\varepsilon_\sigma \beta}.$

9.32. $n = 2,1$, $n_a = 3,5.$

Gatnaşyk $r/d = 0,05$. Grafikden $(k_\sigma)_{D=2} = 1,9$, $(k_\tau)_{D=2} = 1,5.$

$\frac{D}{d} = \frac{50}{40} = 1,25$ üçin

$k_\sigma = 1 + \xi \left[(k_\sigma)_{D=2} - 1 \right] = 1 + 0,85[1,9 - 1] = 1,77;$

$k_\tau = 1 + \xi \left[(k_\tau)_{D=2} - 1 \right] = 1 + 0,8[1,5 - 1] = 1,4.$

Grafikden $\varepsilon_\tau = \varepsilon_\sigma = 0,85$

Normal dartgynlylyk boýunça çydamlylyk çäginin berklik koeffisiýenti

$n_\sigma = \frac{\sigma_{-1}}{\psi_\sigma \sigma_m + \frac{k_\sigma}{\varepsilon_\sigma} \sigma_a} = \frac{22}{0,05 \cdot 0 + \frac{1,77}{0,85} \cdot 5} = 2,2;$

Galtaşma dartgynlylyk boýunça

$n = \frac{\tau_{-1}}{\psi_\tau \tau_m + \frac{k_\tau}{\varepsilon_\tau} \tau_a} = \frac{12}{0,05 \cdot 0 + \frac{1,4}{0,85} \cdot 1} = 7,3.$

Çydamlylyk çägi boýunça ätiýaçlyk koeffisiýenti

$n = \frac{n_\sigma n_\tau}{\sqrt{n_\sigma^2 + n_\tau^2}} = \frac{2,2 \cdot 7,3}{\sqrt{2,2^2 + 7,3^2}} = 2,1;$

Akyjylyk çägi boýunça ätiýaçlyk koeffisiýenti,

$n_\sigma = \frac{\sigma_{ak}}{\sigma_m + \sigma_a} = \frac{30}{5} = 6$, $n_\tau = \frac{\tau_{ak}}{\tau_m + \tau_a} = \frac{18}{4} = 4,5;$

Onda $n_a = \frac{6 \cdot 4,5}{\sqrt{6^2 + 4,5^2}} = 3,5.$

9.33. $n_\sigma = 1,29$, $n_a = 2,13$.

$$a_{\max} = \omega^2 r(1 + \lambda) = \left(\frac{3,14 \cdot 6000}{30} \right)^2 \cdot 0,04(1 + 0,28) = 2,02 \cdot 10^4 \text{ m} \cdot \text{s}^{-2}$$

İn uly tizlenme

Şatuny dartýan inersiýa güýji $P_{\text{in}} = (m_p + m_{y-s}) \cdot a_{\max} = 14,1 \text{ kN}$.

Gazyň basyş güýji

$$P_g = P_z \cdot A_p = 5,5 \cdot \frac{3,14 \cdot 78^2}{4} = 26270 \text{ N} = 26,27 \text{ kN}.$$

Bu güýç şatuny gysýar, şonuň üçin hem tersin bahasyny alýarys. Şatuna täsir edýän ok güýji $P_{\max} = 14,1 \text{ kN}$; $P_{\min} = -26,27 \text{ kN}$.

Assimetriýa koeffisiýenti $\rho = \frac{P_{\min}}{P_{\max}} = -1,86$.

Dartgynlyklary kesgitleýäris ($A = 1,555 \text{ sm}^2$)

$$\sigma_{\max} = \frac{P_{\max}}{A} = \frac{14,1}{1,555} = 9,07 \text{ kN/sm}^2,$$

$$\sigma_{\min} = \frac{P_{\min}}{A} = \frac{-26,27}{1,555} = -16,89 \text{ kN/sm}^2.$$

Sikliň häsiýetleri: Amplituda $\sigma_a = \frac{\sigma_{\max} - \sigma_{\min}}{2} = 12,99 \text{ kN/sm}^2$,

Orta dartgynlyk $\sigma_m = \frac{\sigma_{\max} + \sigma_{\min}}{2} = -3,91 \text{ kN/sm}^2$.

Ätiýaçlyk koeffisiýenti

$$n_\sigma = \frac{\sigma_{-1}}{k_\sigma \sigma_a + \psi_\sigma |\sigma_m|} = \frac{20}{1,11 \cdot 12,99 + 0,286 \cdot 3,91} = 1,29 < [n];$$

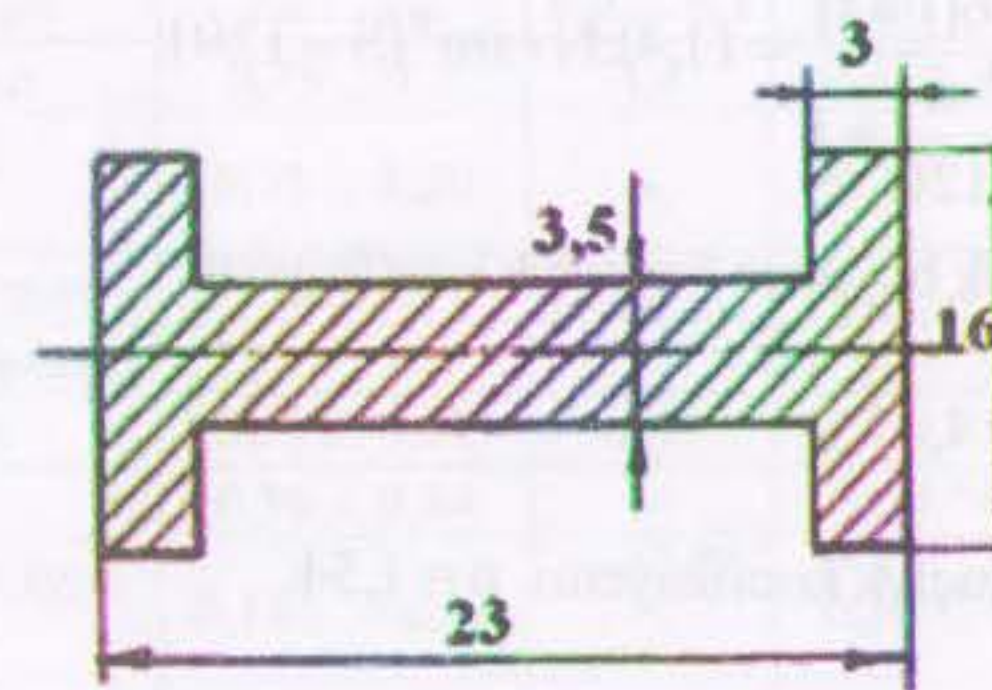
bu ýerde $k_\sigma = \frac{k_\sigma}{k_d \cdot k_v} = \frac{1,27}{0,88 \cdot 1,3} = 1,11$,

Polat üçin $\sigma_{-1s} = 20 \text{ kN/sm}^2$, $\sigma_a = 36 \text{ kN/sm}^2$, $\sigma_b = 70 \text{ kN/sm}^2$,

Onda $\psi_\sigma = \frac{\sigma_{-1s}}{\sigma_a} = \frac{20}{70} = 0,286$,

Statiki berklige ätiýaçlyk koeffisiýenti

$$n_a = \frac{\sigma_a}{|\sigma|_{\max}} = \frac{36}{16,89} = 2,13 - \text{rugsat edilyär.}$$



9.33-nji surat

9.34. $n = 1,54$.

İn uly normal we galtaşma dartgynlyklar

$$\sigma_{\max} = \frac{M_\ell}{W_x} = \frac{80}{0,1 \cdot 5^3} = 6,4 \text{ kN/sm}^2;$$

$$\tau_{\max} = \frac{M_t}{W_p} = \frac{64}{0,2 \cdot 5^3} = 2,56 \text{ kN/sm}^2.$$

Normal dartgynlyk boýunça ätiýaçlyk koeffisiýenti

$$n_\sigma = \frac{\sigma_{-1D}}{\sigma_{\max}} = \frac{\sigma_{-1}}{k_\sigma \beta \cdot \epsilon_m \cdot \sigma_{\max}} = \frac{28}{1,8 \cdot 1,38 \cdot 1,07 \cdot 6,4} = 1,65.$$

Bu ýerde $k_{\sigma} = 1,8$, $\beta = 1,07$, $\varepsilon_m = 1,38$ (tablisadan).

τ_{-1} we τ_a kesgitleýäris:

$$\tau_{-1} = 0,58\sigma_{-1} = 0,58 \cdot 28 = 16,25 \text{ kN/sm}^2.$$

$$\tau_a = 0,58\sigma_a = 0,58 \cdot 35 = 20,3 \text{ kN/sm}^2.$$

Towlanmada çydamlylyk çägi (simmetriýa sikli)

$$\tau_{-1D} = \frac{\tau_{-1}}{k_{\tau} \cdot \varepsilon_m \cdot \beta} = \frac{16,25}{1,8 \cdot 1,38 \cdot 1,07} = 6 \text{ kN/sm}^2.$$

Pulsirleýji siklde towlanmada çydamlylyk çägi ($k = 1$)

$$\tau_{rD} = \frac{\tau_{-1D}(1+k)}{\frac{\tau_{-1D}}{S} + 1} = \frac{6(1+1)}{\frac{6}{120} + 1} = 11,4 \text{ kN/sm}^2 (S = 120);$$

Galtaşma dartgynlylyk boýunça ätiýaçlyk koeffisiýenti

$$n_{\tau} = \frac{\tau_{rD}}{\tau_{\max}} = \frac{11,4}{2,56} = 4,45.$$

Berklige umumy ätiýaçlyk koeffisiýenti $n = 1,54$.

GOŞMAÇALAR

1-nji goşmaça

Materiallaryň fiziki-mehaniki häsiýetnamalary

Material	Maýyşgaklyk moduly $E \cdot 10^5$, MPa	Süýşme moduly $G \cdot 10^4$, MPa	Kese durkuny üýtgetmäniň koeffisiýenti, μ	Udel agram, γ kN/sm ³
Polat:				
Uglerodly	2,0 ... 2,1	8,0 ... 8,1	0,24 ... 0,33	78,5
Legirlenen	2,0 ... 2,2	8,0 ... 8,1	0,25 ... 0,30	77,5 ... 78,5
Çal çöýün	0,78 ... 1,5	4,4	0,23 ... 0,27	68 ... 76
Bürünçli galaýy	0,75 ... 1,20	-	0,32 ... 0,35	87,6 ... 88,2
Sozulan mis	1,0 ... 1,1	4,3	0,28 ... 0,34	89,4
Garyndylar:				
Alýumin	0,69 ... 0,71	2,7	0,33	26,4 ... 28,0
Magniý	0,39 ... 0,44	-	0,34	17,6 ... 18,0
Berklik çägi 20 MPa	0,182 ... 0,232	-	0,16 ... 0,18	-
Agaç boý süýümine	0,09 ... 0,15	0,055	-	4,8 ... 5,4 (sosna)
Tekstolit	0,04 ... 0,06	-	-	13 ... 14,5
Winiplast	0,03 ... 0,04	-	0,35 ... 0,37	13,8 ... 14,3
Kapron	0,014 ... 0,020	0,045 ... 0,048	0,35 ... 0,38	11,0 ... 11,4
Aýna süýümi	0,35	-	0,29	17,0 ... 18,0
Polietilen ND	0,005 ... 0,008	-	0,39	9,2 ... 9,7
Kauçuk	0,00008	-	0,47	-

2-nji goşmaça

Materiallaryň mehaniki häsiýetnamalary

Material	Berklik çägi σ_B , MPa	Akyjlyk çägi σ_a, σ_T , MPa	Otnositel uzalma δ , %	Çydamlylyk çägi, MPa		
				δ_{1s}	δ_{1e}	δ_{1t}
1	2	3	4	5	6	7
Adaty hilli uglerodly polat						
St 2 kp	330 ... 420	200 ... 220	30 ... 33	120...160	170...220	80...130
St 2 ps (sp)	340 ... 440	210 ... 230	29 ... 32			
St 3ps	370 ... 470	220 ... 240	24 ... 27	120...160	170...220	100...130
St 3ps (sp)	380 ... 490	230 ... 250	23 ... 26			
St 4ps	410 ... 520	240 ... 260	22 ... 25	-	190...250	-
St 4ps (sp)	420 ... 540	250 ... 270	21 ... 24			
St 5ps (sp)	500 ... 640	270 ... 290	17 ... 20	170...220	220...300	130...180
St 6ps (sp)	600	300 ... 320	12 ... 15	190...250	250...340	150...200
Hili ýokarlandyrylan uglerodly polat (kadalaşdyrylan)						
10	340 ... 420	210	31	120 ... 150	160 ... 220	80 ... 120
20	420 ... 500	250	25	120 ... 160	170 ... 220	100...130
30	500 ... 600	300	21	170 ... 210	200 ... 270	110...140
40	580 ... 700	340	19	180 ... 240	230 ... 320	140...190
45	610 ... 750	360	16	190 ... 250	250 ... 340	150...200
50	640 ... 800	380	14	200 ... 260	270 ... 350	160...210
60	690 ... 900	410	12	220 ... 280	310 ... 380	180...220

2-nji goşmaçanyň dowamy

1	2	3	4	5	6	7
Legirlenen polat						
20H	720 ... 850	400 ... 650	12	-	310 ... 380	170...230
40H	730 ... 1050	650 ... 900	15,5	240 ... 340	320 ... 480	210...260
45H	850 ... 1060	700 ... 950	9	-	310 ... 380	170...230
40HN	1000...1450	800...1300	-	310 ... 420	460 ... 600	-
30 HGSA	1100...1700	850 ... 1500	7	-	480 ... 700	280...400
60 G	710	420	11	250 ... 320	-	-
Çal we ýokary berklikdäki çöýün						
ÇÇ18-36	süýnme	-	-	35	90	-
	180					
	Egilme					
	360					
	Gysma					
	700					
ÇÇ 24-44	süýnme	-	-	65	120	100
	240					
	Egilme					
	440					
	Gysylma					
	1000					
ÇÇ 21-40	Süýnme	-	-	-	100	80
	210					
	Egilme					
	400					
	Gysylma					
	950					
AÇ 45-5	Süýnme	330	5	-	180 ... 200	-
	450 ... 550					
	Egilme					
	650 ... 750					
	Gysylma					
	1800...2000					

2-nji goşmaçanyň dowamy

1	2	3	4	5	6	7
AÇ 50-2	Süýnme	380	2	-	200..220	170...210
	500 ... 600					
	Egilme					
	900 ... 1000					
	Gysylma					
	1700...1800					
Durkuny üýtgedýän alýumin garyndylary						
АМЦ	100	50	20	-	50	
АД-31						
Tebigy könelişmek	140	70	13	-	90	
Emeli könelişmek	200	150	8	-	-	-
AM r5	270	120	15	-	110	-
AM r6	320	160	15	-	130	-
Д16Т	400...430	280 ...300	10	-	115	-
Miş garyndylary						
Latun L 68:						
Ýumşak	300 ... 380	-	42	-	120	-
Gaty	440 ... 550	-	10	-	150	-
Bürünç:						
Бр.АМц						
9-2	480... 550	-	20 ... 12	-	-	-
Бр.АжМц						
10-3-1,5	60	-	12	-	-	-

2-nji goşmaçanyň dowamy

1	2	3	4	5	6	7
Metal däl materiallar						
Agaç:						
sosna	Süýnme					
	93 ... 115					
	Egilme					
	74 ... 88	-	-	-	-	-
	Gysylma					
	45					
Dub	Süýnme					
	130					
	Egilme					
	95	-	-	-	-	-
	Gysylma					
	52					
Tekstolit	Süýnme					
	90 ... 100	70 ... 80	-	-	-	-
	Egilme					
	140 ... 150					
	Gysylma					
	230 ... 250					
Winiplast	Süýnme					
	40 ... 60	-	10 ... 25	-	-	-
	Egilme					
	80 ... 120					
	Gysylma					
	80 ... 160					

2-nji goşmaçanyň dowamy

1	2	3	4	5	6	7
Kapron	Süýnme					
	50 ... 60					
	Egilme					
	90 ... 100	-	-	-	-	-
	Gysylma					
	85 ... 100					
Epoksid smolasy	Süýnme					
	70 ... 80					
	Egilme					
	120 ... 130					
	Gysylma					
	145 ... 155					
Ftoreplat -3	Süýnme					
	30 ... 37	-	50 ... 70	-	-	-
	Egilme					
	60 ... 80					
	Gysylma					
	50 ... 60					

3-nji goşmaça

Ikitawraly balkalar DÖST 8239-72

Balkanyň belgisi	h, mm ✓	b, mm ✓	s, mm ✓	t, mm ✓	Kesi- giň meý- dany A, sm ² ✓	Massa 1m, kg ✓	Sprawoçnik ululyklary						
							x-x y-y						
							J _x , sm ⁴ ✓	W _x , sm ³ ✓	i _x , sm	S _x , sm ³	J _y , sm ⁴	W _y , sm ³	I _y , sm
10	100	55	4,5	7,2	12,0	9,46	198	39,7	4,06	23,0	17,9	6,49	1,22
12	120	64	4,8	7,3	14,7	11,5	350	58,4	4,88	33,7	27,9	8,72	1,38
14	140	73	4,9	7,5	17,4	13,7	572	81,7	5,73	46,8	41,9	11,5	1,55
16	160	81	5,0	7,8	20,2	15,9	873	109	6,57	62,3	58,6	14,5	1,70
18	180	90	5,1	8,1	23,4	18,4	1290	143	7,42	81,4	82,6	18,4	1,88
18a	180	100	5,1	8,3	25,4	19,9	1430	159	7,51	89,8	114	22,8	2,12
20	200	100	5,2	8,4	26,8	21,0	1840	184	8,28	104	115	23,1	2,07
20a	200	110	5,2	8,6	28,9	22,7	2030	203	8,37	114	155	28,2	2,32
22	220	110	5,4	8,7	30,6	24,0	2550	232	9,13	131	157	28,6	2,27
22a	220	120	5,4	8,9	32,8	25,8	2790	254	9,22	143	206	34,3	2,50
24	240	115	5,6	9,5	34,8	27,3	3460	289	9,97	163	198	34,5	2,37
24a	240	125	5,6	9,8	37,5	29,4	3800	317	10,10	178	260	41,6	2,63
27	270	125	6,0	9,8	40,2	31,5	5010	371	11,20	210	260	41,5	2,54
27a	270	135	6,0	10,2	43,2	33,9	5500	407	11,30	229	337	50,0	2,80
30	300	135	6,5	10,2	46,5	36,5	7080	472	12,30	268	337	49,9	2,69
30a	300	145	6,5	10,7	49,9	39,2	7780	518	12,50	292	436	60,1	2,95
33	330	140	7,0	11,2	53,8	42,2	9840	597	13,50	339	419	59,9	2,79
36	360	145	7,5	12,3	61,9	48,6	13380	743	14,70	423	516	71,1	2,89
40	400	155	8,3	13,0	72,6	57,0	19062	953	16,2	545	667	86,1	3,03
45	450	160	9,0	14,2	84,7	66,5	27696	1231	18,10	708	808	101,	3,09
50	500	170	10,0	15,2	100	78,5	39727	1589	19,9	919	1043	123,	3,23
55	550	180	11,0	16,5	118	92,6	55962	2035	21,8	1181	1356	151,	3,39
60	600	190	12,0	17,8	1380	108	76806	2560	23,6	1491	1725	182,	3,54

Şweller DÖST 8240-72

Şwelleriň belgisi	h, mm	b, mm	s, mm	t, mm	Kesigiň meýdany A, sm ²	Massa 1m, kg	Sprawoçnik ululyklary					
							x-x			y-y		
							J _x , sm ⁴	W _x , sm ³	i _x , sm	S _x , sm ³	J _y , sm ⁴	W _y , sm ³
5	50	32	4,4	7,0	6,16	4,84	22,8	9,1	1,92	5,59	5,61	2,75
6,5	65	26	4,4	7,2	7,51	5,90	48,6	15,0	2,54	9,00	8,70	3,68
8	80	40	4,5	7,4	8,98	7,05	89,4	22,4	3,16	13,3	12,80	4,75
10	100	46	4,5	7,6	10,90	8,59	174,0	34,8	3,99	20,4	20,40	6,46
12	120	52	4,8	7,8	13,30	10,40	304,0	50,6	4,78	29,6	31,20	8,52
14	140	58	4,9	8,1	15,60	12,30	491,0	70,2	5,50	40,8	45,40	11,0
14a	140	62	4,9	8,7	17,00	13,30	545,0	77,8	5,66	45,1	57,50	13,3
16	160	64	5,0	8,4	18,10	14,20	747,0	93,4	6,42	54,1	63,30	13,8
16a	160	68	5,0	9,0	19,50	15,30	823,0	103	6,49	59,4	78,80	16,4
18	180	70	5,1	8,7	20,70	16,30	1090,0	121,	7,24	69,8	86,00	17,0
18a	180	74	5,1	9,3	22,20	17,40	1190,0	132	7,32	76,1	105,0	20,0
20	200	76	5,2	9,0	23,40	18,40	1520,0	152	8,07	87,8	113,0	20,5
20a	200	80	5,2	9,7	25,20	19,80	1670,0	167	8,15	95,9	139,0	24,2
22	220	82	5,4	9,5	26,70	21,00	2110,0	192	8,89	110,	151,0	25,1
22a	220	87	5,4	10,2	28,80	22,60	2330,0	212	8,99	121,	187,0	30,0
24	240	90	5,6	10,0	30,60	24,00	2900,0	242	9,73	139,	208,0	31,6
24a	240	95	5,6	10,7	32,90	25,80	3180,0	265	9,84	151,	254,0	37,2
27	270	95	6,0	10,5	35,20	27,70	4160,0	308	10,9	178,	262,0	37,3
30	300	100	6,5	11,0	40,50	31,80	5810,0	387	12,0	224,	327,0	43,6
33	330	105	7,0	11,7	46,50	36,50	7980,0	484	13,1	281,	410,0	51,8
36	360	110	7,5	12,6	53,40	41,90	10820	601	14,2	350,	513,0	61,7
40	400	115	8,0	13,5	61,50	48,30	15220	761	15,7	444,	642,0	73,4

5-nji goşmaça
Sozma polatdan ýasalan deňgapdally burçluk
DÖST 8509-72

Profi- liň belgi- si	B, mm	d, mm	Kesi- giň meý- dany A, sm ²	Sprawoçnik ululyklary								Mas- sa 1m, kg
				x-x		o-x _o		y _o -y _o		x ₁ -x ₁		
				J _{xo} , sm ⁴	i _{xo} , sm	J _{xo} , max, sm ⁴	i _{xo} , max, x, sm	J _{yo} , min, sm ⁴	I _{yo} , mi n, sm	J _{x1} , sm ⁴	z _o ,sm	
1	2	3	4	5	6	7	8	9	10	11	12	13
2	20	3	1,13	0,40	0,59	0,63	0,75	0,17	0,39	0,81	0,60	0,89
		4	1,46	0,50	0,58	0,78	0,73	0,22	0,38	1,09	0,64	1,11
2,5	25	3	1,43	0,81	0,75	1,29	0,95	0,34	0,49	1,57	0,73	1,12
		4	1,86	1,03	0,74	1,62	0,93	0,44	0,48	2,11	0,76	1,46
2,8	28	3	1,62	1,16	0,85	1,84	1,07	1,48	0,55	2,20	0,80	1,27
3,2	32	3	1,86	1,77	0,97	2,80	1,23	0,74	0,63	3,26	0,89	1,46
		4	2,43	2,26	0,96	3,58	1,21	0,94	0,62	4,39	0,94	1,91
3,6	36	3	2,10	2,56	1,10	4,06	1,39	1,06	0,71	4,64	0,99	1,65
		4	2,75	3,29	1,09	5,21	1,38	1,36	0,70	6,24	1,04	2,16
4	40	3	2,35	3,55	1,23	5,63	1,55	1,47	0,79	6,35	1,09	1,85
		4	3,08	4,58	1,22	7,26	1,53	1,90	0,78	8,53	1,13	2,42
		5	3,79	5,53	1,20	8,75	1,54	2,30	0,79	10,7	1,17	2,97
4,5	45	3	2,65	5,13	1,39	8,13	1,75	2,12	0,89	9,04	1,21	2,08
		4	3,48	6,63	1,38	10,50	1,74	2,74	0,89	12,1	1,26	2,73
		5	4,29	8,03	1,37	12,70	1,72	3,33	0,88	15,3	1,30	3,37
5	50	3	2,96	7,11	1,55	11,30	1,95	2,95	1,00	12,4	1,33	2,32
		4	3,89	9,21	1,54	14,60	1,94	3,80	0,99	16,6	1,38	3,05
		5	4,80	11,2	1,53	17,80	1,92	4,63	0,98	20,9	1,42	3,77
5,6	56	4	4,38	12,1	1,73	20,80	2,18	5,41	1,11	23,3	1,52	3,44
		5	5,41	16,0	1,72	25,40	2,16	6,59	1,10	29,2	1,57	4,25
6,3	63	4	4,96	18,9	1,95	29,90	2,45	7,81	1,25	33,1	1,69	3,90
		5	6,13	23,1	1,94	36,60	2,44	9,52	1,25	41,5	1,74	4,81
		6	7,28	27,1	1,93	42,90	2,43	11,2	1,24	50,0	1,78	5,72
7	70	4,5	6,20	29,0	2,16	46,0	2,72	12,0	1,39	51,0	1,88	4,87
		5	6,86	31,9	2,16	50,7	2,72	13,2	1,39	56,7	1,90	5,38
		6	8,15	37,6	2,15	59,6	2,71	15,5	1,38	68,4	1,94	6,39
		7	9,42	43,0	2,14	68,2	2,69	17,8	1,37	80,1	1,99	7,39
		8	10,70	48,2	2,13	76,4	2,68	20,0	1,37	91,9	2,02	8,37

5-nji goşmaçanyň dowamy												
1	2	3	4	5	6	7	8	9	10	11	12	13
7,5	75	5	7,39	39,5	2,31	62,6	2,91	16,4	1,49	69,6	2,02	5,80
		6	8,78	46,6	2,30	73,9	2,90	19,3	1,48	83,9	2,06	6,89
		7	10,10	53,3	2,29	84,6	2,89	22,1	1,48	98,3	2,10	7,96
		8	11,50	59,8	2,28	94,9	2,87	24,8	2,47	113	2,15	9,02
		9	12,80	66,1	2,27	105,0	2,86	27,5	1,46	127	2,18	10,1
8	80	5,5	8,63	52,7	2,47	83,6	3,11	21,8	1,59	93,2	2,17	6,78
		6	9,38	57,0	2,47	94,0	3,11	23,5	1,58	102	2,19	7,36
		7	10,80	65,3	2,45	104,0	3,09	27,0	1,58	119	2,23	8,51
		8	12,30	73,4	2,44	116,0	3,08	30,3	1,57	137	2,27	9,65
9	90	6	10,60	82,1	2,78	130,0	3,50	34,0	1,79	145,0	2,43	8,33
		7	12,30	94,3	2,77	150,0	3,49	38,9	1,78	169,0	2,47	9,64
		8	13,90	106,	2,76	168,0	3,48	43,8	1,77	194,0	2,51	10,9
		9	15,60	118,	2,75	186,0	3,46	48,6	1,77	219,0	2,55	12,2
10	100	6,5	12,80	122,	3,09	193,0	3,88	50,7	1,99	214,0	2,68	10,1
		7	13,80	131,	3,08	207,0	3,88	54,2	1,98	231,0	2,71	10,8
		8	15,60	147	3,07	233,0	3,87	60,9	1,98	265,0	2,75	12,2
		10	19,20	179	3,05	284,0	3,84	74,1	1,96	333,0	2,83	15,1
		12	22,80	209	3,03	331,0	3,81	86,9	1,95	402,0	2,91	17,9
		14	26,30	237	3,00	375,0	3,78	99,3	1,94	472,0	2,99	20,6
		16	29,70	264	2,98	416,0	3,74	112,0	1,94	542,0	3,06	23,3
11	110	7	15,20	176	3,40	279,0	4,29	72,7	2,19	308,0	2,96	11,9
		8	17,20	198	3,39	315,0	4,28	81,8	2,18	353,0	3,00	13,5
12,5	125	8	19,7	294	3,87	467	4,87	122	2,49	516	3,36	15,5
		9	22,0	327	3,86	520	4,86	135	2,48	582	3,40	17,3
		10	24,3	360	3,85	571	4,84	149	2,47	649	3,45	19,1
		12	28,9	422	3,82	670	4,82	174	2,46	782	3,53	22,7
		14	33,4	482	3,80	764	4,78	200	2,45	916	3,61	26,2
		16	37,8	539	3,78	853	4,75	224	2,44	1051	3,68	29,6
14	140	9	24,7	466	4,34	739	5,47	192	2,79	818	3,78	19,4
		10	27,3	512	4,33	814	5,46	211	2,78	911	3,82	21,5
		12	32,5	602	4,31	957	5,43	248	2,76	1097	3,90	25,5
16	160	10	31,4	774	4,96	1229	6,25	319	3,19	1356	4,30	24,7
		11	34,4	844	4,95	1341	6,24	348	3,18	1494	4,35	27,0
		12	37,4	913	4,94	1450	6,23	476	3,17	1633	4,39	29,4
		14	43,3	1046	4,92	1662	6,20	431	3,16	1911	4,47	34,0
		16	49,1	1175	4,89	1866	6,17	485	3,14	2191	4,55	38,5
		18	54,8	1299	4,87	2061	6,13	537	3,13	2472	4,63	43,0
		20	60,4	1419	4,85	2248	6,10	589	3,12	2756	4,70	47,4

5-nji goşmaçanyň dowamy												
1	2	3	4	5	6	7	8	9	10	11	12	13
18	180	11	38,8	1216	5,60	1933	7,06	500	3,59	2128	4,85	30,5
		12	42,2	1317	5,59	2093	7,04	540	3,58	2324	4,89	33,1
20	200	12	47,1	1823	6,22	2896	7,84	749	3,99	3182	5,37	37,0
		13	50,9	1961	6,21	3116	7,83	805	3,98	3452	5,42	39,9
		14	54,6	2097	6,20	3333	7,81	861	3,97	3722	5,46	42,8
		16	62,0	2363	6,17	3755	7,78	970	3,96	42,64	5,54	48,7
		20	76,5	2871	6,12	4560	7,72	1182	3,93	5355	5,70	60,1
		25	94,3	3466	6,06	5494	7,63	1438	3,91	6733	5,89	74,0
		30	111,5	4020	6,00	6351	7,55	1688	3,89	8130	6,07	87,6
22	220	14	60,4	2814	6,83	4470	8,60	1159	4,38	4941	5,93	47,4
		16	68,6	3175	6,81	5045	8,58	1306	4,36	5661	6,02	53,8

Sozma polatdan ýasalan deň däl gapdally burçluk
DÖST 8510 – 72

Profilin belgisi	B, m	b, m	d, m	Kesigin meýdany A, sm^2	Massa 1m, kg	Sprawoçnik ululyklary										
						$x-x$		$y-y$		x_I-x_I		y_I-y_I		$u-u$		
						J_x, sm^4	i_x, sm	J_y, sm^4	i_y, sm	J_{xI}, sm^4	Agyrlyk merke-ziniň aralygy y_0, sm	J_{yI}, sm^4	Agyrlyk merke-ziniň aralygy x_0, sm	$J_u, \text{min}, \text{sm}^4$	$i_u, \text{min}, \text{sm}$	Ýapgyt burçy
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
2,5/1,6	25	16	3	1,16	0,91	0,70	0,78	0,22	0,44	1,56	0,86	0,43	0,42	0,13	0,34	0,392
3,2/2	32	20	3	1,49	1,17	1,52	1,01	0,46	0,55	3,26	1,08	0,82	0,49	0,28	0,43	0,382
			4	1,94	1,52	1,93	1,00	0,57	0,54	4,38	1,12	1,12	0,53	0,35	0,43	0,374
4/2,5	40	25	3	1,89	1,48	3,06	1,27	0,93	0,70	6,37	1,32	1,58	0,59	0,56	0,54	0,385
			4	2,47	1,94	3,93	1,26	1,18	0,69	8,53	1,37	2,15	0,63	0,71	0,54	0,381
4,5/2,8	45	28	3	2,14	1,68	4,41	1,43	1,32	0,79	9,02	1,47	2,20	0,64	0,79	0,61	0,382
			4	2,80	2,20	5,68	1,42	1,69	0,78	12,1	1,51	2,98	0,68	1,02	0,60	0,379

6-njy goşmaçanyň dowamy

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
5/3,2	50	32	3	2,42	1,90	6,17	1,60	1,99	0,91	12,4	1,60	3,26	0,72	1,18	0,70	0,403
			4	3,17	2,49	7,98	1,59	2,56	0,90	16,6	1,65	4,42	0,76	1,52	0,69	0,401
5,6/3,6	56	36	3,5	3,16	2,48	10,1	1,79	3,30	1,02	20,3	1,80	5,43	0,82	1,95	0,79	0,407
			4	3,58	2,81	11,4	1,78	3,70	1,02	23,2	1,82	6,25	0,84	2,19	0,78	0,406
			5	4,41	3,46	13,8	1,77	4,48	1,01	29,2	1,86	7,91	0,88	2,66	0,78	0,404
6,3/4,0	63	40	4	4,04	3,17	16,3	2,01	2,16	1,13	33,0	2,03	8,51	0,91	3,07	0,87	0,397
			5	4,98	3,91	19,9	2,00	6,26	1,12	41,4	2,08	10,8	0,95	3,73	0,86	0,396
			6	5,90	4,63	23,3	1,99	7,28	1,11	49,9	2,12	13,1	0,99	4,36	0,86	0,393
			8	7,68	6,03	29,6	1,96	9,15	1,09	66,9	2,20	17,9	1,07	5,58	0,85	0,385
7/4,5	70	45	4,5	5,07	3,98	25,3	2,23	8,25	1,28	51,0	2,25	13,6	1,03	4,88	0,98	0,407
			5	5,59	4,39	27,8	2,23	9,05	1,27	56,7	2,28	15,2	1,05	5,34	0,98	0,406
7,5/5	75	50	5	6,11	4,79	34,8	2,39	12,5	1,43	69,7	2,39	20,8	1,17	7,24	1,09	0,436
			6	7,25	5,69	40,9	2,38	14,6	1,42	83,9	2,44	25,2	1,21	8,48	1,08	0,435
			8	9,47	7,43	52,4	2,35	18,5	1,40	112,0	2,52	34,2	1,29	10,90	1,07	0,430
8/5	80	50	5	6,36	4,99	41,6	2,56	12,7	1,41	84,6	2,60	20,8	1,13	7,58	1,09	0,387
			6	7,55	5,92	49,0	2,55	15,8	1,40	102,0	2,65	25,2	1,17	8,88	1,08	0,386

6-njy goşmaçanyň dowamy

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
9/5,6	90	56	5,5	7,86	6,17	65,3	2,88	19,7	1,58	132	2,92	32,2	1,26	11,8	1,22	0,384
			6	8,54	6,70	70,6	2,88	21,2	1,58	145	2,95	35,2	1,28	12,7	1,22	0,384
			8	11,18	8,77	90,9	2,85	27,1	1,56	194	3,04	47,8	1,36	16,3	1,21	0,380
10/6,3	100	63	6	9,59	7,53	98,3	3,20	30,6	1,79	198	3,23	49,9	1,42	18,2	1,38	0,393
			7	11,1	8,70	113	3,19	35,0	1,78	232	3,28	58,7	1,46	20,8	1,37	0,392
			8	12,6	9,87	127	3,18	39,2	1,77	266	3,32	67,6	1,50	23,4	1,36	0,391
			10	15,5	12,10	154	3,15	47,1	1,75	333	3,40	85,8	1,58	28,3	1,35	0,387
11/7	110	70	6,5	11,4	8,98	142	3,53	45,6	2,00	286	3,55	74,3	1,58	26,9	1,53	0,402
			7	12,3	9,64	152	3,52	48,7	1,99	309	3,57	80,3	1,60	28,8	1,53	0,402
			8	13,9	10,90	172	3,51	54,6	1,98	353	3,61	92,3	1,64	32,2	1,52	0,400
12,5/8	125	80	7	14,1	11,0	227	4,01	73,7	2,29	452	4,01	119	1,80	43,4	1,76	0,407
			8	16,0	12,5	256	4,00	83,0	2,28	518	4,05	137	1,84	48,8	1,75	0,406
			10	19,7	15,5	312	3,98	100	2,26	649	4,14	173	1,92	59,3	1,74	0,404
			12	23,4	18,3	365	3,95	117	2,24	781	4,22	210	2,00	69,5	1,72	0,400

6-njy goşmaçanyň dowamy

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17
14/9	140	90	8	18,0	14,1	364	4,49	120	2,58	727	4,49	194	2,03	70,3	1,98	0,411
			10	22,2	17,5	444	4,47	146	2,56	911	4,58	245	2,12	85,5	1,96	0,409
16/10	160	100	9	22,9	18,0	606	5,15	186	2,85	1221	5,19	300	2,23	110	2,20	0,391
			10	25,3	19,8	667	5,13	204	2,84	1359	5,23	335	2,28	121	2,19	0,390
			12	30,0	23,6	784	5,11	239	2,82	1634	5,32	405	2,36	142	2,18	0,388
			14	34,7	27,3	897	5,08	272	2,80	1910	5,40	477	2,43	162	2,16	0,385
18/11	180	110	10	28,3	22,2	952	5,80	276	3,12	1933	5,88	444	2,44	165	2,42	0,375
			12	33,7	26,4	1123	5,77	324	3,10	2324	5,97	537	2,52	194	2,40	0,374
20/12,5	200	125	11	34,9	27,4	1449	6,45	446	3,58	2920	6,50	718	2,79	264	2,75	0,392
			12	37,9	29,7	1568	6,43	482	3,57	3189	6,54	786	2,83	285	2,74	0,392
			14	43,9	34,4	1801	6,41	551	3,54	3726	6,62	922	2,91	327	2,73	0,390
			16	49,8	39,1	2026	6,38	617	3,52	4264	6,71	1061	2,99	367	2,72	0,388
25/16	250	160	12	48,3	37,9	3147	8,07	1032	4,62	6212	7,97	1634	3,53	604	3,54	0,410
			16	63,6	49,9	4091	8,02	1333	4,58	8308	8,14	2200	3,69	781	3,50	0,408
			18	71,1	55,8	4545	7,99	1475	4,56	9358	8,23	2487	3,77	866	3,49	0,407
			20	78,5	61,7	4987	7,97	1613	4,53	10410	8,31	2776	3,85	949	3,48	0,405

Çeýelik λ	Boý egilmäniň koeffisiýenti				
	Adaty hilli polat		Ýokarlan- dyrylan hilli polat $\sigma_a \geq 320$ MPa	Çoýun	Agaç
	polat 1, polat 2, polat 3, polat 4	Polat 5			
0	1,00	1,00	1,00	1,00	1,00
10	0,99	0,98	0,97	0,97	0,99
20	0,96	0,95	0,96	0,91	0,97
30	0,94	0,92	0,91	0,81	0,93
40	0,92	0,89	0,87	0,69	0,87
50	0,89	0,86	0,83	0,57	0,80
60	0,86	0,82	0,79	0,44	0,71
70	0,81	0,76	0,72	0,34	0,60
80	0,75	0,70	0,65	0,26	0,48
90	0,69	0,62	0,55	0,20	0,38
100	0,60	0,51	0,43	0,16	0,31
110	0,52	0,43	0,35	-	0,25
120	0,45	0,37	0,30	-	0,22
130	0,40	0,33	0,26	-	0,18
140	0,36	0,29	0,23	-	0,16
150	0,32	0,26	0,21	-	0,14
160	0,29	0,24	0,19	-	0,12
170	0,26	0,21	0,17	-	0,11
180	0,23	0,19	0,15	-	0,10
190	0,21	0,17	0,14	-	0,09
200	0,19	0,16	0,13	-	0,08

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